AD-778 844

TEST OF AN AXIAL COMPRESSOR STAGE DESIGNED FOR A TOTAL PRESSURE RATIO OF THREE TO ONE

Arthur J. Wennerstrom, et al

Aerospace Research Laboratories Wright-Patterson Air Force Base, Ohio

January 1974

DISTRIBUTED BY:



National Technical Information Service
U. S. DEPARTMENT OF COMMERCE
5285 Port Royal Road, Springfield Va. 22151

INCLASSIFIED
SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
ARL 74-0001		HD 778849	
4 TITLE (and Subtitle)		5. TYPE OF REFORT & PERIOD COVERED	
TEST OF AN AXIAL COMPRESSOR : DESIGNED FOR A TOTAL PRESSURI		Technical	
THREE TO ONE	S NATIO OF	6. PERFORMING ORG. REPORT HUMBER	
7. AUTHOR(e)		CONTRACT OR GRANT NUMBER(*)	
A. J. Wennerstrom		Internal	
G. R. Frost		2.1.001	
R. D. DeRose			
P. PERFORMING ORGANIZATION NAME AND ADDRESS Fluid Dynamics Facilities Rs	oh Ish	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK I'NIT NUMBERS	
Aerospace Research Laborator		DcD Element 61102F	
Wright-Patterson AFB, Ohio 4		Project 70650409	
11. CONTROLLING OFFICE NAME AND ADDRESS	· /*=\	12. REPORT DATE	
Aerospace Research Laborator: Air Force Systems Command	ies (LF)	January 1974	
Wright-Patterson AFB, Ohio 4	5433	13. NUMBER OF PAGES	
14 MONITORING AGENCY NAME & ADDRESS(IL ditterent		15. SECURITY CLASS. (of this report)	
		Unclassified	
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
		SCHEDULE	
16 DISTRIBUTION STATEMENT (of this Report)			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
19. SUPPLEMENTARY NOTES		DDC	
		91 1074	
19. KEY WORDS (Continue on reverse side II necessary and axial compressor		MAY 21 1974	
turbine engines NATION	GENERAL STATE		
turbomachinery	rest for the	D	
gas turbines	to a vA .		
Complete experimental reasons of 1600 ft/sec, a stage total hub/tip radius ratio of 0.75 passed 70 percent of design ratio of 2.25, and achieved the rotor and 0.61 for the stage of 1600 ft/sec.	esults are pre r stage design l pressure rat . At design s flow, achieved Isentropic eff	esented from tests of ned for a tip speed tio of 3.0 and an inlet speed, the compressor d a stage total pressure Ticiencies of 0.74 for	

DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

#### PREFACE

This report was prepared by Dr. Arthur J. Wennerstrom and Captain George R. Frost of the Fluid Dynamics Facilities Research Laboratory, Aerospace Research Laboratories, Wright-Patterson Air Force Base, Ohio, and Mr. Robert D. DeRose of Systems Research Laboratories, Inc., Dayton, Ohio.

The report presents results from a portion of the effort of the Fluid Machinery Research Group, supervised by Dr. Arthur J. Wennerstrom, conducted under Work Unit 09 of Project 7065, "Aerospace Simulation Techniques Research," under the overall direction of Mr. Elmer G. Johnson.

# TABLE OF CONTENTS

SECTION	PA	GE
I	INTRODUCTION	1
II	APPARATUS	2
	1. FACILITY FLOW PATH	2
	2. COMPRESSOR TEST VEHICLE	2
	3. COMPRESSOR INSTRUMENTATION	3
	4. TEST FACILITY INSTRUMENTATION	6
III	TEST PROCEDURE AND DATA REDUCTION	8
	1. TEST PROCEDURE	8
	2. DATA REDUCTION - PHASE I	9
	3. DATA REDUCTION - PHASE II	0
IV	RESULTS	4
	1. OVER-ALL PERFORMANCE	4
	2. BLADE-ELEMENT PERFORMANCE (ACROSS BLADE) 1	4
	3. BLADE-ELEMENT PERFORMANCE (WITHIN BLADE) 1	4
	4. ROTOR TIP DYNAMIC PRESSURE MEASUREMENTS 1	5
v	CONCLUSIONS	$\epsilon$
	APPENDIX A: PHASE II WITHIN-BLADE ANALYSES (COMPUTER PRINTOUTS) 14	5
	1. TEST POINT 208180514040 (40%) 14	7
	2. TEST POIN'T 208220415050 (50%) 16	3
	3. TEST POINT 208221315260 (60%)	9
	4. TEST POINT 208240215670 (70%) 19	5
	5. TEST POINT 208241115882 (82%) 21	1

SECTION			PAGE
	6.	TEST POINT 208300315970 (50%)	227
	7.	TEST POINT 208300915800 (100%)	243
	APPE	NDIX B: COMPUTER INPUT DATA FOR DATA REDUCTION	259
	1.	COMMON PHASE I DATA	261
	2.	COMMON PHASE II FIXED (LOG1) DATA, ACROSS-BLADE	264
	3.	COMMON PHASE II LOG4 - PART 1 DATA, ACROSS-BLADE	266
	4.	COMMON PHASE IT FIXED (LOG1) DATA, ACROSS-BLADE	267
	5.	INDIVIDUAL TEST INPUT DATA	271
	APPE	NDIX C: MODIFIED PROGRAM LISTINGS	313
	1.	PHASE I - SUBROUJINE TPRED	315
	2.	PHASE I - PROGRAM INPUT	317
	3.	PHASE I - SUBROUTINE OUT	325
	4.	PHASE II - PROGRAM B2X	331
	5.	PHASE II - PROCRAM C?	335
	6.	PHASE II - PROGRAM D2	339
	APPE	NDIX D: RAW FXPERIMENTAL DATA	347
	REFE	RENCES	1127

# LIST OF TABLES

TABLE		PAGE
I	INSTRUMENTATION LIST	18
II	CALIBRATION OF SAMPLE THERMOCOUPLES	22
III	CALIBRATION OF TEMPERATURE READOUT ELECTRONICS .	22
IA	MASS-AVERAGED COMPRESSOR PERFORMANCE	23
V	IDENTIFICATION OF SYMBOLS FOR 40%-SPEED ACROSS-BLADE FIGURES	24
VI	IDENTIFICATION OF SYMBOLS FOR 50%-SPEED ACROSS-BLADE FIGURES	25
VII	IDENTIFICATION OF SYMBOLS FOR 60%-SPEED ACROSS-BLADE FIGURES	26
VIII	IDENTIFICATION OF SYMBOLS FOR 70%-SPEED ACROSS-BLADE FIGURES	27
IX	IDENTIFICATION OF SYMBOLS FOR 82%-SPEED ACROSS-BLADE FIGURES	28
X	IDENTIFICATION OF SYMBOLS FOR 90%-SPEED ACROSS-BLADE FIGURES	29
XI	IDENTIFICATION OF SYMBOLS FOR 100%-SPEED ACROSS-BLADE FIGURES	30

# LIST OF ILLUSTRATIONS

FIGURE		PAGE
1	Compressor Facility Flow Path	31
2	Test Facility	32
3	Compressor Cross Section with Instrumentation Locations	33
7	Rotor Blades on Wheel	34
5	Stator Blades	35
6	Vehicle Instrumentation Bulkhead	36
7	Slot Vented Temperature Probe Design	37
8	Temperature Calibration Setup	38
9	Kiel Stagnation Tube Design	39
10	Instrumentation Rakes	40
11	Vane-Mounted Instrumentation	41
12	Compressor Performance Map	42
13	Rotor Relative Mach Number vs Inlet Radius (40% Speed)	43
14	Rotor Incidence vs Inlet Radius (40% Speed)	43
15	Rotor Loss Coefficient vs Outlet Radius (40% Speed)	44
1 $\epsilon$	Rotor Deviation vs Outlet Radius (40% Speed)	45
17	Rotor Diffusion Factor vs Outlet Radius (40% Speed)	46
18	Stator Mach Number vs Inlet Radius (40% Speed)	46
19	Stator Incidence vs Inlet Radius (40% Speed)	47
50	Stator Loss Coefficient vs Outlet Radius (40% Speed)	48
21	Stator Deviation vs Outlet Radius (40% Speed)	<b>μ</b> 8

FIGURE		PAGE
22	Stator Diffusion Factor vs Outlet Radius (40% Speed)	49
23	Rot. Relative Mach Number vs Inlet Radius (50% Speed)	50
24	Rotor Incidence vs'Inlet Radius (50% Speed)	50
25	Rotor Loss Coefficient vs Outlet Radius (50% Speed)	51
26	Rotor Deviation vs Outlet Radius (50% Speed)	52
27	Rotor Diffusion Factor vs Outlet Radius (50% Speed)	53
28	Stator Mach Number vs Inlet Radius (50% Speed) .	54
29	Stator Incidence vs Inlet Radius (50% Speed)	55
30	Stator Loss Coefficient vs Outlet Radius (50% Speed)	56
31	Stator Deviation vs Outlet Radius (50% Speed)	56
32	Stator Diffusion Factor vs Outlet Radius (50% Speed)	57
33	Rotor Relative Mach Number vs Inlet Radius (60% Speed)	58
34	Rotor Incidence vs Inlet RAdius (60% Speed)	58
35	Rotor Losc Coefficient vs Outlet Radius (60% Speed)	59
36	Rotor Deviation vs Outlet Radius (60% Speed)	60
37	Rotor Diffusion FActor vs Outlet Radius (60% Speed)	61
38	Stator Mach Number vs Inlet Radius (60% Speed) .	61
39	Stator Incidence vs Inlet Radius (60% Speed)	62
40	Stator Loss Coefficient vs Outlet Radius (60% Speed)	63
<b>4</b> 7	Stator Deviation vs Outlet Radius (60% Speed)	63

FIGURE		PAGE
42	Stator Diffusion Factor vs Outlet Radius (60% Speed)	64
43	Rotor Relative Mach Number vs Inlet Radius (70% Speed)	65
44	Rotor Incidence vs Inlet Radius (70% Speed)	65
45	Rotor Loss Coefficient vs Outlet Radius (70% Speed)	66
46	Rotor Deviation vs Outlet Radius (70% Speed)	67
47	Rotor Diffusion Factor vs Outlet Radius (70% Speed)	68
48	Stator Mach Number vs Inlet Radius (70% Speed)	68
49	Stator Incidence vs Inlet Radius (70% Speed)	69
50	Stator Loss Coefficient vs Outlet Radius (70% Speed)	70
51	Stator Deviation vs Outlet Radius (70% Speed)	70
52	Stator Diffusion Factor vs Outlet Radius (70% Speed)	71
53	Rotor Relative Mach Numbers vs Inlet Radius (82% Speed)	72
54	Rotor Incidence vs Inlet Radius (82% Speed)	72
55	Rotor Loss Coefficient vs Outlet Radius (82% Speed)	73
56	Rotor Deviation vs Outlet Radius (82% Speed)	73
57	Rotor Diffusion Factor vs Outlet Radius (82% Speed)	74
58	Stator Mach Number vs Inlet Radius (82% Speed)	74
59	Stator Incidence vs Inlet Radius (82% Speed)	75
60	Stator Loss Coefficient vs Outlet Radius (82% Speed)	76
61	Stator Deviation vs Outlet Radius (82% Speed)	76

FIGURE		PAGE
62	Stator Diffusion Factor vs Outlet Radius (82% Speed)	77
63	Rotor Relative Mach Number vs Inlet Radius (90% Speed)	78
б4	Rotor Incidence vs Inlet Radius (90% Speed)	78
65	Rotor Loss Coefficient vs Outlet Radius (90% Speed)	79
66	Rotor Deviation vs Outlet Radius (90% Speed)	79
67	Rotor Diffusion Factor vs Outlet Radius (90% Speed)	80
68	Stator Mach Number vs Inlet Radius (90% Speed)	80
69	Stator Incidence vs Inlet Radius (90% Speed)	81
70	Stator Loss Coefficient vs Outlet Radius (90% Speed)	82
71	Stator Deviation vs Outlet Radius (90% Speed)	82
72	Stator Diffusion Factor vs Outlet Radius (90% Speed)	83
73	Rotor Relative Mach Number vs Inlet Padius (100% Speed)	84
74	Rotor Incidence vs Inlet Radius (100% Speed)	84
75	Rotor Loss Coefficient vs Outlet Radius (100% Speed)	85
76	Rotor Deviation vs Outlet Radius (100% Speed)	86
77	Rotor Diffusion Factor vs Outlet Radius (100% Speed)	87
78	Stator Mach Number vs Inlet Radius (100% Speed) .	88
79	Stator Incidence vs Inlet Radius (100% Speed)	89
80	Stator Loss Coefficient vs Outlet Radius (100% Speed)	90
81	Stator Deviation vs Outlet Radius (100% Speed)	90

IGURE		PAGE
82	Stator Diffusion Factor vs Outlet Radius (100% Speed)	91
83	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 40% Speed)	92
84	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 40% Speed)	92
85	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 40% Speed)	93
86	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 40% Speed)	93
87	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 40% Speed)	94
88	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 40% Speed)	94
89	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 40% Speed)	95
90	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 40% Speed)	95
91	Stator Deviation vs Outlet Radius (Witnin-Blade Analysis, 40% Speed)	96
92	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 40% Speed)	96
93	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 50% Speed)	97
94	Rotor Incidence vs lnlet Radius (Within-Blade Analysis, 50% Speed)	97
95	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 50% Speed)	98
96	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 50% Speed)	98
97	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 50% Speed)	99
98	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 50% Speed)	99

FIGURE			PAGE
99	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 50% Speed)	•	100
100	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 50% Speed)	•	100
101	Stator Deviation vs Outlet Radius (Within-Blade Analysis, 50% Speed)	•	101
102	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 50% Speed)	•	101
103	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 60% Speed)		102
104	Rotor Incidence 's Inlet Radius (Within-Blade Analysis, 60% Speed)	•	102
105	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 60% Speed)	•	103
106	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 60% Speed)	•	103
207	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 60% Speed)	•	104
108	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 60% Speed)	•	104
109	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 60% Speed)		105
110	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 60% Speed)	•	105
111	Stator Deviation vs Outlet Radius (Within-Blade Analysis, 60% Speed)	•	106
112	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 60% Speed)		106
113	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 70% Speed)	•	107
114	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 70% Speed)	•	107
115	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 70% Speed)		108

IGURE		PAGE
1.16	Rotor Deviation vs Outlet Radius (Within-Blade An Tysis, 70% Speed)	. 108
117	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 70% Speed)	. 109
118	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 70% Speed)	. 109
119	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 70% Speed)	. 110
120	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 70% Speed)	
121	Stator Deviation vs Outlet Radius (Within-Blade Analysis, 70% Speed)	. 111
122	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 70% Speed)	
123	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 82% Speed)	. 113
124	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 82% Speed)	. 113
125	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 82% Speed)	. 114
126	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 82% Speed)	. 114
127	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 82% Speed)	. 115
128	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 82% Speed)	. 115
129	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 82% Speed)	. 116
130	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 82% Speed)	
131	Stator Deviation vs Outlet Radius (Within-Blade Analysis, 82% Speed)	. 11,
132	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 82% Speed)	

FIGURE			PAGE
133	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed)	•	119
134	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed)	•	119
135	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed)		120
136	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 90% Speed)	•	120
137	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 90% Speed)		121
138	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed)	•	121
139	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed)	•	122
140	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed)		123
141	Stator Deviation vs Outlet Radius (Within-Blade Analysis, 90% Speed)		123
142	Stator Diffusion Factor vs Outlet Radius (Within- Blade Analysis, 90% Speed)		124
143	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 100% Speed)		125
144	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 100% Speed)	•	125
145	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 100% Speed)	•	126
146	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 100% Speed)	•	127
147	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 100% Speed)	•	128
148	Stator Mach Number vs lnlet Radius (Within-Blade Analysis, 100% Speed)	•	128
149	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 100% Speed)		129

FIGURE		PAGE
150	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 100% Speed)	130
151	Stator Deviation vs Outlet Radius (Within-Blade Analysis, 100% Speed)	130
152	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 100% Speed)	131
153	Axial Static Pressure Distribution (Within-Blade Analysis, 40% Speed)	132
154	Axial Static Pressure Distribution (Within-Blade Analysis, 50% Speed)	133
155	Axial Static Pressure Distribution (Within-Blade Analysis, 60% Speed)	134
156	Axial Static Pressure Distribution (Within-Blade Analysis, 70% Speed)	135
157	Axial Static Pressure Distribution (Within-Blade Analysis, 82% Speed)	136
158	Axial Static Pressure Distribution (Within-Blade Analysis, 90% Speed)	137
159	Axial Static Pressure Distribution (Within-Blade Analysis, 100% Speed)	138
160	Design Rotor Deviation Angle Distribution	139
161	Rotor Mid-Radius Deviation vs Incidence Angle	140
162	Rotor with Splitter Vanes	141

#### SECTION I

#### INTRODUCTION

This report presents the results of an experimental evaluation of the single stage supersonic axial compressor described in Reference 1. This compressor was designed for an over-all stage total pressure ratio of 3 to 1 at an isentropic efficiency of 82 percent. Design tip speed was 1600 ft/sec at standard conditions and the inlet hub/tip radius ratio was 0.75. There were no inlet guide vanes.

The compressor tested was designed for diffusion levels beyond the range of past experience in both rotor and stator. This choice was deliberate in order to provide a suitable test bed for the evaluation of boundary layer control devices applicable to a compressor and to obtain data at values of Diffusion Factor above 0.5. As initially tested, no boundary layer control devices were installed in the compressor. It was not anticipated that design goals would be met with the initial configuration, and indeed they were not.

The second section of this report describes the test facility flow path, the compressor test vehicle, and the complete instrumentation system. Section III describes the procedures used in taking data and subsequently in reducing the data. The results of the test are presented in Section IV. Section V, the last section, summarizes the conclusions drawn from the data and indicates the choice made for the first configuration modification.

# SECTION II

#### **APPARATUS**

# 1. FACILITY FLOW PATH

The test facility used is of the open-loop variety. schematically shown in Figure 1. Air enters the facility through a filter designed to remove five micron particles with a 99.5 percent efficiency. The air then passes through a 30-inch duct to a Dall Flow Tube located about six pipe diameters downstream. About two pipe diameters further downstream, the air is turned 90 degrees with the aid of turning vanes and then passes through a perforated plate designed to reduce inlet pressure approximately three psi at 24 lb/sec flow at standard atmospheric conditions. Following this, the air passes through a tube bundle and subsequently enters a 48-inch diameter settling chamber. The settling chamber contains a perforated conical flow spreader and two screens patterned after the model investigation reported in Reference 2. From the settling chamber, air enters the compressor through a direct-coupled bellmouth. Air leaving the compressor is deflected radially outward to a peripheral throttle. The throttle consists of one stationary and one rotating cylindrical ring, each with 16 circumferentially distributed matching holes. Throttling takes place at a diameter of approximately 47 inches. Downstream of the throttle, the flow enters a collector, from which it is passed through a 24-inch duct to a silencer, and back to the atmosphere. A fast-acting poppet type valve, bypassing the throttle valve, is also available to relieve surge conditions. A cutaway frawing of the complete test facility is shown in Figure 2.

#### 2. COMPRESSOR TEST VEHICLE

A cross section of the research compressor is shown in Figure 3. The design employs a cantilevered rotor supported by four 0.5-inch thick bearing support struts with leading edges located about two stator chord lengths downstream of the stator trailing edge plane. The rotor tip diameter at the leading edge is nominally 18 inches. Oil seals are controlled gap carbon seals with an air barrier. No oil leakage into the flow path has ever been experienced. Cold rotor radial tip clearance with the rotor at rest is .037 to .039 inch. Hot clearance at design speed is predicted to be approximately .020 inch or about 0.6 percent of the mean rotor chord. The rotor shaft is mounted on ball bearings. Radial runout does not exceed .0005 The bulletnose and inlet hub flow path are supported by six bi-convex struts in the inlet. The flow area contraction ratio between the trailing edge plane of the struts and the leading edge plane of the rotor is 2.72 to 1. Surface finish on all surfaces adjacent to the flow upstream of the bearing

support struts is 32 microinches or better. An abradable coating has been employed in the casing adjacent to the rotor tip. However, no rubs have been experienced, even in stall. The rotor is of integral construction, the blades and disc being machined from a single forging of 6Al-4V titanium. The stator blades are individually inserted but are machined integrally with platforms at hub and tip. The gap between adjacent platforms lies in the range of 0 to .002 inch. A photograph of the rotor is shown in Figure 4. Photographs of stator blades are shown in Figure 5.

### 3. COMPRESSOR INSTRUMENTATION

Aerodynamic instrumentation in the compressor consists of measuring points in stator leading edges for total pressure and temperature, rakes downstream of the stators for total pressure and temperature, a large number of static pressure taps distributed on the inner and outer flow path and on the surface of one pair of stator blades, and dynamic wall pressure measurements made over the rotor tip. Measurements of inlet total pressure and temperature, mass flow, relative humidity, and rotor speed are accomplished outside of the compressor and are discussed in paragraph 4 of Section II. The Supersonic Compressor research vehicle has a total of 133 sensors measuring aerodynamic parameters at various points throughout the stage. Refer to Figure 3 and Table 1 for specific locations. Some of the static pressures are sensed at more than one point and are manifolded to become, in each case, a single measurement. Figure 6 shows the vehicle instrumentation bulkhead.

### a. Temperature Measurements

#### (1) Location

A total of thirty-nine Chromel-Alumel thermocouples are used to sense temperature. Four are mounted in the plenum, ten are mounted in the vane leading edges and twenty-five are located in the five discharge plane rakes. The vane leading edge and the rake mounted thermocouples are of the slot vented probe type (Figures 7, 10.a., and 11). A detailed analysis of the features of the slot vented design, along with recovery factor characteristics, may be found in Reference 3. The rakes were designed with the sensors dividing the discharge annulus into equal radial increments while circumferential spacing is on divisions equal to 2.2 times the distance between vane trailing elges. The single exception is one temperature rake which is misplaced three degrees circumferentially.

The ten stator leading edge thermocouple probes are mounted on four vanes with two vanes having two thermocouples and two vanes having three thermocouples. As with the discharge

rakes, these probes are also spaced to radially divide the stator annulus into five equal increments; however, in this case with two sensors per radius.

#### (2) Calibration

All thermocouples were rabricated from individually insulated, single rolls of Chromel and Alumel wire. Samples were taken periodically along the rolls as the thermocouples were made for vehicle installation. These sample thermocouples were calibrated against a model 162 platinum resistance bulb primary standard manufactured by Rosemount Engineering Company. A constant temperature oil bath, made by Lauda Division of Brinkman Instruments, Inc. was used as the heat medium. The bath was set at four different temperatures within the range of interest. The results, indicated in Table 2, show a worst case error of plus or minus 0.5°F at the highest temperature.

With thermocouples calibrated as indicated, the entire electronic system employed to record temperature data was examined. The results are shown in Table 3. Taking the worst case error, at the highest temperature, for both the thermocouples and readout system yields a maximum error of plus or minus 0.9°F. The more realistic RSS error goes from 0.23°F at 150 degrees to 0.65°F at 350 degrees. Finally, when recovery factor variation is added, the RSS error at 350°F becomes plus or minus 1.0°F. Figure 8 depicts the equipment used in the calibrations.

# b. Pressure Measurements

## (1) Location

Thirty-five static (PS) and thirty-five total (PT) pressures are measured in the vehicle flowpath. Twenty-five of the static taps are distributed at various points on the compressor flowpath liners. In particular, ten of these are located over the rotor blade tip, starting at 0.25 inch axially forward of the leading edge and following at 0.25 inch axial intervals extending downstream. A further ten statics are located approximately mid-chord radially on two vanes with seven suction side taps on one vane and three pressure side taps on the other.

The ten vane mounted total pressure probes are of the Kiel stagnation tube design (Figure 9) and are mounted with two sensors on each of two vanes and three on each of two other vanes. All are radially located to divide the annulus into five equal parts, with two measurements per radius. The other twenty-five are impact tubes mounted as five radial rakes of five sensors each, dividing the discharge annulus into equal increments and circumferentially spaced in a manner similar to that of the temperature rakes. An impact pressure rake is shown in Figure 10.b.

Located for use in conjunction with the static taps placed over the rotor blade tips are eight Kistler Model Number 603A pressure transducers and a Bentley Model 316 proximity detector. Because of problems observed at high speed with the Kistler dynamic pressure data, no further mention will be made of this system.

#### (2) Calibration

Four Statham strain gage type transducers are used to convert the various pressures into electrical signals for processing through readout and recording. One transducer is located in each of four, forty-eight port Scanivalve sequential pressure switching Jevices. The pressures to be sampled are connected to odd numbered ports while moderate vacuum is applied to all even (Roughing) ports to minimize hysteresis effects.

Three calibration pressures are sensed by all four Scanivalves on every scan. These are barometric, 15 PSIG and 30 PSIG. The 15 and 30 PSIG standards are supplied by Ametek Model PK-30 self-regulating, primary deadweight type, pressure standards referenced to atmosphere. The computer software used for data reduction corrects these two gauge values against variation in local barometric pressure and creates a new transducer calibration curve for every scan. Two absolute calibration pressures have been added to this system for use in future tests and the barometric calibration pressure has been eliminated.

#### c. Readout Electronics

Data is collected and recorded through use of a Hewlett Packaid 2012B Data Acquisition System (DAS). This system is comprised or a 2911 guarded crossbar scanner, 2547A coupler, 2402A integration digital voltmeter, 5050B digital recorder and a Kennedy 1506 incremental tape recorder.

As previously stated, pressure measurements are routed through four Scanivalve units using Statham transducers for conversion into electronic signals. A "Scanivalve" offers the advantage of using the same transducer to measure many pressures and lends itself to on-line calibration as described above. An interface unit was built to program the Scanivalves, along with other parameters, into the HP DAS in a manner which minimizes scanning time withou compromising transducer settling time. Instead of sampling the same port on all valves sequentially before stepping to the next port, the digital interface causes each valve to move through its next roughing port to its next data point immediately after being interrogated. Each transducer then has an opportunity to settle out at its next test pressure while two others are sequentially interrogated.

This sequence is repeated until all ports are sampled. Approximately six seconds lapse for the entire procedure.

Thermocouple outputs are routed through a Kaye Instruments' Model K170 electronic ice point reference into the interface unit and then to the HP DAS.

# 4. TEST FACILITY INSTRUMENTATION

#### a. Rotor Speed

A Bentley Model 306 transducer senses six grooves nachined into the gearbox/rotor driveshaft coupling. The output is fed into a Model 3115 proximitor for signal conditioning. The proximitor signal is a train of pulses having a repetition rate corresponding to rotor RPM/10. This repetition rate is directly recorded by the HP DAS. A Bentley Model 5030 digital tachemeter provides a visual indication of rotor speed accurate to ten RPM. The tachemeter also includes an adjustable speed limiting switch as a safety feature.

#### b Mass Flow

Inlet pressure is metered through a product series 122 Dall tube venturi manufactured by B.I.F. Industries with a 12.687-inch throat. Metering accuracy has been calibrated to plus or minus one-half percent by the manufacturer. Static pressure taps are located both in the throat and in the inlet cavity.

# c. Inlet (Plenum) Total Pressure and Temperature

Compressor inlet total pressure is assumed equal to plenum static pressure just downstream of the last screen. Four static taps are manifolded into one pressure and recorded on two separate Scanivalves. The maximum error associated with this assumption is 0.06 percent. Temperature is sensed by four bare junction thermocouples located in the same axial plane as the pressure taps, and supported on two crossed cables.

#### d. Analog Compressor Mapping

An on-line plot of stage pressure ratio vs pseudo mass flow was effected through use of a Mosely Model 2FRA X-Y plotter. Teledyne pressure tranducers were used to sense stage inlet PO1, stage exit PO3 from a mid-radius stagnation tube and hub P1 (measured 0.25 inch upstream of the rotor). Operational amplifiers were used to ratio exit PO3 to inlet PO1 and also to ratio hub P1 to inlet PO1. Stage pressure ratio was used to excite the Y-axis while 1 - (P1/PO1) was sent to the X-axis. The approximate compressor map so obtained was used to select a reasonable distribution of throttle settings at which to record detailed data.

# e. Relative Humidity

A Foxboro Dewcel Model 2711TG-K222 was mounted in the inlet stack to monitor humidity. This device continuously measures the moisture content of the air by sensing the temperature at which the partial pressure of its water vapor is equal to the water vapor pressure of a saturated salt solution. The humidity information is acquired by the DAS as a thermocouple reading on every test run and subsequently treated in the Phase I data reduction program.

#### SECTION III

# TEST PROCEDURE AND DATA REDUCTION

#### 1. TEST PROCEDURE

Test data was taken in order of increasing speed, each speed-line being entirely probed before any data at higher speed was acquired. The on-line analog x-y plot capability discussed in paragraph 4.d. of Section II was used to select the test points, since on-line data reduction was not available.

For each speedline, test data was first acquired at a partially-closed exhaust throttle setting, after which the compressor was gradually throttled to induce stall. After recovery, data was taken at several points as the throttle was opened from near-stall to wide-open. Stall was indicated by two sources: the dynamic pressures across the rotor tip, which were displayed on oscilloscopes on the test operator's console, and a microphone in the plenum. Sudden oscillations of the above-mentioned x-y plotter were further indicators that stall had occurred.

Data was acquired at the rate of about one speedline per hour. On dates when elevated speed lines were investigated, a single test point at each of several lower speeds was taken to assure data integrity by comparison to previously-acquired data at these lower speeds.

Prior to each test, an atmospheric pressure reading was obtained from a mercury barometer at the test site. The rig was initially brought up to speed and then monitored for about ten minutes, when it was assumed equilibrium had been reached. A five-minute dwell at each throttle setting was observed prior to data acquisition. One data scan per test point was acquired for speeds below 90 percent, with two scans per point at 90 and 100 percent design speed.

A 12-character test identification number was manually assigned to each test point and acquired by the DAS as the first item of information during data acquisition at that point (character 1: last digit of year; characters 2-3: numerical month; characters 4-5: numerical day of month; characters 6-7: test point number on that particular date; characters 8-10: numerical throttle setting; characters 11-12: last two digits of the nominal percent-speed (e.g., 82% = 82; 100% = 00)). Where two scans were taken at a particular test point automatically, each scan bears the same test identification number.

A spike in the facility vibration signature corresponded to 80 percent corrected design speed on the date this data was to be acquired. This required an increase to 82 percent of design speed before vibrations were judged adequate for continuous running and data acquisition purposes.

Finally, a listing of all raw experimental data which was acquired during testing of this stage is provided in Appendix D and all computer input data used for Phases I and II of the data reduction is provided in Appendix B.

# 2. DATA REDUCTION - PHASE I

Phase I reduction of the test data was accomplished using a slightly modified version of the computer program described in Reference 4. One of the equations of that reference, and the associated computer coding, is in error; hence several input and output data changes were made.

The erroneous equation is Equation 18, which is used to correct the measured mass flow for standard inlet conditions. The correct relationship is

$$W_{c} = W \cdot \frac{P_{std}}{P_{01}} \cdot \sqrt{\frac{T_{01}}{T_{std}}}$$

This requires a modification to card CALC 266, which should read

WCORR (I) = WACT (I)/
$$FAC2 * SQRT(FAC1)$$

The experimental data was acquired on magnetic tape, but in different format from that described in Reference 4. The twelve characters of each data item were recorded in two ten-character computer "words," the first consisting of seven leading zeroes (or blanks) and the first three data characters, the second consisting of a leading blank and the final nine data characters. A specia. subroutine (TPRED) was written to accommodate this data configuration and allow for high-speed data transmittal from tape to computer. A call to this subroutine replaces cards MAIN 52-53 in the main program, and also appears in subroutine INPUT, a current listing of which appears in Appendix C, as does a listing of Subroutine TPRED.

Other changes in Subroutine INPUT (Program INPUT, in this use, since the overlayed version of REDUC was used) reflect changes in the instrumentation configuration from the time the program was published until the vehicle was tested. These changes are briefly discussed below.

Three additional types of pressure data were available at the time the vehicle was tested, which required extensions of data items "Ll" and "ITPR" of Program REDUC, as follows:

<u> []</u>

- L1 = 14 Flowpath static pressure between blade rows
- L1 = 15 Flowpath static pressure just upstream of rotor
- L1 = 16 Atmospheric pressure

# ITPR

Data Type (See L1)	Sequence of Channel Codes in Array ITPR
L1 = 14	Similar to Ll = 7
L1 = 15	Similar to Ll = 7
L1 = 16	Any sequence

The pressure calibration system (described in Section II.3.b.(2)) required a modification to the program of Reference 4 also. A new input item, IATGG, was added just prior to item PSI, the array of calibration pressure magnitudes, to indicate whether each such pressure was an absolute or gauge (relative to atmospheric) measurement (IATGG = 0, absolute; IATGG = 1, gauge).

The magnitude of rotor wheel speed was provided as RPM divided by ten, rather than in cycles per second as anticipated in Reference 4. This required a slight change in the relevant computer coding in Subroutine INPUT.

Only minor modifications to other routines were required in program REDUC. The number of data acquisition channels is now required on the first data card as well as in the "Instrumentation Data Deck." This is to allow the program user to select the data-skip option if he so desires.

Minor additions and changes to the format of the output data were also made. The version of Subroutine OUT used in the presentation of this data is listed in Appendix C.

#### 3. DATA REDUCTION - PHASE II

Phase II reduction of the test data was accomplished using a modified version of the computer program described in Reference 5. The important elements of the modifications are described in this section.

Two erroneous FORTRAN statements were detected during the data reduction, necessitating revision of cards U2 1849 and U2 1862. Pespectively, these cards should read

IF (NCALC(I+1).LE.1.OR.IC1.GT.2) GO TO 600

IF (X2.EQ.O.) GO TO 584

It was found necessary to strictly control the manner in which extrapolations were made from the experimental data toward each flowpath boundary. This control was achieved through use of a new input item NEX (NEX = 0, the radial gradient between the last two data points nearest a wall is extrapolated linearly to the wall; NEX = 1, the data value at the outer casing is assumed to have a value midway between the value it would have with NEX = 0 and the value of the data point nearest the wall; NEX = 2, the data at both hub and case is extrapolated as with NEX = 1). The coding associated with the implementation of this option is presented in Appendix C, where Program C2 as modified is presented.

In many cases, it was also found necessary to change the manner in which deviation angle is specified within the blade in order to obtain converged through-the-blade solutions. Rather than specifying rotor deviation chordwise as a percent of trailing edge deviation, as suggested in Reference 5, the program was modified to treat data item RDEV as an absolute angle, in degrees. This required a modification to card U2 1961, which becomes

TANR(J) = TAN(ATAN(TANA(J)) + XX3(J)/C1)

Another change in the computational scheme involves the limiting of the range of allowable blockage estimates when analyzing data by iterating on casing static pressure measurements. Without such restraints, the program may increase or decrease blockage to unrealistic levels in an attempt to compute static pressures which match the measured casing static pressures. The boundary layer and wake blockage was constrained between 0. and 30 percent by two cards.

IF(BLCKGE(I).LT.0.0) BLCKGE(I)=0.0

IF(BLCKGE(I).GT.0.3) BLCKGE(I)=0.3

inserted between cards U2 2130 and U2 2131.

A similar change involved the establishment of a minimum allowable level of computed static temperature. This required modification of two subroutines:

<u>E2</u>

<u> </u>			
	Q = FF1(TIN)/1.25	U2	1982A
228	IF (XZ.GE.Q) GO TO 228 XZ = Q CONTINUE	U2	1985A 1985B 1985C
<u>12</u>			
	X2 = FF1(TIN)/3.0 IF(X1.LT.X2) X1 = X2		2126A 2126B

A jump statement was required in Program C2 because the corrections to the measured thermocouple data in the stage discharge plane are made during the Phase I data reduction. This statement, inserted between cards U2 1569 and U2 1570, is illustrated in the listing of Program C2 (Appendix C).

A jump statement was also used in Program B2X to skip the read-in of flow angle data in the stage discharge plane, since no such test data is available. This statement, and related coding changes, are presented in the listing of Program B2X (Appendix C) in the vicinity of card U2 1425.

The static pressure at the stator trailing edge was defined as equal to the static pressure at the downstream instrumentation plane in the program in order to obtain more realistic computed static pressures across the stator. The related coding appears near cards U2 1441 and U2 1452 (Program B2X).

Also presented in the listing of Program B2X is the deck re-ordering which was utilized in the multiple-data-set reductions whereby the final streamline pattern of the previous data set may be used as a first guess of the streamline pattern for the subsequent set. This option (new input item NSAVE = 1) resulted in significant savings of computer time in multiple-set reductions.

Several new convergence and diagnostic aides have been incorporated into Program D2. Among the more significant of these changes is one which involves a skip of the continuity sums until the momentum equation sums have nearly converged. Other changes are presented without comment in the listing of Program D2, which appears in Appendix C.

Three other program modifications were made, one essential and two merely convenient. In several instances, it was found necessary to change the damping factor  $\frac{K'}{8}$  in the "streamline relaxation factor" (Reference 5) in order to obtain converged solutions within a reasonable number of iterations. A new input data item DAMPF was devised whereby, if DAMPF is other than zero,  $\frac{K'}{8}$  becomes  $\frac{K'}{DAMPF}$ . The associated computer coding is illustrated in Program D2 (Appendix C) in the vicinity of card U2 1897.

The "convenient" changes referred to in the above paragraph are in regard to producing on-line plots of the Phase II data reduction. Data input items PLOWER and PSCALE were added to allow the program user to set the vertical axis minimum and scale, respectively, of the axial static pressure plot. Furthermore, the plot of stator incidence was constrained to have a maximum spread of twenty-eight degrees. Thus the plots of stator incidence referred to in the "Results" section of this report must be considered appropriately.

The new data items PLOWER, PSCALE, DAMPF, NSAVE, and NEX described above are read in the main program (UD0200) and transferred to routines B2X, C2, D2, and F2 via a labeled COMMON statement.

#### SECTION IV

#### RESULTS

#### OVER-ALL PERFORMANCE

The mass-averaged performance of the rotor and of the complete compressor stage is tabulated in Table 4 and plotted in Figure 12. As shown on the compressor map, the performance of this machine in terms of flow, pressure ratio, and efficiency deteriorated rapidly with increasing speed. At 100 percent design corrected speed, corrected flow was approximately 30 percent low, rotor efficiency was 14 points low, stage efficiency was 21 points low, rotor total pressure ratio was 2.63 versus approximately 3.3, and stage total pressure ratio was 2.25 versus 3.0. The compressor was throttled to stall at each corrected speed shown on the map. The data point nearest stall in each case was taken at a throttle opening approximately 0.5 percent further open than the setting which precipitated stall. This change in throttle area is equivalent to about 0.9 percent of the annulus area at the rotor inlet.

# 2. BLADE-ELEMENT PERFORMANCE (ACROSS BLADE)

The radial distributions of relative inlet Mach number, incidence angle, loss coefficient, deviation angle, and diffusion factor for both rotor and stator are presented in Figures 13 through 82, using Tables 5-11, for each data point shown on the compressor map. One set of these five radial distributions is presented for each blade row at each corrected speed. In each of these sets, the distributions for all throttle settings are superimposed on each respective plot. As described earlier in Section III, this data was reduced using the full radial equilibrium equation with the equations of momentum, continuity, etc. satisfied at each computing station for each streamline. This data, also used for the compressor map, was reduced with computing stations only at blade-row edges and in free spaces; there were no computing stations internal to blade rows.

# 3. BLADE-ELEMENT PERFORMANCE (WITHIN BLADE)

The data point nearest maximum stage efficiency for each operating speed was selected for more detailed analysis. The more detailed analysis involved the introduction of four additional computing stations within the rotor. The data reduction was then accomplished in the same manner as before, with blockages and deviation angles internal to the rotor adjusted so that calculated and measured static pressures along the casing adjacent to the rotor tip were as nearly coincident as possible. The results of these analyses include plots of the

radial distribution of the same five parameters for rotor and stator described in the preceding paragraph (Figures 83 through 152), plots of the experimental and calculated axial distribution of static pressure at hub, mean, and case (Figures 153 through 159), and a complete aerodynamic description at each computing station - streamline intersection (Appendix A). Tables giving the stator suction- and pressure-surface static pressures for these test points have been included in Appendix B.

#### 4. ROTOR TIP DYNAMIC PRESSURE MEASUREMENTS

The dynamic distribution of static pressure over the rotor tips was measured during operation. This data was primarily of interest for determining shock patterns in the rotor tip region. Signals obtained at low speeds were clean and consistent. However, at high speeds where measurements were recorded, it was found that extreme unsteadiness resulting from high rotor incidence angles made the data unuseable. Consequently, none of this data is presented. The principal value of these measurements proved to be a means of qualitatively assessing flow stability during the test.

## SECTION V

#### CONCLUSIONS

The performance of this compressor stage was so far below its design point in all respects - flow, pressure ratio, and efficiency - that it seemed pointless to pursue the boundary-layer-control investigations originally planned at this time. No form of boundary layer control practical to install in a gas turbine engine was thought capable of producing a useful improvement on this stage. Such forms of control as massive suction were not considered to be of practical interest for this application.

Principal attention at this point was devoted to an attempt to understand why this stage performed as it did and in turn to determine what kind of configuration change might allow it to perform more closely to its design objectives. Low rotor total pressure ratio and low flow logically occur together in a stage of this general type because the stator operates choked over a significant portion of the speed range. In this instance, the stator first choked at about seventy percent corrected design An examination of the radial distributions of rctor deviation angle from forty through seventy percent corrected speed shows that, except for a steep increase very close to the tip, the experimental distributions were relatively near the design distribution. The design distribution shown in Reference 1 is reproduced in Figure 160 in this report. However, between seventy and eighty-two percent corrected speed, deviation increased nearly fifty percent and remained high up to design speed. To see what relationship rotor deviation might have to rotor incidence, the mid-radius values of these parameters were cross plotted for the data sets presented in Appendix A. cross plot is shown in Figure 161. The interesting result is that rotor deviation is seen to be a steep and linear function of incidence from forty to eighty-two percent corrected design speed. Deviation increases approximately three degrees for every degree increase in incidence angle. Deviation peaked at ninety percent speed and declined slightly at design speed. Whether this apparent peaking and decline is meaningful or is simply a result of the arbitrary mid-radius location selected to make this plot was not investigated.

The main conclusion drawn from the collective body of data is that the behavior of the rotor deviation angle as a function of incidence was such that, as the rotor was forced to operate at high incidence angles at part speed, the relative turning angle across the rotor was reduced too rapidly for the compressor to recover as design speed was approached. If the compressor were operated above design speed, the pressure ratio might increase sufficiently rapidly to allow rotor incidence to drop

significantly. However, the slope of peak roter efficiency versus flow on the compressor map indicates that a relatively large overspeed might be required and increasing shock losses would probably make a significant reduction of incidence unrealizable. An increase in stator throat area would allow the rotor to operate more efficiently and at a higher pressure ratio. However, it appears unlikely that this alone would be sufficient to cause the rotor to operate reasonably near its design point, and part-speed performance might still pose a problem.

The solution to this problem appears to lie in achieving better control of rotor deviation angle. Better control, in this instance, means both a reduction in the absolute value of deviation angle at high back pressures and a reduction in the variation of deviation with incidence angle to improve partspeed operation. The obvious method of achieving both of these goals is an increase in rotor solidity. However, since the solidity of the tested rotor was already approximately 2.0, an increase in solidity sufficient to control the deviation angle would lead to higher diffusion losses, probably also to higher shock losses due to increased incidence resulting from higher blade blockage, and would naturally result in greater weight. So little camber exists in the front part of the blade between the leading edge and the shock impingement point that higher solidity in this region becomes a distinct disadvantage, particularly in view of the high local blade angle, which magnifies the blockage effect of additional blades. On the other hand, near the trailing edge of the blade, the radius of curvature of the camberline is approximately equal to the blade spacing and the local blade angle is much lower. Increased solidity in this region should greatly improve flow guidance and the blockage effect should be minor. These considerations led to a decision to incorporate partial blades or "splitter vanes" in the aft portion of the rotor such as shown in Figure 162. Details of this redesign and its performance will be published in future reports.

Because this compressor operated so far from its design point at design speed, no serious attempt was made to draw additional conclusions from the data. At the time of writing this report, the above described rotor modification had already been tested and was largely successful. The discussion of other performance factors will be expanded in the next test report.

TABLE I
INSTRUMENTATION LIST

075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         69°7¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.440         243°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           083         T/C         6.181         8.120         4°28¹         Disch. Rake Elem           084         T/C         6.181         8.120         36°48¹         Disch. Rake Elem           085         T/C         6.181         8.120         36°48¹         Disch. Rake Elem           086         T/C         6.181         8.120         208°38¹         Disch. Rake Elem           089         T/C <td< th=""><th>057 058 059 060 061 062 063 064 065 066 067</th><th>T/C T/C T/C T/C T/C T/C T/C T/C T/C T/C</th><th>LE LE LE</th><th>7.800 8.371</th><th>4°28' 45° 135° ?25° 315°</th><th>Was No. 095  Not In Use)  Plenum  Plenum  Plenum</th></td<>	057 058 059 060 061 062 063 064 065 066 067	T/C	LE LE LE	7.800 8.371	4°28' 45° 135° ?25° 315°	Was No. 095  Not In Use)  Plenum  Plenum  Plenum
OS7	058 059 060 061 062 063 064 065 066 067	T/C T/C T/C T/C T/C T/C T/C T/C T/C	LE LE LE	8.371	4°28' 45° 135° ?25° 315°	(Not In Use) Plenum Plenum Plenum
O58   T/C	059 060 061 062 063 064 065 066 067	T/C T/C T/C T/C T/C T/C T/C T/C	LE LE		45° 135° ?25° 315°	(Not In Use) Plenum Plenum Plenum
OS9   T/C	060 061 062 063 064 065 066 067	T/C T/C T/C T/C T/C T/C T/C	LE LE		135° ?25° 315°	(Not In Use) Plenum Plenum Plenum
O60	061 062 063 064 065 066 067 068	T/C T/C T/C T/C T/C T/C T/C	LE LE		135° ?25° 315°	Plenum Plenum Plenum
061         T/C         325°         Plenum           062         T/C         315°         Plenum           063         T/C         315°         Plenum           064         T/C         LE         8.371         Vane 22         L-ading Edge           065         T/C         LE         8.371         Vane 42         Le ling Edge           066         T/C         LE         8.251         Vane 24         Leading Edge           067         T/C         LE         8.251         Vane 44         Leading Edge           068         T/C         LE         8.121         Vane 22         Leading Edge           069         T/C         LE         8.001         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 44         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           071         T/C         LE         8.001         Vane 42         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Le	062 063 064 065 066 067 068	T/C T/C T/C T/C T/C T/C	LE LE		135° ?25° 315°	Plenum
063         T/C         LE         8.371         Vane 22         Leading Edge           064         T/C         LE         8.371         Vane 42         Leading Edge           065         T/C         LE         8.251         Vane 44         Leading Edge           066         T/C         LE         8.251         Vane 44         Leading Edge           067         T/C         LE         8.121         Vane 42         Leading Edge           068         T/C         LE         8.121         Vane 42         Leading Edge           069         T/C         LE         8.001         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 42         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         8.001         Vane 42         Leading Edge           074         T/C         6.181         8.440         36°48¹         Dis	063 064 065 066 067 068	T/C T/C T/C T/C T/C	LE LE		315°	
064         T/C         LE         8.371         Vane 22         Lrading Edge           065         T/C         LE         8.371         Vane 42         Le ling Edge           066         T/C         LE         8.251         Vane 24         Leading Edge           067         T/C         LE         8.251         Vane 24         Leading Edge           068         T/C         LE         8.121         Vane 22         Leading Edge           069         T/C         LE         8.001         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 42         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leadi	064 065 066 067 068	T/C T/C T/C T/C	LE LE			Plenum
065         T/C         LE         8.371         Vane 42         Le ling Edge           066         T/C         LE         8.251         Vane 24         Leading Edge           067         T/C         LE         8.251         Vane 44         Leading Edge           068         T/C         LE         8.121         Vane 42         Leading Edge           069         T/C         LE         8.001         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           071         T/C         LE         7.871         Vane 42         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           075         T/C         6.181         8.440         36°48°         Dis	065 066 067 068	T/C T/C T/C	LE LE		17 00	
066         T/C         LE         8.251         Vane 24         Leading Edge           067         T/C         LE         8.251         Vane 44         Leading Edge           068         T/C         LE         8.121         Vane 22         Leading Edge           069         T/C         LE         8.121         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         242°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         36°48¹ </td <td>066 067 068</td> <td>T/C</td> <td>LE</td> <td>8.371</td> <td>vane 22</td> <td>Leading Edge</td>	066 067 068	T/C	LE	8.371	vane 22	Leading Edge
067         T/C         LE         8.251         Vane 44         Leading Edge           068         T/C         LE         8.121         Vane 22         Leading Edge           069         T/C         LE         8.121         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         4°28¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         206°38¹         Disch. Rake Elem           077         T/C         6.181         8.440         243°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           080         T/C         6.181         8.280	067 068	T/C			Vane 42	Le ling Edge
068         T/C         LE         8.121         Vane 22         Leading Edge           069         T/C         LE         8.121         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 42         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         36°48'         Disch. Rake Elem           075         T/C         6.181         8.440         36°48'         Disch. Rake Elem           076         T/C         6.181         8.440         69°7'         Disch. Rake Elem           077         T/C         6.181         8.440         243°58'         Disch. Rake Elem           079         T/C         6.181         8.280         4°28'         Disch. Rake Elem           079         T/C         6.181         8.280         36°48'         Disch. Rake Elem           081         T/C         6.181         8.280	068			8.251	Vane 24	Leading Edge
069         T/C         LE         8.121         Vane 42         Leading Edge           070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 22         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         4°28°         Disch. Rake Elem           075         T/C         6.181         8.440         36°48°         Disch. Rake Elem           076         T/C         6.181         8.440         208°38°         Disch. Rake Elem           077         T/C         6.181         8.440         208°38°         Disch. Rake Elem           078         T/C         6.181         8.280         4°28°         Disch. Rake Elem           080         T/C         6.181         8.280         36°48°         Disch. Rake Elem           081         T/C         6.181         8.280         208°38°         Disch. Rake Elem           082         T/C         6.181         8.280 </td <td></td> <td>T/C</td> <td></td> <td></td> <td>Vane 44</td> <td>Leading Edge</td>		T/C			Vane 44	Leading Edge
070         T/C         LE         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 22         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         4°28¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.440         242°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181 <td< td=""><td>069</td><td></td><td>LE</td><td>8.121</td><td>Vane 22</td><td>Leading Edge</td></td<>	069		LE	8.121	Vane 22	Leading Edge
070         T/C         LB         8.001         Vane 24         Leading Edge           071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 22         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         4°28¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.440         243°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181 <td< td=""><td></td><td></td><td>LE</td><td>8.121</td><td>Vane 42</td><td></td></td<>			LE	8.121	Vane 42	
071         T/C         LE         8.001         Vane 44         Leading Edge           072         T/C         LE         7.871         Vane 22         Leading Edge           073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         4°28¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           079         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181				8.001	Vane 24	
073         T/C         LE         7.871         Vane 42         Leading Edge           074         T/C         6.181         8.440         4°28¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         69°7¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.440         243°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181         8.280         243°58¹         Disch. Rake Elem           083         T/C         6.181         8.120         4°28¹         Disch. Rake Elem           084         T/C         6.181         8.120         36°48¹         Disch. Rake Elem           085         T/C         6.181 </td <td></td> <td></td> <td>LE</td> <td>8.001</td> <td>Vane 44</td> <td></td>			LE	8.001	Vane 44	
074         T/C         6.181         8.440         4°28¹         Disch. Rake Elem           075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         69°7¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           079         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           083         T/C         6.181         8.280         243°58¹         Disch. Rake Elem           084         T/C         6.181         8.120         243°58¹         Disch. Rake Elem           085         T/C         6.181         8.120         36°48¹         Disch. Rake Elem           087         T/C			LE	7.871	Vane 22	Leadina Edae
075         T/C         6.181         8.440         36°48¹         Disch. Rake Elem           076         T/C         6.181         8.440         69°7¹         Disch. Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch. Rake Elem           078         T/C         6.181         8.440         243°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         69°7¹         Disch. Rake Elem           082         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           083         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           084         T/C         6.181         8.280         243°58¹         Disch. Rake Elem           085         T/C         6.181         8.120         4°28¹         Disch. Rake Elem           085         T/C         6.181         8.120         208°38¹         Disch. Rake Elem           087         T/C <td< td=""><td>073</td><td></td><td></td><td>7.871</td><td>Vane 42</td><td>Leading Edge</td></td<>	073			7.871	Vane 42	Leading Edge
076         T/C         6.181         8.440         69° 7¹         Disch, Rake Elem           077         T/C         6.181         8.440         208°38¹         Disch, Rake Elem           078         T/C         6.181         8.440         243°58¹         Disch, Rake Elem           079         T/C         6.181         8.280         4°28¹         Disch, Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch, Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch, Rake Elem           082         T/C         6.181         8.280         208°38¹         Disch, Rake Elem           083         T/C         6.181         8.280         243°58¹         Disch, Rake Elem           084         T/C         6.181         8.120         4°28¹         Disch, Rake Elem           085         T/C         6.181         8.120         36°48¹         Disch, Rake Elem           086         T/C         6.181         8.120         208°38¹         Disch, Rake Elem           087         T/C         6.181         7.960         243°58¹         Disch, Rake Elem           089         T/C			6.181	8.440	4°281	Disch. Rake Elemen
077         T/C         6.181         8.440         208°38'         Disch. Rake Elem           078         T/C         6.181         8.440         243°58'         Disch. Rake Elem           079         T/C         6.181         8.280         4°28'         Disch. Rake Elem           080         T/C         6.181         8.280         36°48'         Disch. Rake Elem           081         T/C         6.181         8.280         208°38'         Disch. Rake Elem           082         T/C         6.181         8.280         208°38'         Disch. Rake Elem           083         T/C         6.181         8.280         243°58'         Disch. Rake Elem           084         T/C         6.181         8.120         4°28'         Disch. Rake Elem           085         T/C         6.181         8.120         36°48'         Disch. Rake Elem           086         T/C         6.181         8.120         208°38'         Disch. Rake Elem           087         T/C         6.181         8.120         208°38'         Disch. Rake Elem           088         T/C         6.181         7.960         4°28'         Disch. Rake Elem           090         T/C         <	075		6.181	8.440	36°48'	Disch. Rake Elemen
078         T/C         6.181         8.440         243°58¹         Disch. Rake Elem           079         T/C         6.181         8.280         4°28¹         Disch. Rake Elem           080         T/C         6.181         8.280         36°48¹         Disch. Rake Elem           081         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           082         T/C         6.181         8.280         208°38¹         Disch. Rake Elem           083         T/C         6.181         8.120         4°28¹         Disch. Rake Elem           084         T/C         6.181         8.120         36°48¹         Disch. Rake Elem           085         T/C         6.181         8.120         36°48¹         Disch. Rake Elem           086         T/C         6.181         8.120         208°38¹         Disch. Rake Elem           087         T/C         6.181         8.170         243°58¹         Disch. Rake Elem           089         T/C         6.181         7.960         4°28¹         Disch. Rake Elem           090         T/C         6.181         7.960         26°43¹         Disch. Rake Elem           092         T/C <td< td=""><td>076</td><td></td><td>6.181</td><td>8.440</td><td>69° 7°</td><td>Disch. Rake Elemen</td></td<>	076		6.181	8.440	69° 7°	Disch. Rake Elemen
079         T/C         6.181         8.280         4°28'         Disch. Rake Elem           080         T/C         6.181         8.280         36°48'         Disch. Rake Elem           081         T/C         6.181         8.280         69°7'         Disch. Rake Elem           082         T/C         6.181         8.280         208°38'         Disch. Rake Elem           083         T/C         6.181         8.280         243°58'         Disch. Rake Elem           084         T/C         6.181         8.120         4°28'         Disch. Rake Elem           085         T/C         6.181         8.120         36°48'         Disch. Rake Elem           086         T/C         6.181         8.120         208°38'         Disch. Rake Elem           087         T/C         6.181         8.120         208°38'         Disch. Rake Elem           088         T/C         6.181         8.170         243°58'         Disch. Rake Elem           089         T/C         6.181         7.960         4°28'         Disch. Rake Elem           091         T/C         6.181         7.960         26°43'         Disch. Rake Elem           092         T/C	077	T/C	6.181	8.440	208°381	Disch. Rake Elemen
080         T/C         6.181         8.280         36°48°         Disch. Rake Elem           081         T/C         6.181         8.280         69°7'         Disch. Rake Elem           082         T/C         6.181         8.280         208°38°         Disch. Rake Elem           083         T/C         6.181         8.280         243°58°         Disch. Rake Elem           084         T/C         6.181         8.120         4°28°         Disch. Rake Elem           085         T/C         6.181         8.120         36°48°         Disch. Rake Elem           086         T/C         6.181         8.120         69°7°         Disch. Rake Elem           087         T/C         6.181         8.120         208°38°         Disch. Rake Elem           088         T/C         6.181         8.170         243°58°         Disch. Rake Elem           089         T/C         6.181         7.960         4°28°         Disch. Rake Elem           090         T/C         6.181         7.960         208°36°         Disch. Rake Elem           092         T/C         6.181         7.960         243°58°         Disch. Rake Elem           093         T/C <td< td=""><td>078</td><td></td><td>6.181</td><td>8.440</td><td>243°581</td><td>Disch. Rake Elemen</td></td<>	078		6.181	8.440	243°581	Disch. Rake Elemen
081         T/C         6.181         8.280         69° 7'         Disch. Rake Elem           082         T/C         6.181         8.280         208°38'         Disch. Rake Elem           083         T/C         6.181         8.280         243°58'         Disch. Rake Elem           084         T/C         6.181         8.120         4°28'         Disch. Rake Elem           085         T/C         6.181         8.120         36°48'         Disch. Rake Elem           086         T/C         6.181         8.120         69°7'         Disch. Rake Elem           087         T/C         6.181         8.120         208°38'         Disch. Rake Elem           088         T/C         6.181         8.170         243°58'         Disch. Rake Elem           089         T/C         6.181         7.960         4°28'         Disch. Rake Elem           090         T/C         6.181         7.960         26°43'         Disch. Rake Elem           091         T/C         6.181         7.960         208°36'         Disch. Rake Elem           093         T/C         6.181         7.960         243°58'         Disch. Rake Elem           094         T/C <t< td=""><td>079</td><td></td><td>6.181</td><td>8.280</td><td>4°281</td><td>Disch. Rake Elemen</td></t<>	079		6.181	8.280	4°281	Disch. Rake Elemen
082         T/C         6.181         8.280         208°38°         Disch. Rake Elem           083         T/C         6.181         8.280         243°58°         Disch. Rake Elem           084         T/C         6.181         8.120         4°28°         Disch. Rake Elem           085         T/C         6.181         8.120         36°48°         Disch. Rake Elem           086         T/C         6.181         8.120         69°7°         Disch. Rake Elem           087         T/C         6.181         8.120         208°38°         Disch. Rake Elem           088         T/C         6.181         8.170         243°58°         Disch. Rake Elem           089         T/C         6.181         7.960         4°28°         Disch. Rake Elem           090         T/C         6.181         7.960         26°43°         Disch. Rake Elem           091         T/C         6.181         7.960         208°36°         Disch. Rake Elem           092         T/C         6.181         7.960         243°58°         Disch. Rake Elem           093         T/C         6.181         7.800         4°28°         Disch. Rake Elem           095         T/C <td< td=""><td>080</td><td></td><td>6.181</td><td>8.280</td><td>36°48'</td><td>Disch. Rake Elemen</td></td<>	080		6.181	8.280	36°48'	Disch. Rake Elemen
083         T/C         6.181         8.280         243°58°         Disch. Rake Elem           084         T/C         6.181         8.120         4°28°         Disch. Rake Elem           085         T/C         6.181         8.120         36°48°         Disch. Rake Elem           086         T/C         6.181         8.120         69°7°         Disch. Rake Elem           087         T/C         6.181         8.120         208°38°         Disch. Rake Elem           088         T/C         6.181         8.170         243°58°         Disch. Rake Elem           089         T/C         6.181         7.960         4°28°         Disch. Rake Elem           090         T/C         6.181         7.960         26°43°         Disch. Rake Elem           091         T/C         6.181         7.960         208°36°         Disch. Rake Elem           092         T/C         6.181         7.960         243°58°         Disch. Rake Elem           093         T/C         6.181         7.800         4°28°         Disch. Rake Elem           094         T/C         6.181         7.800         36°48°         Disch. Rake Elem           095         T/C			6.181	8.280	69° 7'	Disch. Rake Elemen
084         T/C         6.181         8.120         4°28'         Disch. Rake Elem           085         T/C         6.181         8.120         36°48'         Disch. Rake Elem           086         T/C         6.181         8.120         69°7'         Disch. Rake Elem           087         T/C         6.181         8.100         208°38'         Disch. Rake Elem           088         T/C         6.181         8.100         243°58'         Disch. Rake Elem           089         T/C         6.181         7.960         4°28'         Disch. Rake Elem           090         T/C         6.181         7.960         26°43'         Disch. Rake Elem           091         T/C         6.181         7.960         69°7'         Disch. Rake Elem           092         T/C         6.181         7.960         208°36'         Disch. Rake Elem           093         T/C         6.181         7.960         243°58'         Disch. Rake Elem           094         T/C         6.181         7.800         4°28'         Disch. Rake Elem           095         T/C         6.181         7.800         36°48'         Ciach. Rake Elem           096         T/C         6.			6.181	8.280	208°38¹	Disch. Rake Ele. 90
085         T/C         6.181         8.120         36°48°         Disch. Rake Elem           086         T/C         6.181         8.120         69°7°         Disch. Rake Elem           087         T/C         6.181         8.120         208°38°         Disch. Rake Elem           088         T/C         6.181         8.170         243°58°         Disch. Rake Elem           089         T/C         6.181         7.960         4°28°         Disch. Rake Elem           090         T/C         6.181         7.960         26°43°         Disch. Rake Elem           091         T/C         6.181         7.960         69°7°         Disch. Rake Elem           092         T/C         6.181         7.960         208°36°         Disch. Rake Elem           093         T/C         6.181         7.960         243°58°         Disch. Rake Elem           094         T/C         6.181         7.800         4°28°         Disch. Rake Elem           095         T/C         6.181         7.800         36°48°         Cisch. Rake Elem           096         T/C         6.181         7.800         69°7°         Disch. Rake Elem           097         T/C         6.	083		6.181	8.280		Disch. Rake Elemen
086         T/C         6.181         8.120         69° 7°         Disch. Rake Elem           087         T/C         6.181         8.120         208°38°         Disch. Rake Elem           088         T/C         6.181         8.170         243°58°         Disch. Rake Elem           089         T/C         6.181         7.960         4°28°         Disch. Rake Elem           090         T/C         6.181         7.960         56°43°         Disch. Rake Elem           091         T/C         6.181         7.960         69°7°         Disch. Rake Elem           092         T/C         6.181         7.960         208°36°         Disch. Rake Elem           093         T/C         6.181         7.960         243°58°         Disch. Rake Elem           094         T/C         6.181         7.800         4°28°         Disch. Rake Elem           095         T/C         6.181         7.800         36°48°         Disch. Rake Elem           096         T/C         6.181         7.800         69°7°         Disch. Rake Elem           097         T/C         6.181         7.800         69°7°         Disch. Rake Elem	084		6.181	8.120	4°28'	Disch Rake Elemen
087         T/C         6.181         8.120         208°38¹         Disch. Rake Elem           088         T/C         6.181         8.100         243°58¹         Disch. Rake Elem           089         T/C         6.181         7.960         4°28¹         Disch. Rake Elem           090         T/C         6.181         7.960         6°43¹         Disch. Rake Elem           091         T/C         6.181         7.960         69°7¹         Disch. Rake Elem           092         T/C         6.181         7.960         208°36¹         Disch. Rake Elem           093         T/C         6.181         7.960         243°58¹         Disch. Rake Elem           094         T/C         6.181         7.800         4°28¹         Disch. Rake Elem           095         T/C         6.181         7.800         36°48¹         Disch. Rake Elem           096         T/C         6.181         7.800         69°7¹         Disch. Rake Elem           097         T/C         6.181         7.800         208°38¹         Disch. Rake Elem	085		6.181	8.120		Disch. Rake Elemen
088         T/C         6.181         8.170         243°58°         Disch. Rake Elem           089         T/C         6.181         7.960         4°28°         Disch. Rake Elem           090         T/C         6.181         7.960         26°43°         Disch. Rake Elem           091         T/C         6.181         7.960         69°7°         Disch. Rake Elem           092         T/C         6.181         7.960         208°36°         Disch. Rake Elem           093         T/C         6.181         7.960         243°58°         Disch. Rake Elem           094         T/C         6.181         7.800         4°28°         Disch. Rake Elem           095         T/C         6.181         7.800         36°48°         Disch. Rake Elem           096         T/C         6.181         7.800         69°7°         Disch. Rake Elem           097         T/C         6.181         7.800         208°38°         Disch. Rake Elem			6.181	8.120		Disch. Rake Elemen
089         T/C         6.181         7.960         4°28'         Disch. Rake Elem           090         T/C         6.181         7.960         £6°43'         Disch. Rake Elem           091         T/C         6.181         7.960         69°7'         Disch. Rake Elem           092         T/C         6.181         7.960         208°36'         Disch. Rake Elem           093         T/C         6.181         7.960         243°58'         Disch. Rake Elem           094         T/C         6.181         7.800         4°28'         Disch. Rake Elem           095         T/C         6.181         7.800         36°48'         Elem           096         T/C         6.181         7.800         69°7'         Disch. Rake Elem           097         T/C         6.181         7.800         208°38'         Disch. Rake Elem			6.181	8.120		Disch. Rake Elemen
090         T/C         6.181         7.960         26°43¹         Disch. Rake Elem           091         T/C         6.181         7.960         69°7¹         Disch. Rake Elem           092         T/C         6.181         7.960         208°36¹         Disch. Rake Elem           093         T/C         6.181         7.960         243°58¹         Disch. Rake Elem           094         T/C         6.181         7.800         4°28¹         Disch. Rake Elem           095         T/C         6.181         7.800         36°48¹         Ciccl. Rake Elem           096         T/C         6.181         7.800         69°7¹         Disch. Rake Elem           097         T/C         6.181         7.800         208°38¹         Disch. Rake Elem			6.181	8.170		Disch. Rake Elemen
091         T/C         6.181         7.960         69° 7¹         Disch. Rake Elem           092         T/C         6.181         7.960         208°36¹         Disch. Rake Elem           093         T/C         6.181         7.960         243°58¹         Disch. Rake Elem           094         T/C         6.181         7.800         4°28¹         Disch. Rake Elem           095         T/C         6.181         7.800         36°48¹         Ciscl. Rake Elem           096         T/C         6.181         7.800         69° 7¹         Disch. Rake Elem           097         T/C         6.181         7.800         208°38¹         Disch. Rake Elem			6.181	7.960	4°28'	Disch. Rake Elemen
092         T/C         6.181         7.960         208°36'         Disch. Rake Elem           093         T/C         6.181         7.960         243°58'         Disch. Rake Elem           094         T/C         6.181         7.800         4°28'         Disch. Rake Elem           095         T/C         6.181         7.800         36°48'         Disch. Rake Elem           096         T/C         6.181         7.800         69°7'         Disch. Rake Elem           097         T/C         6.181         7.800         208°38'         Disch. Rake Elem						Disch. Rake Elemen
093         T/C         6.181         7.960         243°58¹         Disch. Rake Elem           094         T/C         6.181         7.800         4°28¹         Disch. Rake Elem           095         T/C         6.181         7.800         36°48¹         Disch. Rake Elem           096         T/C         6.181         7.800         69° 7¹         Disch. Rake Elem           097         T/C         6.181         7.800         208°38¹         Disch. Rake Elem				7.960	69° 7'	Disch. Rake Elemen
094         T/C         6.181         7.800         4°28'         Disch. Rake Elem           095         T/C         6.181         7.800         36°48'         Disch. Rake Elem           096         T/C         6.181         7.800         69° 7'         Disch. Rake Elem           097         T/C         6.181         7.800         208°38'         Disch. Rake Elem						Disch. Rake Elemen
095         T/C         6.181         7.800         36°48°         Disch. Rake Elem           096         T/C         6.181         7.800         69°7°         Disch. Rake Elem           097         T/C         6.181         7.800         208°38°         Disch. Rake Elem						Disch. Rake Elemen
096         T/C         6.181         7.800         69° 7°         Disch. Rake Elem           097         T/C         6.181         7.800         208°38°         Disch. Rake Elem				<del></del>	·	
097 T/C 6.181 7.800 208°38 Disch. Rake Elem						Pisch. Rake Elemen
<u></u>						Disch. Rake Elemen
098   T/C   6.181   7.800   243°58' Disch. Rake Elem						Disch. Rake Elemen
	098	T/C	6.181	7.800	243°58'	Disch. Rake Elemen

TABLE I (continued)

ITEM.	TYPE	LOCATION		T DELLANCO	
NUMBER	SENSOR	AXIAL	RADIAL	CIRCUMPERENTIAL	REMARKS
101	Atmos				Barometric Pressure
103	PS				Venturi Throat
105	PS				Venturi Cavity
107	PT				Plenum
109	PS	-0.25	ID	315°	Casing (Same as 751)
111	PS	-0.25	OD	315°	Casing
13.3	PS	0.00	OD	306°	Casing
115	PS	0.25	OD	29 <b>4</b> °	Casing
117	PS	0.50	OD	180°	Casing
119	PS	0.75	OD	190°	Casing
121	PS	1.00	OD	310°	Casing
123	PS	1.25	OD	170°	Casing
125	PS	1.50	OD	290°	Casing
127	PS	1.75	OD	301.°	Casing
129	PS	2.00	OD	160°	Casing
131	PS	3.227	8.163	Vane 16	Suction Side Vane
133	PS	3.393	8.175	Vane 16	Suction Side Vane
135	1:5	3.361	8.184	Vane 16	Suction Side Vane
137	PS	3.837		Vane 16	Suction Side Vane
139	PS	4.115	8.191	Vane 16	Suction Side Vane
141	Ref.				Not Used
143	Ref.				Atmos.
145	Ref.	1			15 PSIG Reference
147	Ref.				30 PSIG Reference
			•		
201	Atmos				Barometric Pressure
203	PS				Same as 103
205	PS				Same as 105
207	PT				Same as 107 and 752
209	PS	4.281	8.192	Vane 16	Suction Side Vane
211	PS	4.559	8.194	Vane 16	Suction Side Vane
213	PS	-2.00	ID	45° & 135°	Two Manifolded Taps
215	PS	-2.00	ID	225° & 315°	Two Manifolded Taps
217	PS	-2.00	OD	45° & 135°	Two Manifolded Taps
219	PS	-2.00	OD	225° & 315°	Two Manifolded Taps
221	PS	2.25	OD	Vanes 18,22,	Four Manif. Taps
			]	40 & 44	
223	PS	2.25	ID	113.5°.156.5°	Four Manif. Taps
				290.5°&334.5°	
225	PS	6.181	OD	60°	Casing
227	PS	6.181	OD	120°	Casing
229	PS	6.181	OD	252°	Casing
231	PS	6.181	OD	300°	Casing
233	PS	6.181	ID	60°	Casing
235	PS_	6.181	ID	120°	Casing
237	PS	6.181	ID	252°	Casing
239	PS	6,181	ID	300°	Casing

TABLE I (continued)

ITEM	TYPE	LOCATION		DEMARKS	
NUMBER	SENSOR	AXIAL	RADIAL	CIRCUMFERENTIAL	REMARKS
241	Ref.				Not Used
243	Ref.				Atmos.
245	Ref.				15 PSIG Reference
247	Ref.				30 PSIG Reference
301		<del></del>			Not Used
303					Not Used
305	PS	3.393	8.175	Vane 17	Pres. Side of Vane
307	PS	3.837	8.189	Vane 17	Pres. Side of Vane
309	PS	4.281	8.191	Vane 17	Pres. Side of Vane
311	PT	LE	8.371	Vane 20	Leading Edge
313	PT	LE	8.371	Vane 40	Leading Edge
315	PT	LE	8.251	Vane 18	Leading Edge
317	PT	LE	8.251	Vane 47	Leading Edge
319	PT	LE	8.121	Vane 20	Leading Edge
321	PT	LE	8.121	Vane 40	Leading Edge
323	PT	LE	8.001	Vane 18	Leading Edge
325	PT	LE	8.001	Vane 47	Leading Edge
327	PT	LE	7.871	Vane 20	Leading Edge
329	PT	LE	7.871	Vane 40	Leading Edge
331	PT	6.181	7.800	20°47'	Disch. Rake Element
333	PT	6.181	7.800	52°57'	Disch. Rake Element
335	PT	6.181	7.800	195°29'	Disch. Rake Element
337	PT	6.181	7.800	227°491	Disch. Rake Element
339	PT	6.181	7.800	260° 81	Disch. Rake Element
341	Ref.				Not Used
343	Ref.				Atmos.
345	Ref.		·		15 PSIG Reference
347	Ref.				30 PSIG Reference
	· · · · · · · · · · · · · · · · · · ·				
401	PT	6.181	7.960	20°47'	Disch. Rake Element
403	PT	6,181	7.760	52°57'	Disch. Rake Element
405	PT	6.181	7.960	195°29'	Disch. Rake Element
407	PT	6.181	7.960	227°49'	Disch. Rake Element
409	PT	6.181	7.960	260° 81	Disch. Rake Element
411	PT	6.181	8.120	20°47'	Disch. Rake Element
413	PT	6.181	8.120	52°71'	Disch. Rake Element
415	PT	6.181	8.120	195°29'	Disch. Rake Element
417	PT	6.181	8.120	227°49'	Disch. Rake Element
419	PT	6.181	8.120	260° 8'	Disch. Rake Element
421	PT	6.181	8.280	20°47'	Disch. Rake Element
423	PT	6.191	8.280	52°57'	Disch. Rake Element
425	PT	6.131	8.280	195°29'	Disch. Rake Element
427	PT	6.181	8.280	227°49'	Disch. Rake Element
429	PT	6.181	8.280	260° 8 °	Disch. Rake Element
431	PT	6.181	8.440	20°47'	Disch. Rake Element
433	PŢ	6.181	8.440	52°57'	Disch. Rake Element

TABLE I (concluded)

ITEM	TYPE	LOCATION			1
NUMBER	SENSOR	AXTAL.	AXIAL RADIAL CIRCIMFERENTIAL		REMARKS
435	PT	6.181	8.440	195°29'	Disch. Rake Element
437	PT	6.181	8.440	227°49'	Disch. Rake Element
439	PT	6.181	8.440	260° 8'	Disch. Rake Element
441	Ref.				Not Used
443	Ref.				Atmos.
445	Ref.		<u> </u>		15 PSIG Reference
447	Ref.				30 PSTG Reference
700	XPT	-0.25	OD	67°16†	Flush MTD. Kistler
701	XPT	0.00	OD	75°28'	Flush MTD. Kistler
702	XPT	0.25	OD	60°	Flush MTD. Kistler
703	XPT	0.50	OD	68°49'	Flush MTD. Kistler
704	XPT	0.75	OD	53°51'	Flush MTD. Kistler
705	XPT	1.00	OD	63°16'	Flush MTD. Kistler
706	XPT	1.25	OD	49° 81	Flush MTD. Kistler
707	XPT	1.50	OD	59°23†	Flush MTD. Kistler
708					
709	<u> </u>		<u> </u>		
710	Prox.	1.25	OD	39°	Bentley Transducer
			<u> </u>		
				<u> </u>	
		L	ļ		
			<u> </u>		
	<b></b>		<u> </u>		
	<b></b>	<u> </u>	<b></b>		
	<u> </u>		ļ		
	<b> </b>	<b></b>	<b></b>		
<u></u>	<u> </u>	<b></b>	ļ	ļ	
	<del></del>	<b></b>		<u> </u>	<del></del>
	<del> </del>		<del> </del>		
	<b></b>	ļ	<b>}</b>		
<b></b>	<del> </del>	ļ	<b></b>		
<del></del>	<del> </del>		<u> </u>		<del></del>
<del></del>	<del> </del>	<b> </b>	<del>                                     </del>	<del> </del>	<u> </u>
<del> </del>	<del> </del>	<del> </del>	<del> </del>		<del>                                     </del>
<u> </u>	<del> </del>	<del> </del>	<del> </del>		<u> </u>
<b> </b>	<del> </del> -	<del> </del>	<del> </del>		
<del> </del>	<del> </del>	<del> </del>	<del> </del>	<u> </u>	<del>                                     </del>
<del></del>	<del> </del>	<del>                                     </del>	<del>                                     </del>		
<del></del>	<del> </del>	<del> </del>	<del> </del>		
<del> </del>	<del> </del>	<del>                                     </del>	<del> </del>		<del> </del>
<u> </u>	<del> </del>		†	<del>                                     </del>	
	<del> </del>	<b>†</b>	1		
<b> </b>	<del> </del>	<del> </del>	<del> </del>	·	<del>                                     </del>
	<del></del>	<del></del>	.l	<del></del>	

TABLE II CALIBRATION OF SAMPLE THERMOCOUPLES

BATH °C <sup>A</sup>	SET PT	AVG. OF 9 SAMPLES	MAX. SPREAD ± °F
65	148.1	148.4	0.1
100	211.4	210.9	0.1
150	300.8	301.4	0.4
175	346.5	346.4	0.5

TABLE III CALIBRATION OF TEMPERATURE READOUT ELECTRONICS

SET PT. Avg+ °F	PRINTER OUTPUT Avg* °F	MAX. SPREAD ± °F
148.2	148.3	0.2
210.7	210.7	0.2
301.7	301.7	0.3
345.4	345.5	0.4

<sup>+</sup> Average of two calibrated T/C's.
\* Average of eight channels.

A Oil Bath Set Pt.
B Mueller bridge readout converted to temperature.

TABLE IV

MASS-AVERAGED COMPRESSOR PERFORMANCE

		RO'	TOR	STA	AGE		
TEST I.D.	SPEED	PR	η	PR	η	MASS FLOW	M
208180106840 0315240	40%	1.209 1.23 1.23	.99 .927	1.161	.772 .871	9.63 8.91	
0415840 0514040 0612740 0711240 0806840	*	1.23 1.224 1.218 1.214 1.21	.901 .957 .966 .981 .988	1.215 1.204 1.192 1.179 1.16	.844 .879 .859 .829	10.34 10.88 11.21 11.59	
0901340 208220215850 0315550 0415050	50% *	1.208 1.377 1.376 1.368	.989 .899 .915 .925	1.151 1.35 1.35 1.341	.729 .841 .857 .866	11.60 11.48 11.93 12.48	
0514450 0613650 0712550 0810950 0907550		1.366 1.363 1.361 1.362 1.36	.944 .958 .966 .968	1.331 1.31 1.292 1.266 1.237	.861 .83 .80 .732 .661	12.86 13.38 13.49 13.63 13.66	
1215860 1315560 1315260 1514860	60% *	1.58 1.577 1.573 1.57	.903 .913 .92 .924	1.529 1.525 1.515 1.498	.834 .841 .840 .823	14.15 14.67 14.88 15.26	
1614460 1713660 1812760 1911060 208240215670	70%*	1.573 1.57 1.57 1.57 1.828	.93 .927 .927 .925 .889	1.475 1.438 1.414 1.38 1.724	.791 .737 .701 .648 .795	15.25 15.23 15.19 15.23 16.92	
0315570 0415370 0515070 0614270		1.827 1.83 1.829 1.828	.889 .893 .897 .892	1.717 1.697 1.668 1.616	.79 .773 .750 .698	16.90 16.91 17.08 16.99	
1115882 1215782 1315682 1415582 1515382	82%*	2.057 2.065 2.07 2.076 2.079	.810 .815 .814 .818 .819	1.883 1.876 1.868 1.861 1.838	.702 .698 .686 .684	18.12 18.18 18.21 18.20 18.31	
208300215890 0315990 0415890 0515690	90% *	2.262 2.28 2.292 2.296	.764 .773 .778 .779	2.035 2.049 2.041 2.013	.655 .662 .658 .643	19.04 19.25 19.33 19.60	
0615090 0915800 1015700 1115500 1215100	100%*	2.299 2.594 2.616 2.624 2.635	.784 .733 .741 .743 .746	1.944 2.247 2.24 2.226 2.173	.611 .609 .607 .601 .581	19.56 20.76 21.10 21.15 21.21	

<sup>\*</sup> To be further considered in within-blade data reduction.

TABLE V

## IDENTIFICATION OF SYMBOLS FOR 40%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
208180901340	Z
208180806840	×
208180711240	4
208180612740	<b>\$</b>
208180514040	×
208180415840	÷
208180315240	<u> 4</u>
208180106840	Ø

TABLE VI

# IDENTIFICATION OF SYMBOLS FOR 50%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
208220907550	Z
208220810950	Z
208220712550	4
208220613650	₫.
208220514450	×
208220415050	<del>-i-</del>
208220315550	<u> 4</u> 5,
208220215850	O

### TABLE VII

### IDENTIFICATIC ' OF SYMBOLS FOR 60%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMPOL
208221911060	Z
208221812760	X
208221713660	4
208221614460	Φ
208221514860	×
208221315260	÷
208221315560	₫,
208221215360	Ф

### Table VIII

## IDENTIFICATION OF SYMBOLS FOR 70%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
208240614270	<b></b>
208240515070	×
208240415370	÷
208240315570	<i>ι</i> Δ.
208240215670	<b>O</b>

TABLE IX

IDENTIFICATION OF SYMBOLS
FOR 82%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
208241515382	$\Diamond$
208241415582	×
208241315682	+
208241215782	⚠
208241115882	0

TABLE X

IDENTIFICATION OF SYMBOLS
FOR 90%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
208300615090	Ŷ
208300515690	X
208300415890	÷
208300315990	Δ
208300215890	O

TABLE XI

## IDENTIFICATION OF SYMBOLS FOR 100%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
208301215100	×
208301115500	+
208301015700	Z
208300915800	O

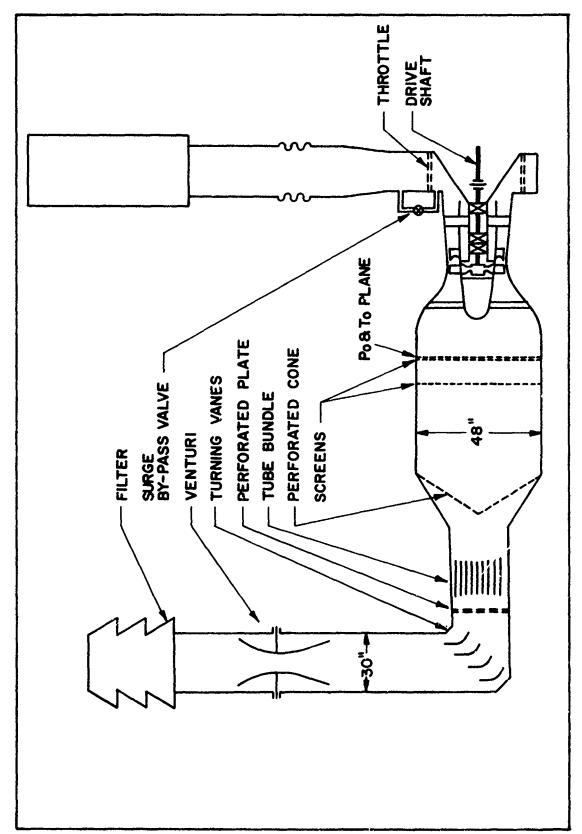


Fig. 1. Compressor Facility Flow Path

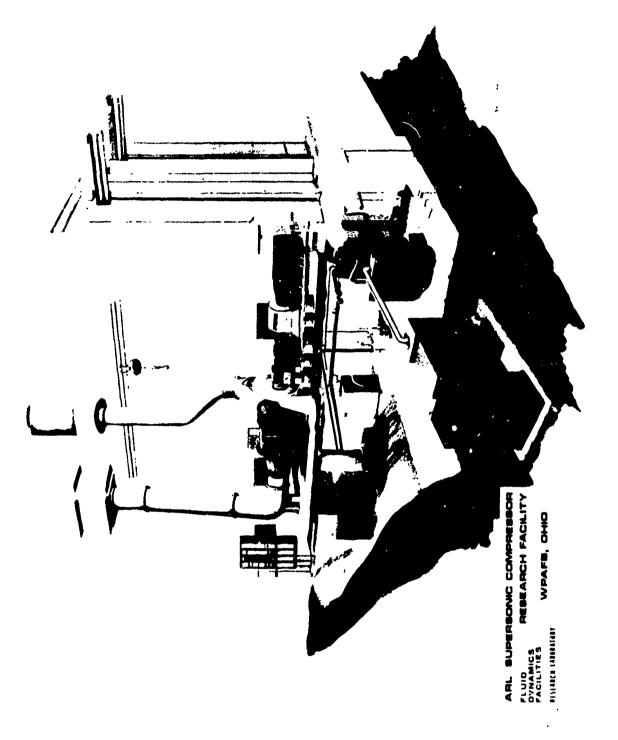
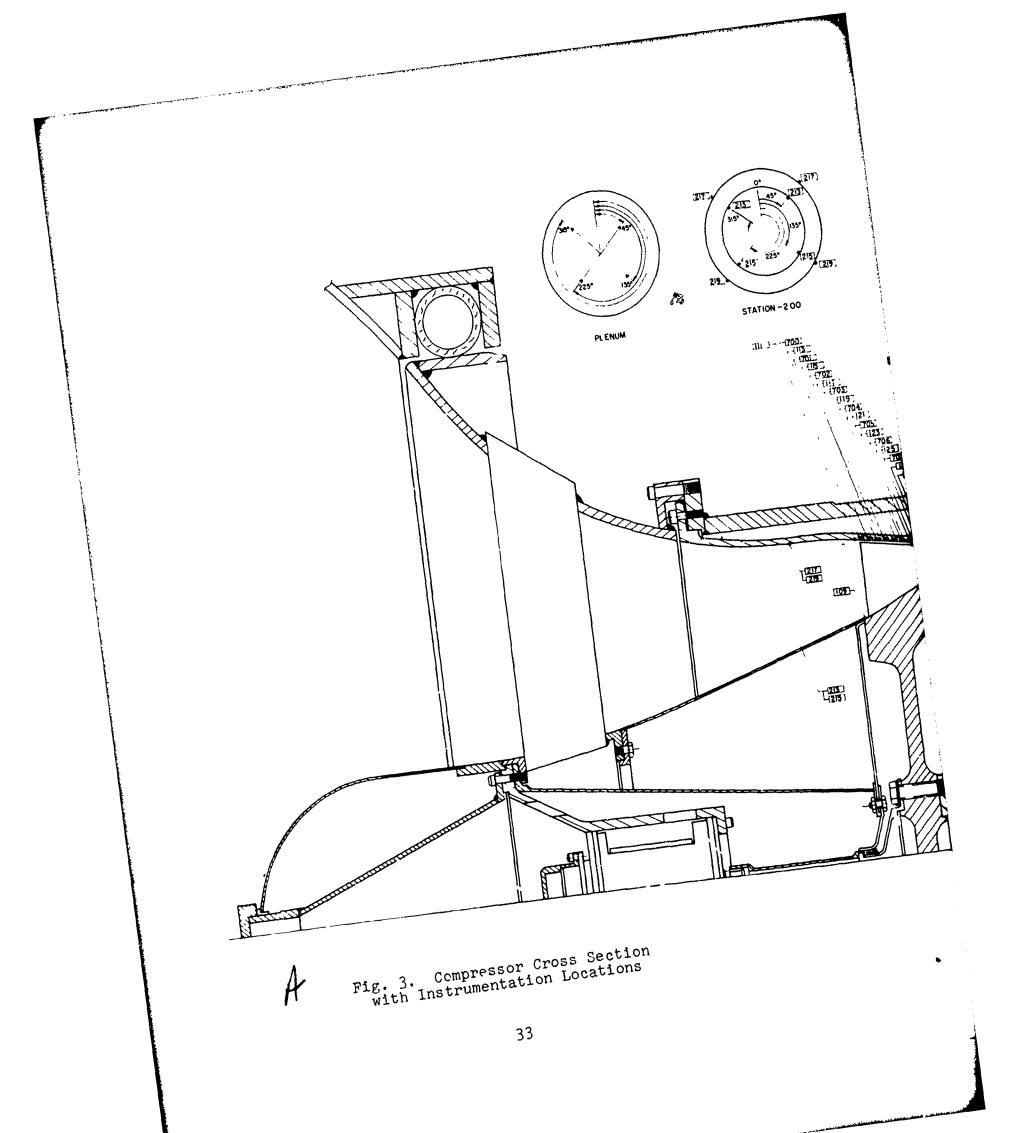


Fig. 2. Test Facility



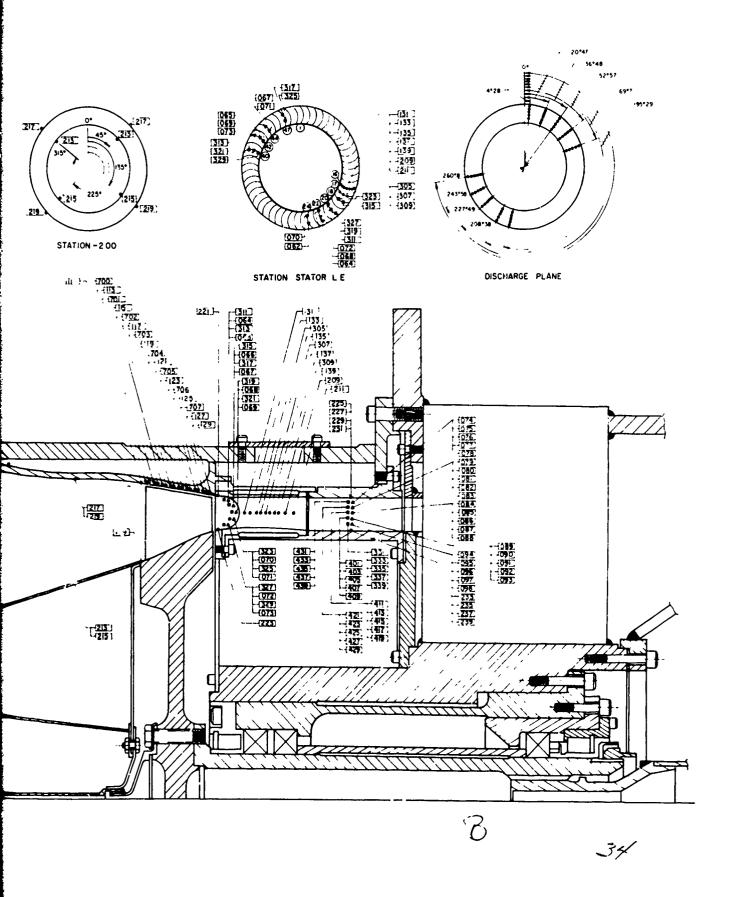




Fig. 4. Rotor Blades on Wheel

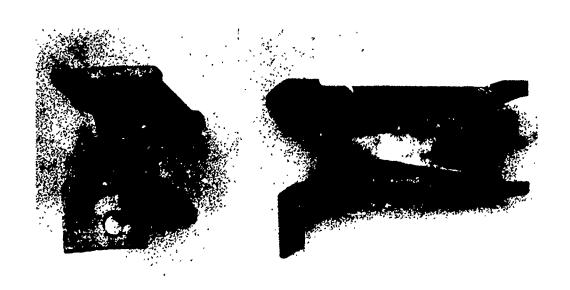


Fig. 5. Stator Blades



Fig. 6. Vehicle Instrumentation Bulkhead

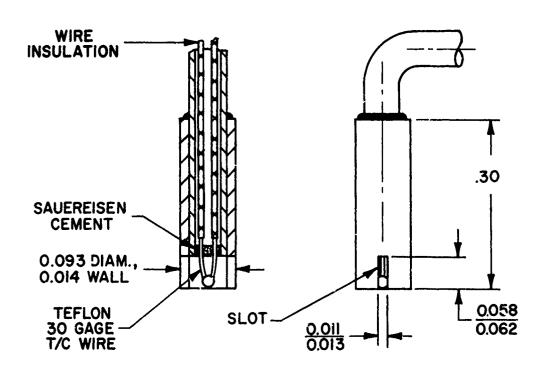


Fig. 7. Slot Vented Temperature Probe Design

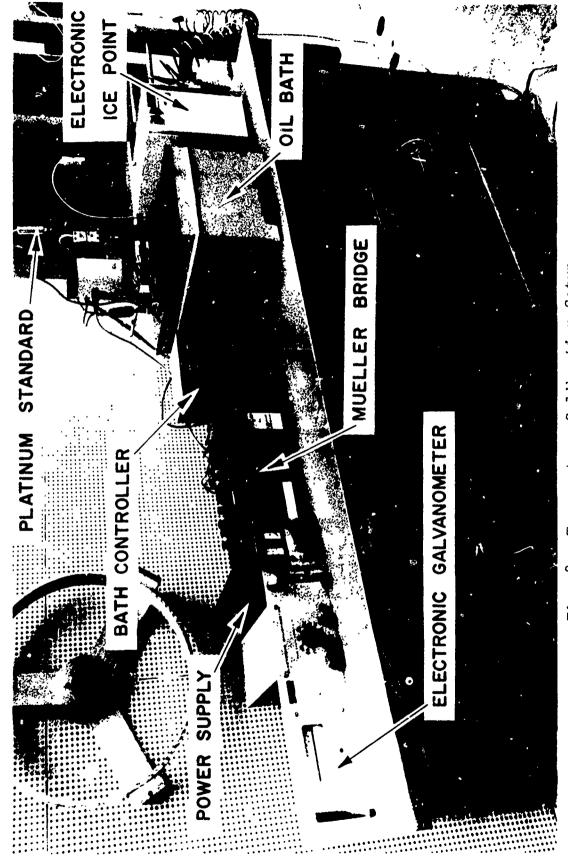


Fig. 8. Temperature Calibration Setup

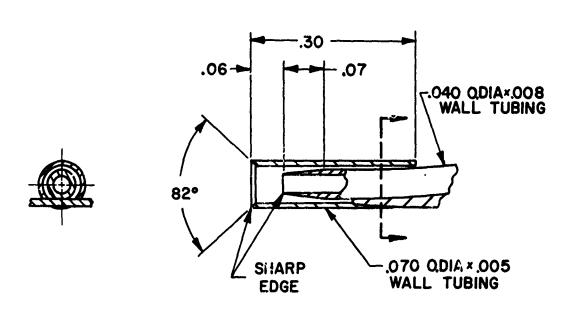
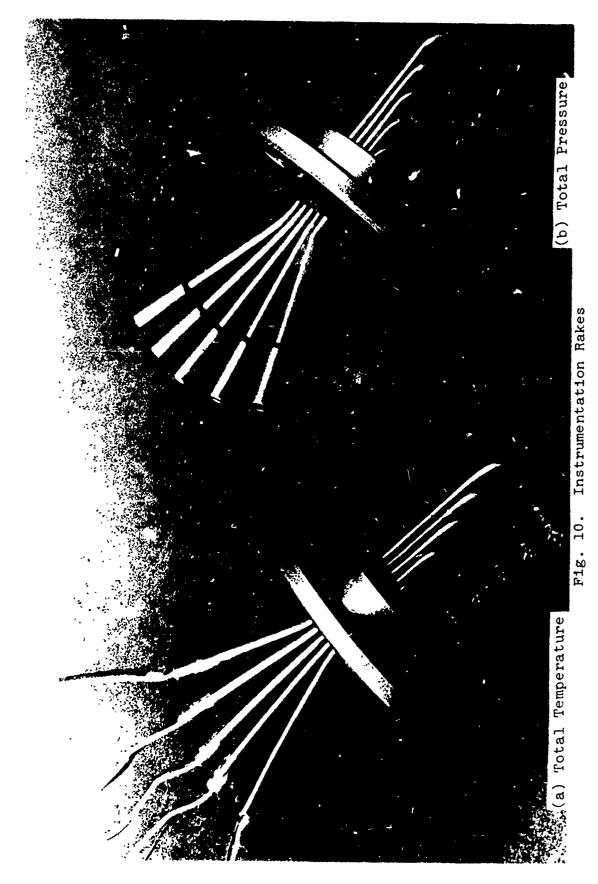


Fig. 9. Kiel Stagnation Tube Design



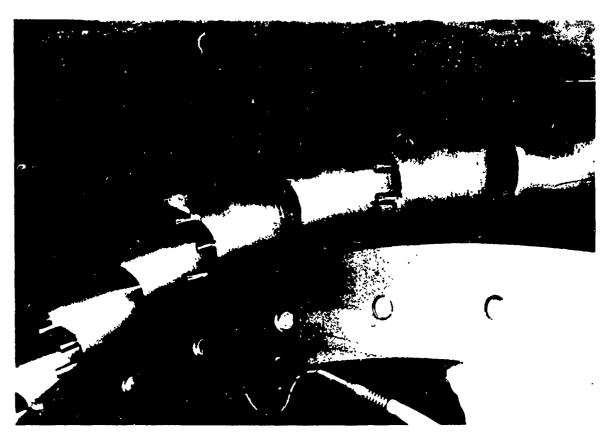


Fig. 11. Vane-Mounted Instrumentation

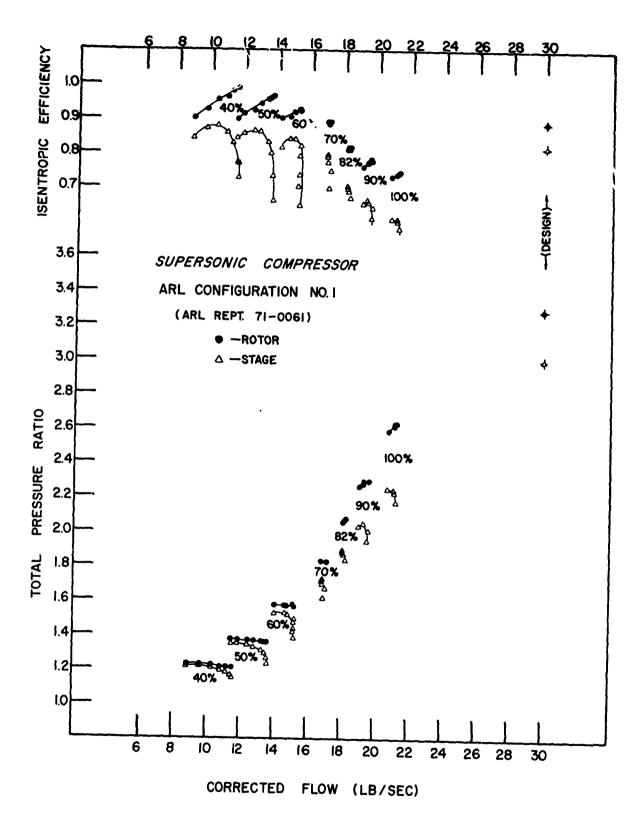


Fig. 12. Compressor Performance Map

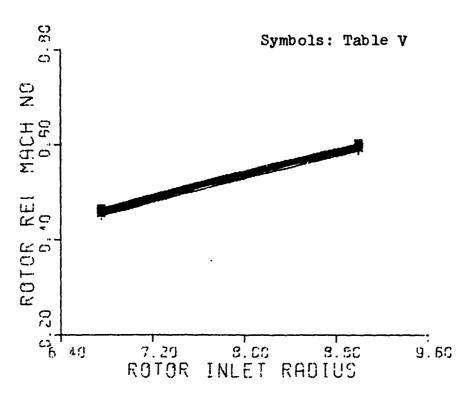


Fig. 13. Rotor Relative Mach Number vs Inlet Radius (40% Speed)

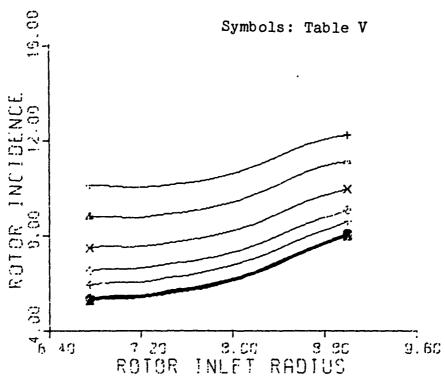


Fig. 14. Rotor Incidence vs Inlet Radius (40% Speed)

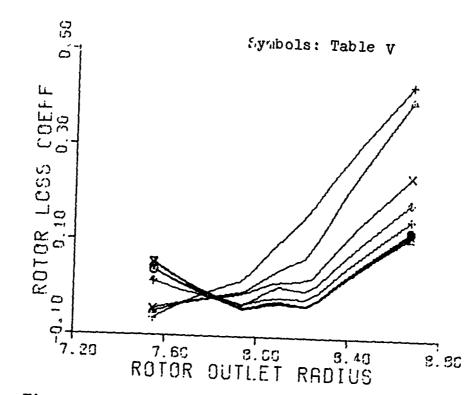


Fig. 15. Rotor Loss Coefficient vs Outlet Radius (40% Speed)

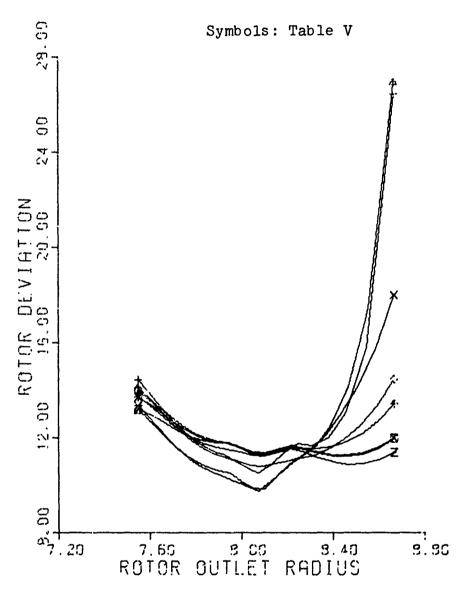


Fig. 16. Rotor Deviation vs Outlet Radius (40% Speed)

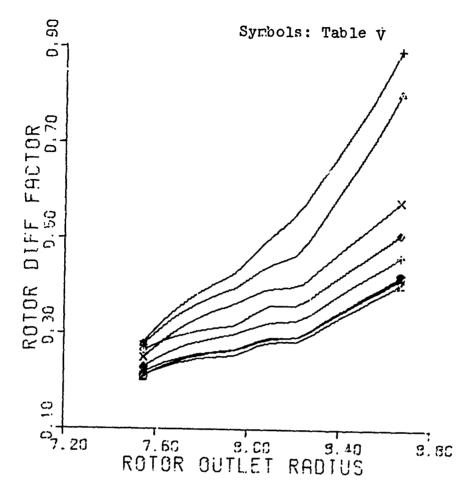


Fig. 17. Rotor Diffusion Factor vs Outlet Radius (40% Speed)

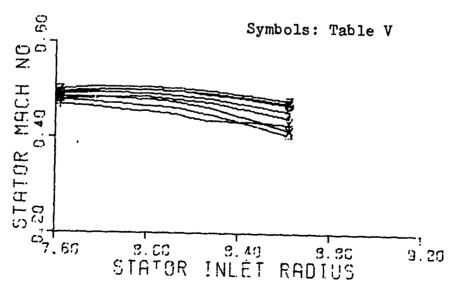


Fig. 18. Stator Mach Number vs Inlet Radius (40% Speed)

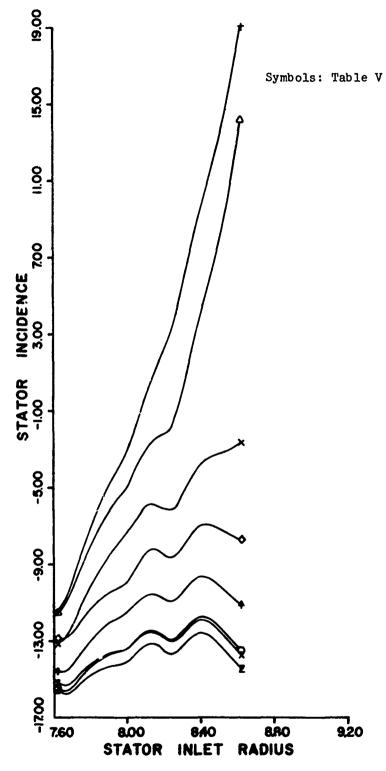


Fig. 19. Stator Incidence vs Inlet Radius (40% Speed)

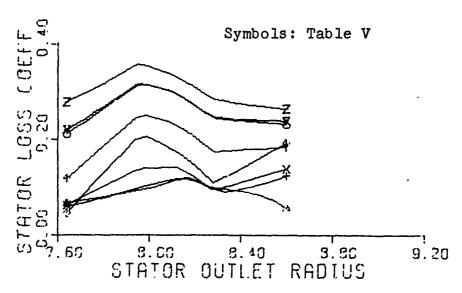


Fig. 20. Stator Loss Coefficient vs Outlet Radius (40% Speed)

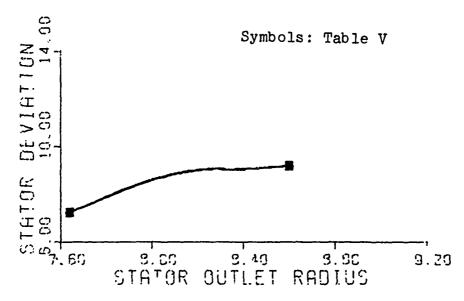


Fig. 21. Stator Deviation vs Outlet Radius (40% Speed)

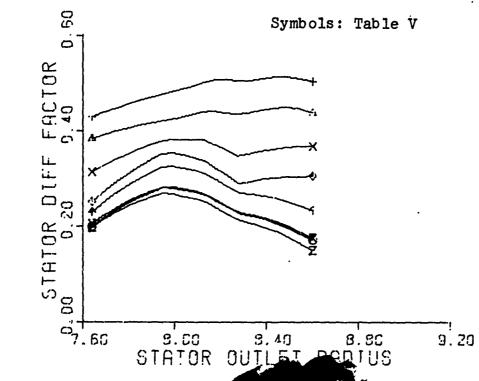


Fig. 22. Stator Diff on ractor vs Outlet Radius (40% Speed)

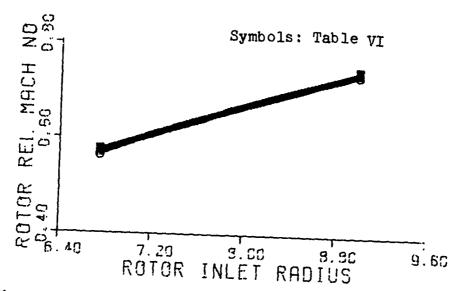


Fig. 23. Rotor Relative Mach Number vs Inlet Radius (50% Speed)

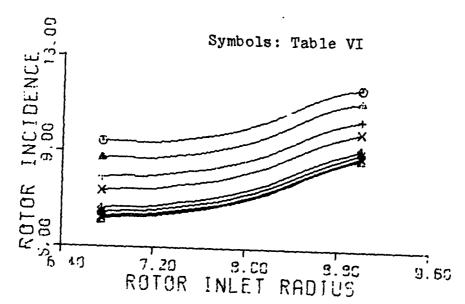


Fig. 24. Rotor Incidence vs Inlet Radius (50% Speed)

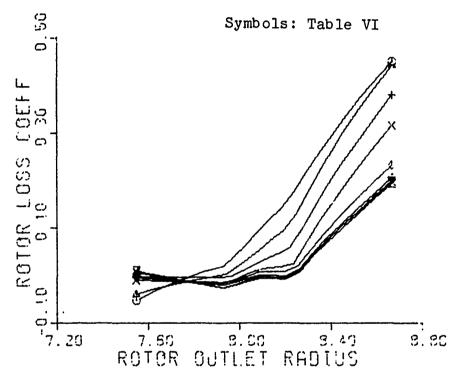


Fig. 25. Rotor Loss Coefficient vs Outlet Radius (50% Speed)

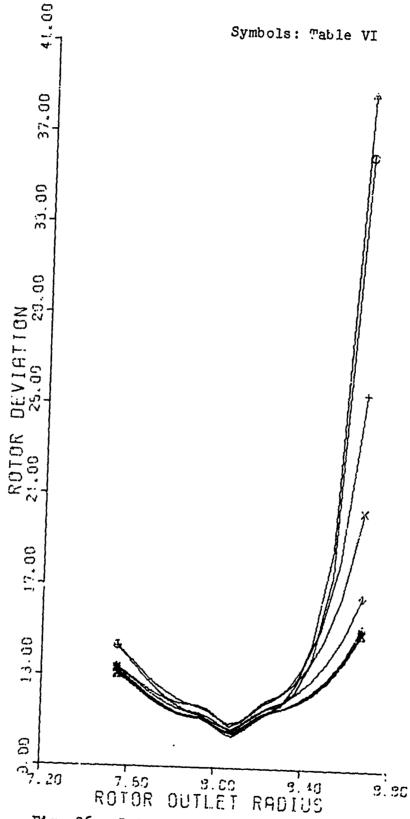


Fig. 26. Rotor Deviation vs Outlet Radius (50% Speed)

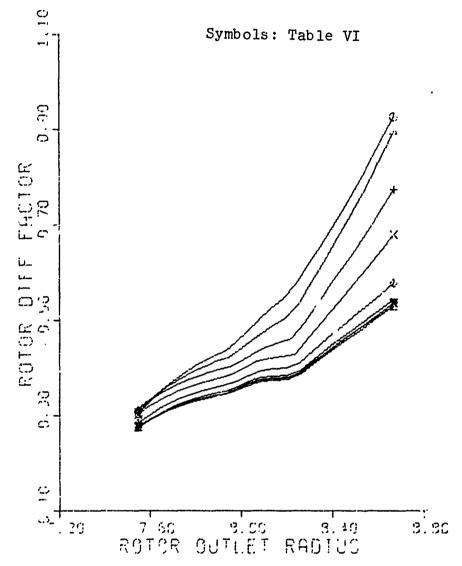


Fig. 27. Rotor Diffusion Factor vs Outlet Radius (50% Speed)

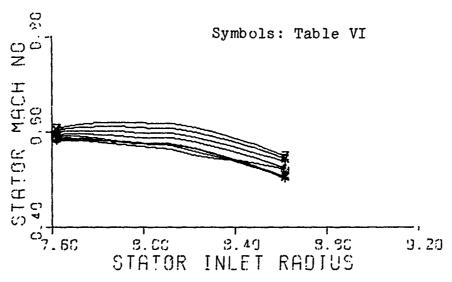


Fig. 28. Stator Mach Number vs Inlet Radius (50% Speed)

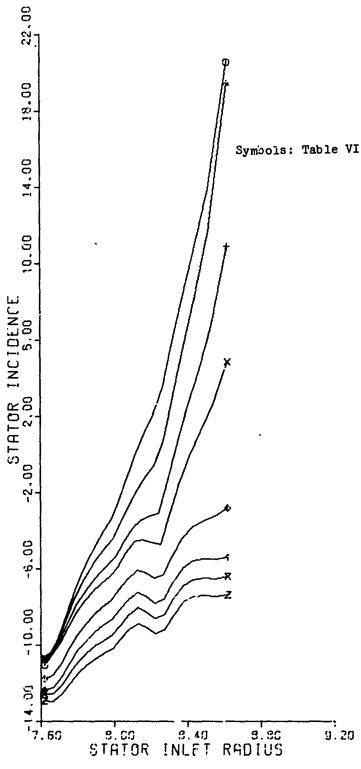


Fig. 29. Stator Incidence vs Inlet Radius (50% Speed)

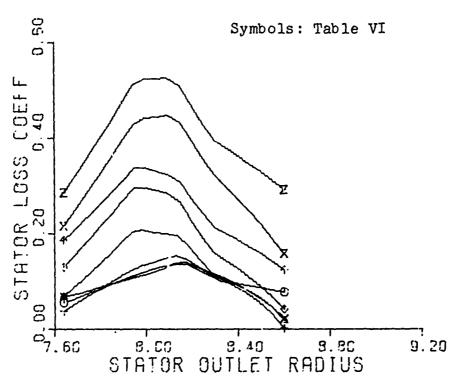


Fig. 30. Stator Loss Coefficient vs Outlet Radius (50% Speed)

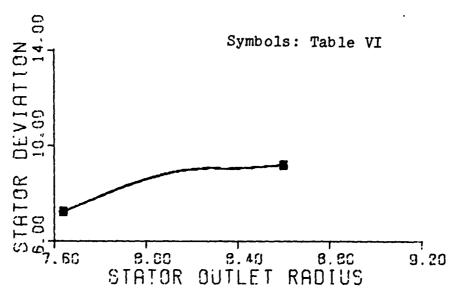


Fig. 31. Stator Deviation vs Outlet Radius (50% Speed)

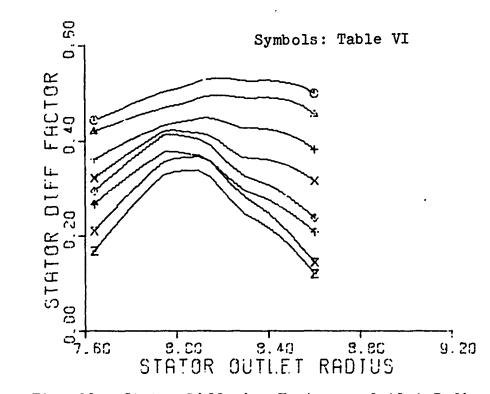


Fig. 32. Stator Diffusion Factor vs Outlet Radius (50% Speed)

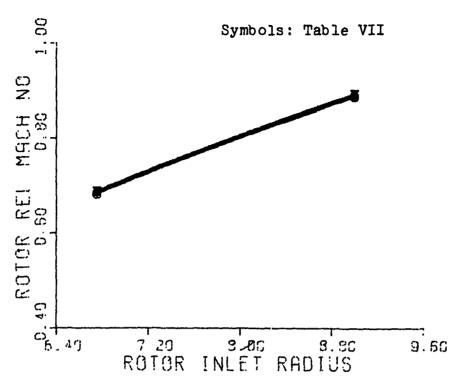


Fig. 33. Rotor Relative Mach Number vs Inlet Radius (60% Speed)

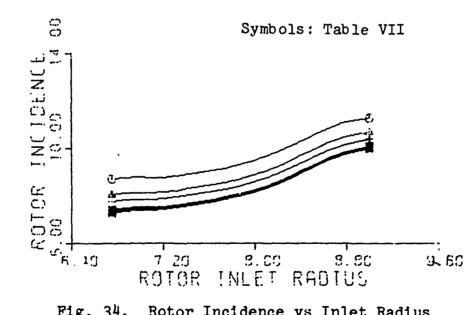


Fig. 34. Rotor Incidence vs Inlet Radius (60% Speed)

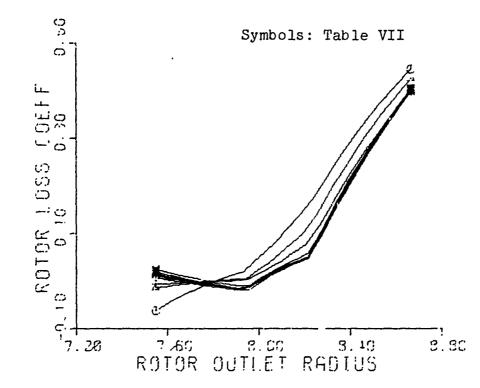


Fig. 35. Rotor Loss Coefficient vs Outlet Radius (60% Speed)

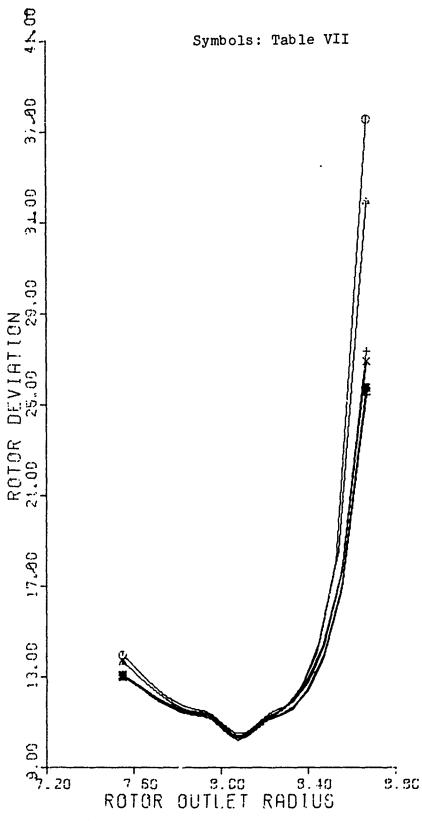


Fig. 36. Rotor Deviation vs Outlet Radius (60% Speed)

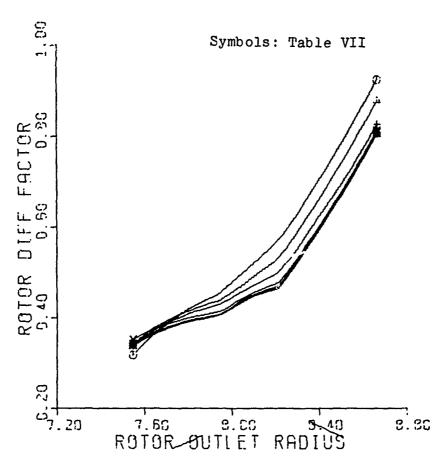


Fig. 37. Rotor Diffusion Factor vs Outlet Radius (60% Speed)

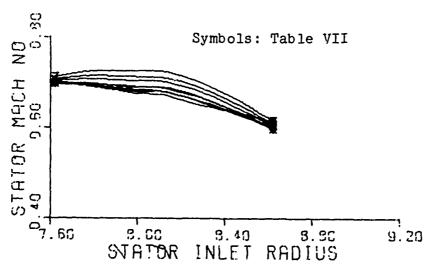


Fig. 38. Stator Mach Number vs Inlet Radius (60% Speed)

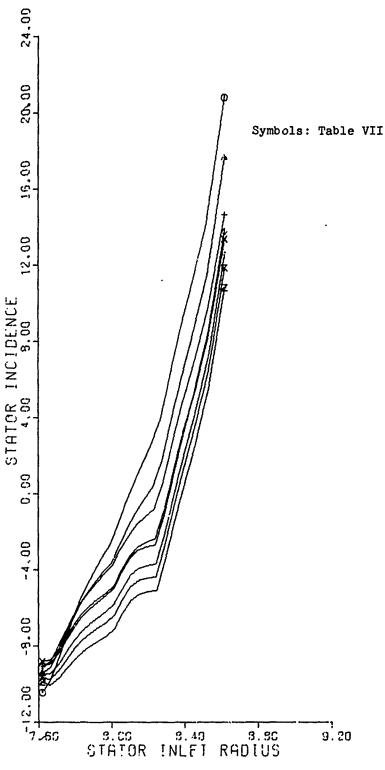


Fig. 39. Stator Incidence vs Inlet Radius (60% Speed)

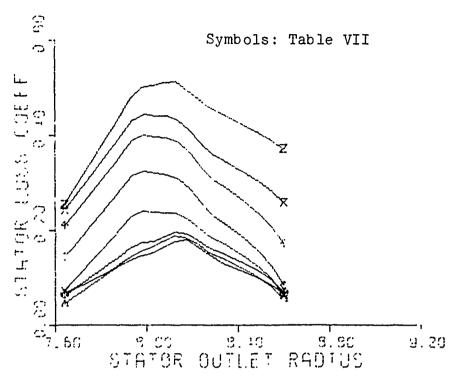


Fig. 40. Stator Loss Coefficient vs Outlet Radius (60% Speed)

在在外的,这个人的,也是是一个人的人,也是不是一个人的人,我们也是有一个人的人,我们也是一个人的人,我们就是我们的人的人,我们也是我们的人的人的人,我们的人的人

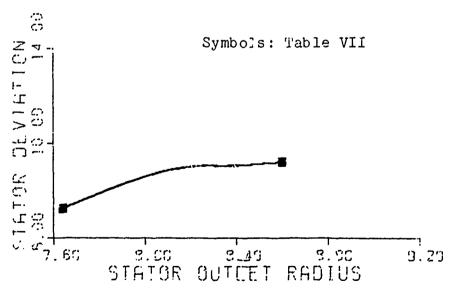


Fig. 41. Stator Deviation :3 Outlet Radius (60% Speed)

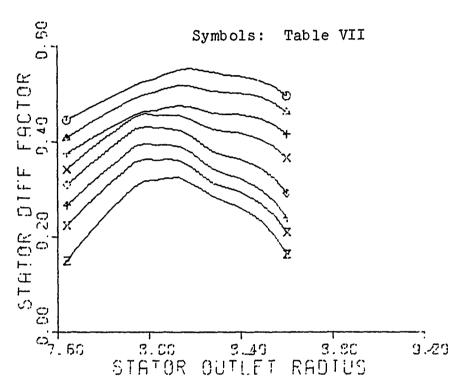


Fig. 42. Stator Diffusion Factor vs Outlet Radius (60% Speed)

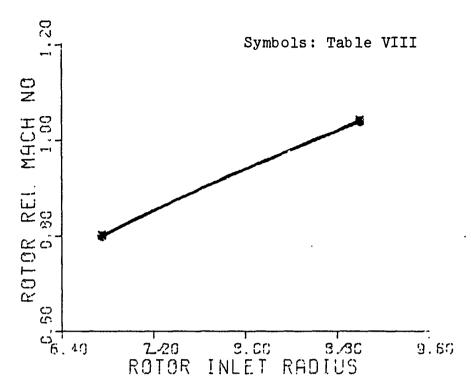


Fig. 43. Rotor Relative Mach Number vs Inlet Radius (70% Speed)

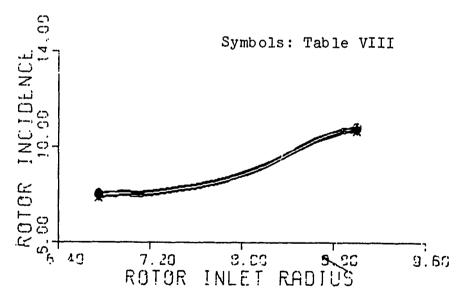


Fig. 44. Rotor Incidence vs Inlet Radius (70% Speed)

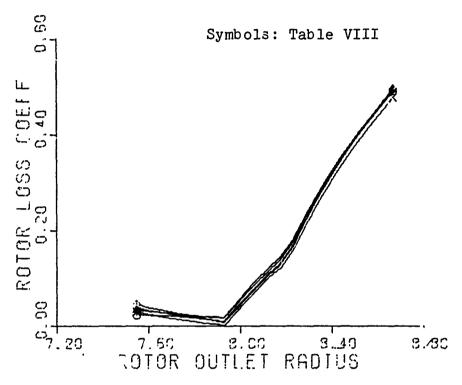


Fig. 45. Rotor Loss Coefficient vs Outlet Radius (70% Speed)

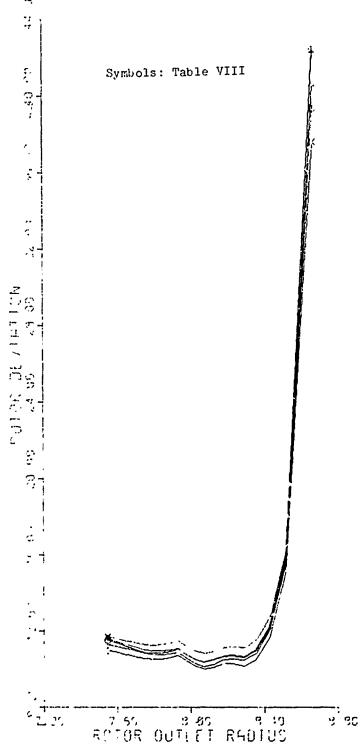


Fig. 46. Rotor Deviation vs Outlet Radius (70% Speed)

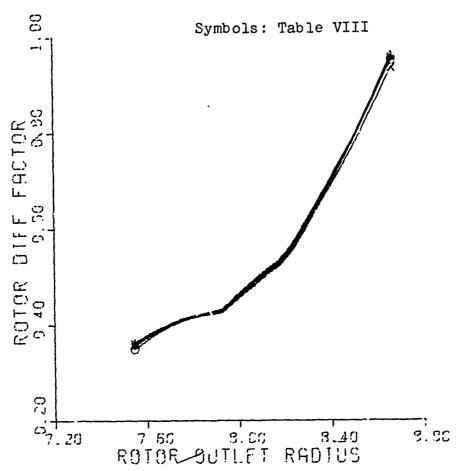


Fig. 47. Rotor Diffusion Factor vs Outlet Radius (70% Speed)

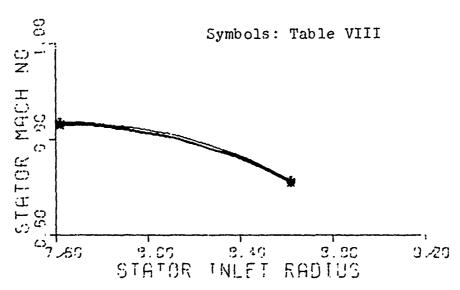
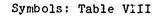
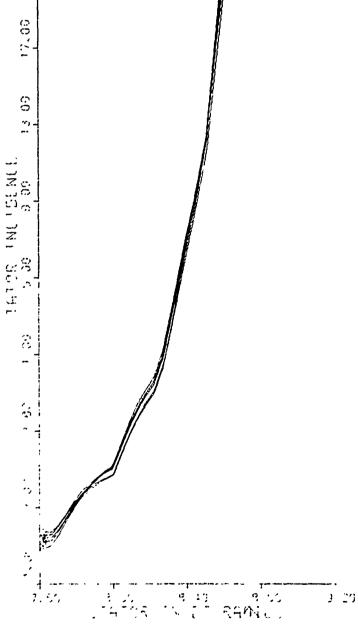


Fig. 48. Stator Mach Number vs Inlet Radius (70% Speed)







S

Fig. 49. Stator Incidence vs Inlet Radius (70% Speed)

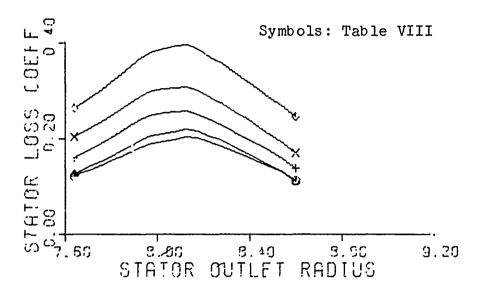


Fig. 50. Stator Loss Coefficient vs Outlet Radius (70% Speed)

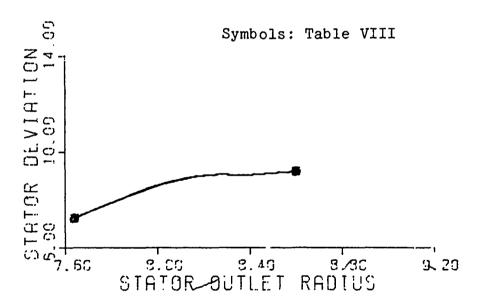


Fig. 51. Stator Deviation vs Outlet Radius (70% Speed)

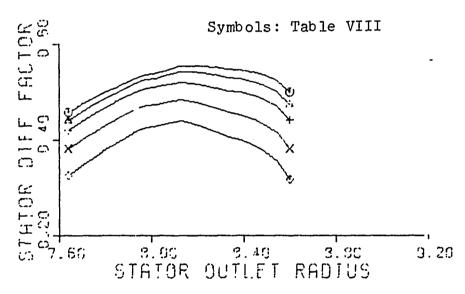


Fig. 52. Stator Diffusion Factor vs Outlet Radius (70% Speed)

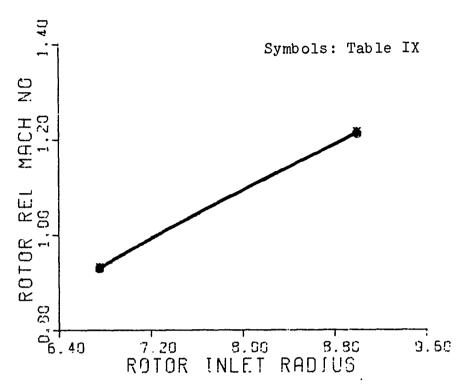


Fig. 53. Rotor Relative Mach Numbers vs Inlet Radius (82% Speed)

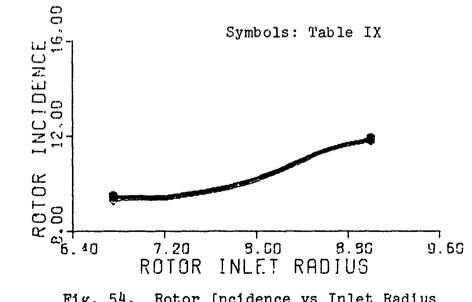


Fig. 54. Rotor Incidence vs Inlet Radius (82% Speed)

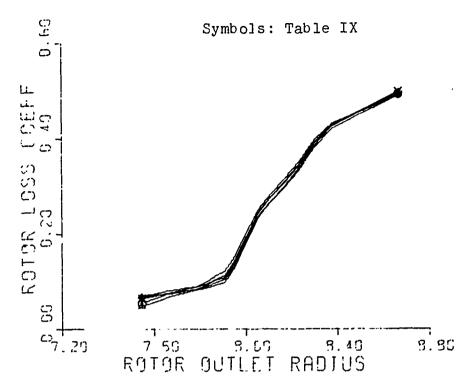


Fig. 55. Rotor Loss Coefficient vs Outlet Radius (82% Speed)

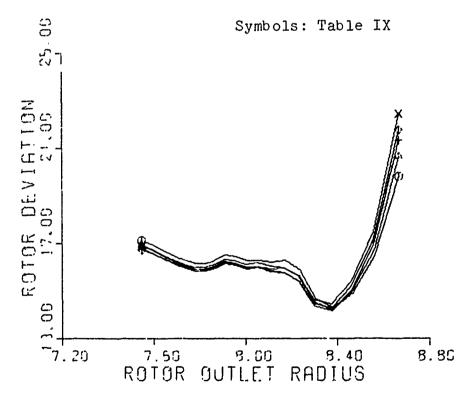


Fig. 56. Rotor Deviation vs Outlet Radius (82% Speed)

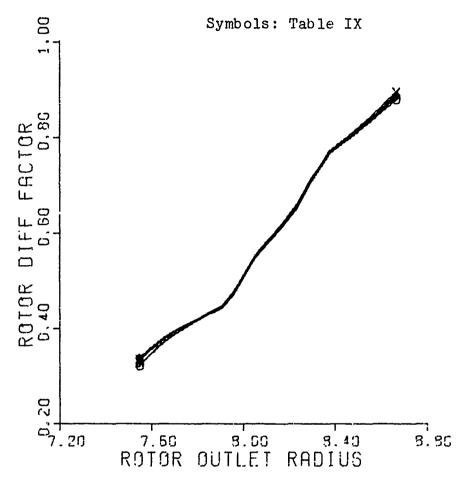


Fig. 57. Rotor Diffusion Factor vs Outlet Radius (82% Speed)

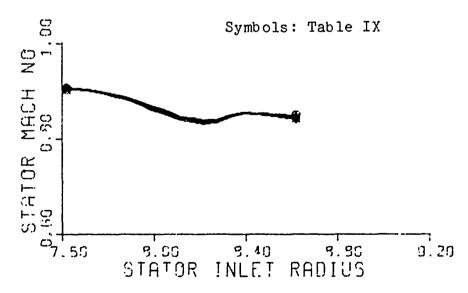
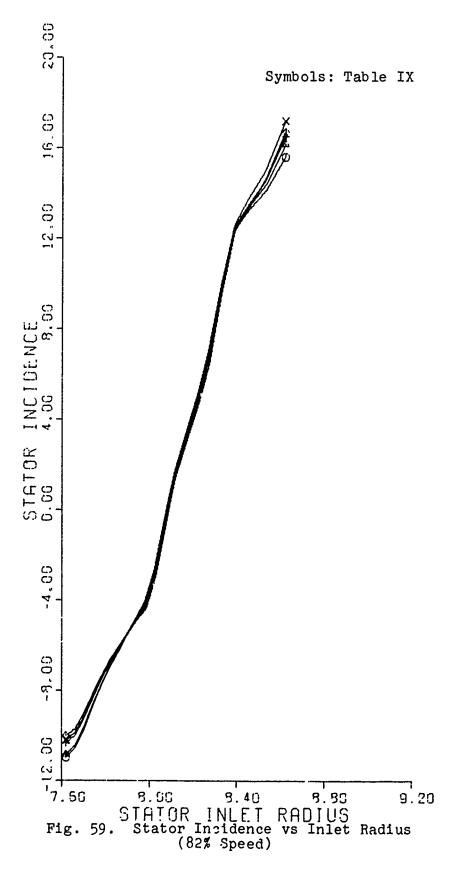


Fig. 58. Stator Mach Number vs Inlet Radius (82% Speed)



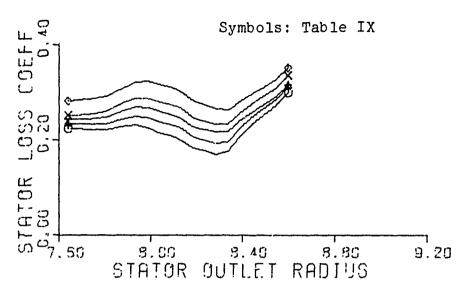


Fig. 60. Stator Loss Coefficient vs Outlet Radius (82% Speed)

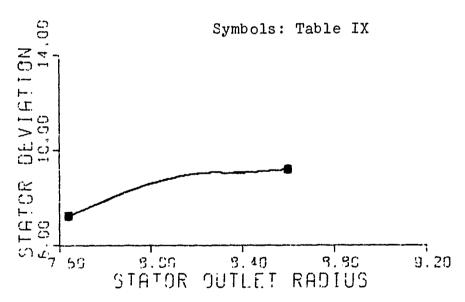


Fig. 61. Stator Deviation vs Outlet Radius (82% Speed)

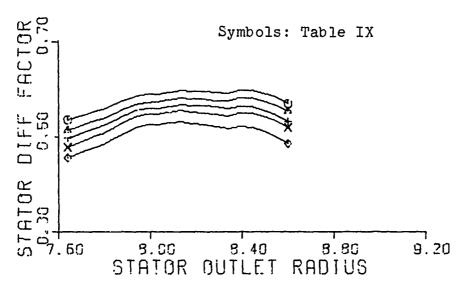


Fig. 62. Stator Diffusion Factor vs Outlet Radius (82% Speed)

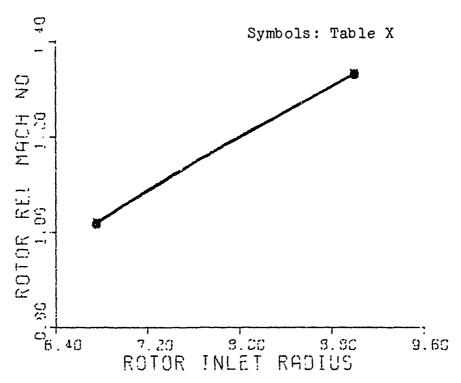


Fig. 63. Rotor Relative Mach Number vs Inlet Radius (90% Speed)

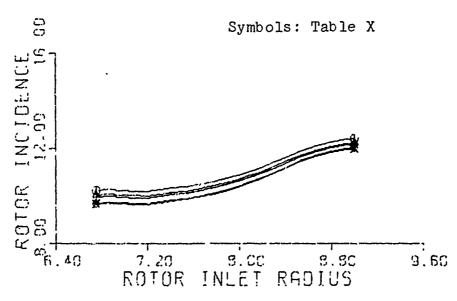


Fig. 64. Rotor Incidence vs Inlet Radius (90% Speed)

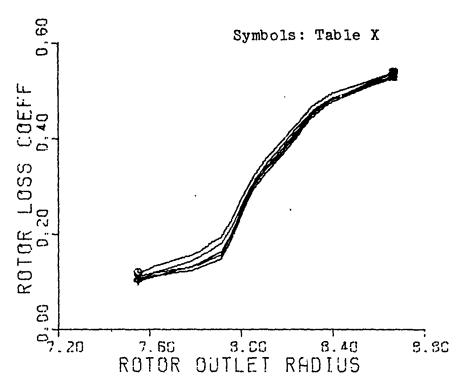


Fig. 65. Rotor Loss Coefficient vs Outlet Radius (90% Speed)

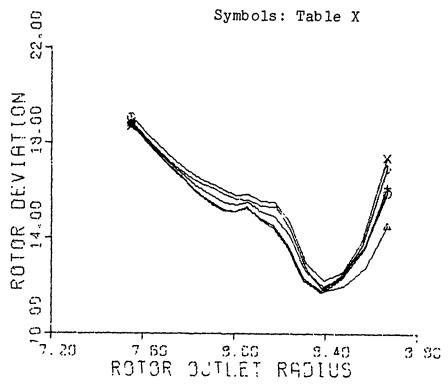


Fig. 66. Rotor Deviation vs Outlet Radius (90% Speed)

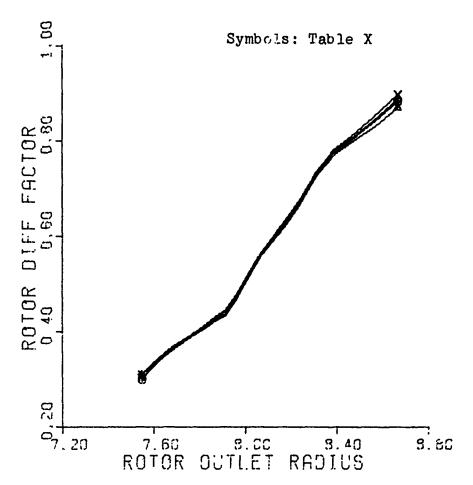


Fig. 67. Rotor Diffusion Factor vs Outlet Radius (90% Speed)

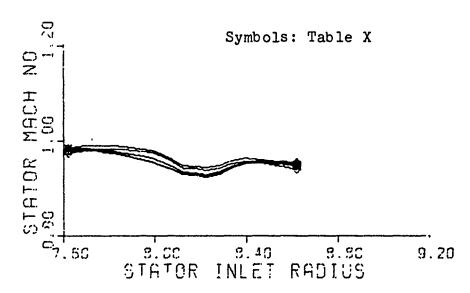
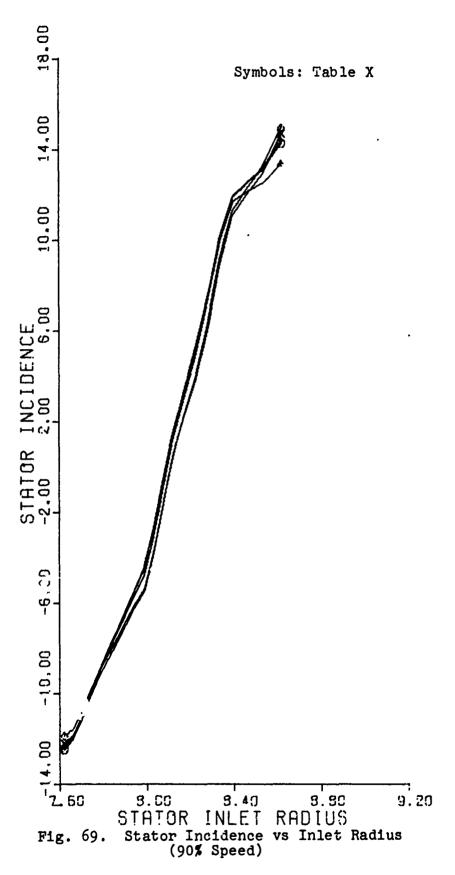


Fig. 68. Stator Mach Number vs Inlet Radius (90% Speed)



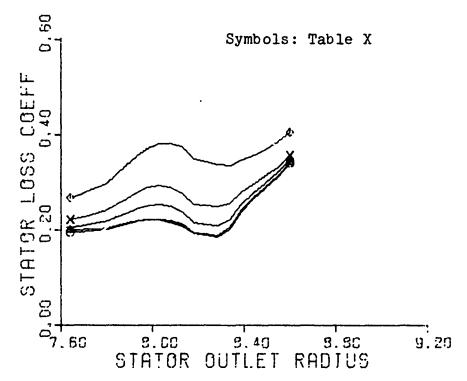


Fig. 70. Stator Loss Coefficient vs Outlet Radius (90% Speed)

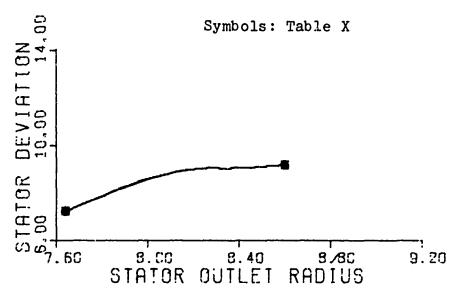


Fig. 71. Stator Deviation vs Outlet Radius (90% Speed)

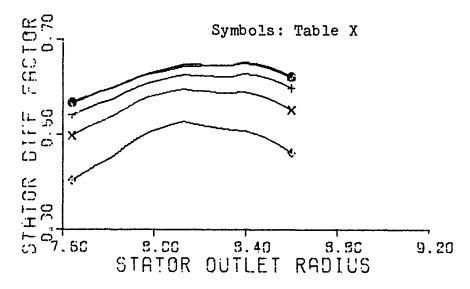


Fig. 72. Stator Diffusion Factor vs Outlet R. ius (90% Speed)

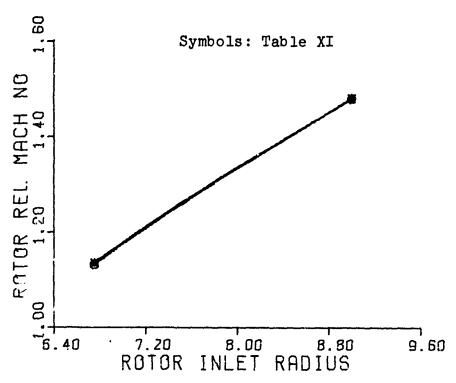


Fig. 73. Rotor Relative Mach Number vs Inlet Radius (100% Speed)

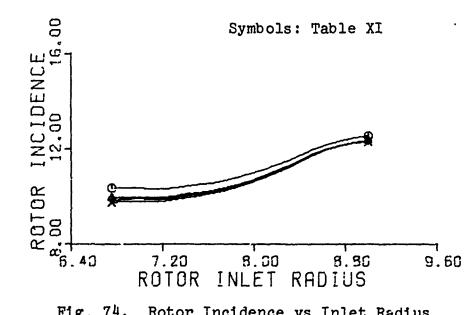


Fig. 74. Rotor Incidence vs Inlet Radius (100% Speed)

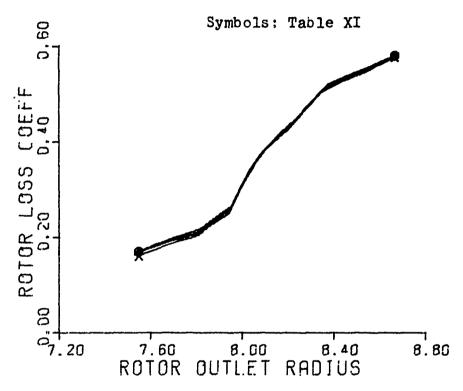


Fig. 75. Rotor Loss Coefficient vs Outlet Radius (100% Speed)

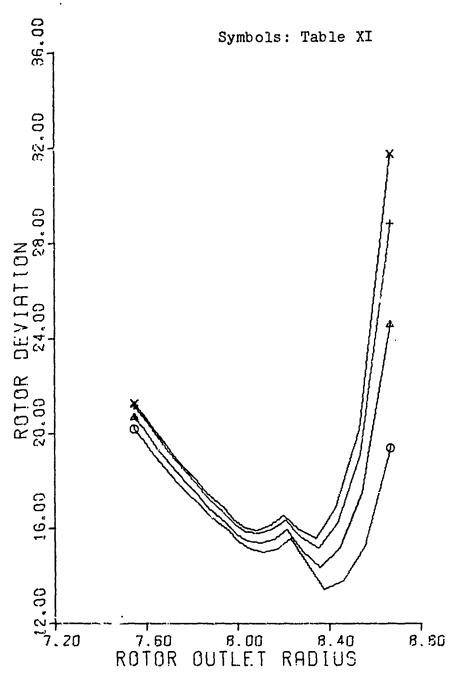


Fig. 76. Rotor Deviation vs Outlet Radius (100% Speed)

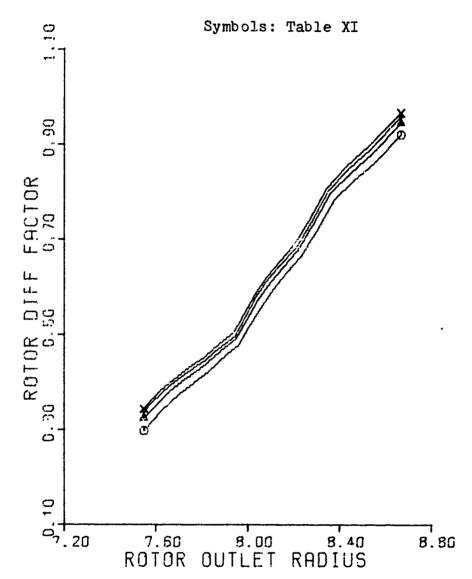


Fig. 77. Rotor Diffusion Factor vs Outlet Radius (100% Speed)

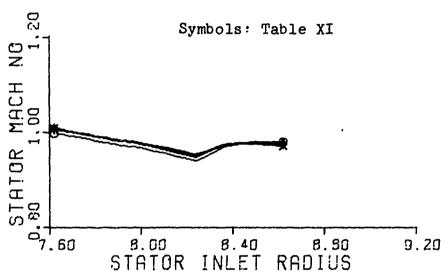


Fig. 78. Stator Mach Number vs Inlet Radius (100% Speed)

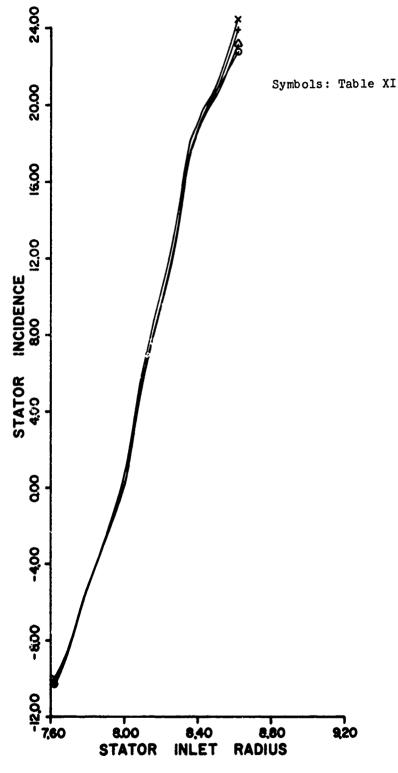


Fig. 79. Stator Incidence vs Inlet Radius (100% Speed)

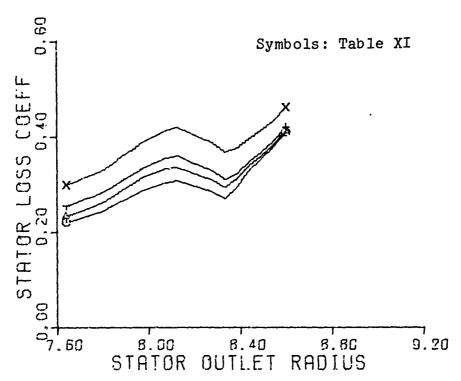


Fig. 80. Stator Loss Coefficient vs Outlet Radius (100% Speed)

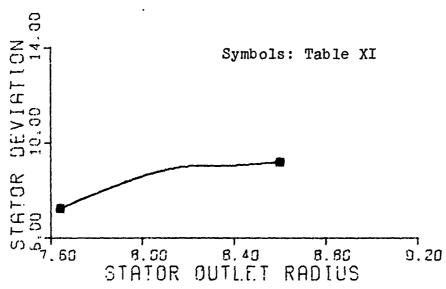


Fig. 81. Stator Deviation vs Outlet Radius (100% Speed)

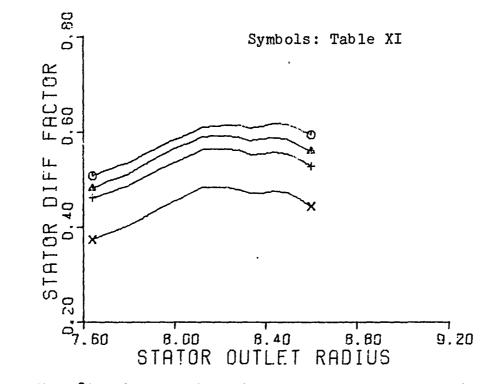


Fig. 82. Stator Diffusion Factor vs Outlet Radius (100% Speed)

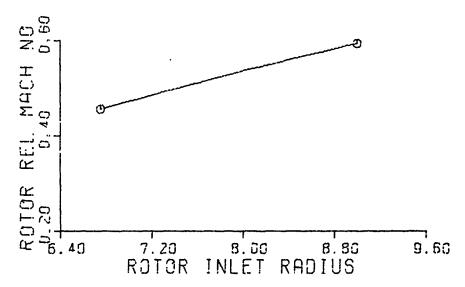


Fig. 83. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 40% Speed)

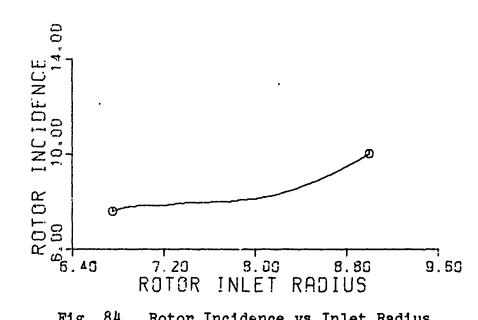


Fig. 84. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 40% Speed)

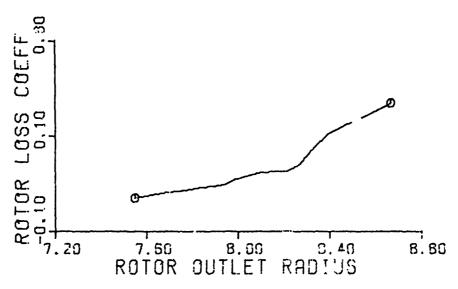


Fig. 85. Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 40% Speed)

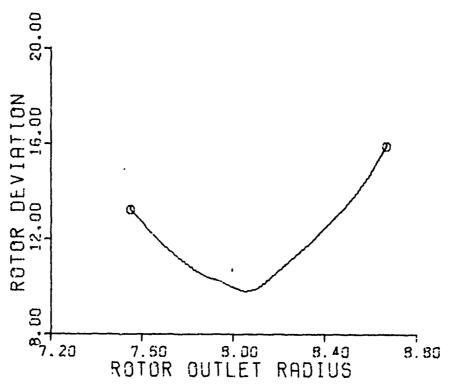


Fig. 86. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 40% Speed)

1

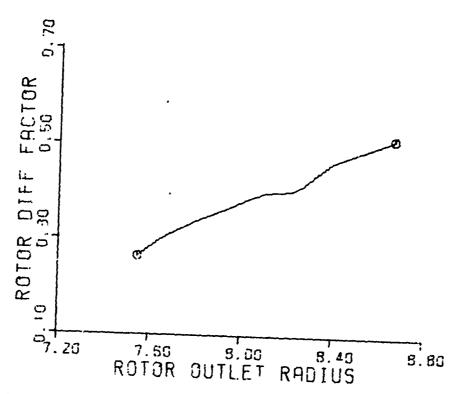


Fig. 87. Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 40% Speed)

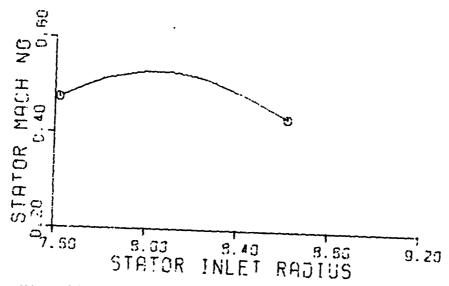


Fig. 88. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 40% Speed)

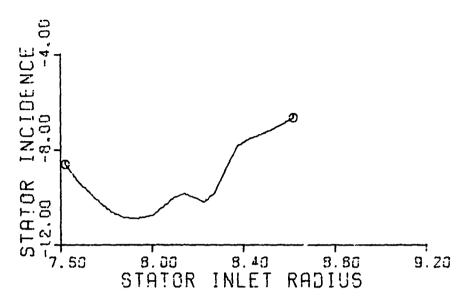


Fig. 89. Stator Incidence vs Inlet Radius (Within-Blade Analysis, 40% Speed)

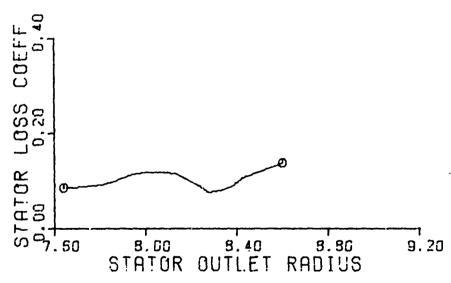


Fig. 90. Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 40% Speed)

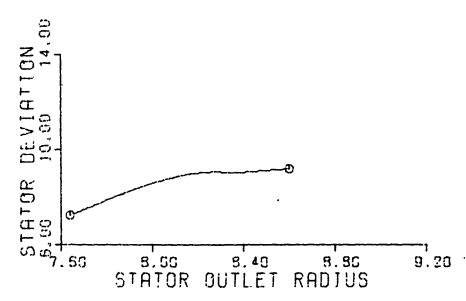


Fig. 91. Stator Deviation vs Outlet Radius (Within-Blade Analysis, 40% Speed)

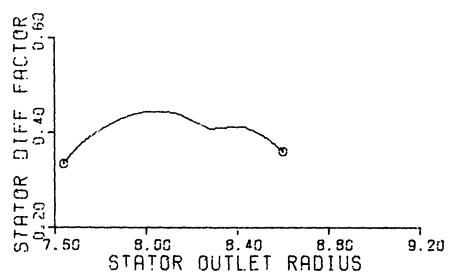


Fig. 92. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 40% Speed)

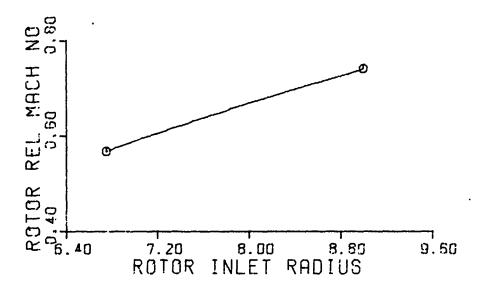


Fig. 93. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 50% Speed)

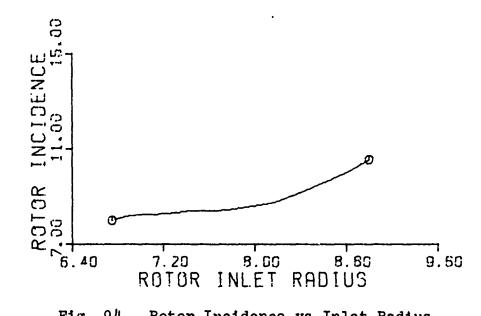


Fig. 94. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 50% Speed)

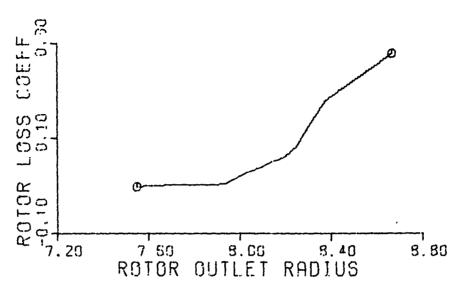


Fig. 95. Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 50% Speed)

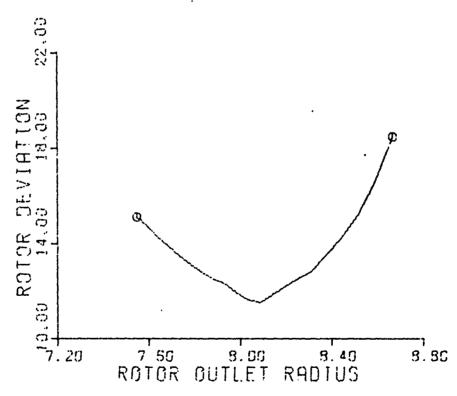


Fig. 96. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 50% Speed)

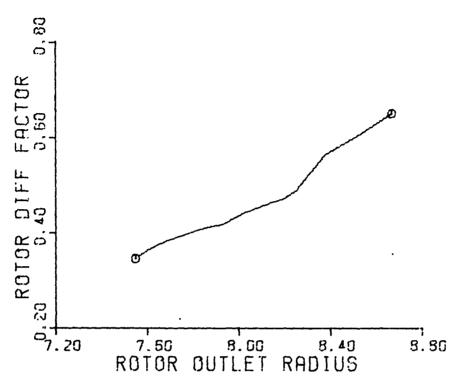


Fig. 97. Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 50% Speed)

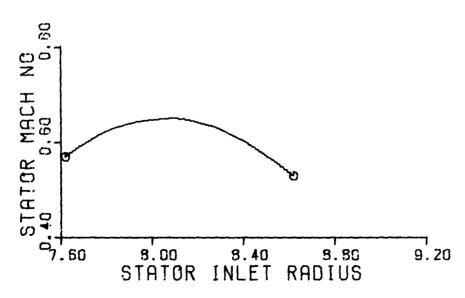


Fig. 98. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 50% Speed)

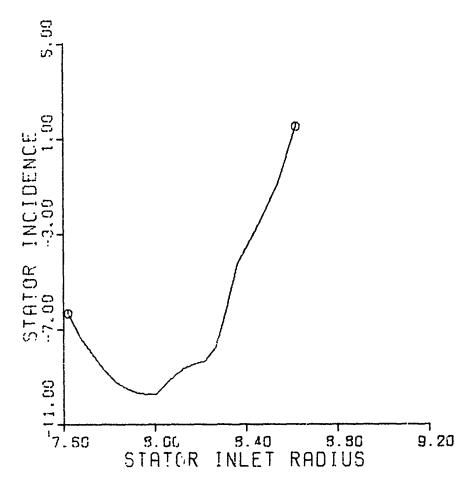


Fig. 99. Stator Incidence vs Inlet Radius (Within-Blade Analysis, 50% Speed)

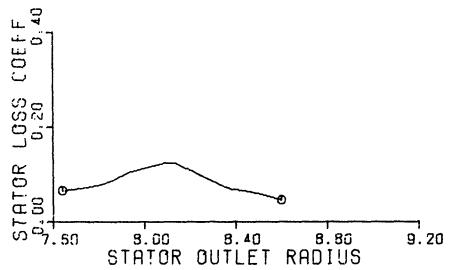


Fig. 100. Stator Loss Coefficient vs Outle Radius (Within-Blade Analysis, 50% Speed)

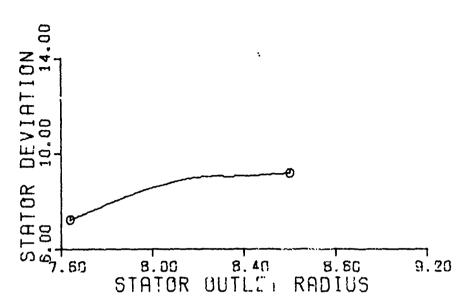


Fig. 101. Stator Deviation vo Outlet Radius (Within-Blade Analysis, 50% Speed)

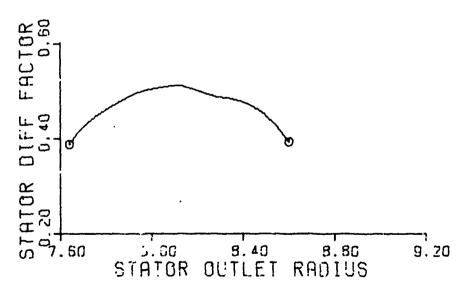


Fig. 102. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 50% Speed)

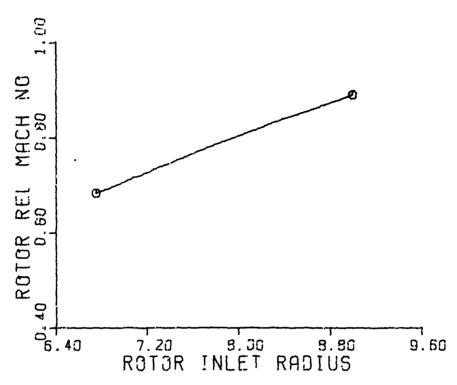


Fig. 103. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 60% Speed)

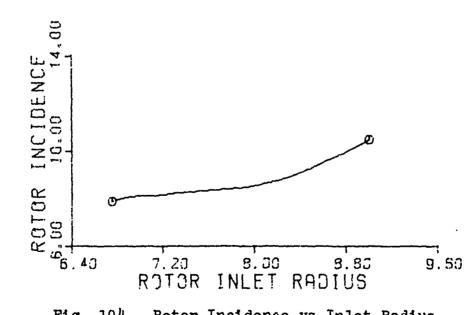


Fig. 104. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 60% Speed)

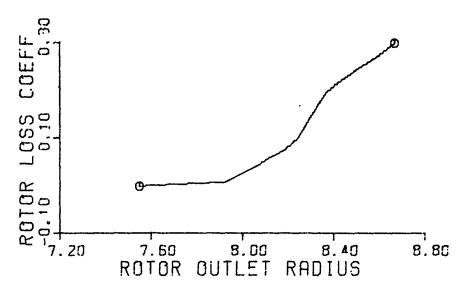


Fig. 105. Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 60% Speed)

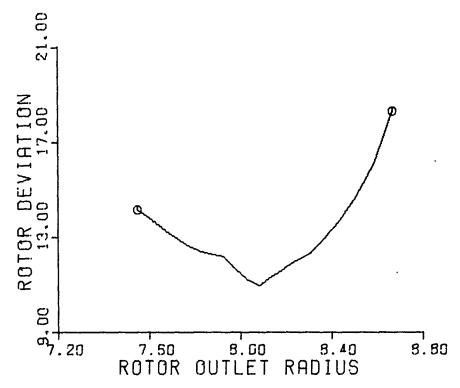


Fig. 106. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 60% Speed)

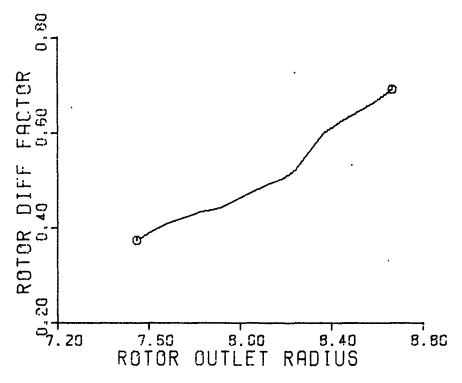


Fig. 107. Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 60% Speed)

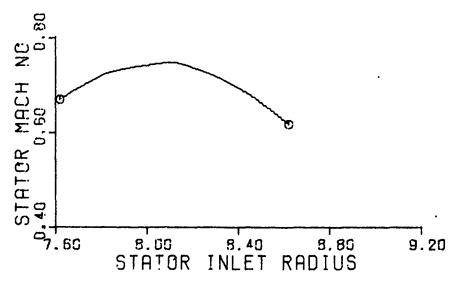


Fig. 108. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 60% Speed)

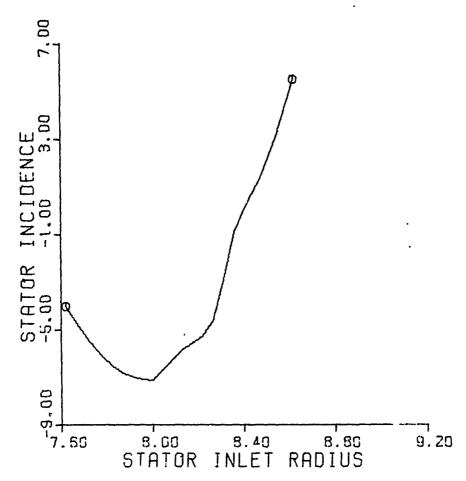


Fig. 109. Stator Incidence vs Inlet Radius (Within-Blade Analysis, 60% Speed)

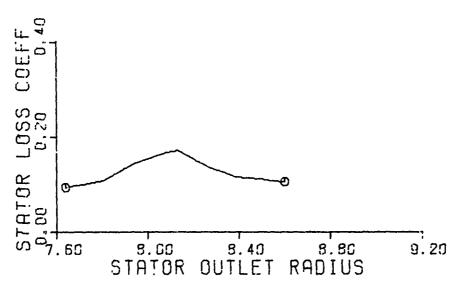


Fig. 110. Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 60% Speed)

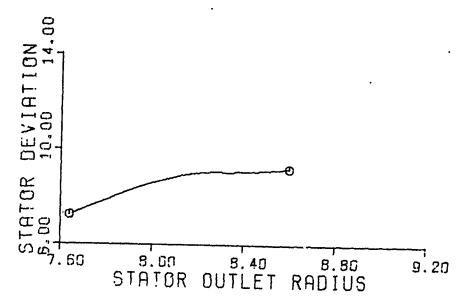


Fig. 111. Stator Deviation vs Outlet Radius (Within-Blade Analysis, 60% Speed)

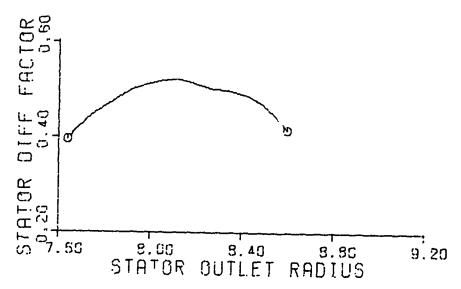


Fig. 112. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 60% Speed)

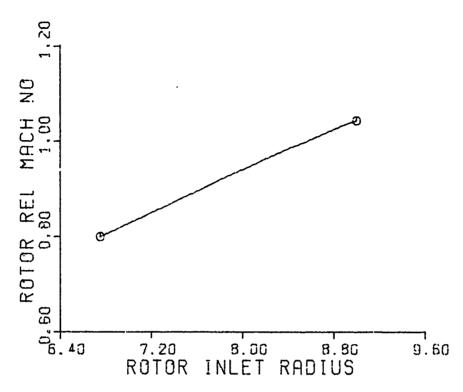


Fig. 113. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 70% Speed)

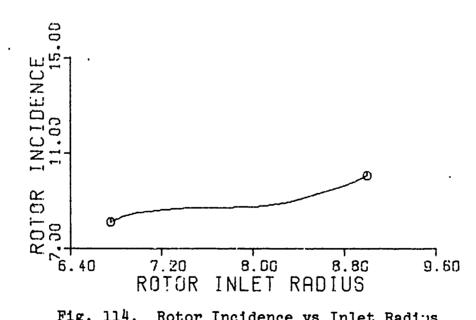


Fig. 114. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 70% Speed)

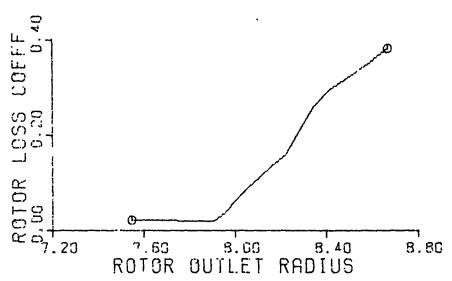


Fig. 115. Rotor Loss Coefficient vs Outlet Radius (Witnin-Blade Analysis, 70% Speed)

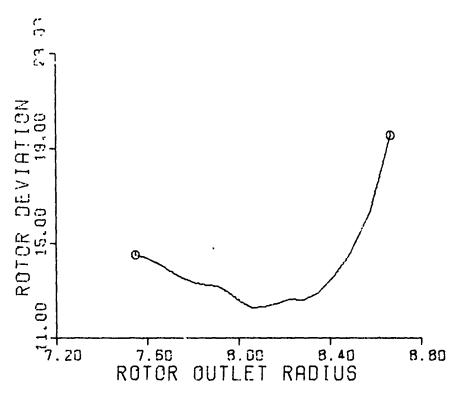


Fig. 116. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 70% Speed)

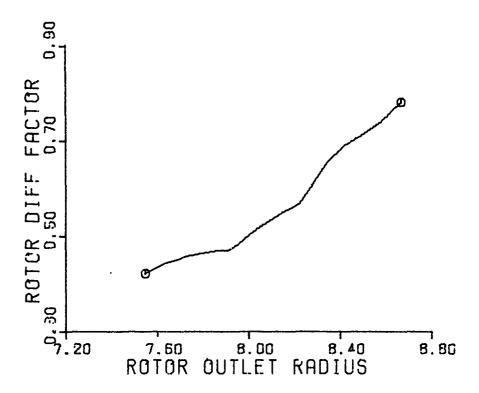


Fig. 117. Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 70% Speed)

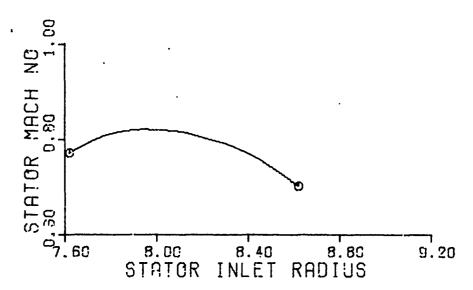


Fig. 118. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 70% Speed)

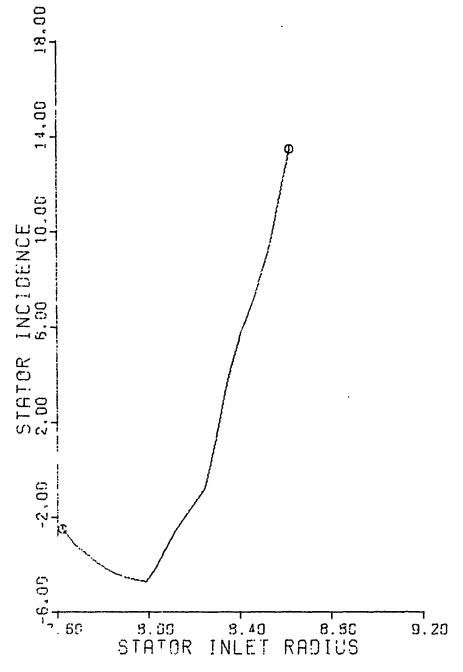


Fig. 119. Stator Incidence vs Inlet Radius (Within-Blade Analysis, 70% Speed)

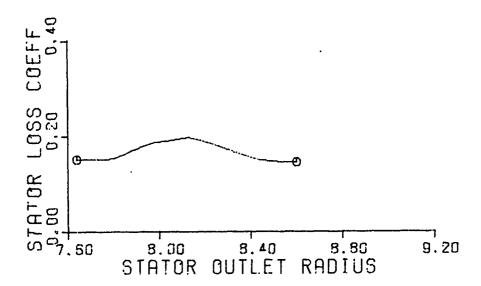


Fig. 120. Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 70% Speed)

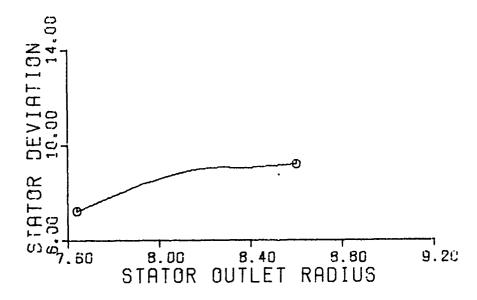


Fig. 121. Stator Deviation vs Outlet Radius (Within-Blade Analysis, 70% Speed)

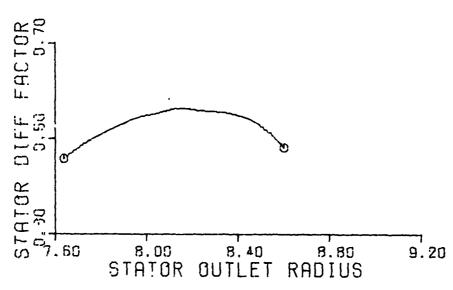


Fig. 122. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 70% Speed)

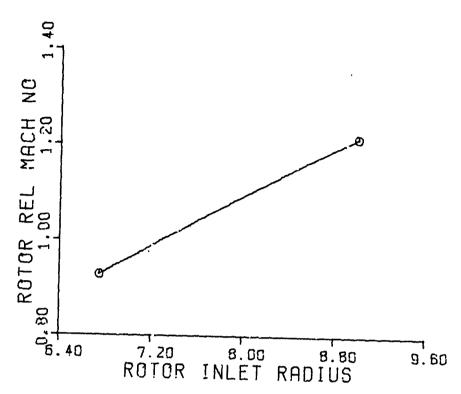


Fig. 123. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 82% Speed)

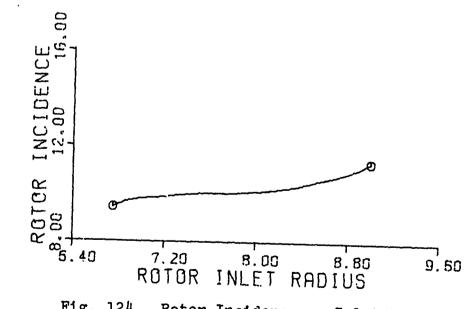


Fig. 124. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 82% Speed)

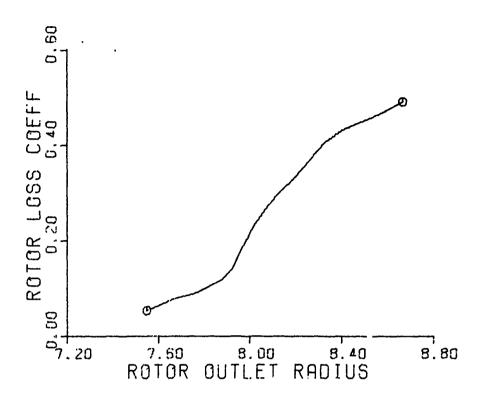


Fig. 125. Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 82% Speed)

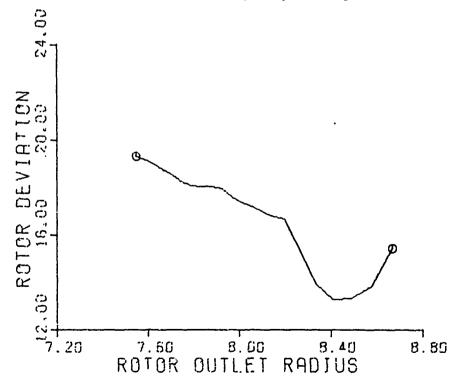


Fig. 126. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 82% Speed)

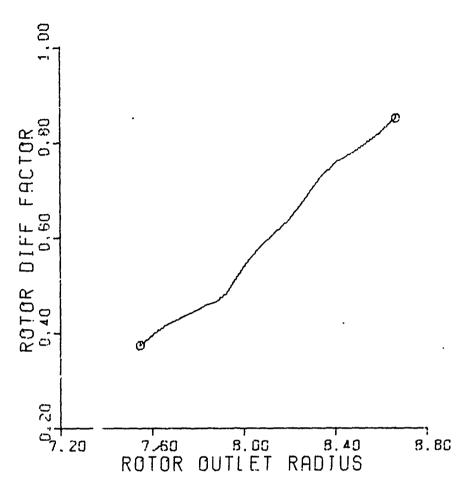


Fig. 127. Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 82% Speed)

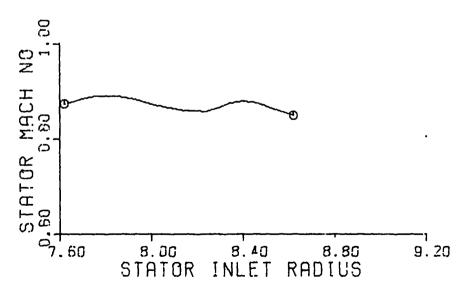


Fig. 128. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 82% Speed)

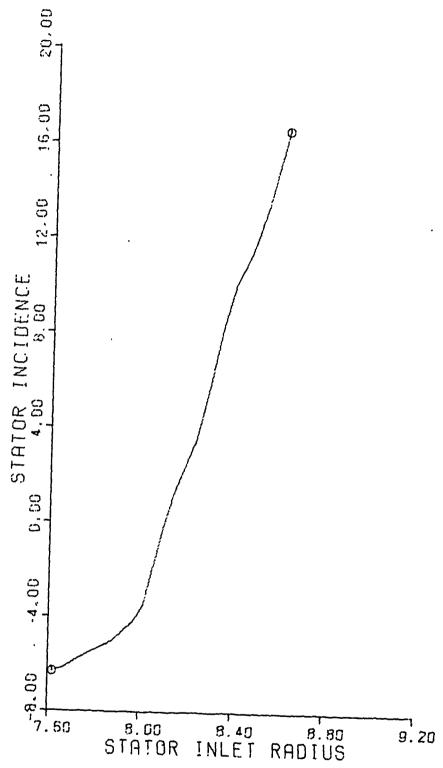


Fig. 129. Stator Incidence vs Inlet Radius (Within-Blade Analysis, 82% Speed)

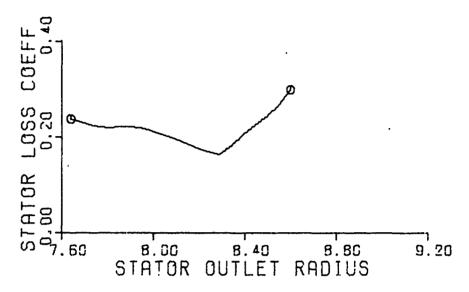


Fig. 130. Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 82% Speed)

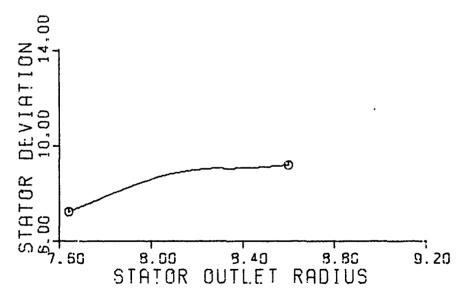


Fig. 131. Stator Deviation vs Outlet Radius (Within-Blade Analysis, 82% Speed)

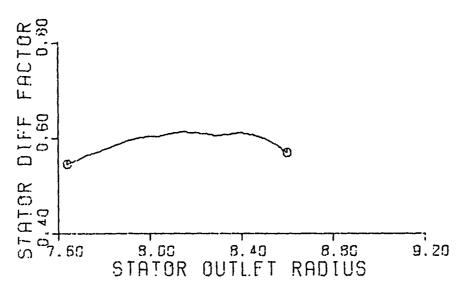


Fig. 132. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 82% Speed)

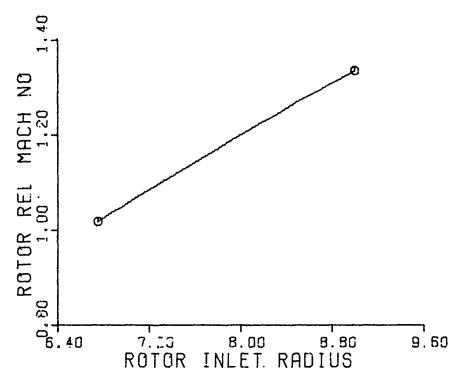


Fig. 133. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed)

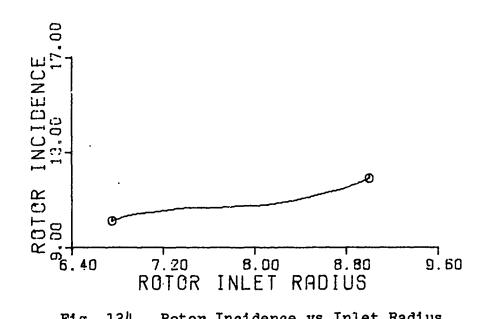


Fig. 134. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed)

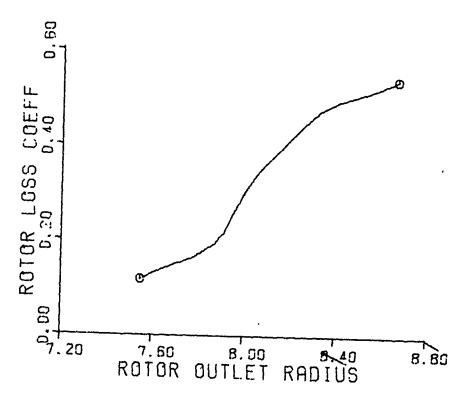


Fig. 135. Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed)

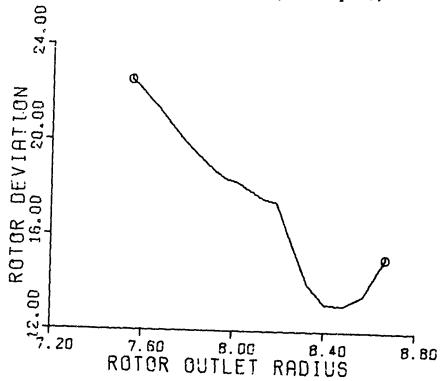


Fig. 136. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 90% Speed)

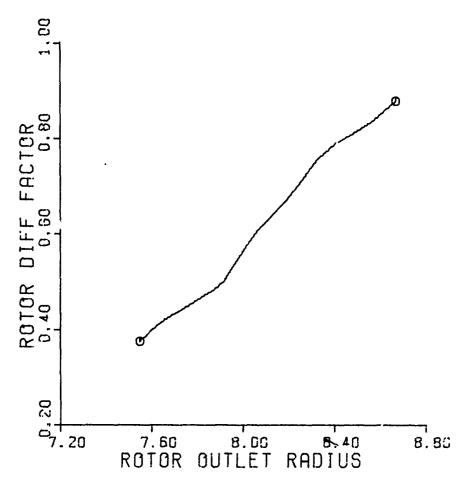


Fig. 137. Roter Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 90% Speed)

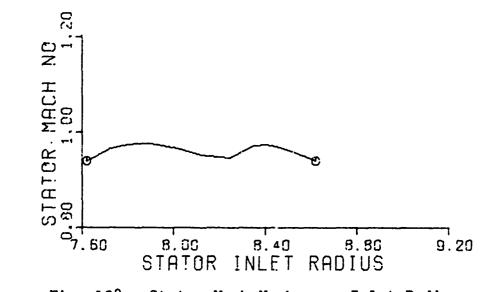


Fig. 138. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed)

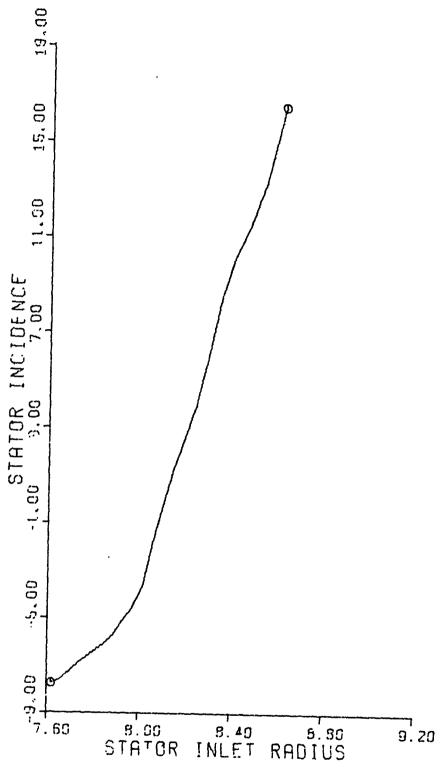


Fig. 139. Stator Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed)

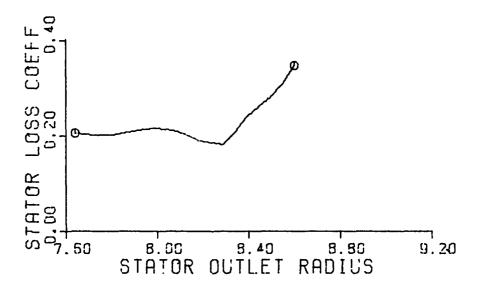


Fig. 140. Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed)

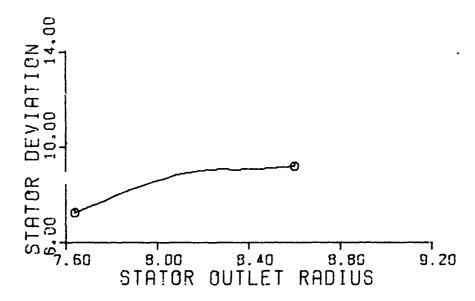


Fig. 141. Stator Deviation vs Outlet Radius (Within-Blade Analysis, 90% Speed)

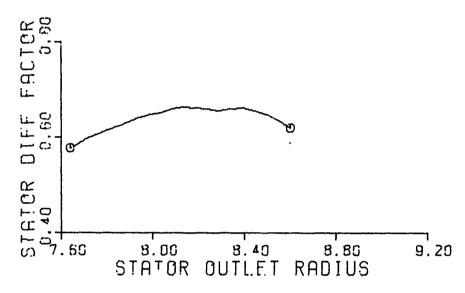


Fig. 142. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 90% Speed)

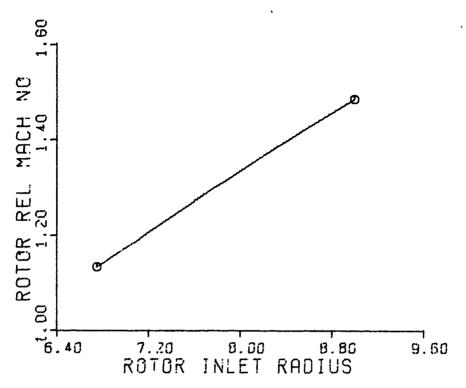


Fig. 143. Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 100% Speed)

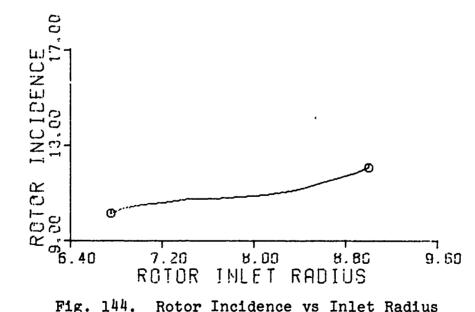


Fig. 144. Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 100% Speed)

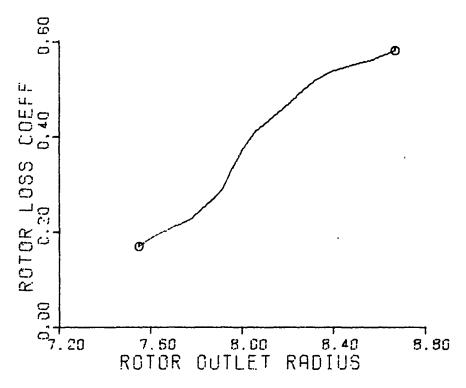


Fig. 145. Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 100% Speed)

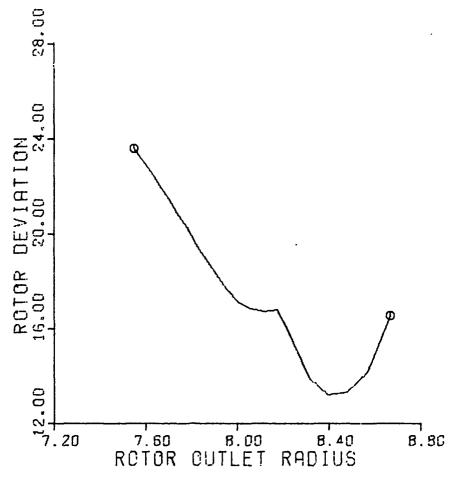


Fig. 146. Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 100% Speed)

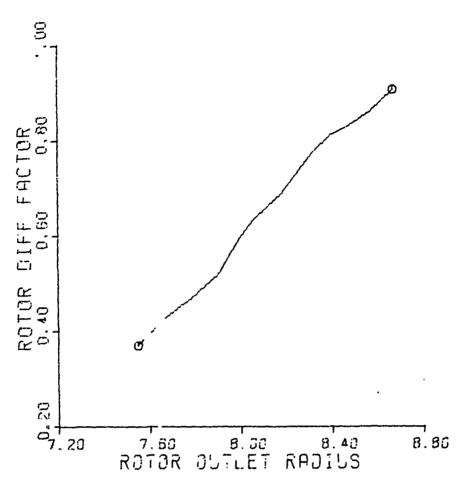


Fig. 147. Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 100% Speed)

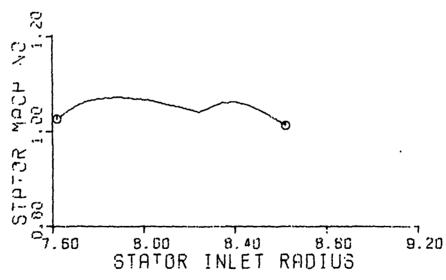
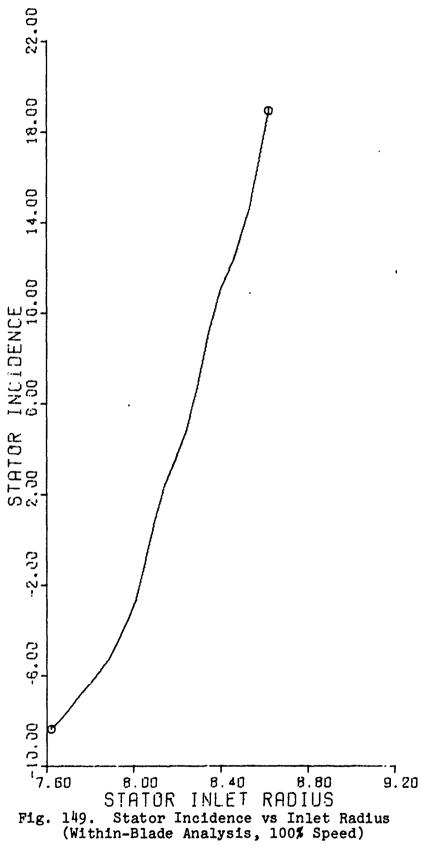


Fig. 148. Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 100% Speed)



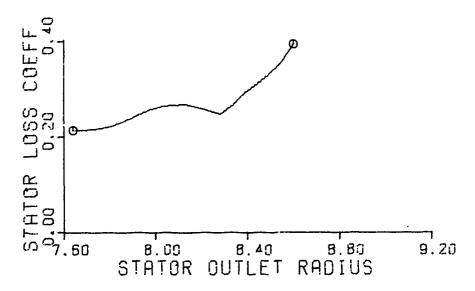


Fig. 150. Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 100% Speed)

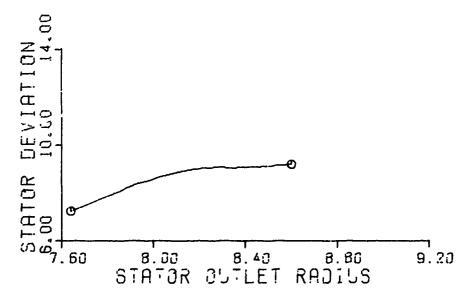


Fig. 151. Stator Deviation vs Outlet Radius (Within-Blade Analysis, 100% Speed)

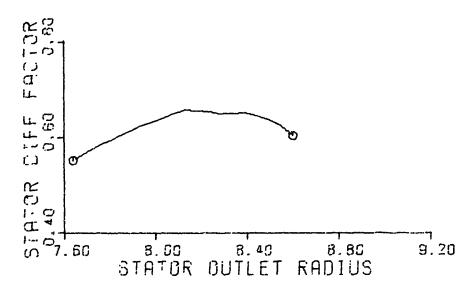
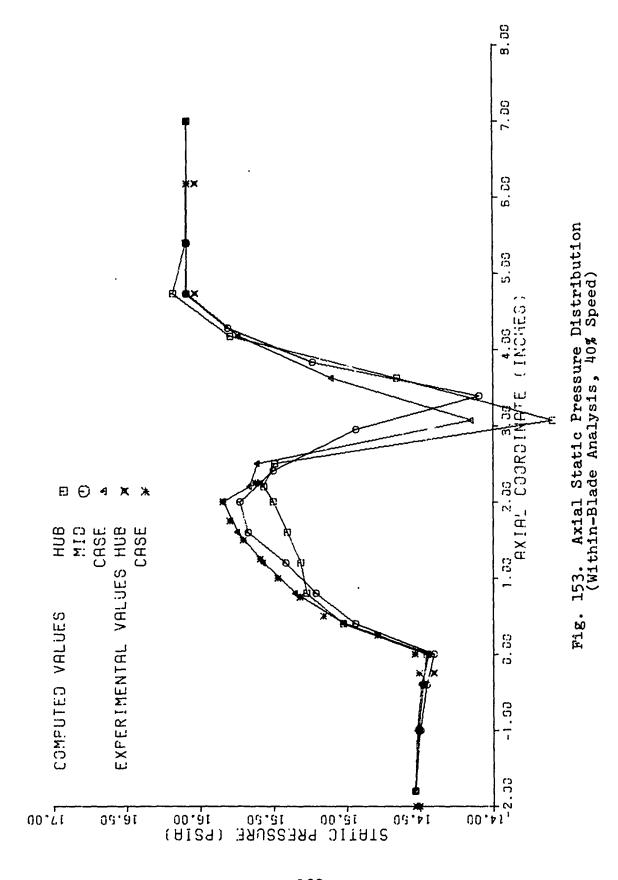
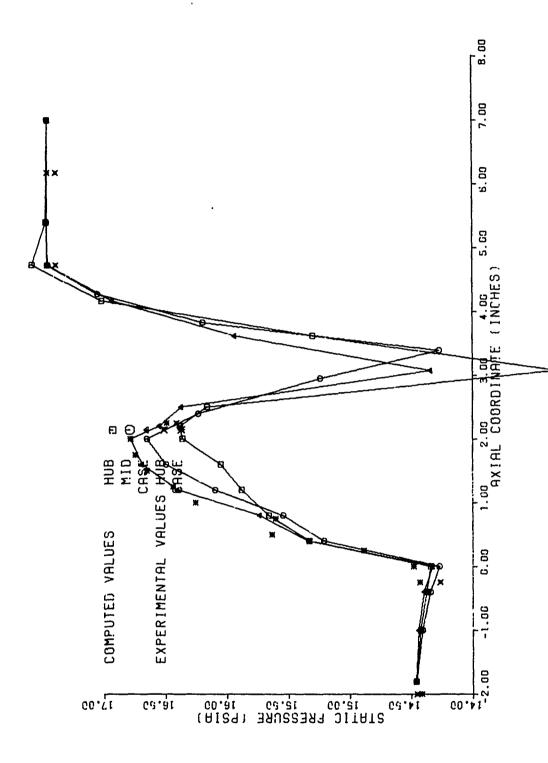


Fig. 152. Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 100% Speed)





的情况,我们就是一种的情况,我们就是这种的情况,我们就是不是不是一种的,我们也不是我们的,我们也是我们的,我们也是我们的,我们也是我们的,我们也是我们的人,我们 "我们是我们的是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的人,我们们

Fig. 154. Axial Static Pressure Distribution (Within-Blade Analysis, 50% Speed)

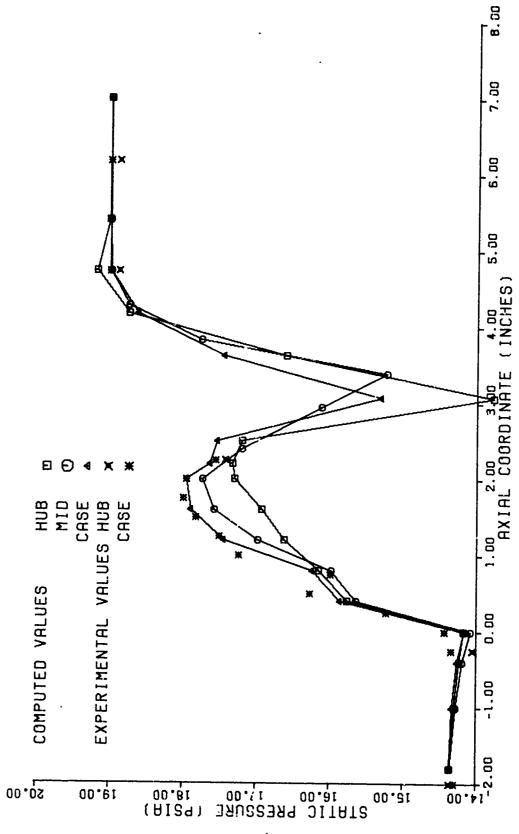
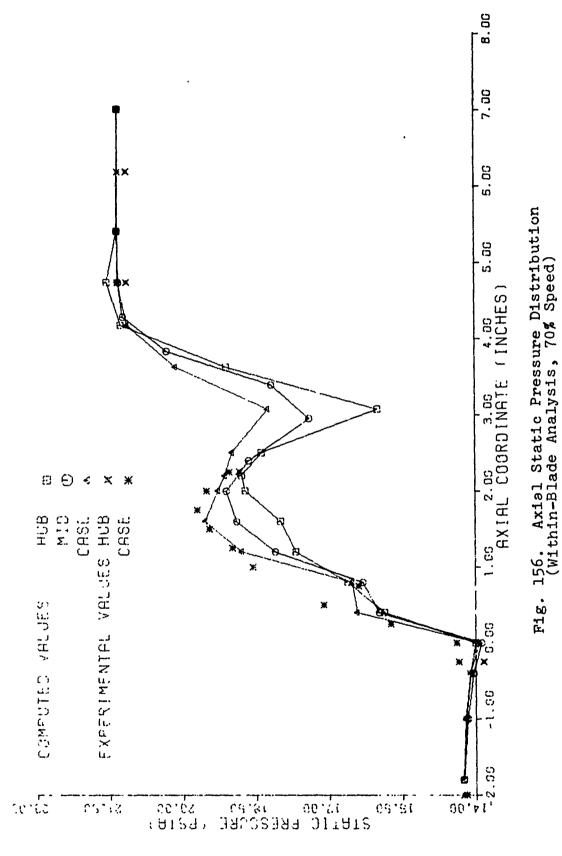
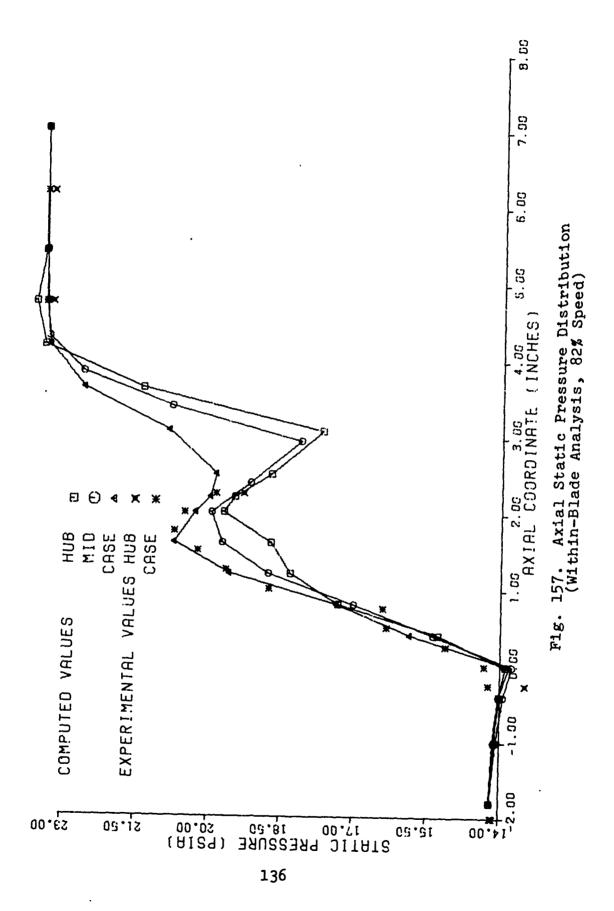
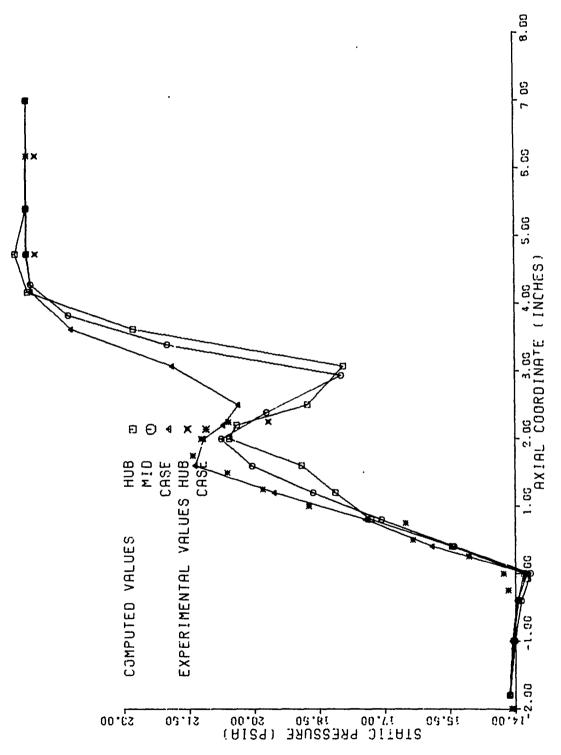


Fig. 155. Axial Static Pressure Distribution (Within-Blade Analysis, 60% Speed)

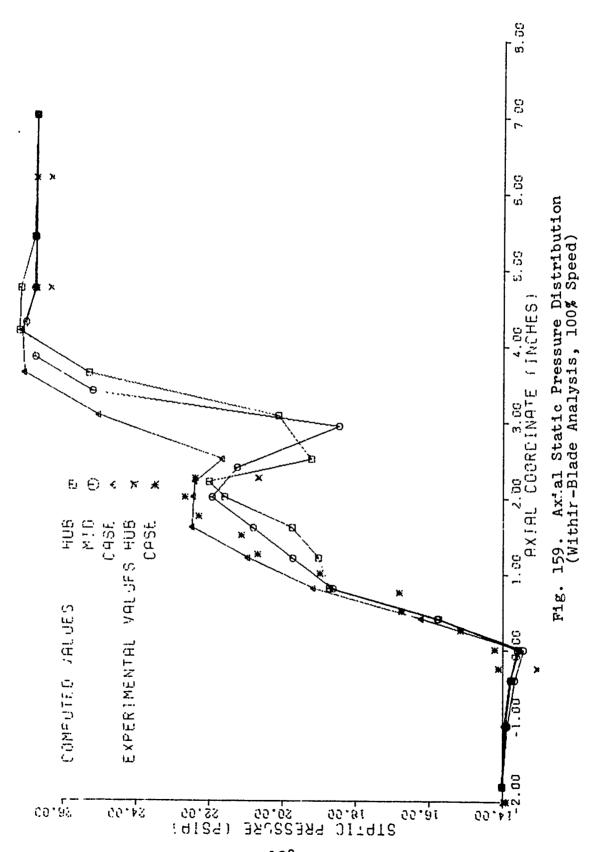






,就是这个人的,我们就是这个人的,我们也是这个人的,我们也是不是一个人的,我们也是不是一个人的,我们也是不是一个人的,我们也是一个人的,我们也是一个人的人的人的 "我们是一个人的,我们就是一个人的,我们也是一个人的,我们就是一个人的,我们就是一个人的,我们就是一个人的,我们就是一个人的,我们就是一个人的,我们也是一个人的

Fig. 158. Axial Static Pressure Distribution (Within-Blade Analysis, 90% Speed)



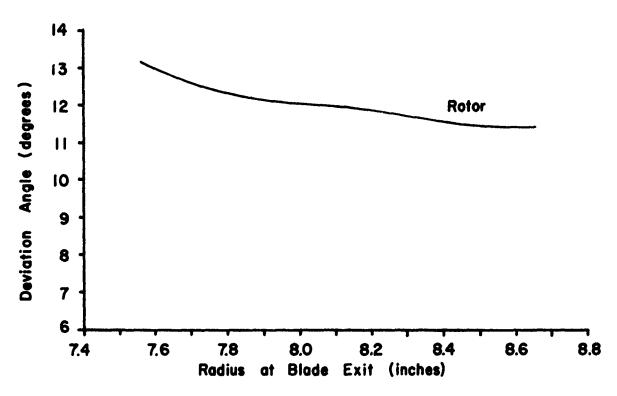


Fig. 160. Design Rotor Deviation Angle Distribution

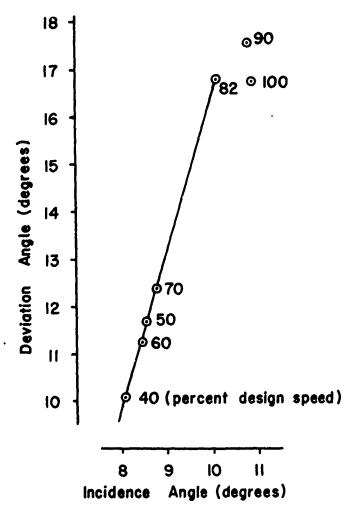


Fig. 161. Rotor Mid-Radius Deviation vs Incidence Angle



Fig. 162. Rotor with Splitter Vanes

APPENDICES

TEST DATA

## APPENDIX A

## PHASE II WITHIN-BLADE ANALYSES (COMPUTER PRINTOUTS)

This appendix presents the aerodynamic results (in the form of computer printouts) of the Phase II within-blade analyses for the seven test points selected for that analysis. The printout of input data which precedes the material presented herein has been removed in order to keep the number of pages to a minimum. The input data used in each of these analyses is presented in Appendix C.

I. PHASE II WITHIN-BLADE ANALYSIS (40% SPEED) TEST POINT 208180514040

STATION 1 FLOW FIELD DESCRIPTION

....

SPECIFIC WEIGHT	16/19	.0758	. 675	1528	. 6750		.0751	1678.	. 6758		1975	.0750	1671.	. 1750	. 1750	.1750	-1521	0670.	• • • • • • • • • • • • • • • • • • • •		SPECIFIC	HETCHT	- 8478-	6428*	6448		87.49	6478.	6448	6528	64/6.	9769	6849	6420.	6320		64.49	6470	
RADIUS OF CURVATURE	0.00	0000			0.000	008.0	0.00	0.00				00000	0.00	000.0	0.000	0.00	000.0	0.000		!	RADIUS OF	. CURVATURE	-205.758	-143.172	-119:658	100.010	-87.439	-78.427	-69.574	-61.133	-53,330	290-04-	-34.603	-29.854	241.52-	161.22-	-15-150	14.214	
SCOPE	20.93	19.76	10.50	16.20	15.00	13.81	12.62	11.43	10.26	7, 95	6.83	5.74		3.71	-82.2	1.93	1.18.	-52	,		.ES	SLOPE-	20.83	19.61	18.40	16.19	14, 77	13,55	12.33	11.10	9.88	7.46	6.25	2.07	3.92	2.01	10.7	23	
HHIRL S	0.00	00.00		00.0	0.00	00.0	0.00	0.00	0000		00.0	0.00	_ 00 0.	00.0	00.0	0.00	00.0	8	•		ANGLES	WHIRE	00.0	00.0	86	00.0		0.00	0.00	0.00	0000		00.0	0.00	0.00	0000		00.0	
A CH	.1253	1253	1253	1253	.1253	.1253	.1253	.1253	1253	1253	. 1253	.1253	.1253	.1253	. 1253	.1253	.1253	\$621.			ᇙ	- 0N	.1352	.1358	.1363	-	1376	•	.1383	.1386	н.	1387	.1386	.1383	.1378	13/2	1354	1345	,
URES STATIC	14.536	14.536	14.536			14,536	14.536	14.536	14.536	į	14.536	14.536	14.536	14.536	14.536	14.536	14.536	14.556			JRES	STATIC	51	20	14.507	14.000	14.503	14.502	14.501	14.500	14.500	14.500	14.500	14.501	14,503	14.004	14.509	14.512	, , , ,
TOTAL STA	14.696	14.696	, ,	14.696	•	j	•	<b>.</b>	\$ 4		3		÷	j.	j,	j,	14.636	;	5		PRESSURES	TOTAL	14.696	•	14.696	14.696	14.696	;	14.696	•	; ;	14.696	;	14.696		•	14.696		
TURES STATIC	517.072	517.07.2	517.072	517.072	517.072	517.072	517.072	517.072	511.01/2	517.072	517.072	517.972	517.072	517.072	517.072	517.072	517.072	270-716			TURE S	I	516.809	516.793	516.773	516.752	516.740	516.730	516.721	516.714	516./UJ	516.703	516.714	516.722	516.735	2100/22	516.803	516.335	)
TEMPERATURES TOTAL STATIC	•	0 4	18.5	18.6	18-6	18.6	18.6	9	0 4	9	19.6	18.6	18.6	18.6	9.6	9.01	9.01	9			TEMPERATURE	TOTAL	518.688	518.688	518.538	0 4 0 4 C	510.688	518.688	518.688	518.688	21 de 5 de	518.688	518.688	518.688	518.688	0000016	518.588	:	
TOTAL	140.42	<b>-</b>	140.42		3	3	140.42	⊋ :	140.47	140.42	140.42	1+0.42	140.42	140.42	140.42	9	140.42	<b>5</b> 6	i i		:	TOTAL	151.41	152.05	152,64	153.73	154.10	154.57	154.92	155.13	155.57	155.33	155.20	154.40	154.35	123.07	151.67	150.33	
TANGEN	0.00	<b>-</b> -	9 0	0	0	0	О,	Э :		0	0	0	0	0	0	9	9 0	<b>5</b> 6	ELD .		OCITIES	TANGEN	0.00	0	٠, د	<b>,</b> c	, 0	0	0	9 (	<b>&gt;</b>	, 0	c	0	9	<b>5</b> C	000	0	
YERIO	1+0-42	140.47				3	¥ .		140.40		140.42	3	3	•	9,		140.47	, ,	•		VEL	RERIG	÷	សំ	152.64	, M	154.15	154.57	154.92	155.13	12203/ 155. IL	155.33	155.20	154.85	154,35	100.00	151.67	150,33	
KABIOS	6.0536	V 1	ט כ	·	9	or.	- 1	n.	7 4		or.	0	-	m.	٠.	01	~ 0	n c	•		2401JS		6.3746	6.5141	6.7836	. F. 975.		•	•	•			•	•		•	6.6720		
STREAM -LINE	<b>ન</b> (	u M	) .g	ĸ	ø	~	<b>10</b> (		7 F												STREAM		<b>+4</b> (	<b>~</b> 1	7 3		۰ ب	7	€ (	Ť •		12	13	4 I	٠ د د		. 6	61.	•

OF SPECIFIC URE HEIGHT	31 0746						•	74.00							•		•	1	24/11.	OF COFFIFTE	j					•						20.00		24.00					•	19 18746
RADIUS OFCURVATURE		1 - P. A	174.665	196.6	185.715	520-155	166.6616-	-104.774	-69-	-46.346	34.5	-27,255	-21:936	-18.0	-15.096	- 12.825	-11:855		169:3m, I.	DANTIIC (				-134.414	200	06/ 60-	-59.551		-41.6	37°918	-35.195	949°55	256 - 15	-28.176		-23.525	-21.421	-19.024	16.228	-13.249
SLES - "SLOPE"	20.54	130.25	17.08	15. 36	14.61	l !	i	10.70	1	ۀ	į	'n	- 2.49	1.11	92.	-1.61	5°.	j,	-5.47			SLUTE	26.32	19.29	18.17	16.39	12.65	164 47 .	11.74	10.33	8.89	10 to	5. 45	6.00	1000	17		-3.34		-6.59
ANGL	00:0	20.5	0.00	8	0.00	00.00	9.00	•		00.0	00.00	0.00		0.00	۲.	•	•	•	00.00	a tony	10455	MUTKL	0.00	0	0	9 (		Þ			0.00	0.00	9 (	900				0.00	0	00.00
MACH		1400	1483	2641	.1502	.1510	•••	4761.	חברי.	1535	.1534	.1531	1526	.1518	.1507	.1492	3	.1454	.1430	, 6		2	. 1539	.1559	.1579	.1598	1616	2010	1561	-1673	.1682	.1689	1694	1601.	1691	.1687	- 1676	.1662		1518
PRESSURES OTAL ""STATIC	<b>.</b>	14.47	14.472	.694.41	14.467	14.464	j,	004.41	14:450	14.457	•	14.458	14.459	14.462	14:465	14.470	14.475	. 40	14.488	(	;	SIATIC	564:41.	14.449	14.443	14.437	14.431	14.400	14.420	14.412	14.409	14.407	14.405	**************************************		14.407	16.411	14.416		4
P2ES	14.696	7 4	14.696	4.6		4.6	• • 69	۰	, do	j	J	*	j	j	4:69	4.69	14.696	4.69			2	TOTAL	14.698	;	j	14.696	•	÷.	•	,	•		14.696	14:696	14.695	14.696	;	9	;	6.40
TURES STATIC	516.500	516.460	516.423	515.400	516.371	516.345	516.321	516.300	510.004	516.269	516.271	516.280	516.297	516.322	516,355	516.400	516.453	516.515	516.585	. (	ERFERA OREST	STATE	516.295	516.191	916.127	516.065	516.007	712.456	712.3 UI	515,816	515.784	515.759	515.742	515.734	510.f34 E+E-746	515.768	111111111111111111111111111111111111111	515.852	515.916	E + E . D 00
TEMPERAT Total	518.688	10.0	18.6	18.6	18.6	18.5	18.6	9	0.0	, A	18.5	10.6	18.5	18.5	18.6	13.6	518.688	18.6	18.5	•		TOTAL	.518.588	ō		518.688			710000				۰	ď	ŏ	318.588	9	9	10	3
TOTAL .	63.		166.05	67.	68.	169.03	169.95	170.68	1/1.25	171.80	171.74	171.42	170.81	169.91	158.67	167.03	165.14	152.84	160.13		•	TOTAL	172,28	$\sim$	~	~	180.87		0 .		, -	•	~	•		188.47		_ ~		
ELOCITIES. TANGER	0	o :	00.0	0	0	0	0	0	<b>"</b>	2 6	<b>,</b> e		0	0	0	0	0	0	0		٦:	TANGEN	0.0	0	0	0	0	0	0.0	<b>,</b> c	, 0	0	0:0	•	90		> ⊂	<b>,</b>	, 0	
MERTO	163,39	164.12	166,05	167.03	168.12	169.08	169.95	170.68	171.25	17 1. 63		17 1 - 42		i ch			55.1	N	0.1		•	MERID	N	17 4.55							168.23	189.03	189.58	-189.85	189.83	169.47		186.01		
RADIUS	6.6016	6.7250	0.0433	7, 0953	7.2170	7.3330	7.4595	7.5796	7.6983	7 0275	A. 1157.3	9.1775	8,2983	5.4200	. 8: 5427	8.6658	8.7925	•	•		KAULUS		- 8, 7500	6.8667	6.9822	7.0965	7.2097	7, 3219	7.4552	7.6537	7. 7632	7.8725	7.9618	8.0912	8.2009	8. 5111	712 W . #	A. 5677	.8.7628	

١,

_
=
=
C
w
5
ì
and the

TO MANAGEMENT TO A STATE OF THE PARTY OF THE

是一个人,我们就是一个人,我们就是一个人,

	POL YTROPIC EFFICIENCY	E. 1101	1.000	1:1011	1.880	1:00:1	1.0040	1:101:1	1.0000	T. TOTAL	1.000	1:000	1.000	1.0000	1.111	1000.1	1.0000	1.0000	1.000	1000	1.000																!							
:	ISENTROPIC POLYTROPIC EFFICIENCY EFFICIENCY	ì		1	.0860				1.0001	1.6036		1		1.0000		1.0016	į					1.111		Š	- WEIGHT	- 28788		•			•	99.1	f		:1765				•	17.65	• '		•	.0766
	DELTA T I	0.00	00000	000.0	0.000	100.0	0.00	0.00	0.00.0	0.000.0	0.000	. 0.00.0	0.000	0.00	0.00	. 000 · D	0.00	000.0	0000	3.000	8 C C C C C C C C C C C C C C C C C C C	0.00	;	RACAUS OF	- CURVATURE	6.144	6.336	6.735	7.425	8.472	9.973	211.21	70.813	31.674	62.556	605.617	-91,003	-46.672	162°52	29.000	74.424	38.966	-64.330	-1665.883
:	PRESSURE RATIO	1.000	1.000	1.000	1.000	1.000	1.800	1.000	1.900	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1,000	1.069	1.000	1.000	1.000	1.000	•	ANGLES	SLOPE'	. 22.47	21, 16	19.87	18.46	16.98	15.64	13.65	10.58	8.92	7.27		•				- K - 00	-5.45	-7.6k	-9.38
	RELATIVE TEMPEZATURE	685	1.248	116-1	1.578	. 052	1.326	1.507	. 293	.386	1.587	382	.114	545.343	.584	.338	109	1.397	.704	1.535	.393	.282	:	ANG	- WHIRL	. 25, 95						,	20.03		19,70		į		19.47	19.00	20.02	20.74	21.00	21.29
								:				:				53	841 548	ı	54	20	19	23	i	HACH	-0N	.2442.	2502	:2129	.2155	.2180	.2207	.2232	.2276	.2295	.2312	.2329	-2342	.2360	.2373	25333	102.0	22.2	, v	.2386
	E RELATIVE Y PRESSURE		16.738											17.583		17.	17.	17.	18.	18		18.3		PRESSURES	STATIC	15. 825	15,016	'n	14.995	14,984	14.974	÷	14.950	14.945	14,942	14.942	14.943	14.946	14.951	14,959	14.950	17, 489	2 5	15.013
	RELATIVE VELOCITY	510.24	518.83	527.31	535.68	543.94	552.08	560.11	568.03	575.85	583.56	591.19	598.73	605.21	613.62	620.97	623.28	635 - 55	642.80	_	•	564.54		P2ESS	TOTAL	152451	15.484	15.487	15.487	15.488	15.490	15,492	15.434	15.502	15.508	15,516	15,525	15.536	15.548	15.561	15.573	15,548	15.609	15.619
	RELATIVE MAC+ 10	7	4633	. 47 11	. 47 85	.4960	. 4933	. 50 05	. 5075	. 51 46	. 52 15	. 5283	.5351	.5413	. 5484	. 5550	. 5615	. 5680	.574	. 58 09	. 5873	. 5937		URES	STATIC	524.845	521.771	521.685	521.592	521.496	521.402	521.324	521.735	521.219	521.244	521.270	521.290	521.328	521.479	521.739	562.015	177.665	522.5AN	522.934
	BLAGE	E. 80 . 3	8	8.96	504.3	513.0	521.0	528.9	536.8	244.6	552.4	560.2	567.9	575.7	583.5	591.4	599.3	607.2	615.3	623.5	631.8	÷0+9		-TEMPERATURES-	TOTAL	402.406	26.356	6.390	6.410	6.427	6.453	6.591	56.52 56.55 56.55	6.680	6.788	6.895	6.993	:7.10,	7.3.0	7.736	97.0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A. 6.26	128.856
	LOSS	2	9	8	2	0	0	8	9	8	00	00	8		00	8	9	8	2	0	8	00	TION	:	OTAL TO	. 4		19	14	32	52	6		12	10	66	. 81	25	86	*		2 2	3 2	300
	DEVIATION		7.7.7-			•	•				•	•		-8.203	٠	•	÷	•	÷	÷	•	•	DESCRIPT	IES	_	23	A5 236.1	36	75	65	69	35	17	. 6	29	73	70	83	66	5	5 1	0 1		60 268
	FLOW	70.25A	-70,339	70.413	70.492	70.578	70.073	70.778	70.897	71.031	-71.183	71.353	71.541	-71.749	71.979	72,235	-72.518	72.832	73.180	73.267	-	-74.501	FLOW FIELD	VELOCITIES	TANG	70		92.	91.	90.	κ 9.	90 80		87.	87.	87.	87.	87.	6	46	, ,	יי מ	ď	97.
	INGLES REL				4.148	2.766	1.443	0.299	9.331					5.640 -									۱ <b>۵</b>		HERID																	•		25 0 . 50
	BLADE-AN	. 23	. M	MOS	620	23	259	316	321	949	172	262	118	946	299	763	352	939	644	.181	.336	• 476	STATION	RADIUS	,		7.0050	7,1125	7.2174	7.3210	7.4234	5,25:1	7.6248	7.8234	7,9223	8.0210		8.2186	8.3177	8.4176	6,5133	1020.0	1001	8.9340
:	LOCAT	•				•						_		- 13 -63-				,	9		٠	- 22		STREAM	-LINE		• •	ı m	•	<u>ب</u>	•		<b>10</b> G	· a	#	12	13	14	15	16		91		12

AND THE PROPERTY OF THE PROPER

The property of the rest of th

POLYTROPIC EFFICIENCY	1.0156	. 8118	1.0103	-6986-1	1.0875	r. 1693	1.0132	. 9226	2466	1000	7 P D P 0 P 0 P 0 P 0 P 0 P 0 P 0 P 0 P 0	9834		9519	9338	.9236	.9143	. 9843	. 6933
ENTROPIC FICIENCY	1.8157	<b>5</b> + + 5	1104	1601	9101	9093	0032	. 9800		•	2486	7000		9515	9324	9231	9136		
DELTA T IS	• 115		919	610	.015	. 015	• 015	. 015	. 015		970	910	210	414	.018	• 018	.019	.019	.020
PRESSURE RATIO	1.053	ׅׅׅׅׅׅׅׅׅׅ֓֞֝֝֟֝֟֝֟֝֜֟֝֜֜֟֝֜֜֜֟֜֜֜֓֓֓֓֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡֡	50	. 05	• 05	• 05	•92	.05	. 05	: 05	50.		֓֞֜֜֜֜֝֓֓֓֓֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֡֓֜֜֜֓֓֓֡֓֜֜֜֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֡֡֡֡	֭֓֞֝֝֞֜֜֝֓֜֜֝֓֡֓֜֜֜֜֜֓֓֓֡֓֜֡֡֓֜֜֡֡֓֜֜֜֡֡֡֓֜֜֡֡֡֡֡֡֓֜֡֡֡֡֡֡	9	• 06	.05	• 06	30.
KELATIVE EMPERATURE	538.426	10.179	10.295	10.321	41.546	42.174	42.303	43.437	920-44	44.721	45.574	# 0 0 0 d	7 . 7 . 7	3200	5.784	19.507	50.248	51.009	51.791
ATIVE F	.770	2	472	039	.108	.175	.244	315	378	445	514	200	200	7.85	44	914	386	• 050	133
PRE	85 16	77 27 27	79	92 17	85 17	45 17	80 17	81 17	18 17	31 17	41 17	170	17 77	17	62 17	13 17	£1 17	06 18	53 18
VE RELATIVE O VELOCITY	• 6 4 4	•	•		•	•	•	•	•	•	•	•	•					-	_
RELATI MACH V		•	7.7	£4.	**	*	• 45	9.	•	<b>*</b> + + <b>*</b>	•	•	1 4	ט ט	200	. 5.1	. 51	. 52	. 52
3LADE : SPEED	8.064		2 t	520	528	535	245	549	556	563	570	250	ָ ה ה ה ה ה	4 60	5.05	613	620	628	635
ON LOSS CE 30EF				- 00	00	- 00	- 00	00	•	6.	96	•	•	2	25	. 02	• 02	.03	.03
DEVIATION INCIDENCE	+ 1	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		7	÷	7	ij	<u>-</u>	÷	ij	ij	;	•		; ;	-	÷	-1-	.:
REL FLOW	-51.714	07.10	0 0	2.08	2.17	52.25	2.36	52.49	52.03	2.77	52.92	00.0	**************************************	•		54.05	54.35	64.58	5.03
-ANGLES IN LEAN	10.432	р с	<b>5</b> 60	S LO	S	~	-	~	m	•	3 9	Э 4	0 4	ט כ	? `	•	•	۲.	· v
3LADE SECTIO	-00.252	2 4	7	32	93	.07	2	35	50	5	50	3 6	5	1 6	6	5	7	38	9
LOCAT	+1 6	<b>U</b> P	7 4		9	~	•	σ		::1	71	3 ;		3 5	27	97		<b>8</b> 0	

Carrollon			POLYTROPIC	EFFICIENCY	102801	1.0188	1:1157	1.0137	5:	07.00	1.2862	10012	9266	. 9848	. 9888	.9793	. 9786	- 426	0 2020	3131	9768	. 8786	. 1643															 					
### \$100   FALTIC   PACKET   COLUMN   C				1	T-1216	1.0102	1.1159	1.0136	1.0119	- RATE -	1.0063	20001	.9925	9496	.979	16.6	.9784	7000	93.00	9025	2869	.8778	. 8625		j	ر اند	.177	!				•			• •	:	•	•	•		•	•	18/18
## 400 C ANT   BLACE DATA   BLA			-		- 023	• 023	\$20.	. 023	920	200	023	420	. 024	921:	. 025	- 925	920	900	120	020	020	.031	•			CURVATU	•	-3.50	•	10.	14.4	-5.59	-6.41		-10.44	-12.69	-15.64	-13.42	-30°18	-37.87	6	-69	-125.601
## 400 CMA ## 12	] 	-	PhESSURE	RATIO	1.064	1.083	1.083	1.053	7000	) A C	1.084	1.085	1.086	190.1	1.089	1.090	1.091	9 11 1	1.00	1.096	1.097	1.097	1.198	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		າທ	26.61	23.72	20.99	18.40	15, 55	11.42	9.34	1.50 1.44 1.44	3,70	2.00 -	. 37		20.7-	-5.34	-6.50	-7.55	-6.52
### CADIC DATA    Color Lan	!	1	- 1	EXATURE	24.5	.051	026	.100			300	146.	.502	. 165	.537	.215	.601	, 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	CM	.274	225	.506	.303		1	보	32,57	32.42	32,35	32,30	36.65	32,23	32,23	32.50	32,66	32, 75	32.69	33.07	34, 05	0	<b>60</b> ·	- 1	36.75
## RADE_ANGLES REL_FLOW DEVIATION LOSS BLADE RELITIVE RELATIVE  1. \$\frac{1}{2}\triangle \text{Times} T		İ	- 1	ı	i			ļ		1				į					:					, ,	1	50			,	r,,	., ,,	, ,,	r,,	- 1981.	3312	.3310	.3306	3297	. 3235	.3273	.3261	.3248	.3233
### PADRE DATA ###################################	!	1	-		!	,		١				:	17.45	17.4	17.5	17.5	17.6	7.7.1	7.7.	17.8	17.61	17.89	17.9		1	STATIC	15, 313	15,317	15.324	15.333	15. 455	15.366	15.378	15.390	15.414	ığ ı	מי ע	15.455	15.478	15.493	15.510	15.527	15.545
## ADD DATA  ## BLADE -ANGLE SEL FLOW DEVIATION LOSS BLADE RELATIVE  ## SECTION TEAN ## WILLE INCIDENCE JOEF SPEED ## KRY 40    -54.590 3.782 -56.587 -1.937 -0123 503.6 .3829    -54.687 1.477 -56.890 -1.787 -0105 511.6 .3931    -55.857 -1.99 -1.727 -1.695 -1.926 -1015 511.6 .3931    -55.857 -1.99 -1.727 -1.695 -1.057 523.9 .4105    -55.951 -1.00 -57.218 -1.657 -01075 523.9 .4105    -55.951 -1.00 -57.218 -1.657 -01075 523.9 .4105    -55.957 -1.00 -57.218 -1.657 -01075 523.9 .4105    -55.957 -1.00 -57.737 -1.695 -01075 523.9 .4105    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.641 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.651 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.641 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.641 -01075 523.9 .4400    -55.957 -1.00 -57.737 -1.641 -01075 523.7 .7600    -55.957 -1.00 -57.737 -1.641 -01075 523.7 .7600    -55.957 -1.00 -1.642 -2.740    -56.957 -1.00 -1.642 -2.740    -56.958 -1.00 -1.642 -2.740    -56.959 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.950 -1.00 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740    -56.900 -1.642 -2.740		;	RELATIVE	VELOCITY	431.86	443.32	453.59	402.00	471.35	FAS. 44	492.37	498.18	502.88	507.34	512.03	517.22	522.34	505.00	527.26	530.53	533.89	3	0		ě	OTAL	.6.507	6.514	.6.527	5.542	0.000 5.15.8	6.580	5,542	6.677	6.629	3	5	8 %	: 🗠	3	69:	2:	7
## SADE DATA ## SADE SADE SADE SADE SADE SADE SADE SADE			ELATIVE	MCH 40	.3829	. 3931	• 40 23	• 41 05	1014	4311	.4368	. 44.19	. 4460	66 14.	. 4539	. 4563	• 4c 30	***	- FE 67	7697.	.4722	.4751	.47.80			TIC	•	4.516 1	4.628	4.755	4.00% 1.00%	5,192	5.353	7.763 1 F. F. N.	5.671	5.290	5.431 1	5,998 1	7.703	5.435 1	5.914	?	9.965
BLADE DATA	•				503.6	510.6	517.4	520.5	7.00.4	542.9	549.1	555.2	561.3	567.4	573.5	579.0	767.0	596.0		611.0	617.6	624.2	631.0		01.10101	L ST	753 9	999	620	202	202	574	836	710	646	260	191	280	333	265	97	53	25
## BLADE DATA  ## SECTION LEAN  ## SECTION LEAN  -54.59			055	0 = 1 = 0	0123	0105	900	0000		0035	0021	7000	0037	0075	6600	1101	0103	2770	0423	0463	2450	1190	0682	ž:	1	101	535.	535.	536	536	900	536	936.	727	537.	537.	537	0 10	53.0	5 39.	10.	240	046
### BLADE DATA    SECTION   CEAN   MACLE    -54.59			_ i		9.97	928	200	707	7 6	618	581	929	245	541	225	0/6	414	2 4	28.0	770	238	654	200	SCRIPTI		101	·	å	*	<b>.</b>	: :	: :	.:	•	: :	:.		: .:		: -	÷.	ᡱ.	٤.
### BLADE DATA    SIGNATE   STATE   ST			3.	ш	587	655	?	9 0	24.5	375	533	769	906	112	330	556	, e	3 1	b32	966	÷405	249	308	IELD 0	31418	TANGEN	00	96.	Ġ.	6	ה ה ה	96	e c	,	4	ė,	# F	. K	8	8	÷,	<u>.</u>	÷ (
######################################	€ !		S REL		782 -56	3.6 -36	140	75.	X	204 -57	105 -57	151 -57	114 -57	74 -58	85- 001	96-	00- 05.	900	99	-5.	-50	-50	-51	7 FLD	7.000	RIO	'n	;	ů,	٠.	ی ہ	6	ر ق	ي ه		<b>:</b>	÷ .	• .		m	å,	٠,	•
	AOE	•	₹!	5	2 . 16	727	70	1	, M.	. 7.5	51	.53	. 29	: 		50	200		. 05	51 1.	64 10	183 2.	0.8	ATION	Antile		.312	.381	. 451	520	550	.729	.795	0 0	.00	.080	154	304	361	199	54	524	3
	الحسا		™ ! = :	, -	12.	ν, i	D 1	0 10		1 20	-55	150	-55	-55	156	0.0	100	7	-5.	-57	-59	-58	-53		A.	, w								P C		~ 1	m d	• •	ص ۱	~	<b>so</b> (	or c	<b>.</b>

!	POLYTROPIC EFFICIENST	1.1219	1.0107	1.8138	1.8118	1.0099	1.0642	1.0886	• 9925	9546	4785	.426	. 962	.9356	. 2005		. 8630	. 8688	. 6536		i			•	!		•					•	1	1			!		k
;	ISENTROPIC P EFFICIENCY E	. 6120-1	2100	.0140	0210:	0181	5,00	0000							į					•	1	MEIGHT	. 8783	10/0.	00 / D •		.1789	. 6796	1674	16.20	. 1791	.8791	.0791	1610.	6948	.8786	. 8788	.0788	- 6767
•	DELTA T IS	033	7 M	926	034	934	035	35	036	936	, K	037	038	039	, 050	140	240	m	<b>.</b>			CURVATURE	-1.883	-2.255	14.12	-4-374	-5.822	-8.248	-13,636	5	ģ	23.458	16.698	13.517	11.298	11.600	13.044	16.878	29.725
	PRESSURE RATIO-	1.123	7	12	.12	445	12	13	•13	.13	7	13	13	.13	.13	.13	.13	• 13	. 13			SLOPE		•	•			•	•	•		1.58	.33	•					
	GLATIVE YPZZATURE	•	٠,	: =	i	ď.	• •	m	•	Ň	٠,	! ^	٠.	•	m	Ū	w	=	en.		;	HHIRL	37.8	38.3	38.6	000	39.1	39.5	39.0	20.0	39,3	39.3	39.03	38.7	200	40.4	41.2	41.6	50.0
	IVE R	67 540	£ 6	1 15	39	<b>3</b> 1		· •	20	92	. ·	? <b>«</b>	) +i	±	6		5	31				Z O	.4357	.4319	1724.	4533	4188	• + 166	.4146	1104	7604	.4072	2404.	.4053	7 C D D E T	3965	3930	.3912	. 3 888
	RELAT	17.0						17.6														RES STATIC	Š	ŝ	'n.		Š	ŝ	'n.	'n	, 10	6	15.679	'n.			Š	Š	ı,
	RELATIVE VELOCITY	6.24	52.5	69.7	64.6	4.60	75.7	479.33	81.7	84.3	200	96.5	7.76	95.5	93.4	94.7	95.8	95.7	m			TOTAL	7.54	7.55	7.56	7.58	2.59	7.59	. 59	֓֞֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֡֓֓֡֓֡֓	7.1.7	7.56	17.563	7.55	7.54	7.48	7.46	7.55	7.44
	RELATIVE MACH 10	3370	9 5	3	. 41.15	7	7 3	****	45	4.	. 4315	? "	10 44	3	M	3	+374	. 43 80	. 4383			URES STATIC	25.5	25.7	26.2	27.00	27.3	27.5	27.8	, c	28.5	28.8	523.833	28.9	29.3	31.0	31.45	32.0	32.6
	BLA0E SPEED	5.0.3	52	2 6	3	3	r t	559.7	3	69	22	9 6	36	98	20	07	2	20	26			-TEMPERATIOTAL	5.026	5.188	0*2*	יים ליים ליים ליים ליים ליים	5.694	5.790	5.856	216.6	5.172	5.247	237	5.215	0.476	7.604 7.604	7,462	6.231	8.691
	1638 332FF		5 :		00.				00	01	5	3 6	•	3	9.0	0.7	80	60	10	TYON		A. 7.	6 √6	'n	· · · · · · · · · · · · · · · · · · ·	27	77 5		30	0	999	33	.28 5	13	47 65	18 5	25.	, TC	13
	VIATION	*	٠.	•	'n	v.	•	-2.281	Ň	'n.	ů.	• .	: :	í	ċ		m	*	ň	ESCRIP		N 101/	154	446	2 P P	6 6 7	7	471	694	9	25.0	401	150	0 W 1	450	450	2 4 2	**	255
	FLOW DE.	519	029	702	220	794	361	. 551	030	÷1.	41,			7 70	190	593	154	73.8	330	FIELD D		ELOCITIC TANGEN	02.0	01.9	01.6	7 7 7	3 6 6	98.3	90.8	ግ . ለ . ፓ (		92.2	289.81	87.3	7.70	1	7.46	95.5	97.4
<b>4</b> I	S Rit	9+- 29	44	36	74- 16	16 -47	74- 64	56 -43	58 -49	67- 52	200	20 20	34	96 - 15.	52 -52	54 -52	13 -53	+7 -53	33 -54	4 FC34		MERIO	6.3	1:3	ا ۋ	•		5.0	*		7		307.03		3 P		, ,	2.0	7:1
ADE DAT	E-ANGLES	-5.9	6.4	7.00	.5.1	D:	2 6		-2.5	-1.9	7:1	711	,	? -		1.5	2,2	2.7	3.0	ATTON		Salo	2 12	230	782	75.7	307	920	994	\$ 00 C	200		1517	151	822	224	5 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	732	530
<u> </u>	T SECTION	57	=:		5	8	3	-45.37	77	÷	38	7 6	2 10	8	29	53	8	7	37	SI		EAN RA	7.7		~ (			7	?					10	10	D 60	9 60		3.0

BLADE DATA

C POLYTROPIC Y EFFICIENCY	. 0161	1.0139	1710	1.0887	1988;	, 8837	1020	9858	.96.	1116	9526	- 3643	.9377	• 5115	1976	2600		. 0769											1				•		•					
ISENTROPIC POL EFFICIENCY EFF	1.0190 17	i	-	1.0869 1.	ļ		1.0000		9885			. 9636	9361	860	8956			• 64.30	*CD* * - E		SPECIFIC	WEIGHT	. 1786	1919	99/0		16.43	. 1791	- 26.20	26.28	26/00	- 10703	+6.40	36.48	.0794	26./8*	. 1791	07670	06.48	.0789
DELTA T IS	. 051		1		!			250.	.053	.153	. 053	. 054	• 655	• 150	• 056	.057	000	640.	UELIA 1 UN		PA DIUS OF	CURVATURE	-5.825	-6.874	-8.317	122.6-	_11.908	-13.576	-15.713	-18.745	4/9*52-	- FAT . IFA .	-454.912	201.08	36.218		18.254	13,532	E	50.749
PRESSURE RATIO	1.194	1.195	1.196	1.197	1,197	1.197	1.197	19197	: 7	1.195	7		1.192	1:190	1.189	1.155	10101	1.187	296 * ===		<u>u</u>	SLO	5.54	8.24	7.86	2 6	55.33	5.71	5.04	4.32	3,56		66.	. 90	91	-1:32	-3.07	14.60	-7-13	-6.95
RE_AFIVE TEMPETATURE	541.591	2.510	2.835	3.516	3.872	4.239	4.517	2000	5.50	6.250	6. 87	7.139	7.511	8.178	6.529	9.173	つき し・か	0.340	PO.Y. EF		AMG	HHIRL	9	3	Ť.	ř		4	41,	4	j:	i -	;;	41.5	41.9	43.1	2		1	47.3
ATIVE RE	TU U	. 0	<del>-</del> 4	? N	. p	m	<b>~</b> (		, =	· IC		ľ	•	~	<b>-4</b> :	ים	Ð I	_	. 961		1	2	•	*	<b>.</b>	•			*	4.	<b>.</b>	•		3	•		<b>.</b>	*		<b>7607</b>
PREL	37 17.19	14	17	1. 17	2	17	51.	7.	-	17	7	17	17	17	17	[7	` :	17	EN. EFF. =		1	STATIC	15.500	ŝ	15,560	15.564	15.61	15,653	15	ŝ	'n,	15. 72.		Ġ	ŝ	15,790	ů,	15.80	Ľ	15.838
E GELATIVE VELOCITY	4F1.3	£5.	• •	****	4.5	447.7	450 •	451.	155	460 4	465.4	465.7	5	26.	57.	57.	٠	•	.194 ISE		750	. ₹	2	35	2	2	9 4	9	2	2	2	22	18.054	2	6	ž	5	90		o 🏊
RELATIVE HAC4 40	.3998	. 3941	. 3929	7368	3967	~	. 3975	. 3984	10 CC •	4904	. 4108	• +109	. 4067	• 40 25	. +0 27	4054	• 40 14	*3994	ATIO = 1		105%	STATE	26.0	26.3	26.7	27.0	27.50	27.3	28.1	28.4	28.5	29.52	29.7	29.9	30.5	31.6	32.6	33.3	2	535.524
BLADE SPEED	532.2	539.2	245	5.65.0 5.0.5	5000	558.4	5 6 5 • 5	566.8	575.5	580.0	5.84.6	589.3	594.5	599.3	5.04.5	610.0	615.7	621.5	RESSURE R		* MOFOA	<u> </u>	49.342	49.437	49.525	49.603	49.673	9.859	696.65	57.105	5.0.423	50.740	50.678	25408	50.700	51.294	51.693	52,221	20°20	553,366
103S	0251		50	5 5	10	S	00	0 0	7 5	4 6	0 2	03	9	8	9	2	12	13	ANC: J	PTION	:	AL 1	.61	•	¥:	9	ייי מימי	2 6	33	3,4		~ C	•• ••		 	35	35	51.		6.75
DEVIATION Incidence	-5.224	**	5.5	, .		4	3.9	e .	ه د	֓֞֜֝֞֜֜֝֓֓֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֓֜֜֜֜֜֓֓֓֓֡֓֡֓֡֓֜֜֡֡֡֓֡֓֡֡֡	•	٧.	£ . £	<b>*</b> :	5.1	ď.	9.5	•	O PERFORM	DESCRI	1000	) Z	7 53	26 53	13 52	85 52	47 52 ar	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	12 51	36 51	53 51	62 51	25 24 50 50		64 68	67 . 09	22 45	94 46		11 46
ANGLE }	9 :	32.23	32.30	3.67	35.05	32.74	36.42	7.11	0.000	30.05	69.5	0.34	41.05	1.83	45.64	36	44.21	4.97	NIEGRATED	LOW FIELD	10.10	ြ	36	347	m	ň	45 G43		ň	8	75 34	20	76 07	, P.	25	2	29	61.	` .	5 34 3. 44 34 3.
NGLES KE LEAN	6.276	•	4.6 38	3,950	2.346	1.530	865	216	100	2 4	247	954	166	624	. 522	0 32	530	m	I & NO	ON 9 FL	1	MERI	• • 0 • 6	*****	0 397.	395.	393	7 480.	386.	9 336.	9 363.	381.	9 37 8. A 17 7.	775.	336	7 357.	5 345.	339.	999	9 316.
3LADE-A! SECTION	429	1 6 5 5	386	279	9 4 5	739	3	2 2	ָהָ נָת ניי	, 6	9	3	59	9	\$	5	.37	133	STATE	STATE	ā	201048	543	595	7.542	683	739	2 4	683	940	. 993	740	102		273	333	396	161	22.	6.540 6.669
LOCAT		i i																	:		-	-LINE	-	~	m	*	<b>.</b>	D N	. 🗢		: 01	다 ! 다	27	? 4	1 51	1.6	17	<b>6</b>	<u>.</u>	27

	POLYTROPIC EFFICIENCY	1:0196	1.0171	1:010	1.0129	T.B.T.	1.00%	1.0000 1.0061		.9927	1986:	9796	9783	3776	9319	9639	8876	27	,8544	3	2																					
	ISENTROPIC PO EFFICIENCY S	Ì	_			1.115					. 9843	. 9626		.9/65	2896	2000	2465		4584	129	298° = 1-NO		•	E WEIGHT		İ			•	.0786		•  •		****	;		•		•		. 6763	
	DELYA T I		5	-: 620 :	99.	ю.	. 060	990	1	1981	290.	• 062	198	.061	290	100	100	590	456	190	. DELTA T 0	!	PADTUS -OF-	CURVATUR	9.349	10.555	13, 394	21.782	762.73	33.270	145 BB	661.04	36.929	32.610 	262.02	20.962	17:71	14.564	11.524	つきれ ・ ロ	3.053	
,	PRESSURE - RATIO	1.228	1.229	-1,229-	1.229	1.229	1.229	6221	00707	1.230	1:231	1.230	1.228	1.22.1	1.22.1	17567	1100	1.216	212	1.209	F;= ,'959			25	7.82	7.71	7.40	0 93 44 6	5. 87	5.28	•	:	ณ์	<b>તં</b> :	-		<i>;</i>	ij	-2.63	2.5-	-4-87	•
	RELATIVE TEMPERATURE	.42.332	542.518	216.24	43.214	43:325	+3.843	291:45	77447	46.044	45:353	45.321	46.298	46.583	547.380	06.5-4			207	42.04	PO. V. EFF	, }		*	41.	41.		• c	6.6	5 39.51	e c	ļ				39,22			5 42.3	10° 10° 10° 10° 10° 10° 10° 10° 10° 10°	<b>.</b> .	
	ELATIVE RESSURE	. 256	280	:305	.332	191	191		0 !	2 6	261	116	. 226	594	17.580 5	113	- 4	5 5 7 5 9 9	7.606	17.180 5	F.= .958			TIC	564	260	551	505	516	508 .4725	m c	- d	664	205	508	529 .4534	546	568	595	623	649 • <b>4</b>	•
	RELATIVE RI	446.26	86.444	444.33	444.25	. 64		60 . 60 f	* :	0		*	23	5	449.50		٥.	429.00	•	3 4	ISEN. EF		230(122300	ST	1 054 1	1 056 1	.058	56.	1063	.066	1069	1 070	085	.079.	.054	1 620	1 446	1 395	.868 1	.839		7 7
	RELATIVE R		3937	3930	3928	. 02 62		3939	346	5452		3938	3962		3961	5000	37.92		. 57.43	36.70	4TIO = 1.225		1	STATIC TO	531 1	572 1	550 1	593	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	26.483 15	515	1 000	087 19	280 18	370 1	1 20 1	750 17	17	252 17	104 17	32.984 17 77.815 17	1 670.
	BLAUE F		3	3	4	20	ž	22	5:	94	36	2.5	8	ž	588.7	2	5	205	ġ ;	011.0	RESSURE RAT			OTAL S	342 5	9.437 5	9.525 5	9.503 5	9.07.0	9.859 5	9.969	0.105	2017	0.858 5	0.678 5	492	700	200	וה	.568 5	52.945 5	30.00
	N LOSS	F. C.	- 02	- 12	01	01	01	- 00	00:			20.	. 02	-05	.0423	20.	. 10	71.	71.	61.	HANGE P	PTION	. !	14L 1	5,53	7.17	9.44 5		2,470	6.13	5.09	5.63	7.35	0.00	3.43	0.00°	1111	5 1991	5.98	9,85 5	3,57	3.26
	INCIDENCE		-12	-12	-11-	-11:	-10.	-10.	-	10.		6	-10.	-10	-11.303	11:	-12		.13	+ 1	ED PERFOR	ורט ספפכאו		CI NESNI	2,13	5.97	4.73	0 t 0	0 ° c	9.79	8.90	٠, د د د د د د د د د د د د د د د د د د د	200.00	30.0	6.04	2,00	ה ה ה ה	300	0.77	1.75	P4 98 5	7.00
	REL FLOW ANGLE	,			-27.	-27.	-26.	-58	ָרָרָ הַיּ	-30		-31	-32	-33.	-34.441	35	20	-37	-38	. 33	INTEGRAT	FLOW FIE		141 0 14	6	7.70	0.51 3	3.67	20.0	2.12	5.03		5,37	4.98 3	4.29 3	3.05 W	5.30	5 CT CT C	. 20	6 77 3	5.15	• 0•
	SE-ANGLES CON LEAN	2 2	2.5	2.9	3.5	2 3.5	3.9	8 4.1	7			9	6.4	6 · + · •	\$66.4 61	6.4	9**	m :	5 4.1	ν. Υ	ATTON 9	ATION 10		AUIOS A	575.5	: 2	6229	7222	77:2	<b>1</b> 10	117.	9202	5610	7	1650	2170	2020	26.29	60.4	5037	57.00 35	6339
ř	DOCAT SLAD		-12.9	1.4	-15.2	-15.3	-17.4	-15.3	-13.2	-20.0	7.02	-72.0	22.5	-23.0	15 -23.53	-23.9	-24.3	54.5	2.		ST.	S	, ,	STREKA KA -LINE								σ.	<b>.</b>	• ~	m	•	<b>.</b>	٥ ٨	. 60	6	3.	-

NCILATION
FILLO
11 FL3W
STATION 1

ł

SPECIFIC	иетонг	.0766				.0768	. 121B.	. 0766		.0764	.0764	.0764	. 17 03	00/0*	10.00		.8770	.0773	.0777	1824	OPIC POLYTROPIC	EFFICTENC				į	1.0094			-		• •	876.		1961		2006			
2	CURVATURE TH	~ .	9.070	0 2 4 5 0	649	.477	-15.607	-16.764	3.031	-22.766	9.030	542	7.44.0	77.664	1.424	37,987	5.199	78	m	r.461	<b>;</b> ⊢		6	1.0	,	ì	1.060 1.0097	Ì	-	ř	i	5404.		•		•		Ì	1020 · 6500	֓֜֜֜֜֜֜֓֓֓֓֓֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֓֓֜֜֜֜֜֜֓֓֓֡֓֜֜֜֡֓֜֜֜֡֓֡֓֓֡֓
	1	,	٠,		-						•	19		•		-	28	20	23 1	$\sim$	URE DELTA	ð		•	•	•	• •	-	•	!	!		-		250 1		•	•	•	• ;
NGLES	WHIRL SLOPE	20 9.06			72		87 4					۰.	å,	į	•	į	Ċ	91 -2.	-3	-4-		RE RATIO	822:1	1.22	1.22	1.22	1.229	1.22	1.23	1.23	1.23	1.231	1.22	1.22	1.224	1.22	1.21	1.216	1.21	216
	•	732 40.2	8	36.		, K	34.	34	34.	34.	34.	36	÷ ;	• • •	9 1	32	36	39.	41.	3. 44.	PE. AT IVE	TEMPERATURE	245.545	549.437	549.725	506-646	549.970	549.859	249.369	550-1.05	550.423	350.740 160 eee	550.578	550.492	550.700	551.294	551 :393	552.221	552.566	776.347
	IC NO.	3	*·	* "	2.5		978 .52	ı	r.	ď.	ů	•		ů.	•	1 13		- T	4.	. · ·		PRESSURE TE	:				18.061	ì					i		i		į	ĺ	600	000
SSURES	STATIC	4 15.49	15	15.2	12.	, L	1.5	7	14.	14.	16.	14.	1.		, ,	2	15	9 15,32	15	15.		VELOCITY PR					550.43 I	:					į					i		!
ed	TOTAL	13,05	18.03	18.02	4 0 4 7	18.16	18.066	18.06	18.07	19.07	13.03	19.07	18.05	13.02	17.93		17.86	17.83	17.80	17.77			ų,	<b>u</b> 1									!					1	w e	· ·
TIRES	STATIC	525.928	24.73	23.0	76.77	24.0	521.298	21.1	21.0	521.285	21.5	21.5	22.0	522.405	23.5	2 K	27.6	529.232	31.1	~		SACH YO	. 47 32	. 4865	•	•		•	•	•	•	i	Ì	•	•	Ĭ			•	
A SA	STAL STATE	9.3	4.0	9.0	0 4		959	7	7	*	~	•	ဖ္	* 1	٠,		•	ī	6	m	_	SPEED		•	0	o 1		•	•	•	0	-	<b>-</b>	•			•	•	٠	
	ا ا	4.63 5	9.11 5	2.13	2 2 2 2 2	200	01.0	3, 39	5.23	5.33	6.67 5	4.95	0000	5.52	6.71	0.00 0.00	ייר ייר	3.77	5.45	5.21	-	E SOEFF	000	0.00	0.00	0.00	00000		0000	0000	3.000	0.000	) L		0.000	0.000	0.000	0.000	מים	
4 1-	ı Z	07 53	52 54	10 55	לה הם	7	200	F5 25	55	12 59	65 49	35 59	31 59	53 63	83 57	200	43	69	74 51	10 49	011411	INCIDENCE	-8.619	-9.315	-3.854	-10.309	-10.630	140 041	-10.837	-10.710	-10.350	-10.002	145 650	-10.203	-9.83	-8.812	-7.821	-7.512	-7.314	つまつ・・・
6	TANCE	ř.	m M	m i	3 6	? ~	•	3	95 33	29 33	57 33	69 33	25 33	23	12 33	3 2	76 34	7 M	96 62	15 345	3		961°B+	38.727	37.433	30.519	35.791	32.640	34.597	34.431	34.537	34.697	240/45	34.15	34.987	36.134	37.+68	38.522	39.915	41.677
•	HERI	40 8.	420	9 9	9 .	•	, 44 th	7	064	4.01	064	488.	÷96.	*42	47.4	9 7	2 6	0	386	355.		LEAN	19.941	169.91	13.239	29.837	-26.337	166.23	6.429	12.936	-9.136	-5.202	1.350	5.5 AQ	10.024	16.049	53,193	30.509	112.78	45.134
	44 ULUS																			8.6199	1	SECTION	817	045	337	. 827	121	*	n M	141	188	698	2	9 0	, 0	9	69	34	62	7
	LINE	+1	~	m ·	e i		٥ ٨	. 4	σ	10	-4	12	13	77	15	1	4 -	٠-	55	. T.		NOIT					<b>.</b>						-					97	İ	

FLOW FILLS DESCRIPTION	
FILLS	
FLJ#	
STATION 12	

property of the property of th

1	,	!	}	•					!								:		POLYTROPIC EFFICIENCY	•	1.0014	. 9969	5966	2066.	1986	9808	. 9765	2005	.9559	1786.	. 9585	*****	COTC ·	3636.	. 9530	.8356	. 6166	v i
SPECIFIC MEIGHT	.0715	.0719	.0723	.0726	.0728	0730	0732	.0733	40.00	. B748	4670	. 0733	.0732	.8731	. 1729	.6727	·	r	ISENTROPIC P EFFICIENCY E	1.004I	1.0015	8866.	2966	0000°	.9850	-9802	.9758	9573	9546	.9556.	.9573		. 2142	.8561	8648	.8312	.0116	39. H T X
RADIUS OF SURVATURE	-3.688	-3.791	-4.245	-5.082	-5.673	-6.432	-5.918	-11-141	-14.850	220.22-	287.216	29.586	14.857	9.802	7,331	2,947			DELTA T	. 059	• 023	. 059	999.	90.0	.060	• 06 0	.061	. 061	.062	. 062	.061	290.	796	. 055	. 165	• 066	.067	DELTA T O
ANGLES Rl slope	5.21 4.36	3.56 2.85	2,24	1.37	1.10	. 93 84		• 70	. 688		0 KG	. 35	<b>*0 •</b>	-• 45	-1.11	-2.03			PRESSURE Ratio	-22	•25	.22	225	,,	.22	•25	•25	1.224	22	. 22	25	22.5	•	21.	2	1.207	50	939
ANG WHTRL	32.8 32.6	32°	31.8	31.4	31.3	34.4	30.9	30.8	30.0	200	2 6	31.4	31.9	32.6	33.5	34.5			RELATIVE Emperature	2	*	ů.	ō.	٥,	•	Œ.	ᅻ.	50.423	7	·n	.* 1	٠, ۱	v •	2	in	Œ.	m	PO_Y. EFF
- MACH	3 .6465	 . m	<b>т</b>			ر د د	- 10	•	٠.	•	- ·			•	•	•			ATIVE SSURE T	.997 5	938 5	666	666.	4 786	988	.983 5	982 5	987 5	988	973 5	958 5	935 5	000	797	766 5	.733 5	.695 5	936
SSURES STATI	13.59	13.69 13.75	13.80	13.91	13,96	14.01	14. 19	14.12	14.15	14.10	14.01	14.22	14 - 22	14.20	14.18	14.14			REL	17	17	17	17	11	: 5	17	17		17	17	17	11	1	17	+	17	17	EN. EFF.
PRE TOTAL	66	17,939 17,999	8	J. W.	93	86	66	8	97	2 3	2 8	2 20	2	2	2	59			/E RELATIVE	717.	712.	708.	703	697.	687.	682.	679.	674	200	• +99	660.	657.	655	0 40	3	ıŭ.	645.	1.220 IS
TURES STATIC	07.1 07.7	508.434 509.098	7.60	10.4 11.1	11.9	12.4	13.7	14.2	14.5	7667	12.	17.7	18.0	13.5	18.8	19.1			RECATIVE	35.	- 642	.03	.63	29.	19	. 61	• 60	-		. 59	.53	. 58 		. 57	57	.57	•	RATIO = 1
–TE4PERA Otal	4.04 4.04	149.525	9.0	,	6.6	50.1	50.7	50.8	50.6	2 C	) U U V	51.9	52.2	52.5	52.9	53.3			BLADE SPEED	0	-	0	0	<b>5</b> C	96	•	•	0.0	-	•	0	0	-	<b>&gt;</b> c	, 0	0	0	₹£SSURE
07 AL T	7.34	<b>6</b> M	7.83	7.32	2.39	9.03	1.67	9.32	6.33	67.9	5.50	9.16	5.72	4.31	5.03	26.5			N LOSS	• 32	• 02	• 02	• 05	20.	125	• 02	• 02	.0292		. 02	• 02	• 01	200	200	. 92	.03	. 63	MANCE P
LITIES	N M	9.00 79 3.35 70	35	e .s	93	110	42	101	90	÷ .	<b>3</b> C	6 6	, ,	37	25	39			DEVIATIONI INCIDENCI	9.0	.85	. 86	. 38	. 901	346.	. 96	•	1.006	• •	•	•	•	•	•			•	±ŋ PE₹F0२
15 T	.92 38	21 37 73 37	9° -	o/ 55 21 35	85 35	. CO 35	**************************************	45 64	.11 34	.63 23	55 T4.	10.	34	.85 34	.75 35	. 95 36			REL FLOW	2.80	2.51	2,35	2.37		1.40	1.33	1.13	31.051	7 7	0.89	0.93	1.00	1:1	7.0	2.66	3.52	4.55	INTEGRAT
DIUS	0 10	57 53 66 72	17 59	96 28	95 58		13 57	31 57	56 57	٠,	25 27 11 11	32 25	33	4	36 53	30 53	E DATA		ANGLES LEAN	24.5	23.3	21.3	19.0	15.6	m	10.2	8.1	-5.957	2.0	. M	S	-	2 · S	~ ^		4.2	8.2	ION 12
* &	~ ~	7.79	•	თ თ	• Φ	0	<b>&gt;</b> ~	•	-	N (	٧ĸ	2 M	•	•	S	S	3L AU	:	3LADÉ- SECTION	.95	.75	64.	.13	. 6	52	36	• 13	30.044	76	3	. 37	6	60.	200	50	. 45	£ 2.7	STAT
STREAP -LINE	40	m s	<b>10</b>	٥ ٨	. 🕏	σ,	3 +	15	13	# L	<u>.</u>	1 7			. S	~			LOCAT	**	~	m	.\$	<b>.</b>	۰,	•	6	2;	: £	: ::	*	15	9 :	;	5	20	12	

. :	, in	_	1				_	•-	_	1 1.			1		!	_	:		_	į			EFFI	!•	•	•	•		• ;	• '	•	•		• .	• •	1	•	ļ.		•	• !	•
: :	RADIUS OF CURVATURE	-5.196	-6.744	-7.811	-6. 113	10.690	-14.624	-16.876	-19.110	-21:113	-22.717	050.52-		-25.686	-27.627	-32.793	45.598	-168.841	76.314		i		- <sup>'</sup>	650	• 059	. 059	090•	. 068	990	000	. 161	.061	• 062	202	145	. 062	. 063	• 1064	• 165	. 165	9000	•
i	GLES	-2:23	-24 -2-	-2.45	£4°Z=	-2.36	-2.04	=1.61	-1.55	-1.28	-1.00		*	100			.75	. 87	80		1	: 000	RATIO	1.721-	1.221	1.221	1.220	1.220	1.219	1.210	1.217	1.218	1.218	1.216	1.217	1.217	1.213	1.209	1.206	1.204	1.202	C C T • T
	WHIRE.	17.58	17.5	17.5	17.5	17.	# C F	17.3	17.3	£7.4	17.4	17.4	17.5	17.0	17.7	18.0	16.3	18.7	19.2	:		- :	PERATURE	3.34	. 43	9.52	9.50	3.57	2.6		01.0	9.45	0.740	0.35		7.0	1.29	1.39	2.5	292	2.34	0
	MACH	5457	.5292	.5215	5142	ומו	nι	4907	- 3	. 4 861	10 to t	1204	104.	0 10 4	1731	4712	4714	4730	.4755				JYE TEMPI	35	ņ	30	24	ù,	יני ו	r d	50.0	55	99 55	ינט ה	א מ ה ע	י ני	50	52	ν. Σ	23	TO I	0
	RES STATIC	14.657	•	•	14.974	٠ د	ů	, ,	15.206	ŝ	15.248	, i	٠,	15. 267		,	15, 197	ŝ	15.099			i	PRESSUR										17.3									
	PRESSU TOTAL	17.942	8	.93	92	5	2 6	6	8	8	<u>چ</u> :	68.	8	9 3	7		9	65	62				VELOCITY										549.27					ŝ	33.	m	536.17	5
	URES STATIC	518.629	20.00	21.4	25.2	23.0	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	26.3	25.5	26.0	26.3	292	2002	2000	7	3 6	2 5	29.3	29.5				MACH NO	.5457	. 5373	. 5292	. 5215	. 51 42	• 50 70	. 50 C	7064	. 48 80	.4861	. 4843	1704	6083	. 4769	. 4731	. 4712	. 47 12	05.24	C: 14 •
	-TEMPERAT OTAL	545.64	49.5	49.6	49.6	19.7	0 0 0 0	50.1	3000	50.7	50.8	50.5	\$ 0 0 1 1 2 0 4	7 O C ::	7.1.0	, ,	5,5	6.75	53.3			:	SPEFD	-			•	-	•			•	0	<b>.</b>	•			5	•	ė	<b>.</b>	•
NOIL	AL T	2.59	7.0	60	93	21	* C	7 6	22	27	7	3		10 11 3 11	2 2	2 %	3 7	. ~	. 10			- 6	20EF	. 04.35		3	ŝ	0	.0477	9	.0563	0	• 05 92	.0573	<b>,</b>	0382	0	0	.0537	.0533	.0635	, coo.
ESCRIPTION	101	612	506	586	578	571	* •	200	551	549	547	5,42	26.	240	200	2 2	2 4 5	2.00	984				VIATION	•	•		•	•	•	•			1.624	•	•	• •		1.683	•	•	1.699	1.71
FIELD 0	ELOCITIE TANGEN	184.98	79.0	76.5	<b>*</b> . 2	71.6	9.0	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	9	64.5	~	63.9	63.3		, t		14	7.2.	7.5				LON CONTRACTOR	100	9.39	.516	.516	.516	.445	426	330	.360	.428	.465	- C - C - C		637	.738	.030	.377	.783	.223
3 FLOW	YERIO	59 3. o?	::	6	'n	;	÷,	; ;		;	å.	<b>.</b>	ů.	å.	•	•	: .		Ġ	a	,	į	N REL FI	14 17	21 17	17	22 17	92 17	55 17	28 17	17 69	37 17	00 17	05 17	21 22	32 17	33 17	21 29	98 1.8	70 18	22	67 24
ATION 1	orus	7230	918	276	249	019	ا ا ا		633	061	264	はかり	334	855	100	24.0	700	7 7	795	ial O	;		MI PANGLE	4	-8-9	-8.3	-7.7	-6.9	-6.1	. 5.2	3.2	12.3	1.5		•	? -	2	3.0	4:1		σ: 	Q.0
12	AH RAC	r. 6				•	•				•		•	•	•	•					į		SECTI	5.23	13	15	5.13	5.10	5.03		7.0	5.78	15.80	5.81		, A .	36.5	5.10	6.35	5.68	2.08	7.51
	STREA-LINE	40	u m	*	ĸ	9	~ 4	9											21				-10A	•	۰ ۸	m	•	'n	<b>9</b>		o	10	=======================================	75	2 :	<u>.</u>	19	17	18	13	20	12

ISENTROPIC POLYTROPIC FFECTENCY

9757 9757 9777

\*

١

1

i

SPECIFIC

i

ļ

EFF. 1.215 ISEN. EFF.# .918 PGLY. EFF.# PRESSURE RATIO = PERFORMANCE INTEGRATED STATION 1

FLOW FIELD DESCRIPTION	
FLJW FIELD	
STATION 14	

0.40, 75   50.00   41.45   549.475   510.165   17.00   18.700   426.5   610.40   41.45   549.475   510.165   17.00   420.5   420.5   41.45   549.475   510.70   17.00   420.5   420.5   41.45   549.475   510.70   17.00   420.5   4		7 T	N.1 28.4	TOTAL	TOTAL		STATIC	TOTAL	STATIC	0	"WHIRL"	SLOPE	RADIUS OF CURVATURE	OF SPECIFIC Ure height	2 E
77.45 7 137 137 147 137 135 147 147 157 157 147 157 147 157 147 157 147 147 147 147 147 147 147 147 147 14	0 2	80 0	~ 6	33.	¥ 5.4 %	21	20	17.887	15.789	.4263	6s 18	-4-74			
177.65	, m	ď		•	5 d	37 25	2 2	17.881	15.792	.4253	6.05	-4.05	17.34	70.	46
1,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0	2	~	*		10	) M	2 5	17.074	15.795	. 4243	5:94	-3.81	13-61	41.	
10.15	. ^	٠		6	5+9	73	2 5	47:357	100 100	• 4232	5.04	-3.56	20.07		*6
10.1		<b>.</b>	٠	ě	9+0	Ş	2 =	17.840	120001	0224.	5.77	+3:31	21.79		*
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		Ň		•	9.49	29	덮	17.822	15.886	0021	5.7	-3.05	23.84	•	*
## 10.12		Š			040	69	ᆵ	17.604	G	1014	* 0		26.33	j• :	
10.10 15. 15.10 15.10 15.00 15		ře	<u>.</u>	3	550.	35	=	17.796	5	1157	7	0	14.62	•	m
11.155		š	:		350.	 	Ñ	17.800		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		21.2	33.26	•	
47.15.		Š,	•	3	550.1		Ñ	17.805	'n	14469	2000	1:03	38.15	•	<b>2</b>
	٠.	٠,	•	3	520°	58	Ň	17.608		4467	70.0	-1.60	90.54		2
1.0   1.0		ů٠	•	•	550.6	<b>8</b> 0	Ñ	17,813	-	111	7.00		34.26		2
## 17.77   17.72   17.		•	:	:	550.4	92	4	17.820	ú				63.93		2
#55.47	_	'n,		ָייַ	550.7	00	Ñ	17.823		0000	2.00	10:	61.85		2
900-47 55.59 46.77 55.26.21 5-4.65 17.72 15.772 4106 5.59 4.13 17.656.9 1873 4.00 5.59 4.51 17.656.9 1873 4.00 5.59 4.00 5.50 4.51 1.656.77 55.62 17.656 15.75 4.00 5.50 4.51 1.656.72 4.00 1.656.72 4.00 1.657.83 5.53.56 5.55.42 17.554 15.75 4.00 5.50 1.05 1.05 -6.10.60 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.0		<u>.</u> و	•	:	551.2	36	N	17.772	'n	7 7 7	7.01	. 59	113.15	,	21
90 1-5 1-5 12 12 12 12 12 12 12 12 12 12 12 12 12		ۀ.	ŝ	67.7	551.8	93 5		17.712	·	1	30.0	37	176.64		9
971-31 53.10 454.63 555.56 535.27 17.619 15.752 4015 50.80 4.15 1200-122 0706 451.31 53.10 454.63 555.56 535.27 17.619 15.752 4011 60.85 1.06 -610.607 0708 451.31 53.10 454.63 555.36 535.56 17.504 15.772 4011 60.85 1.06 -610.607 0708 451.31 53.10 454.63 555.36 535.56 17.504 15.772 4011 60.85 1.06 -610.607 0708 451.31 53.10 454.63 555.36 535.56 17.504 15.772 0.011 60.85 1.06 -610.607 0708 451.31 53.10 454.63 555.36 536.35 17.504 15.772 0.011 60.85 1.06 -610.607 0708 451.32 55.32 5.32 0.043 0.0 4.25 40.35 17.805 599.38 1.227 0.059 0.059 0.008 451.32 5.32 0.053 0.0 4.27 0.008 17.807 549.37 1.217 0.059 0.059 0.008		ċ	3.	62.7	552.2	21 5	•	17.656		7 (	n,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	340.51		1
45.434		:	۲.	59.3	552.5	58		17.60	20.00	<b>7</b> .	9	• 15	1260.72		
Solid   Soli		;	٠.	57.3	232.9	i.		17.584	170 (73	3 :	•	. 45	-1393.45	•	· · · · · · · · ·
FELATIVE RELATIVE RELATIVE RELATIVE RELATIVE RELATIVE RELATIVE RESSURE DELTA TISENTROPIC COEF- SPEED MACH NO VELOCITY PRESSURE TEMPERATURE RATIO ON T EFFICTENCY PRESSURE TEMPERATURE RATIO ON T EFFICTENCY PRESSURE TEMPERATURE RATIO ON T EFFICTENCY PAGE 5-379 2-240 0.053 0.04 -4223 461.49 17.604 549.437 1.217 0.99 -9562 5.904 2.227 0.053 0.04 -4223 461.49 17.604 549.437 1.217 0.99 -9562 5.904 2.227 0.053 0.04 -4222 460.35 17.604 549.437 1.217 0.99 -9562 5.904 2.277 0.053 0.04 -4222 460.35 17.605 549.437 1.217 0.99 -9562 5.904 2.277 0.05 0.0 -4220 47.60 17.605 549.437 1.217 0.99 -9562 5.904 2.277 0.00 0.00 0.00 0.00 0.00 0.00 0.0		:	7	34.6	553.3	9.9	5.43	2 0	15.742	9 C	<b>-</b> 1	•	-553.12		
E3 NEL FLUM DEVIATION LOSS BLADE RELATIVE RELATIVE RELATIVE RELATIVE RELATIVE PRESSURE DELTA T ISENTROPIC NATIONAL LOSS BLADE RELATIVE RELATIVE RATIO ON T EFFICIENCY PRESSURE LAISE RATIONAL PROPERTY OF THE PRESSURE LAISE RATIONAL PROPERTY OF THE PRESSURE LAISE RATIONAL PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PRESSURE LAISE RATIONAL PROPERTY OF THE PROPERT	• 4							:	1011		200	•	-610.60		2
LEAN GIVELE NICTORINGE COEFF SPEED HACH VO VELOCITY PRESSURE FEMATIVE RELATIVE RATIO ON T EFFICIENCY COEFF SPEED HACH VO VELOCITY PRESSURE TEMPERATURE RATIO ON T EFFICIENCY COEFF SPEED HACH VO VELOCITY PRESSURE TEMPERATURE RATIO ON T EFFICIENCY COEFF SPEED HACH VO VELOCITY PRESSURE TEMPERATURE RATIO ON T EFFICIENCY COEFF SPEED HACH VO VELOCITY PRESSURE TEMPERATURE RATIO ON T EFFICIENCY COEFF SPEED HACH	) _	ن '' '' ر	2		•						,		:		
154	2		5 L	2 4 4 5	20.	w 6	RELATIVE	RELATIVE	_			RESSURE	EL TA T	SENTENDET	*****
17.86   2.22   2.22   2.22   2.22   2.22   2.22   2.22   2.23   2.24   2.23   2.24   2.23   2.24				<b>.</b>		3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	VELOCITY	-	TEMPE	w	RATIO	- NO	FFICTERCY	EFFICIENC
920 5-159 2-222 - 10543		•	33	•	649	•	?	3.5	•	9	,	•	1		
6.3         5.349         2.240         1053         0.0         4243         461.49         17.874         549.525         1.217         1059         9582         9584		•	2	•	649	0.0	. 4253				10	Ņi	•	·	9546
7.47 5.750 2.313 0.063 0.0 0.4232 4.60.35 17.865 549.572 1.6216 0.06 0.9569 9969 666		2.0	19 2	•	553	0	3	7 7 7	•			Ņ	• 059	o	• 969
747         5,756         2,372         0,682         0,00         4220         479,08         17,857         549,573         1,215         0,60         9589         9689           650         5,570         2,372         0,722         0,00         476,01         17,840         549,742         1,215         0,60         9472         9489           515         5,542         2,431         0,731         0,00         4460         476,01         1,211         0,60         9472         9489           515         5,543         2,431         0,70         4467         17,80         550,10         1,211         0,60         9362         9369           458         5,544         2,617         0,941         0,00         4467         17,80         550,40         1,211         0,60         9362         9369           5,547         2,617         0,941         0,00         4467         477,73         17,80         550,10         1,211         9466         9436         9466         9436         950,10         950         950,10         950,10         950,10         950,10         950,10         950,10         950,10         950,10         950,10         950,10         950,10		50	٦٠ *	•	563	0.0	3	An				Ņ	• 059	or.	- 4496
5570         5.372         0.732         0.60         0.9542		.5	50 2	•	585	0.0	: 3			0.540	· ·	Ñ	• 060	6856.	.968
533 5:542 2.431 .0791 0.0 4181 474.77 17.822 949.542 1.214 .066 .9472 .9466 15.55 5:55 5.54 2.657 .0864 0.0 4181 474.77 17.822 949.569 1.213 .066 .9322 .9322 949.369 1.213 .0864 0.0 4452 471.73 17.860 550.105 1.213 .0661 .9240 .9322 9422 473.10 17.860 550.423 1.213 .0661 .9240 .9322 9422 473.10 17.860 550.423 1.212 .0661 .9240 .9322 1.213 .0662 .9462 .9462 2.713 .0869 0.0 4467 473.10 17.860 550.423 1.212 .0662 .9462 .9462 1.212 .0662 .9462 .9462 1.212 .0662 .9462 .9462 1.212 .0662 .9462 .9462 1.212 .0663 0.0 4467 473.74 17.860 550.494 1.212 .0662 .9462 .9462 1.212 .0663 0.0 4467 473.74 17.860 550.494 1.212 .0662 .9462 .9462 1.212 .0863 0.0 4467 473.74 17.860 550.494 1.212 .0662 .9462 .9462 1.212 .0662 .9462 .9462 1.212 .0662 .9462 .9462 .9462 1.212 .0662 .94		50 5.	2 00	•	32	0	1000	76.0	_	549.0	<b>6</b> 0 (	<u>ټ</u>	. 060	2456	- 9566
515 5-593 2-494 -0653 0-0 -166 472-61 17-804 549-359 1-213 -1868 -9483 -		33	5	•	16.		41.81	•		7.64.0	~	ភ្	•	.9472	9446
478         5 - 55         0.864         0.0         -4152         471.73         17.904         5949459         1-211         0.60         9322         9328           407         5 - 524         2 - 617         0.845         0.0         -4156         472.35         17.805         550.423         1.211         0.61         -9159         -9159           243         5 - 524         2 - 713         0.845         0.0         -4167         473.10         17.805         550.740         1.212         0.62         -9162         -9162           142         2 - 742         0.750         0.0         -4177         473.74         17.805         550.740         1.212         0.62         -9163         -9162           142         2 - 742         0.750         0.0         -4177         473.74         17.813         590.77         1.212         -062         -9163         -9163           142         2 - 743         0.600         -4177         477.37         17.823         550.70         -062         -9163         -9163           144         2 - 743         0.600         -4159         477.37         17.823         550.70         -063         -9163         -9163		2	33 2	•	153	0.0	7		-	ָהָ ה		Ņ	•	9386	
\$\begin{array}{c} \begin{array}{c} \begi	•	0	33.	•	184	0.0	3	•	•	, c	ו ת	7	• 060	*9302	0
555 5505 2.670 .0841 0.0 .4162 473.10 17.808 590.740 1.212 .065 .9182 .9182 .242 5.496 2.713 .0863 0.0 .4167 473.10 17.808 590.858 1.212 .0652 .9055 .			١٠	•	195	0.0	7	472.35	-		0.6	Ş	. 161	- 0540	1926
2 2 7 13 0 8 6 9 0 0 4 1 6 7 4 7 3 0 7 4 1 7 8 1 8 5 9 1 5 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2		5.	2	•	14.	0.0	7	473.10	-	200	2 6	112-1	190	-9159	.9182
139 5.494 2.742 0.0760 0.0 4477 474;79 17.813 590.576 1.212 0.062 99880 1.422 5.743 0.083 0.0 4490 476.05 17.823 590.576 1.217 0.062 99880 1.42 5.743 0.083		, ה ה ה	بن م	•	693	0.0	. 4167	473.74	. ~		<b>.</b>	717	- 290	- 1896 ·	- 9116
155 5-512 2.747 0570 0.0 4490 476.05 17.820 550.492 1.21. 0051 9193 9215 2-45 5-512 2.747 0570 0.0 4459 477.37 17.823 550.700 21.3 051.93 9215 2-45 5-514 2.714 0.060 0.0 44159 477.37 17.823 550.700 0.0 21.3 0.079 2-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5		<u>.</u>	Š	•	90	. 0.0	. 4177	474:79		) E	;	717:1	290	. 9055	0906 .
2-5 5-512 2.747 -0570 0.0 -4201 477.37 17.823 550.700 -213 -05193 -9215 2-4 5-5-1 2.730 -0600 0.0 -4159 43.00 17.772 551.294 1.209 -063 -0639 -0639 3-5-1 5-5-1 2.712 -0603 0.0 -4108 467.70 17.712 551.294 1.209 -064 -8921 -8950 -065 3-5-1 5-5-1 5-5-1 5-5-1 5-5-1 5-5-1 1.205 -064 -8921 -8936 -065 -0651 -			ě.	•	83	0.0	.4190	476.05	•	ט ני ט ני	. פ	717	290.	- 1122	- 3776
27 2-271 2.772 0.0600 0.0 4.159 4.73.00 17.772 551.294 1.209 0.05 4.0339 4.0379 2.0714 0.053 0.00 4.103 4.0772 551.294 1.209 0.053 4.0339 4.0379 2.0714 0.053 0.0 4.103 4.057 17.772 551.294 1.209 0.053 4.0339 4.0379 2.021 1.209 0.053 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 4.057 17.554 552.555 1.199 0.05		0.0	Ņ,		20	0.0	• 42 01	477.37	_	280	įE		193	.9193	. 9215
20 2-734 2-714 0063 0.0 4108 467.70 17.712 551.593 1.205 0064 8521 1.205 0064 8521 1.205 0064 8521 1.205 0064 8521 1.205 0.064 8521 1.205 0.064 8521 1.205 0.064 8521 1.205 0.064 8521 1.205 0.064 8521 1.205 0.065 0.03				•	8	0.0	•4159	473.00	_	534.2			200.	: 5416.	- 9166
25 5.829 2.728 .0877 0.0 .4052 462.73 17.655 552.221 1.201 .065 .0291 .0335 .035 .055 .0551 .055 .0551 .055 .0551 .055 .055		16	•	•	63	0.0	. +108		•	5.00	· •		200	6555	. 687
.972 0.045 2.754 0.951 0.0 4011 4.7.38 17.584 552.345 1.197 0.059 1.059			20	•	51	0	• 40 62	•	w	552.2		֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓			- 2266
. 055 5.326 2.818 .1038 0.0 .4011 457.38 17.584 552.345 1.197 .056 7931 7.9582 5.326 2.818 .1038 0.0 .3985 454.68 17.548 553.865 1.197 .874.	9	10	,	<u>.</u>	٠:	0	• 4035		•	552.3	1 40	. 00		0 1	. 8 4 4 5
2962 - 1032 - 1032 - 1032 - 1032 - 10323 - 103	` =	יי כ יי כ	ų e	•	14	0	-	٠	.u	552.3		-	600	3 5	2
	2	;	,	•	53	0.0	€0	-	S.	553.3		5		?;	•

\*

!

14 91	,	2	- 20	ا ا	. ·	•	<u>.</u>	2 5	2 :	71	1 -	: 5	널	<u></u>	9		2		Z.	16				POLYTROPIC PEFICIENCY		.9527	6946	. 9414	-9328	.9272	. 9170	.9178	.9083	0360		6933	.9828	.9116	.8718		. 6149	• 7965	26.7.10	• 7010
SPECIFIC WEIGHT	10	•	2	9 1	•		•	9 6					.0801	.0801	.080	96.49	. 070	.0796	.079	5.0.5	!			ISENTROPIC EFFICIENCY	. 9256	.9513	1516	.9398	9340	.9252	94.16	.9045	1169		-	2869	.9002	6969	.8684	.8357	.8181	*197.	07736	.(351
CURVATURE	10.624	11.252	•		•	i	٠.	76.07	25.00	20.190	38.578	50.863	70.631	107.304	216.335	-126°5921-	-138.838	-69.433	-45.697	-31.905			•	DELTA T IS	660	. 059	650	.060	.060	.060	0.90	. 060	190	700	966	-105	.061		.063	100	• 165	• 065	• 000	/90.
SCOPE	-1.66		-1.56	הבינו	7 1	110	10.00		71.	177	9	. 1	F. 43	-, 32	25	01.	70.	•19	• 35	• 52	:			PRESSURE RATIO	1.213	1.213	1.212	1.211	1.210	•	1.207	7.205	1.205		1,285	1.207	1.208	T.209	1.205	102.1	1.197	10194	10191	1.169
ANGLE . WHIRL	0.00	•	<b>.</b>	<b>.</b>	• •	•	•	• •	• •		; ;	6	•	ċ	ċ	ċ	ċ	ė	ċ	ö				ELATIVE MPETATURE	9.342	1.437	3.525	0.503	1.573	242.645	r:359	9.369	501.1	.75.0		876	1.492	00.7.1	51.294	551.893	52.221	295.566	56.345	9000
NO N	.3754	.3757	.3759	2000	377	47.7	07/0	2770	4570	3737	3746	3769	.3790	.3811	.3755	.3683	.36"7	.3558	.3513	.3465				A H	36						,					i		,		!	2		H	
STATIC .	16.182	170	16.158	747	126	777		0 *	101	ď	5. I.S.	080	_	920	120	7.4	6.075	376	σ	• 084				RELATIVE PRESSURE	17.832	17.821	17.810	17.799	17.785	17.762	17:73	17.712	20/1/1	***	17.717	17.73	17.750	,	17.714	17,650	17.584	٠,	17.50	•
TOTAL S	17.832	•	•	:,		•	٠,	:,	:,		`.			•	•	17.650	ů	ı,	3	17.474				RELATIVE VELOCITY	1.5. 129	427 . 86	428.09	428.22	428.11	426.55	424.82	422 . 89	955.00	425.75	427.21	99-624	431.99	434 . 36	•	•	412.28	. ·	40C-03	•
STATIC	534.371	ž.	534.515	734.204			200	. 4	, u	21.0	35.	35.	535.209	35.	36.	37.4	30	39.0	39.	40.47				RELATIVE MACH 10	3754	. 3757	.3759	. 3759	. 37 55	. 3744	.3728	. 37 10	37.05	12.62	3745	3769	.3790	. 3811	. 3755	. 3683	. 35 07	. 3558	2013	• 2402
-TEMPERATURES OTAL STATIC	6		49.525	יינו הפ			•		•		9 . 0	9.0	50 * 4 92	0.7	1.2	1.8	å			۳, س				3LAO <sub>C</sub> SPEEJ	0.0	0.0	•	•	•	0.0	•	•	•	•		• ; •	•	•	•	•	6.0	D 0		•
AL T	5.	, V	63	n u	1 6		) ii	י ני	22	21.0	24	55	93	10	34	00	:O	† ;	in	10	t			COSS	. 1862	90	8	8	60	• 0988	10	Ξ;	.11.02	::	1155	10	9	.0760	9	8	2	Ξ:	1/210	2
TIES	.03 427	724 0	0 0 0	, ,	1 4	101	100	100	100	00 425	3 427	00 429	0 431	727 0	0 428	0 420	415	0 406	0 402	J 396				DEVIATION ENCIDENCE	23	33	• 56	.73	.91	20	'n.	3!	,	3	6	66.	.04	8	9	9	9 1	<u>`</u>	7	7
V.LOCI 0 TAN	5+	n c	F (	; :	4 IF		יייי פיייייייייייייייייייייייייייייייי	9 4		75	21	00	99	35 0.	34	ic :	53	96	0	90			1	ange I	5	.00	9	.00	ទុ	0.000	6	900	•		00.	00:	90.	900	8	56	3 :	9		•
A II	427.	٠.	* C C C		3	; ;				10		ď	=	:	å	ė.	v.	å	~ 0+	ů.	A	-		N Z	020	0	• 019	.017	.015	.013	<b>6</b>	<b>-</b>	900	, c	, 0	-100-	•	0	۰ د	•	<b>&gt; 1</b>	9 0	<b>•</b> •	•
AA DIUS.	7.6400	900	7.7		85.0	700	0.10	0	7 7 7	. 081	129	. 177	. 226	.275	. 326	377	431	400	545	. 600	0. 30 YO .			SCADE-ANGLESTION LE	523	•39	• 56	.73	•	8.079	52.	<b>→</b> u		1	91	66.	- 043 -	90	6120	620	200	771.6		7 7 7
STREAM	<b>~</b> (	<b>)</b> 1	<b>1</b>	· v	ı ve	۸ (	. «	o					<b>4</b>			-1			~ 1		:			LOCAT -IUN S	1					9						:						• (		

SPECIFIC	1.				•	•	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֓֓֓֓֓֓֓֟֓֓֓֓֓֓֓		2191		•	•	. 1882	•	•		•		•		ì	SPECIFIC		198.			•	.0803	•		7108			1000	2080.	2000		7678.	96.46	.0795
RADIUS OF	-	0:00	1004-014	9845-486	3930871	364.236	262:22	251.288	248-463	252.468	222.592	281.191	345.342	396.596	477.751	500.000	623.650	2995.874	0.00			RADIUS OF	CORPAIGN	980.0	900.0			0000	101	0.00			0.00	900:0	0.00				900°0	0.00
- 4NG1 E S		0.00	03	90 •-	60.	100	57	- 14	11.	14	-113	-, 13	- 10	60	•• 08	90.	* P = 1	10	00:00	1		LES	SLUTE	10.0	00.			- 01	10.0	01	10:4-	100	01	10.	01	10.		100	00:-	90
SM4	WHIPL	_0.00 -	0.00		0.00	•		00.0	.01.0 _	0.00	00.0	00.00	0.00	00.0	0.00	•			0	1		ANGLES	MATK	4.00	0.00		0000		0: 00.	0.00	0.00		9.00	.00:0	00.0	<b>9</b> • • •			0	
MACH	NO	.3863	.3851	.3639	.302/	*107*	3762	.3735	-3724-	.3730	.3736	.3743	3781	3800	.3742	3671	0.000. 0.000.	3507	.3465		;	E C	2	-3872	.3860	. 5.04.0 	0.5050	3796	.3769	.3741	.3729		.3747	-3769	.3783	1000.	75-76	2.00.0	6365	3507
HOFS	STATE	.16:03L	16.091	I61:9I	10.090	10.030	10.00	16.088	16.088	16.087	16.087	16.086	16.085	16:085	16.084	. فا	16.004	ġ	9	,		PRESSURES	SIAILC	16.083	16.083	10.004	10000	15.054	16.084	16.084	16.084	10.00	16.084	16.084	16.084	ė,	200.01	10.00	16.083	16.083
POPER	TOTAL" - STATE	-17,832	17.821	17.810	17.799	17.100	74.71	17.712	17,702	17.706	17.71	17.717	17.75	17.767	17.714	17:650	17.554	17.509	17,474			PRES	IOIAL	17,832	17,821	17.810	17.73	17.762	17.737	17.712	17.702	17.74	17.717	17.734	17.750	17.767	11.0114	17.584	17.544	17,500
11080	STATIC	533.515	533.701	533.880	534.351	224.625	3040404 14404 14404	535.132	535.348	535.613	535.874	535.930	535.280	535.334	536.362	537.495	538.388	539.00	540.473			TURES	SIAILC	533.445	533.631	533.513	555.387	534.437	534.762	535.085	535.307	535.977	535.905	535.588	535.265	535.323	3000000	124.485	539.074	5 30 7 A
TO MUTT.	FOTAL	49.3	40.4		9 6 t	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֜֜֓֓֓֓		6	50.1	50.4	50.7	50.8	000000000000000000000000000000000000000	50.7	51.2	51.8	52.5	7 C C C C C C C C C C C C C C C C C C C	53.3	: •		TEMPERA	OTAL	49.3	40.0	0 ·		10.0	49.0	+9.9	50.1	2 C	350.858	50.0	300	50.7	71.5	71. 72.	52.5	0
	TA	39.	38.	37.	35.	*	21.	2 2	24.	25.	26.	9	420.97	9 6	\$	19.			96	CKIPTION			TOTAL		39.	37.	פיני	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֡֓֓֡֓֡	29.	26.	in O	,,	427.28	29.	31.	M	•	, , ,	05.	
į	TANGEN	0.00	0		0 (	200	<b>=</b> 0	<b>,</b>	0	0.0	0	0		, 0	0.0	0	C (	<b>-</b> c		FIELD DES		-0CITIES-	ξ Σ		0.00	0.00	00.0		0.00	00.0	0.00	) •	0000	00-0	0.00	0.00	90.0	00.00	00.00	
1	RID	+39.58	438.33	437.05	435.75	454.23	451.47	42 5, 62	424.45	5.24	5• 02	420.93	47.00.32	433014	420.99	+19.28	410.58	00 ° C 04	396.80	17 FL34			MERIO	0	ຫ	~	Dι	$\sigma$	i o	.9	S I	n 1	427.29	ഗ	~	וכיו	•	J +	15	•
2010	3	•	•	•	•	•	•	• •		•	٠	•	3. 1755 8. 22-11	•	•	•	•	•	• •	STATION		RAUIUS		. 640	.673	. 723	761		. 891	.936	.983		8.1262	.179	. 254	27.3	* 55¢	6 3 7 5	683	
1000	-LINE	-	~	n	<b>3</b> (	y. s	۱ ۵	<b>~ «</b> 0	•	0			S 4							•		STREAM	LINE		(1)	m .	<b>.</b>	v .	۸ د	20	<b>6</b>	<u>.</u>	12	13	14		9 !	<u>.</u>	5	, ,

	LEAN- INLET	17.205	15.434	12:766	11.4443	10.299	9,351	0.00	6.864	6.170	5.640	5.243	4.923	4.147	3.510	3.610	2.397	1.835			LEAN-	u	-39.94T	-33.289	-29.837	-26.387	-22.991	19:697	-12,986	-9.196	-5.202	-1.356	7. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	10.026	16.049	23,193	37.25	42.734	46.652
	-ANSLES OUTLET	-11.816	14.12	39	17.44	18.39	19,25	70.07	21.40	22.00	22,56	6!	23.53	76.37	2,5	24.81	6	96	1		I-ANGLES	נ	-7.239	ט ה היינ	25	91	6	Ž,	5 C	69	2	56	7	92	5	25	12	15	17
	SECTION	-62,567	ıŭ 4	<u>, , , , , , , , , , , , , , , , , , , </u>	^	•0	י פ	2.	1 0	3	w	ا بِي	· •	0 0	١,		7	-\$			SECTION	48	48.517	40.44	46.827	46.421	46.074	45.749	45.141	44.887	44.698	44.602	10 TO 77	44.800	946.44	45.289	45.034	48.817	50.814
	Jel T4 H/U**2	.6483	63	2	61	-4	9	9		5	57	26	5 4 1	D 10	מינ	50	55	55			DELTA		60.		000	.000	.000	000		.000	000	900	•	000	.000	.000	0000	000	. 000
	REL V RATIO	. 4577	4	. 32.93	8	5	2	2777.	2 10	7	7	. 7373	22	67.43	3 ,6	55	3	62			REL V	44110	7997	7613	7473	.7375	.7277	.7195	7101	.7114	.7135	.7131	7278	.7505	.7517	. 7523	.757.	7792	. 3013
	DELTA P ON 3	.4731	75	200	62	53	120	ָרָ בְּי	4 4 4	32	25	413	110	2 4	1 (f 0 (f 0 (f 0 (f	"	9	9			DELTA	Z Z Z	69	2 K	1	5	4	368	2 5	369	365	3	200	352	347	338	.3218	: 4	202
	3-0 D FACTOR	.2639	298	7 5	335	346	356	365	0 6	399	405	404	417	7 t	100	. 6	501	16			3-0 0	200	m,	7	3.345	-3	.т	J.	0 1 2 2 3 4 5		J	ът.		707.		.4115	• 4114	0 0 0	•3605
	2-3 D FACTOR	.2553	291	319 319	330	345	352	303	389	397	401	9	417	\ + + + -	700	֡֝֟֝֓֓֜֝֟֓֓֓֟֝֟֝֓֓֟֝֟֝֓֓֟֝֓֓֓֓֟֝֓֓֓֟֝֟֓֓֓֟֝֓֓֓֓֟֓֓֓֓֓֡֓֡֓֡֓֡	504	518			2-2	5	5	2 6	3943	3	7	<u>ن</u>	3 3	3	ţ	. 4411	•	3	3	7	. 4114	2000	. 3503
	LOSS	0309	25	55	5	8	3	88	. 0137	20	8	. 0258	36	> =	3 0	4 -	1528	7			L03S	-	. 0362	. 000	3 E SO •	.0920	. 0938	<b>;</b>	3 =	. 1185	Ħ	# :	3 3	56	. 0802	8	1176	1221	1380
	JEVIA -TION	13.230	2.5		6.0	0.5	•	200	, e	6.6	0.3	6.0			֓֞֜֜֝֓֜֜֝֓֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֡֓֓֡֓֡֓֓֓֡֓֡֓֡֓֡	) M		•			JEVI A	7	23	יי נייני		.91	.07	.†.	⊃ (f † (f	0.00	.81	4		50.	0.0		9.082	1 G	2
	INCID	7.002	92	٠ د د د	91	9.	6	ê,		12	• 20	.31	•	ອີ ເຄື່ອ		1 K	9	-03			LINCIO	ก ร															-7.512		
- 10 E	1777 X	.4553	77	n	3.0	03	502	÷.	52.5	5.0	5+1	Ŷ.	000	40.0	200	1 6	50.00	593		:	1376		73	0 7 0 7	, t. t. t. t. t. t. t. t. t. t. t. t. t.	515	521	52.	1000	33,	330	529	1 C	7 17	204	÷6+	. 4342	4 1	. 4353
PERFORMANC	JUTEST RAJIUS	7.54.99	545	200.0	78.7	337	.333	- ·		102	158	. 215	273	222	0.00	,	960	00.	PE 2F 02.4		OUTLET	AJIO	70	3 ,	2.0	2	35	e i	1 6	2 2	3	27	7,6	27	32	37		1	3
20103	I HLE T RADI US	5.7500 6.3607	.38	55	32	7	10.	0	9.4	.99	• J3	-20	. 31	* "	2	2 .	88	60.			INLET	TC.	.51	;;	2 6	.82	.87	16.	מיני	.05	• 03	.13	֓֞֜֜֜֜֝֓֓֜֜֝֓֓֓֓֓֜֜֜֜֓֓֓֓֓֜֜֜֓֓֡֓֓֡֓֜֜֜֓֓֡֓֡֓֡֡֡֜֜֜֓֡֡֡֡֡֓֡֡֓	.22	32	.37	8.4278 8.4255	15	.61
	LOCAT -ION	4 2	m.	a t	, vo	7	€ (	σ,	3 =	15	13	4	15	10	33	•	61	· ~			LOCAT	NOIT	₩.	ν.	, <b>,</b>	ď	9	۲	<b>0</b> 0	` #	11	21	3	15	91	17	9 5	66	;ដ

(PERCENT)
3LOCKA3E3
LAYER
30 UND&? Y
ANO
MAKE

		- 7	O. 1 THE CALCU	SUMMARY POINT NO.	SUMMARY
3 9.3 10.5 T	9.1 9.1 9.2 9.2 9 1.0 1.0 1.0 1 9.0 9.1 9.2 9	5.9 '6:3 7.2 8.7 6.1 0.0 1.0 1.0 6.1 8.6 7.8 8.7	1.3 1.0 .5 .5 0.0 0.0 9.7 4.1	0 0 0	JIST FACTOR 1.0 INT BLOCKAGE 0.0
14 15 16	12 13	7 8 9 10	4 c	٠ و و و	

TEST POINT TITLE = 720318104505

.0620 DEL T/T = FLOW = 10.34 SPIED = 81>3.5 PRESSURE RATIO = 1.204 ISENTROPIC EFFY = .8770 POLYTROPIC EFFY = .8602

:

## 2. PHASE II WITHIN-BLADE ANALYSIS (50% SPEED) TEST POINT 208220415050

SPECIFIC	. 1767	.1747	7476	7.71	. 1747	1918.	.9747	. 8747	1420.	/4/00	7375	7470.	1928.	.8747	1918.	. 0747	2920	19/19		SPECIFIC	WEIGHT	18784	. 87 46	94/80	. 1746	.0746	.9746	. 0746	1743	. 1745		.0745	60/00	47.4	.0746	94/8.	.0746	94.48	3746
RADIUS OF CURVATURE	0.00	9000		000.0	0.8.0	000.0	0.8.0	0.00	909.0			0.00	0000	•	•	0.00		• : •	† : :	RADIUS OF	CURVATURE	-285.758	-139.003	-113.682	-99.393	- 58. 658	-79.778	+62°1/-	-55.842	-49.024	-45.884	-37.422	-32.608	-24:662	-21.432	-15.619	-16.170	-14.034	143 4KE
ANGLES RL SLOPE	20.93	19.76	17,38	15.13	14.98	13.78	12.58	11.39	10.20	70.00	6.76	5.68	49.4	3.65	2.74	1.90	1.15	100 °C	,	LES		- 28.83-	19,60	18.39	17.17	15.95	14.72	12.25	11.02	9.79	-9:20	7.35	6.73	. 83 ·	2.72	1.66	• 66	92.	7,7
ANG WHIRL	0.00	8		00.0	0.00	00.0	0.00	00.0	0.00			00.00	00.0	00.00	0.00	00.00	•			ANG	WHIRL	00 00 .	0.00	0.00	0.00	0.00	00.0		0.00	00.00	. 90.0.	96			0.00	00	0.00	00.0	•
MACH NO	1520	1520	1520	.1520	.1520	.1520	.1520	.1520	.1520	0631	1520	.1520	1251.	.1520	1520	.1520	1261	.1520	i ,	MACH	O.Y.	1641	.1649	.1655	_	1667	.1672	1582	1683	.1685	.1685	.1684	1677	11671	1 41	1653	.1641	.1620	
ESSURES STATIC	14.461	14.401	14,461	14.461	14.461	14.461	14.461		14.461	140401	14.461	14.461	14.461	14.461	14.461	14.461	14.451		:	URES	STATIC .	3	14.420	14.418	14.416	14:41	14.412	14.410	14.409	14.408	14.408	14.408	14.409	14.413	14.415	614.41	14.423	24.	
TOTAL	- <b>-</b> 3 .	•	j	j	÷	÷	14.696	<b>.</b>	<b>.</b>	• 4	•	•	;	<b>.</b>	<b>.</b>	<b>.</b>	14.696			PRESSURES	TOTAL	14.696		÷	÷.	•		14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696 "	14.696	14.696	
TURES STATIC	516.315	ָם <del>ו</del>	16	16	16.	91	9	ġ	ي ۾	2	16	16.	16.	9,	9	9,	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	9		က်	H	515,922	515.897	515.875	515.854	515.835	515.515	515.790	515.781	515.775	515.774	515.777	515.800	515.821	515.848	515.882	515.924	512.574	
TEMPERATUR	518-688	9	3.68	8.68	8.58	8.58	ů.	9	0 . U	9	3.68	3.68	5.68	80.0		9 4	9	3.68			FOTAL STA	8.6	8.6	3.6	9.0	3.5	0 «	518.688	8.5	ð. 5	8.5		9	18.5	18.5	8.5	9.0	٥.	•
TOTAL	170-12	•	0.1	0.1	0.1	3.1		היי	, ,		1	1.0	7.0	<b>.</b>	٠ •	۲ • د	•	1:0	CRIPTION		TOTAL	83.6	84.5	85.2	95.9	0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	87.5	188.01	88.3	88.4	55.55 5.55	* * *	2 · · · ·	87.0	86.1	85.0	m :		
LOCITIES- TANGEN	0.00	<b>-</b>	0	0	0	~	C	<b>&gt;</b> 0	<b>-</b>	9	C	C	0	<b>-</b>	<b>-</b>	<b>,</b> c	<b>-</b>		SEO CTEL	OCITI	TANGEN	9	9	0	0	9,	7 0	000	0	0	0	<b>&gt;</b> c	9 0	0	0	0	0	3	ē
FRIO	176.12			0.1			₩.	•	•		7		=	7	: :	•		1.0	2 FLJW F	;	MERID	m	;	ů.	ů.	ė٠	: .	188.01	å	å.	Ď,	ė «	: .		ġ	ŝ	'n.	• .	d
RADIUS	6.0630 6.2263	9 K	539	• 693	. 847	665°	151	200.	505	752	905	051	139	2007	2.7	704	941	060	STATION	RADIUS		37	'n	9	<b>8</b> 6	7 6	2 4	7.3303	46	29	2	00	3,	26	33	23	9	3	3
STREAM -LINE	40	ı m	٠.	ī.	ا ب	~	<b>•</b> 0 0	n c	7 F	12	13	<b>*</b> !	51	<b>→</b>	6:	4 +	50	21		STREAM	-LINE							· •o	σ	<b>.</b>	<b></b> (	u M	•	2	9	~		P c	

STATION 3 FLIM FIELD DESCRIPTION

STREAM	RADIUS	A	VELOCIFICS-	•	a	ERATURES	PRESSURES	3URES	HACH	ANGLES	ES	RADIUS OF	ัก
		MERID	TANGEN	TOTAL	TOTAL -	STATIC	TOTAL	STATIC	0	WHIRL"	SLOPE	CURVATURE	WEIGHT
•	. K. 6016	198,92		198,92	18.68	515.444	14.696	14:376	\$ 177 £	00.0	20.54	-83.831	
۰ ۸	6. 7260	199.87	0.00	199.87	8.68	515.413	14.696	14.373	.1787	0.00	19.39	-262.785	++20
m	6.8496	200.93	0.00	200.93	518.588	515.376	14.696	14:369	797	0.00	18.21	1152.407	- 124.C
*	6.9725	20 2 2 21		202.21	80	515.335	14.696	14,365	1 803	00.00	17.00	343.501	**/1
2	. 2:60:4	-203.44		203.44	18.68	515.295	<b>.</b>	14.501	6171	•	12.00	5000	11/0
؛ و م	7.2161	204.63		204.65	0 4	2629614	14.090	140.327	1840		C+ - + T	-945-536-	18743
	7. 5550	27.602	<b>5</b>	2000	10.50	515.5 19 515.185		14.350	6467	0.0	11.87	-214.030	.0743
: o c	110401	20 00 00 00 00 00 00 00 00 00 00 00 00 0	•	207.46		545,453		14.348	1855	00 0	10.52	-109:951	. 1743
P =	7. 6964	20.8.06		208.04	8.58	515-140	,	14.346	.1860	00 00	9.17	-70.393	.0743
	A358	20 82 38	•	708.33	18.65	515.125		14.345	1.863	00.0	7.80	-50.154	- 6743
12	7.9353	20.8.45	3.00	208.45	18.68	515.125		14.345	.1864	0.00	6.43	-38.026	. 6743
, j je j <del>je</del> l	8.0551	208.24	0	208.24	8.68	515.133	14.696	14:345	. Z98.I.	. 00.0	-5:15	26.997	
*	8-1753	207.72	G	207.72	18.68	515.151	14.696	14.347	.1858	0.00	3.67	-24.314	. 6743
.15	8:2962	206.85	0.00	¿ū 5• 83	18.68	515.180	14.636	14.350	.1850	0.00	2.30	-21.112	
91	8.4180	205.64		205,64	518.688	515.221	14.696	14.354	•1639	0.00		-16.907	. 0743
- 43	- 8-5419-	204.03	0	204:03	16.68	515:275	14.696	14.359	.182	0.00	14.	204°4I	10.0
18	8.6653	202.03	•	202,03	18.68	515.342	<b>.</b>	14.366	.1506	00.0	-1.74	-12.426	*****
61	23	199.61	<u>د</u>	193.61	8.68	515.455	ġ.	14:373	1785	? •	50.5-	010.01	****
20	8. 913b	196,77	0.00	96.	17.68	515.514	÷	•	1759	) · o	07.4	110.6-	****
12	9.0500	193,55	00.00	193,55	518.688	515.617	14.696	14.393	.1730	00.0	-5.47	269.8-	64/0.
					!	1	:	i	;				
STREAM	RADZUS	7	VELOCITIES-		TEMPER	ERATURES	PRESS	P2ESSJRES	HACH	ANGLES	.ES	RADIUS OF	SPECIFIC
LINE .		MERID	TANGEN	TOTAL	· TOTAL ·	STATIC	TOTAL -	- STATIC	NO.	WHIRL	SLOPE	CURVATURE	
	- P4.00	100	92.00	7+0:47	-51-8-8-38-	519:09F	14.696	14:338	2881	0.00	-20.32	-366:054	. 8448
۰ ۸	6.8563	21.3, 25	00.0	213.25	18.68	514.360	14.696	14.528	.1907	0.00	19,23	-117,333	2420.
1 PO	6.9813	215.90	00.00	215,90	18.68	514.867	14.696	14, 319	.1931	. 60.6	18:07	.75.671	2141
<b>.</b>	7.0951	21 8. 41	00.00	218.41	68	514.778	14.696	14.310	.1954	0.00	16.84	-59.233	2428
	1:2078	-220.74	00.0	. 520 • 74	•	. 514.593	. 14.696-	-14: 305-	. 1975	0.00	15.57	-200419	1940
9	7.3196	22 2 . 90	0.00	222.90	68	514.615	14.696	14.295	•1994	9.00	14.24	-44.375	.8741
1	- 4.4303 -	69:422		-554:33	18.68	214:040	14.696	992.41	21020	00.0	18-21	104:65	14/00
••	7,5406	22 6. 55	00.0	226.56	518.688	514.480	14.696	14.281	2021	0.00	11.47	-35.370	74./8
5	7:6502	£6°122	00.0	- 66 . 755	16.65	124.416	14.090	14.670			10.03	100 100	67/0
	7.7595	22 9. 12	20.0	220 03-	10000	274.302	14000	740-260	05020				4444
H	7.5636	26.622		24.622	9	514.334	14.696	14.267	2000	00.0	5,61	-26.381	0420
7	111601	24 00 00		75-11-20	8.00		14.898	14.287	2003	00.0	4.11	960:63	- 8748
2 4	8401.8	23 0 27	20.0	230.27	518.688	514.341	14.696	14,268	.2061	00.0	2,59	-23.594	1420.
	- 44.3077	22.9.58	30.00	- 229.53	15.58	514.367	14.696	TA: 270	-5502	00.0	1:06	149:17-	0440
10	8.4186	22 8 . 44	00.00	228.44	518.688	514.410	14.696	14.275	**02*.	00.0	P. + 3	-20.314	. 8749
41.	8.5311	226.8I	. 00 00 .	226,81	18.68	-214.471	14.696	14:581	- 12021	00.0	-2:01	18:956	19.40
8	8.6451	224.65	0.00	224.65	518.688	514.551	14.696	14.288	.2010	00.0	-3.55	-17,341	.0741
	8.7610	22.I.85	Þ	221.38	73.68	214.652	!• ≥• .	14.298	1985	00.0	11.65	442961-	10/20
20		•		218.37	18.68	514.779	14.696	14.311	.1953	00.0	90.00	256.21-	2430

4	
-	
ă	
_	
8	1
9	
2	i
~	

ENCY		9			•		• •				<b>.</b>	<u> </u>		-	-	•		•						   					]															,	1
	1.000	1.666	1011-1							1.6162				7.166	1:010	1.1111	1.0	1.1111	1.1111			1:22																							l
EFFICIENCY EFFICIENCY		_							L							1.1	! L	_				1.000	V)	WEIGHT	5248:		1		1111	.8777	• 1776	•1776	67779	.8775	-1775	*2.20	2110	. 8774	6//0	*228	h//8°	c2/10	61/19	.1775	
OFF T	0.000								3 <b>20.</b> 0		000.0		į	<b>9</b> 00.0	000:0	0.00		0.00	# FOR 6				RADIUS OF	·· CURVATURE	"6.199	6.318	. 6.681	7.312	8.274	9.650	11:683	14.528	19:377	58.82	295:45	316.704	+95 .335	-45.6/6	-32-174	-28.289	614:12-	-29.871	625.75-	-62.866	
KATIO	1.000	1.000	f. 98 G	1000	1.000	1000	1.000	T • 000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.11.0		1000	1.500	LES	SLOPE	22.32	21.10	.19.75	18.31	16:79	15.21	13.00	11.94	10.27	8.58	6.89	5.21	3.53	1.86	61.	-1.45	-3.04	-4.60	-6.17	-7.76	
TEMPERATURE	. 222	842	558.280	0710	295.266	- 4 P	27.2	1941	556.520	711	1815	. 335	. 276	.230	410	516	.351	567-119	425	110	*	.173	ANGLE	WHIRL	- 25.76	26.11	25.45	24.82	24.20	23,62	- 23:08	22.61	22,21	21.99	21.84	21.74	-21:-69	21.68	21.90	22.45	23, 04	23, 38	23.71	24.07	
VE KE, N RE TEMPE				ļ							•						į					+ 571	MACH	0	-222	.2611	.2643	.2674	.2704	.2736	.2767	.2795	.2821	.2845	.2867	.2888	.2908	.2928	.2945	.2958	5362	.2975	• 2976	.2972	
PRESSURE		17.97	18.090		16.552	ĕ.	ŏ	ö	18.834	ė	5	19.231	19,36	19.510	19.65	19.803	19.4	20.113	26.27	111100	***	20.62	2ES	STATIC	15, 328	15, 316	15.302	15.287	15.271	15,256	15:242	15.230	15.220	15.214	15.210	15.210	15.213	15.219	15.228	15.241	15.256	15.274	R	15.314	
VELOCITY	636.19	646.87	637.40	50.790	6/8-83	21.000	696 09	26.202	717.61	727.19	736.65	746.03	755 • 32	764.55	773.71	782.84	791.95	801.07	A10.20	3 9	•	828.58	PRESSJRES	TOTAL	16.051	16.058	16.062	16.064	16.056	059	073	8.40	6.084		16.102	16.115	16.131	16.150	16.171	ġ	ė	16.240	. 561	16.280	
MACH NO	• 56 90	. 57.85	.5881	*2:5:	• 50 05	7619.	64245	• 6335	• 6422	. 0508	. 65 93	. 6677	. 67 60	- 58 42	•6954	• 70 05	7087	.7163	72.40	647.0	• /3 30	.7411	RES	TATIC	124.927	24.816	524.589	524.548	524.400	124.255	524.125	54.005	53.913	:23.945	24.000	524.086	54.206	524.358	524.654	55.185	525.761	526.180	56	527.071	ì
SPEED	9,009	610.7	650.9	651.1	: : :0	651.0	660.9	670.7	6.80.4	8	6.659	6	5	23	38	748.8	Š	768.9	2	7.00	ŝ	800.5	TEMPERAT.	OTAL STATIC				32.006													4.976	5.443	5.834	6.330	
COEF	00	90	0.0000	3 (	9	3 6	3	3	8	00	8	8	3	9	0	3	5	9		3 6	9	8	٠	AL T0	***	69	23	~	90	53		23	15 5	82 5	in H	75	36	28	30	اد 8	24 53	21 53	10	23	
NCIDENCE	é	•	10 1	ė,	'n,	ċ,	ů	•	•	•	-8.515						6	,		•	-10.215	ė	ES	TOT	4 290	7 29*	2 298	62 301	4 305	2 308	5 31	33	0 31	4 320	8 32	3 32	3 328	+ 33	2 33	3 33	.†	33	336	336	,
ANGLE IN	0.63	.75	-70.827				5	.33	~	٣,	1.31	2.01	2.23	2.47	2.73	.03	35.45	7.7.5		971	4.743	5.036	=	TANG	130	129	128.	120	125.	123.	122.	121	120.	120.	120.	120.	121.	122.	123.	127.	131.	133	135.	137.	
EAN SE	205 -	454	5.443 -7	105	667	n .	324	<b>+ 0</b> 5	581	725	œ	193	657	N	934	593	20.0	200		֓֞֜֜֜֜֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֜֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֓֡	- 204	836 -	•	MERID	259. 6.	:	ď	27 3 92	÷	å	:	÷	;		.;	302,5	;	306.91	ė	å	ė	398.65	ė	å	
CTION	667 1	1 265	601 1	1 699	736 1	1.73	426 1	933	,059	180	.298	421	545	629	756	343	425	032		0 71.	• 329	۵	RADIUS		.89	00	=	7.2147	.31	13.	. 51	.61	.71	.81	. 51	.03	.11	.21	33	. 41	. 51	• 61	.7	422	֡
-ION SE			3 -62																) (	9	Ġ	io	STREAM	-LI ME	-	۱.۸	מו		ĸ	ø	~	•0	6									18			

POLYTROPIC EFFICIENCY	1-1809.	0003	6666	• 9995	- 2666	.9990	. 9987	. 9985	- 9766.	2313	6406	27.67	9776	2000	9526		2468	. 8631	8711	•		!			:			9 11 0000000000000000000000000000000000									-					
ISENTROPIC PC Eppiciency ep	1.0889 - 1	.0804	1		2666			.9985	. 9979	2166.	1496	27.04	77164	9000	92.66		8927	-8816-	8697		ON T = - 128			<b>P</b>	MEIGHT			68/8	00/0	10.00	. 0786	9848	. 6786	. 07.00		.8787		. 0787	10.00	-944	. 8787	
DELTA T ES	. 025	• 026	• 026		920.	. 026	• 1126	• 026	. 026	920	120	/20		0 00	20.	1 1 1 1 1	0.32	033	1 0 % A		DELTA T			-RADIUS OF	CURVATURE	4.382	S - 643	3.451	250 61	167.734	-40.842	624-12-	-15.795	622.61	-11:196	-10.925	-11.00¢	-11-426	026.21	-44.044	-23.898	
PRESSURE Ratio	8	8	1.093	8	1.093	1.003	1.094	1.094	1.094	50.1	1. d	. 600	53	r (	•		1 1 2 2	1	=	:	: !			:	SLOFE	27.37	25.22	\$0 ° 8 6				12.20		11.0	5 ,5	2	•		64.22	15.60	4.95	
RELATIVE FEMPERATURE	-	50.15	11.460	32.426	33.394	64.364	55.337	6.315	557.298	26.290	<b>.</b>	315.00	7 6 6 4 6	0000	744.144			67.360			,			DNE	WHIRL	32.	ij	i	ı					10:12			•		-	01.10	32,	
RELATIVE REPRESSURE TEN	005	116	227	339	. 155	565	679	252	911	21.0	72	10 t	7.	0 4	n q					101	. 952			¥	o Z	3 062	m I	•	•	127.00	•	"			•		Ť	Ī	95.5	POPPO TOPO TOPO TOPO TOPO TOPO TOPO TOP	333	
i	**	7	ec.	~	. €	-	28 18.	-	•	۰,		2.61 96				•				3 6	EFF.			PRESSURES	STATIC	15.659	'n,	15.587	13.50	12, 24	15.524	15.52	15.525	256.61	15.55	15.574	19.592	15.612	100.00	12.672	15.698	
RELATIVE VELOCITY	•		571.6		_	_	_	_	638	_		3;	20	5 :	0000	. 6				9 8	SI			P2E3	TOTAL	70	•	16.657	70001	100001	16.696	16.711	ě,	19-790	16.797	16.824	16.852	16.880	16.90	0 0 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	25	
RELATIVE MACH VO	,4355		. 5065	. 5170	. 5273	.5374	.5473	. 5569	. 5561	. 57 42	.5820	. 58 95	4050	. 50 40	6505	. F. 78	62.43	50 0 C	22.73	6000	15 co.			URES	STATIC	528.115	527.752	527.459	622.126	56.035	526.877	526.864	526.903	527.153	527.767	528.112	520.476	523.080	530.119	751.134 541.042	532.609	776.000
9LA0E SPEED	13.	623.0	632.4	7	650.8	5	8	2	5.86.3	5	5	25	;;	5 5	7 •	2 4	70.00	2 K	١,	n.	2FSSURE R			-TEMPERATURES-	JTA:									338.582				696	-220		5.84	•
1.05S	0	00	0	90	0	0	8	8	.0003	9	0	5	5	5	٠,	) F	3 :	1 1	3	5 6	econ.		PTION	•	۳ ۲			<b>เ</b>			· · ·	27	•••	3,64 ·· 48,2			•	•••		v it	, 15	***
OCTATION A VCTDENCE									-1.141				-1.145	-1.172	-1.569	4 6 6	6 4 : • • • • • • • • • • • • • • • • • •	77.4		****	בי מנו מנו		CESCAL	£S	EN 101	£3 ? .	2 11	. ' ! & !	71 55	351	366	24 369	00 37	36 37	55 37	38 37	24 37	93 38	88 86	20.00	30	2
REL FLOM S									-52.518									100.400		•	<u>ت</u> د		FLOW FICES	VEUOCITI	U TANG	07 18	42 18	85	55		17	17 17	55 17	99 173	27	27	18	18	0 - 19		2 6	
ANG1.ES &	32	9.969	: :5	4		22	53		29	_					_				9 (	r •	, 10 to 10 t		٥	•	#.RI	292,	299.	305	311		323	326.	329.	330	332	333	334.	333.	530.	327.	2 2	300
3LADE-4	60.252	50.351	62.529	60.692	50.346	03.975	61.038	01.233	-61.375	520	:1.662	-01.799	61.931	950-20	6/1.29	062.22	F 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	500.040	000.00	000.70	57.47.02	1	STATION	- RADIUS		7.073	7.174	7.263	7.359	が ウ ウ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・	7.623	7.709	7.795	2088		A. 1354	8.222		966.58	0.400	200000	· P . O . O
LOCAT									6		,	12	P.	• •	• •	0 1		Ç 0	16	,	5		•	STREAM	1 NE	-	~	m .		n v	۰ ۸	. 40	g.	-	• • • • •	e m	*			<b>~</b> 1	10 c	P.4

	POLYTROPIC EFFICIENCY -	4	1.8005	2666.	. 8893	6866	9865.	. 5982	1866.	.9971	0886	9793	60/6	6296	786	* L 100	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1,69.		4629 •	.3067	<u>.</u>			_	-	-			••	•				0.4		i.							
	SENTROPIC	7	1.0005	800	o	or	o	œ	.9979	or ·	<b>.</b>	<b>3</b> 00 (	<b>49.26.</b>	<b>3</b> 1	or a	J (	/206.	о •	ю (		9129	•			E WEIGHT											0000		•		•				9880	•
	OELTA T I	.037	.037	.037	.037	. 637	. 037	.037	.037	.038	000	. 039	0 0 0	140.	240 •	940.	0 t	***	640	• 020	. 051	. 053			RADIUS OF CURVATURE	•	-3.427	•	m	•	-4.36	-4.791	-5.306	-5.923	999.9	- 00 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		-11.47	-13.206	-15.206	-17.774	-21.747	-29.421	-52	56875.
	PRESSURE PATIO	M	13	13	.13	.13	.13	.13	1.137	.13	*	*	4		<b>.</b>	:	::		:12	•15	• 12	• 15			SLOPE	26.61	23.80	21 • 12	18.57	16.14	13.62	11.60	0 · 6	7.45	5.51	3.65	16	-1.48	40 · E -	-4.47	-5.74	-6.85	ō.		•
	AFIVE PERATURE	_		-				-	7.213		<b>T</b>	☎.				• 1	<b>~</b> •	vn.	٠.		•	'n			ANGLES	36.0	35.8	35.7	35.6	35.5	35.5	35.5	30.4	35.4	35.7	56.11	36.7	37.0	37.8	39.4	41.0	42.0	42.9	43.9	45.1
	E TEMPI								557																A CA	.4053	.4.060	4 07 1	0604	-4095	.4037	.4087	3	6604.	4 08 7	00004	1001	4073	4 073	.4065	• •	• 4 055	.4047	.4039	.4031
	RELAT IVE	•		-		•	6		18.900	÷	÷	ġ.	Ġ,	ö	٠,	ö,	ġ,	÷.	ō,	ċ	Ġ	ċ			RES STATIC	5.87	6	5.90	5.92	5.94	5,97	96	c,	*	5	16.097	7 5	1:	2 5	23	26	29	33	36	39
	RELATIVE V-LOCITY		•	•	•				603.07	•	•	٠	٠	•	٠	•	٠	•	•	•	٠	•			PRESSUR TOTAL	7.778	7.797	7.825	7.856	7.885	7.913	7.94	7.96	7.99	5.02	13.055	3.03	11.	3.16	3,13	8.21	3.24	3.27	5	33
	RELATIVE MACH NO		•	Ţ	50	:	. ~	53	.5383	ič	10	33	. 5502	3	. 55 91	. 27 15	57	• 55 90	. 57 12	. 5737	. 57 61	.5781			UZES STATIC	30.204	333	30.502	30,701	30.919	31.145	31.385	31.527	31.892	32.414	532,938	3.5.460	24.00	35.646	36.995	38.525	39.713	40.795	41.9	43.2
	BLADE SPEED	90	; %	1	2	3	20.2	73	6.35.7	93	8	8	15	23	31	33	3	22	7	7	8	38			-TEMPERATI OTAL	525	7.716	110	3.265	8.532	3.784	9.034	9.288	3.271	6.098	0.629	1.159	760-1	3.098	638	6.278	7.350	3.390	9.518	0.790
	1.05S 30c F?	3	<b>,</b> c	, c	2		. =	2	. 00 11	5	0 0	5	5	5	2	m	02	0	S	5	ŝ	디	z	l	10	,, 1	11	ייר	10	10	10	'n	in in	•	iv.	72 55	in 11	ניי	, u	, 10	, .c.	, IU	10	5	10
	VIATION CID: MCE	700	200	3	200		. `	2		55	. 54	5.	3,5	35	. 29	\$0.	• 72	. 83	٠,	. 13	£.	73	JESCHIPTI		S	,050,	1001 1001	17.7	127	10 m	1 454.	. 464.	2 +64.	3 404.	.404.	454.	7 404		, to to	, tot	404	6	6 463.	4 403.	7
	ANGL IN		•				``	57.3	57.	57 7	57.3	53.0	53.3	58.2	>:	٠.۴	7•6	3.0°	54.3	53.3	50.7	51.309	04 F1c C)		-VELOCITI TANGE	27.0.	2 40	2010	4 4 4	9.00	253	253.	26 3.	209.	27.1.	3 273.8	275		4 C	30.0	40 S	310	315	321.	323
<i>a</i> 1	A X	ç			115	, 5	. 1	1	32	51 -	13	75 -	- *	l Mt	- 01	- 56	- 10	- 26	- 36	- 52	- 24	- 50	5.	)	4ERIO	-	: ~	;	•	; ;			ċ		ŝ	375.43	'n,	i.	• 6	•	•	;	6		ؤ
TAC 34	ANGLE		• ^	,	ۍ ۲	١u	٠.	e ic	- 7	- 10	30	~	~	8	30	••	-	m	•	Š	9	m	NO I		Sc	ć	J 1	n -	2 6	2 4	10	8	124	.13	601	41	č.	0.0	# N		r C	2 .d	2.5	90	61
36.405	3LADE-	Č	•	,			, ה ה	7	.93	.1.	*	10.	5	• 96	• 16	. 35	.53	.72	• 92	.13	35	3.503	STAT	1	10 AA	~	? *	? 1	·	۱,	9		۲.	•	e.	9.00	٠,	٠, ١	,,	٠,	• 4	'n	ŝ	`	•
	LOCAT -ION		•	•	•	٠	•	•	•	•	•	٠ -	٠	·			•	٠	•	- 61	•	- 12			STREAM -LINE	•	- n	u ~	n 4	·	۰ ۵	~	-	σ		# (									

_	
4	
-	į
်	
C	
u	
O	
•	
_	
E.	

POLYTROPIC	1.0013	1.000	1999	. 3333	. 9989	1986	2000	1366		6996	7806	9719	.280	1666		-616.		1/68.	91490	1629	. 1967			<b>1</b>	98		#	13	15	91			2.	2		<b>8</b> 2			919		813		#
ISENTROPIC PPFICIENCY	10	1.0005	2666	****	6966	2200			2166	1926		.9711	9795	9245	1000		6608	9268	η.	5				RE WEIGHT	=	#.	•				:	4 .0828	j			•				Ţ	•		•
DELTA T	986	• 056	960.	, en.	950	0 0 0	660.	. 059	. 050	. 061	-296	. 163	***	1000		. 009	2/0.		- 877	• 620	. 881		0 - 011 A C 00 -	CURVATURE	-1.883	•	•	•	-4.22	15.531		-21.114	71.22	76.105	28.43			13.40			1.67	Š	916564.76
PRESSURE RATIO"		•	•	•		•	•	•	•	1.227	.•	1.230	٠	•	•	•	19291	•	1.244	1.246	1.248		7	SLOPE	16.	1.	13.	11.	10.	ė,	: 2		'n	<b>~</b>	•	•	i'	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓			·-	9	ę
RELATIVE HPERATURE	553.342	24.006	54.569	55.333	20.00	56.575	57.353	58.042	58.741	59.453	50.180	60.325	61.586	074.20	92.50	411.40	266.19	65.910	66.353	67.855	68.390		•	* *	4 40.7	2 41.2	6 41.	3 41.7	3 41.9	2,5		61.8	2	0 42.	1 42.4	5 42.6	42.7	,	* *	6.69	8	50.1	51.6
RELATIVE RIPRESSURE TE	8.451	8.526	8.602	8.679	6.756	8.835	8.915	8.996	9.077	9.128	9.181	9.235	162 6	9.550	9.565	9.506	842.6	9.254	9.273	9.286	9.285		1	IC NO	.0	•52	.52	.51	.51	2				.50	.58	21 .49	6 a .	*	•	593. 595			688 .4795
RELATIVE RE Velocity PR	•	5.0	910	.36	:	1 72.9	*0	87 1	+	55	1 : 22	T :	37	200	1 ·	24.	1 24	9	64.31	. 46	9.54 1		6	STAT	8 15.	16.	1 16.	16.	16.	. 16.	•	16,	93 16.	46 16.	9 16.	3 16.5	16.5	19:	10.	12.	86 16.	16.	27 16.
4.4	85 531	39	87	32	75 553	17	53	<del>1</del> 9	39	55	•	63 69						£. €.	25.	03	73 55		,		21 19.	15 19.	19.	57 19.	37 19.	11 19.		19.	19.	19.	51 19.	55 19.	60 19.	61 12	6.6	12 13.4	93 19.4	51	• •
BLAGE RELATIVE SPEED MACH NO	50.3 .46	. 47	~*·	. 4	# ·	£ .	£4.	67.	. 50	. 50	•	.50	•	•	•	•	•	. 43	64.	64.	8** 6*2			STATE STATE	531	532	533.3	534.8	534.3	534.9	1000	535.7	536.3	536.9	537.3	537.8	N. 60 K. 6	539.3	1.146	566.6	545	547.1	548.8
OSS BL	013 6	005 6	9 25 6	007	010	0 12	015 6	017 6	023 6	2 260	167 . 7	233 7	2 662	362 7	7 905	787	690	215 7	352 7	2 664	667 7	)		TOTAL	561.67	561.92	562.16	552.38	562.58	552.762	- NOC	2000	363.41	563.74	564.07	164.42	7.40	65.5	1.0	750.00 15	70.9	72.2	3.9
ATION L	. 040 -	.917	. 795	. 678	. 570 . 0	• 475	. 395	. 332	. 286 .	. 259	. 250	. 260	. 288	. 336	. 412	. 525	. 691	. 923	. 216 .	. 562	. 958	NC11d1b3S		TOTAL																557.53			553.4+
FLOW DEVIJ NGLE INCI	- 719·	- 010	. 343	. 575		. 441	- 678.	- 842.	- 513	- 906.	. 384 -	- 2773	-170	- 164.	- 716	- 564.	- 330 -	- 194.	- 140.	- ġċa•	.334 -	FIELD OF		TANSEA	9.	9.6	÷	×	å	٠.	٠,	: :			*	ń	ú.	å.	ů,	* *	: 6	: 2	434.15
A RCL	952 -45	9+- ++9	593 ~46	483 -46	74- 76	827 -47	368 -47	815 -48	197 -49	F+- 925	64 120	64- 065	241 -50	069	16- 855	23 -51	.789 -51	*435 -52	.176 -53	,732 -53	.083 -54	A FLOW	;	MERIO	457.07	ó	;	43 3, 34	436.47	433.99	43.24.13	43.1.00	426.71	423.79	421.29	41 9. 06	417.05	+11.06	٠,	36 2 - 20	; ;	: .	34 3. 23
BLAUE-ANGLE: ECTION LEAP	- 11	3.093	3.5+8 -	- 166.	.474 -5	** 365 -*	4- 254.	916 -3	347 -3	2- 052	134 -2	1- 215	688 -1	- 555	205	958	.239.	.538 1	.826	.104 2	.0	STATION		KAUIUS	674.	527	577	. 628	.680	. 733	200	? 6	957	015	. 076	.138	- 202	. 267	335		556		6. 7359
LOCAT S	7	•		•	5.	ì						12 21	•	•		•	•	ĭ	19 -	î	21 -5			SIREAN -LINE	+1	~	מיו	*	S	•	٠.	6 0						s.					2.5

⋖
-
4
C
IJ
0
⋖
_

EFFICIENCY—	fronts -	1:111	9888	1666	9868	9984	2966	- 3975	.9891	0196	97.69	49864	4367	9486	21/4.	. 8526	. 8358	. 6160	-1986.
EFFICIENCY E	2300-1		8666	4000	.9987	1266	.9981	.9973	.9887	2006	11.50	7450	-9367	, 6	1999	.6468		.6186	162
ON T	. 083	.063	100	202	. 0.85	. 185	. 085	. 086	.086	1900	900			. 093	260	660 •	. 101.	.103	-107
KATIO	•	32	1.327	• . •	1.332	1.333	1.333	1.334	1.333	1.333	1.332	1.336		1.328	1.327	1.326	1.326	1.327	1.329
TEMPERATURE.	446.4	5.+16	555.363	K. 377	7.453	7.399	8.359	9.133	9.724	0.335	4.165	1.017	200	3.717	1.503 ··	5.339	5.22U	7.151	8.141
PRESSURE TEN	149.		18.746 55	:					1	)					- 626	246	. 923	.831	841
	18	_	_,			٨.		Φ.	.0			<b>-</b> -		2.5	18	16	69 18	23 18	
. VELOCITY	531.	2	525.30		3	2	530.	* # P	•	535	•	•	•			•			
NACA AC	. 4577	0494.	.4617		. 4615	. 45 32	. 4657	. 4585	. +585	1694	10 / 4.	\$1 /*·	46.99	i i	3		. t.	•	+504
C33dS .	665	699	674.0	2 4 4		692	697	7 02		713	718		7 45	741	747	7.54	761	769	777
: 30EF=	0	9	.0002	9 (·	90	8	0	8	5	20	2 6	2 5	5 4	2	4	· vo	13	5	N
CHCIDENCE	•	í	-4.787	; ;		115	-4.011		•		•	•	•	; ;	,	•	'n	ç	-5.835
ANGLE I	65	.60	-32.241		26	ŝ	7.	38	MC.	3	2 5	9 0	•		'n	-+2.372	.21	97	• 96
LEAN	6.270	5.433	-5.362	4 L T . K	3.133	2.402	1.6.7	7.7.0	305	592	3.	) d 1	7	66.0	4.20	7.51	0.05	220	m
SECTION	25 . 42	25.+0	-27.454	74.27	30.12	30.92	31.70	45.44	53.14	33.30	9 to 10 to 1	54.47 54.45	44.44	35.42	35.39	37.31	37.66	.91	35.13
-ION			m .													19		•	-

					i		•		,		1			ļ		-		:		;	:	i	3		:	ı		1		:	1		i		1	- 1	1	i		İ	
POLVTROPIC EFFICIENCY		ZIANTI	1.0005	2666	5666	5966.	9966	2000	1.66	9416	9788	9696	1006	9510	. 3300	8936	. 6325	4210	. 7908	6994					: :																
ISENTROPIC EFFICIENCY:	•	1.0015		2666	5666.	6066	9866	9000	9470	.9873	.9778	<b>.9684</b>	9886	1040	. 8873		.8252	2409	.7817	.7565		SPECIFICATIONS NETCHT	,	200				1		2198										;	
DELTA TO	į	*	*60	<b>160</b>	* SO * :	* 1	2.00	200	045	160.	. 198	660 •	. 699	7.60	101.	. 901	.110	.112	.114	.117		RADIUS OF		9.349	11.000	14.09	22.677	- 27.24	31.02	32.90	30	26.86	23.51	20.479	-17.882	15.675	13.67	11.740	7.846	5.56	3.053
PRESSURE Ratio		1.371	1.372	1.372	1.57.5	1.57.5	1.373	1.375	1.376	1.377	1.376	1.379	1.376	1.573	1.265	. 1.360	1.357	1.354	1.351	1.347		LES:	2000	7.62	7.78	16-7	99.99	6-12	5.58	50.03		3.35	2.77-	2.17	1.55	. 87	٠	1001	-3.15	-4.57	-6.18
RELAT IVE TEMPERATURE		25.5.5	170.00	12.00	20.00	0111	20.40	30.40	644.6	9.973	it.5 11	1.063	561.530	****	01007	16.1.45	56.983	5.564	96+.99	17.397		*** *** ANGLE	101	4.5	•	• • • • •	42.62	42.	11.	į	ļ		ł		:			47.15		•	54.
RELATIVE REPRESSURE TEN			2	125	2 (	726	200	9 6	155	160	. 291	175	103	25.	123	188	150	584	505	96		HACK.	2	.552	. 0.000 to	•		:			i		:		ŧ	.5605	i	. 545	• •	225	.513
	•		P			3 :	1 7	1 +		19	51	19	5 C	2 :	7 4	81	18	18	13	-		SURESUL	2	16.379	16.365	10.545	15,295	16.274	16.258	10.246	626:34 <u>.</u>	16.230	165-231	16.237	- 16.247	16.265	162-91	16.329	16.435	16.496	16.548
RELATIVE VELOCITY		•	•	•		•	•	• •	•	•	•	•	517.23	•	•					•		TOTAL	, 5	20.154	20-161	20.167	20.179	20.185	20.196	20.206	- 110 · 02	20.258	20.250	20.218	20.176	20.124	\$0.00	19.986	19.903	19.857	19.803
RELATIVE MAC4 40	:	かのます。	C5 44 •	0 t t t	10 **	044.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	6 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1 1	.4563	.4044	. 45 35	. 4525	. 4523	1104.	. 4400	32.03.	. 3985	3900	. 3794	6465.		CAREST	2	534.882	534.789	554.616	534.208	534.029	533,895	533.799	3000 CO	534.611	525.085	535.616	536.203	537.444	539:674	542.535	546.235	548.309	550.555
BLADE SPEFJ	•	21.0	6/20	6/9.5	0000	6000	2.269	6.007	7.05.4	709.9	714.5	719.2	724.0	4.827	7.04.0	6.447	750.9	757.3	764.0	771.1		-TEMPERAT:	,	7.379	7.474	7.550	7.700	7.762	7.868	7.966		9.395						74.527			
1.08S			•	2	3 3	Э (	9 6	9 6	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜	20	20	03	.0498	2 6	9 7	11:	202	22	. 3	27	NCIL		•		10 1	n (		ייח -	'n	01.5	, W	, ic	. IN	·n		w (	in i	n v	יטי	. 10	in,
DEVIATION INCIDENCE	,	-15.101	;	÷ :	-10.00+	÷ ;	<u>.</u> .	2 .	5	: :	11.	11.	-11.836	2	10	, ,	14.	15	10.	14.	D DESCRIPTI	FIESTE	2	15	20	, ,	16	<b>60</b>	7	e .	- ·	2 2	0.00	92	55.	76	, po	66 626 05	3 2	. <del></del>	23
MEL FLOW	•	٠ تر	Öι	٠,	<u>ءِ</u> ا	٠.	3 0		,	۲.,	10	ň	-34.192	Ţ,	ŗ	2 10	`	39.9	M . 1	3.5	FLOW FIELD	TO TANE	•	۲۵	::'	<b>;</b> :	13	2:0	<b>5</b> 1	ಸ :	<b>†</b> 4	) <b>4</b>	# # # # # # # # # # # # # # # # # # #	35	20	īč.	7	63 45	: 2	54 47	92 482
INGLES	;	2.399	6+3	256.7	5.249	5,573	3.831	175	4.557	200	4.811	4.893	5,6.4	196.4		2000	4.457	4.136	3.8.27	3.617	<b>#</b> !	SI		6 449.							:					9	<b>*</b> (	555 425	- F	55	ħ
SECTION	;	-11.516	2.94	90	12.61	D\$ • 50	7.33	# 1 7 ° C 1 =	13.482	20.576	21.515	-21.894	13 -22.356	796.22	22.554	75:153	24.471	24.727	24.897	.24.964	STATION	· RADIUS		S.	•	ОΓ		• 60	-	ው ር	,,	, 0	, 44	7	N	8	,	8.363	7	·	•
LOCAT								. 1	ι • σ	10,	- 11	12 -	21	<u>,</u>	4	27	18		े । । १८		š	STREAM	-	#	<b>~</b> 1			ص د		<b>e</b> 0 (	,	11	15	13	71	-	91. 	<b>~</b> F	3 6	50	21

DESCRIPTION	
FLOW FIELD O	
STATION 11	:

,我们是是一个人,我们就是一个人,我们就是一个人,我们是一个人,我们是一个人,我们是一个人,我们是一个人,我们是一个人,我们也是一个人,我们也是一个人,我们也会 我们是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们也是一个人,我们

•	. :	٠ •
!		POLYTROPIC EFFICIENCY 1.0012 1.0005 9993 9993 9993 9996 9980 9980 9980 9980 9980 9880 9880
SPECIFIC WEIGHT		1SENTROPIC FFICIENCY E 1.00055
RADIUS OF CURVATURE	-26.367 -21.9887 -17.44687 -16.3446 -16.3446 -16.3446 -17.9689 -21.0442 -21	00 T EFF 00 T EFF 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SLOPE	2000 2000 2000 2000 2000 2000 2000 200	PRESSURE RATIO 1.372 1.372 1.372 1.373 1.376 1.3
HHIRL S	709	RELATIVE THPERATURE 567.379 567.760 567.760 567.760 567.760 568.395 568.395 568.395 568.395 570.395 570.391 570.391 570.391 572.761 572.761
S MACH	30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RELATIVE RESOLVE TO 154 CO. 154 CO. 154 CO. 155 CO. 156 CO. 156 CO. 173 CO. 174 CO. 175 CO. 17
PRESSURE TOTAL ST	20.154 20.154 20.151 20.173 20.173 20.173 20.273 20	QELATIVE VELOCITY 649.22 669.07 710.63 711.06 710 710 710 710 710 710 710 710 710 710
TURES	50.00000000000000000000000000000000000	RELATIVE MAC-1 VO 57 09 53 95 60 61 61 93 65 19 65 19 65 10 65 10 65 10 65 10 65 11 65 11
-TEMPERAT OTAL	667.373 667.373 667.775 667.775 667.775 667.776 667.776 667.776 667.776 667.776 667.776 677.726 77	A P P P P P P P P P P P P P P P P P P P
T 4. T		N. 1
CT 83-1-10	3.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6	05.VIATION INCIDENCE -5.32 -7.342 -9.737 -9.729 -9.
VELOCIFI RIC TANGE	7.8.	AL AM ST. COM
01 JS	149 277 277 277 277 277 277 277 27	100 100 100 100 100 100 100 100 100 100
Ψ Y		
STREA!		100 100 100 100 100 100 100 100 100 100

STATION 11 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.369 ISEN, EFF.= .926 PO.Y. EFF.= .929 DELTA T ON T \* .101

						<b>1</b> 0			2 11			-	~					2	-			ISENTROPIC POLYTROPIC	EFFICIENCY	9866	4686	1000	- 9854	. 9833	186.	9785	9656	- 6666	4946	9399	• 5350 • 5454	.8792	*****	. 8232	**09.	340/	21919
	SPECIFIC E HEIGHT	#0.40 T	i	. 6716	1			١	94.45	1		!	2928-				.8735	1	1			SENTROPIC	FFICIENCY	2865	9889	9869	98486	.9825	6646	.9773	0496	.9539	9446	- :- 90000 · ·		8739	. 8366	.6155	S i	94.2.	.7510
	CURVATORE	- 4.644 - 4.644	-3.736	-3.862	860.h-	-4.318	809° 21	-5.016		14.9-	-7.753	-9.113	-11.120	-14.588	-23.242	-97.303	36.143	14.175			ı	DELTA T	⊢ NO	. 460 .	460.	100	*60	. 095	560	- 1995	.040	960	660•	660.		104	108	.110	. 112	• 114	.117
	SLOPE	5.21			٠		,			,				•		:			75			PRESSURE	RATIO		1.367				•	•	1.367		•	•	1.554		1.355	•	•	1.348	•
	HATRL	32.81																				ELAFIVE	MPEZATURE	67.379	567.474	67 525	67.75	67.762	67.368	67.366	60.149	69.395	69.909	70.085	70.256	72.761	74.527	75.726	76.796	066.77	79.386
	I MACH	26 .7891								777.						_	N.	<b>.</b>	~ 1	•		RELATIVE R	<b>E</b>	980	060	200	, M	087	084	080	100	104	104	078	250	120	911	876	9.844	9.806	9.762
	-PRESSURES	13.32		7	3 13	7 13.	4 13	<b>.</b>		7 4	· · ·	14.	2 14.	1 14.	7 14.	1.4.	ய	15.	9 :	<b>1</b> 2.44 3			VELOCITY PRE		866.59 20,														*	-	++
i	TOTAL	20.08			20.	20.0	20.0	20.	0 0	<b>u</b> n	25	20.	20.	20.	19.	19.	13	6.	→ ·	4.7																					
	ATURES STATIC	504.860		1 7 7 7	509.491	10.6	511.864	12.9		12.6	17.5	18.5	519.330	20.6	22.8	25.1	26.3	27.2	528.081	•			E0 48C4 40	•	.0 .7520	•	•		•	•	•	•	•	٠	•	• •	•	. •	.68	•	. 69
	TEMPEPATURE TOTAL STA	567.379	7	7	67.7	67.7	67.8	9.70	68.0	000	6.69	70.0	70.2	70.9	72.7	74.6	75.7	76.7	577.990	?		BLA	FF SPEE	6	<u>67</u> 0.	-	<b>5</b> C	•	0	<b>.</b>	<b>5</b> C		•	•	<i>o</i> (	<b>&gt;</b>			6	0	<b>e</b>
	T0TAL	873.54		•		•	•		•					•	•	•	•	•	•	•		2	DENCE 30E	3 .01		5		.02	20 7	20.	20.		8 .03	20. 7	× 0.2	20.		10.	3 .01	2 .01	10. 6
	OCITIES	473.30	9 0	7.1.0	90	37.1	31.2	25.6	20.5	\$ C	M .0	7.7	÷	. 3	٠.	7.1	2.3	1:5		•		IAEG PO	I INCI	•		•	•	• •	•	•	••	•	<b>:</b>	<u>,</u>	<b>.</b> .	<b>:</b> -	: :	<b>.</b>	÷	+	-1
	YERIO	734.20	725. 73	721.34	716.54	710.99	105.47	700-21	595.04	536.66	582,53	580.69	67 b. 02	671.73	667.14	56 2. 15	56.735	553.38	64.00	•	⊲ į	3 REL	7.	47 32.	32.	32.	32.	75 31.	+8 31.	50 31.	34 51	31 30	62 30	12 30.	57	35 31.	32	32.	25 32•	92 33.	25 34.
	2401US	7.7150	( : O 6	2440	8726	.9113	. 9512	6066.	. 6312	61.13	1551	1970	.2438	. 2947	. 3293	. 3749	. 4210	. 4637	. 51 39	20.00	9LADE DAT	ADE-ANGL	CTION LEA	959 -24.	.750 -23.3	475 -21.	155 -19.	658 -14.	484 -12.	326 -10.	165 -3.	912 -3.	863 -1.	373	931 6.	206	536 11.	175 15.	774 20.	573 24.	478 28.
	STREAY -LINE	0	۰, ۱	0 1	• W	م ،	7	•	σ (	D •	1 2	. F.	7	15	16	17	16	19	20	10		AT 3	-ION SEC	31	2 31.	3:	7 6	30	30	30		0 0		67	29		2	31			33

原列は何名の大学では、日本では、日本では、「Andertain Andertain A

,这种种种,我们是一个人,我们是一个人,我们是一个人,我们是一个人,我们是一个人,我们也不是一个人,我们是一个人,我们是一个人,我们是一个人,我们是一个人,我们

5			•						. 10	2	<b>~</b>		<b>S</b>		-	<u>.</u> #						EFFICIENCY	*886*	.9781	- 97.98	-9730	11/6.	1298	.9581	- 9943	.9431	1256-	.9230	9167	6668	.8668	. \$326	. 6135	. 7960	2///0
OF SPECIFIC	7771 36			1			89 . 9842			1				•	•	10/9° 91		ì	200			ISENTROPIC - EFFICIENCY	.9795	.9771	1976	\$2.5¢	9898	9814	.9563		9446	- 9291	.9196	10 · 0 ·	8995	.8682	-8528·	. 6055	.7873	7,07
RABIUS	-5.136	1.4	-7.823	-4.163	-10.867	-12.7	-15.0	-17.6	-20-410	-23.885	-25.4	-27.37	-28.589	-29.3	-30.5	-35.51E		7.000-	2 6	:		DELTA T	#60.	<b>560</b>	*60 ·	# CO .		860.	660	.195	.097		660		101	+01•	- 106 -	.110	211.	. 117
SLOPE	-2.23	20000	-2.48	27: 27	130	-2.28	-2.09	-1.86	-1.59	-1.29	98	67	36	06	22.	•		9 0		†	1	PRESSURE RATIO	1.362	1.362	1,362	1.362	1.351	- 5 SE	1.358	1.357	1.357	1.358	1.357	1.35	1,355	1.352	1.350	1.348	•	1004
WHIRE	17.58	•							17.38	17.43	17.47	_	_	17.56	17.65	17.00	00.01	6	10.01			r IVE RATURE	67:379	\$ \cdot \cdo	• 560	50.35	567.700		.366	.399	1.748	.395	906.	240	578,391	.761	15527	.726	.795	06.5°
MACH	.5.325	. U T T U	400	. 2 44 2	5818	5734	5662	ľ	5572	.5546	.5525	.5506	• 5496	1645.	•5474	0040	10400	7727	# 7 7 7 4 F F F F F	•		-	•														٠			55 577 727 E70
TA TIC	15.298		٠,	15.795	5.895	5.693	16.056	16.134	16.160	16:193	16.217	16.231	16.236	N	15.218	15.193	•	•	9 C	•		RELATIVE PRESSURE		ċ	•	• •	200.02	19.954		6	ė	ó,	19.948	'n	19,916	6	Ġ	9.	9.1	19.75
PRESSURES TOTAL STATE	20.021	0 10	100		1 4	, «S	3,951	200	9 4		<b>*</b>	939	626	6	19.876	7 0		7 2 2 2	n r			RELATIVE VELOCITY	714.43	8	691.84	681.20	671.06	652.21	644.51	638.72	635.28	632.85	630.89	5000 93	627.73	626.97	627.13	29.5	33.1	6466.45 646.64
URES STATIC	525.573	727.004 528.258	5000	530.810	531,974	533.033	000 CC	536.450	535,639	536.539	537 • 315	537.689	537.972	538.725	540.575	7740740	110.040	106.646	744.017			RELATIVE MACH VO	. 9229	. 5215	.6110	• 60 08	5912	57.44	5662	. 56 07	.5572	. 5546	. 55.25	• 55 US	114 40	*24%	. 54 65	9460	. 5511	• 55 54 • 6 6 6 6
-TEMPERATURE	379	* 4	200	200	762	966	996	900	7 63 7		606	.085	• 260	•991	.761	770	100	000	20 E			BLADE SPEED	•	•	0.0	0.0				•	0.0	0.0	o .	900		0	•	•	0.0	•
AL 10	55	00 to	100	100	1		11.0	72 15	23 55	35 56	83 55	99 57	9+ 57	73 57	75 76	13 57	70 07	7.0	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			COEFF		.0337	0	.0357	0	> =	, -	_	0	0	0 (	⇒ c	68.40		0	0	0	0 6
ES	714.	- 4		3.5	3 2	 		•	100	7 63	5 63	2 628	29 /	9 627	626	<b>.</b>	200	6 J	i i			EVIATION ACIDENCE	•	•	•	•	•	•			•	•	•	•	1,633			•	•	•
/eLOCITI TANGE	215.3		9 (	,	7	5 6	, ,		6	9.9	83.	83.	3	¥.3.	6.		ה ה ה	ה ה				FLOW DEN	.53	, 10	.51	16	. 52	• •	3.7	33	• 38		7	7 '	7.550		. 33	• 35	.33	
YERIO	631.05	• o	• 0	ď	; ;	: .	: :	d		503.79	÷	å	÷	÷	٠,	٠,		<b>.</b>	•	4 1		ES REL	414 1	919	355 1	71.	1 1 1 .	141	223	245 1	311 1	475 1	7 92 1	2061	1 75 1	35 2	116 1	2+8 1	510 1	יים מיני מיני
240103	7.7230	•			, ,				•	7	7	7	~		~ '	7	. ·	•	•	9. 0≘ 0A		13E-ANGL FION LE	.234 -9.	.183 -B.	155 -8.	130 -7.	,107 -6.	1 N N N N N N N N N N N N N N N N N N N	346	791 -3	.787 -2.	.804 -1.	.814	0116		.967	129 3	.362 **	.715 5.	.100
STREAN -LINE	₩.	<b>y</b> ~	, ,	·	ء. ،	, r	. ~															LOCAT 3L	15	15	12	9	€ .	0 II	1	151	15	15	10.1	61	1 10	10	15	15	16	17

A THE STATE OF THE PROPERTY OF

<u> Content de la content de la </u>

.

FLOW FIELD DESCRIPTION	
STATION 1+	* * * * * * * * * * * * * * * * * * * *

			!		:		:					;				•	:			POLYTROPIC		. 9665	- 9636	.9597	. 9961	.9584	0546		.9200		- 6992	250	.8956	6531		1408.	.7878	.7703	125
SPECIFIC WETGHT	60000 e	90	.0837	• •		•	.0836	•			.8832					. 6191				ISENTROPIC PO			9614	9579	2466					i			.8912			7958		.7607	
RADIUS OF CURVATURE	16.241	18.555	20.011	23,775	26.240	29.242	32.891	37.255	195:29	33.00	65,212	81.827	106.540	150.044	244.958		-610.607			DELTA T IS		760	+60	<b>*60 •</b>	*60 •	• 095	560	1000	. 097	260.	660•	660	660	101	. **	110	-112-	•114	7
LES SLOPE	-4.29	-3.83	-3.59	-34.08	-2.80	-2.50	-2.19	-1.87	-1.54	22.1	61	35	09	• 15	04.	.63	1.05	;		PRESSURE	. 8 34		1.356		1.355	•	16241			•	1.347	٠.	•	10340	•	1.343		1.341	.33
ANGLES	6.18 6.05	ķ			ķ	ŝ	نگ ا				'n	ŝ	ທໍ	<b>i</b> n 1	<b>ب</b> ر و	เก๋ง		i		RELATIVE	'	7-474	7.560	7.535	7.700	7.762	7.555	- Bet-9	8.7.8	9 - 3 9 5	606.6	0.765	0.260	1.391 2.761		575.726	5.796	7.390	9.386
MACH	4,825	•	•	• •	•	•	•	•		• •	· •	3.	3.	4	<b>.</b>	<b>5</b> -	00000	,		RELATIVE REI	Y	940	934	922	7116	378			19.798 561			i				19.737 57	:		683 57
PRESSURES OTAL STATIC	17.022	17.033	17.039	17.049	17,052	17.055	17.057	17.058	17,056	17.047	17.038	02	17.014	8	86	96 1	16, 935	}		4. 4	•	19,	19	19.	19	<b>1</b>	<b>.</b> .	•	_	"	<b>G</b>		30 19.	- •	•	• • •	5	~	1 19.
PRES TOTAL	13,958		13,922	19.878	19.849	19.818	19.801	o,	19.794	19.799	19.807	19,813	13.786	2	2	25				RELATIVE	4 5 2		550.5		547.2	544.0	541.5	535.7	536.7			٠.	540.3				٠.	•	244
JRES STATIC	542.293 542.519	ţ	542,953	) M	Ŋ				545.794								555.145	!		RELATIVE	, 'ĭ,	•	76.74	. 47.83	• 4765	• 47 39	21.74°	16678	4657	. 4665	. 4067	-4878	. 4693	10 45 ·	0000	. 46 87	'n	• 46 90	. 46.83
-TEMPERAT OTAL	67.379	67.560	567.635	07.762	57.868	366	66	0	395	3.5	60	161	7	527	56	.65	3 6 6	•		BLADE			9 0	0.0	0.0	0.0			0.0	0.0	0.0	0.0	0.0				0.0	0.0	0.0
OTAL F	3.43 5	0.54	8.90	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1.35	8.+3	6.73	<b>6.7</b> +	5.30	60.0	0.33	2.23	2.10	1.33	2.2.	2,95	3.32 F. 21	·		N L355		50.		• 05	• 05	• 06	.0.		.09	.09	• 0 •	. 03	.0.	9 6		1840.	. 04	*0	• 03
- N	9.61 55 3.23 55	97 55	3 K	07 54	2+ 54	49 53	90 53	5.5	52 53	55 53	75 24	05 54	30 54	79 54	66	10 54	*6 17 74 24			DEVIATION	2.21	2,223	2.241	2.274	2.320	2.37+	454°2	2,561	2,621	2.673	2,715	2.741	2.743	2,715	\$0.00 \$0.00	2.694	2.710	2,750	2.818
VELOCITI	27 5	59 5	E 1	 	73	35 5	23	54 2	יי היי	17 5	2	5 11	57 5	ب د ما	. S.	in .	יני פיני			ScL FLOW		50.0		4,0	• 76	2.	\$ 0 0	5.5	.52		64.	6.	. tu	֓֞֜֝֓֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֡֓֓֓֓֡֓֓֡֓֡֓֡֓֡֓	) W	6.679	.32	3	• 32
H A	20 550.	3,0	2 2	٠.	9 53	+ 53	<b>.</b>	53	1 53	3 2	2	53	53	53	50	<b>1</b> 0	4 6		4 1	NGLES R			ຳຫ	- ∞	^	ച	N 4	١,				4-1	-140			-,635	- 836	თ (	-1.055
+ RADIUS	7.672	~	`."			5	٠,		•	: :	. ~	5	~	m,	•	. u	, r	•	10476	3LADE-A	3,955	P 60	69	.57	*	32	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֓֡֓֓֡֓֡	6	9	.83	.78	2	2;	: ?		2.986	11	53	Š
STREA'	- ~	m	.T V	ص ۱	~	10								₩,		H (	2 5			LOCAT		۰,	, m	3	Ŋ	و م	- 1	• •	1	11	+4	î.	<b>3</b> 1		? ?	: 2	1.61	ຂ	12

TO SERVICE THE PROPERTY OF THE

:								;					•					:	POL/TROPIC Efficiensy	- 1666.	6756	2056	.9457	. 0146	*****	.3161	9006	. 8968	10 P	. 8757	.6770	.8689	. 8397	.8110	7467	7636	7457	-4 1
SPECIFIC . WEIGHT	.0057	. 8855	0853	.0852	10021	0 4 50 50 50 50 50 50 50 50 50 50 50 50 50	.0847	9780.	.0845	0 to 0	n				9000	4680	.0832	•	SENTROPIC !		•9530	.9481	*8 *6 *	- 8888.	0000	• 9¢15	96063	.8925	6745		.8718	.8633	.6330	18000	. (850 7784	26.26	.7351	
RADIUS OF SURVATURE	10.624	11.865	13.546	14.671	16.145	24.013	25.165	31.663	43.038	65.	, ,	3,1		-56.454	9 0	-39.825	33		DELTA T IS	<b>500.</b>	760.	760.	<b>760</b> .	760			960.	260.	869	550	660	101.				7110	117	30
LES SLOPE	-1.65 -1.62	-1.57	1.4	-1.36	-1.25	11.12	900	73	- 50	m (	62.			•	3.6	12	. 52		PRESSURE RATIO	.35	• 35	. 35	.35	# i	<b>3</b>	1.346	.33	.33	33		33	34	. 34	.33	555	7 .	1.337	"
ANGLE HHIRL	0.00	•		0.0	0	•		0.0	•		•	•	•	•					LAFIVE PERATURE	m	••	ıŭ.	'n	~ '	٠.	ņŋ		~	m (	י כ		יסי	~	ıŭ,	٠, ١	- 0	7 • 4 4 C	
AA CH		•	• •	•	•	•	•	•	•	•	•	•	•	•	• (		• •		LATIVE RELIESSURE TEMPE	31	23	53	3.6	215	7:		0.0	20	모!	~ 6		08	46	30	o a	, J	579	. 85 3
SURES STATIC	17.588 17.571																		& g.	19.	19.	19.	19.	13,	6	91.0	13	19	Ç.	5.0	19	19.	19.	19.	61	5.	13.	EFF.
TOTAL	19.891	19.853	19,812	9.77	13.726	ָ ה ה ה	9.65	<b>3.6</b> 4	19.63/	13.000	13.684	13.768	1000	17,036	1 3,500	13.651	19.644		RELATIVE VELOCITY	1.8.1	408.2	+88+2	483.0	487.5	485.0	482.58	478.0	478.3	479.5	1.6/4	484	487.6	87	8	10.00	• •	467.470	13
1JRES	t. L.	and a	9 00	8	3:	ב ב	5	20	5	5.	ζ:	2:	ი I	C 1	2,0	. מ	3		RELATIVE MAGH 10	. 42 34	• 42 34	. 42 34	• +2 32	• +227	• 42 05	0817	. 4141	7	• +1 40	7 3	4103	?	3	<b>-4</b> .	.4174	н,	4150	;
TEMPERATU	67.379 57.474	~ 1	: .:	~	ĸ,	٠	œ	Ġ	ď	ċ	ġ,		ů	• u		۰,			BLADE SPEED	0	0	0	0	0	۰.	¢. c		0	Φ,	0	<b>-</b>	. 0	0	0	- (	<b>-</b> (		2 .18838
A	23.	21	. יי	.03	33	) i	33.0	.53 3	. 11.	•0•	, d / 6	60.	۱ ۸ ۱ د	• •		10	35.		A C035	.0057	۵	~	~	<b>~</b>	ന	T (	•	-	<b>(1)</b>	N .		m	~	'n	۰ ۵	01	. 0463	n
101 V35	0 0 0 0	3.	000	00 +3	£4	200	000	77 60	7 00		90	9 1 7 1 7 1	70	50	מים מים	000	2.0		SEVILATION ENCIDENCE	23	.39	5.5	.73	3.	60	7	56	99	91	26.0		90	.0.	90•	60	71.	4.213	PERF08
ICC 1	<b>ው</b> ነባ	27.				= -	כי							***			S.S.		L FLOA ANG-É	٠،0	ë.	٠3٥	• 00	. 30	5.0	֡֝֞֜֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֜֜֓֓֓֓֡֓֓֓֓֡֓֜֓֓֡֓֡֓֜֜֜֓֡֓֜֜֜֓֡֡֡֡֓֜֜֜֡֓֡֓֜֜֡֡֓֜֜֜֡֡֡֡֡֡		00.	00	900		00.	.00	• 00	9	. ·	0000	334
X X X	ທີ່ໝໍ	\$ 0 \$ 0		+36+	\$ 0 0 1	4 6	0/1	+7 à.	+79.	+9 S	* 1 * 1 * 1	, t		0 1	7	7 14	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		ANGLES RELEAN	.020	.020	0	.017	.015	9	0 0	63.0	0	0	9	? :	+000-		•	•	•	15 D	N 15 I
دل آل ۵٪	7.6403	.721	800	. 953	47.00	0 4 6 0	. 335	.083	. 132	. 182	. 231	782.	,	* * * * * * * * * * * * * * * * * * * *	2 6		607	LA3	3.ADL-AN SECTION	7.23	7.33	7.56	7.73	7.91	3.08		9 10	69.9	3.81	95.	40.4	90.6	9.05	99	90.0	3.16	17.6- 17.73	SI
STREAY	4 0	m.	<b>,</b> w	۰	~ ∘	0 0	10	11	15	M .	<b>⊅</b> (	٠. ا	9 1	\ a	0 0	-	5. 5.		LOCAT									<u>۔</u>	<b>-</b>	~ ~	າງ	· rv	9	7	20 (	ית ית		;

STATION 15 FLOM FIELD JISCEPPIED

SPECIFIC	.0853	.8552	* CO C C C C C C C C C C C C C C C C C C	1600:	.0851		.0849	6490	7+0B.	9466	. 1846	9480.	54845	7400	.0637	.0336	.0834	. 1832		SPECIFIC	· HEIGHT	2680	1550 1070	.0851	.0851	.0850			1986.		.0845	7446 7446	. 6640	. 1642	6880°	.0837	0 .
RADIUS OF CURVATURE	0.000	1065.068	117.854	343.575	303.563	281.811	272,033	271,538	**************************************	324.695	365.829	425.231	511.989	266.332	1275,371	2194.678	5310.909	0.00	t.	RADIUS OF	SURVATURE	-0.00	•			•	•	•		•	000.0	•		•	•	•	
SCOPE	0.00	03		: DT -	11 ::	12	13	-, 13	715	- 11	10	98	07	90.	# M C		0	00.00		ES	RL SLOPE	0.00	00.		, 00	01	01	5	10.	01	- 01	i i	- 01	01	00	00.	20.
ANGLES WHIRL SED	0.00	•	2 6		0	•	•	9	<b>.</b>	•	0	•	e .	- •	? =		00.00	0		ANGL	WHIRL	0.00	•	<b>-</b> -		0	0		9	0	00.00	9 0	90	0	0	0 (	•
MACH NO.	.4347	.4331	4615	5623	**2**	.4207	.4169	• 4146		• • • • • • • • • • • • • • • • • • •	4150	.4172	•419+	54145	.4170	.4150	7	.4137		MACH	0	.4355	4.339	4525	4287	.4250	.4213	4174	4167	.4133	.4130	2614	4195	.4183	.4170	4157	DCT # "
URES STATIC	17.473	17.473	17.473	17.472	17.471	17.471	17.470	17.469	17.469	17.467	17.467	17.466	17.466	17.465	17.465	17.455	17.465	17.465		1.0ES	STATE										17.465						₽
PRESSURES	13,891	9.87			13.771	9.72	9.68	9,65	3.65	19.640	3.66	19.684	19.708	19.694	13.630	13.658	19.651	9.64		SSER	TOTAL	8	8.	0 %	9	7	9.72	4.68	9,65	9.64	19,637	99.0	9.70	9.69	9.68	9.66	6
FURES STATIC	46.3	47.0		17.7	48	48.5	49.0	604	ם. 20.		51.2	51.2	51.7	53.5		57.72	558.933	60.3		-2=2	STATIC	46.	0.1	10.0	47.7	48.0	48.5	L 60 .	なる。これ	50.3	551,223	21.5	51.7	53.5	55.4	556.622	26.5
TEMPERATURE: Total Sta	67.3	67.4	67.5	67.7	67.7	67.8	67.9	68.0	58.7	, o	70.0	70.2	70.9	72.7	74.0	76.7	577.990	79.3		•	TOTAL	57.3	4 r	7.0	67.7	. ^	67.8	ຫຼ	200	. "	69	0.0	40	72.7	74.6	75.7	9.
TOTAL	30.7	σ	97.2	2 6		5.0	=	9.6	8	? ^	, 6	2.4	5.2	· Q ·		2 6	482.53	2.3	CRIPTIO.	1	TOTAL	•	6	ė	9 4	90	36.	<u>څ</u>	, 4 , 4		477.67	80.	ָאָרָ מיני	40	84.	83.	Ň
OCITIES- TANGEN	6	0	0	<b>5</b> 5	9 0	0	0	0	0	<b>5</b> 9	> ē	G	0	Ö	D (	<b>,</b> =	0.00	0	FIELD DES	-	TANGEN	0.00	0	<b>-</b>	2	9	C	9	<b>7</b> C	, 0	00.0	0	<b>5</b> C	0	0	0	
YERIO	00	å	97.	P 0	; ;	48 5, 34	: #	47 8.05	478.03	477, 33	: 6	2	ı,	;		• •	8 2	'n	17 FL34 F		RIO	50 1. 05	å,		د ه		٥	i	, v	: :		48 0. 17	ی ن	3 0	48 4 • 10	'n	82.
RADIUS	. 640	679	.720	10).	967	392	937	+66	. 032	080.	120	230	.280	, 331	. 383	0 0 0	d. 54+9	• 600	STATION	240706	3	. 640	679		0 6	847	.892	.937	* C		8.1298	179	7 4	331	383	• 436	065.
STREAM -LINE		2	m.	<b>.</b> 1	م د	۸ (	• •••		10								20			1 0 E	-LINE	#	<b>%</b>	ю.	ŧ u	ص ۵	~	€ (			15						19

MANCE	1
PERFOR	
3010x	

-	EAH-ANGLES		5:339	2.643	2.932	3.249	5,5/3	3.851	261.4	4.570	4.780	110.4	4.693	. 4.945	4.961	4.930	4.842	4.682	4.457	4.150	3.617			MGLFS	OUTLET	1 4	130	828.				-	.010	- 800.	988.	- 600	. 883	100	7000	- 000	-2115-	018	#21	031
	LEAN-		17.205	16.454	15.443	14.165	12.789	11.460	10.524	204.6	7,725	268.9	6.193	5.657	5.256	40.934	4.593	4.155	5.623	2.482	1.636			LEAN-A	INCET		196 65-	-20./00	-20-ADD	-26.482	-23,117	-19.855	-16.630	-13:253	-9.548	-5:619	-1.501	1.004	- 401-	14.921	21.940	29.369		45.294
•	N-ANGLES		-11.816	-12,945	-14.085	-12.61-	70000	11/0021	10.01	-10.882	-20.576	-21:512-	-21.804	-22.356	-22.867	-23, 334	-23.759	291.92-	-24-4/1	-24.897	-24.964	!	:	ON-ANGLES	DUTLET		662-1-	0000	-7.739	-7.918		•	-8.409				- 4	74C -0-	- 6.863	-9.059	-9.050	-9.086	-9:126	-9.170
ı	SECTION-ANGL	!	-62.667	165.59-	109.29-	- 62 - 20 -	-62 773	-62.820	-62.944	-64.050	-63,180	-63.298	-63.421	-63.545	-63.659	-63.756	-63.545	- 65. 928	204 - 135 - 156 -	-64,329	-64.476	i		SECTION	INLET	•	10.01	17 20E	46.773	46,357	46.035	45.680	45.371	45.092	44.858	269-44	44.023	44.748	44,959	45.130	ŝ	•	62.7	48.826
	OELTA H7U**2	<b>!</b>	.6591	9269.	00404	5 4 2 2 2	2200	+ 02.22 + 6.4 A.R.	6123	.6062	•6064	. 6663	• 6045	. 5985	. 5925	1264.	3400	.0154	. 61 AE	.6203	.6232			DELTA	H/U**2	ē	5	ē	ĕ	5	ĕ	ĕ	0.000.	5	į	5	<u> </u>		ĕ	9	5	8	5	0.000
	REL V RATID		7945	. 7015	75.01	71.5	7447	7373	7315	.7260	. 7144	• 70 38	• 69 +0	. 5848	.6765	0000	1004	. 296.	5555	. 5353	.5103			REL V	RATIO	75.20	7200	7110	• 6965	. 5857	Φ	: 6657	• 65 78	• 6534	1691	1049.	12000	.6699	.6800	.5877	. 6981	.7101	1821.	1757
	DELTA P ON Q		9246		5556	5473	, ,	٠u	ເຫ	.5121	m	.4930	.4830	9225	<b>;</b>	* :		14400	10	398	T.			DELTA	P ON Q		3862		-3	•4372	.4441	.4476	0044	7 .	7 4	7 4	1000	•	.4361	0 + 2 + 0	.4291	-	0 -	*****
	3-D D FACTOR	;		4774	'n	m	5004	72070	• 4133	.4 188	.4319	6247	.4546	C704.	.4713	1000	2746	3460	20	.6255	2			3-0 0	FACTOR	3886	4130	4341	45.07	•4637	•4766	. 4878	9764.	0000	5447	5122	5040	• 4 965	•4880	.4853	6624	7604.	v	v o
	2-D D FACTOR	•	. 45.7.9	v	) <b>~</b>	. ~	ິທ	403	6604*	ú	. 4298	ω.	45.4	2	1 0		50.0		909	. 6281				2-0	CT 0		.4130	-9	• 45 0 5	. 4535	യ	4876	4/64.	מ מ	ů	5122	50	9964•	. 4881	3	1000	ָ בְּיִרְ בְּיִרְ	7 6 7	30.75
	LOSS	,	1,000	6.003	. 0011	. 0015	. 0020	. 0025	.0028	. 00 38	. 0161	2220 •		06 50	1986	1313	1783	. 2023	. 2255	• 5+99	.2779			L 05S	Ö	. 0657	. 0583	• 0709	• 07 + 0	• 0779	.0861	7560.	1025	1175	1231	1245	.1130	. 1011	• 0876	• 0786	0000	9 4	92.0	0000
	A IV EO		14.710	-	3.36	3.46	3.11	2.73	2.53	2.34	. 35	3 (	700		7	. 6	3.51		5.13	5.53				DEVIA	12	7	33.	• 56	.73	Ę.	ກ .	•	7 - W	, ,	31	56.	66.	ċ	90		9 0		1 7	7
	INCIO	5	9.154	2	2.	- 25	.32	£.	3	7	7 .	2 0	י ע ה		6	13	43	69	9	2	5			INCID	چ	m	7.34	8.11	9.73	6	,		902.6-	9.2	9	3.58	3.4	3.32	D	900	2	3 5	5	. 57
	INCET H. NO	.0	. 57 do	583	597	536	515	52.	5.5	<b>?</b> † €	000	600	67.0	20	592	730	793	71ô	72+	ე.	7	ANCE		INCET	<u>.</u>	_	an .	·n	n (	200	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0.00	950	551	650	10	_	553	300		580	4	529
	OUTLET RADIUS	35	7.2945	٠Ş	3	2	Z.	2	8	Ξ.	ט טא	3 =	3 4	=	5	3	37	‡	7	20	ŝ	2 PERFORMA		001611	3	ā	٠ <u>٠</u>	72			9 0	7	7. 38 75	.03	8	7	2	នូរ	9:	3 6	3	5	ş	8
	INLET	.75	5.4663	. 931	60.	202	7	5	3,	60.		97.	037	196	307	+18	531	045	761	200		STATOR		LACEL		w	9	? ;	֭֭֓֞֜֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֟	•	5	96	3	ð	• 09	13	7	25	ÿř	2 10	.,	3	ij	61
	LOCAT -ION	+1	~	m	J 1	n ·	ا ۵	٠.	<b>.</b>	n ;	3 =	12	13	14	4	16	17	<b>-</b>	ន្ន 27	ν n	j			100		-	۰,	n .	s u	n 4	۰,	- 70	σ	2	=	12	£1 :	<b>.</b>	÷ ÷	27	18	19	20	21

HAKE AND BOUNDARY LAY\_ (ABCES (PERCENT)

15 16 17 19:7 10:4 10:5 1:0 1:0 1:0 9:3 10:4 10:5 9.1 1.0 9.1 SUMMARY POINT NO. 1 THE CALCULATION IS CONVERSED PASS 21 9.0 9.0 9.0 2.4 5.5 1.0 1.0 2.4 5.5 7.3 6.0 0.3 1.3 0.0 11.5 6.3 1.0 .5 .5 0.6 11.8 7.0 STATION 1 2 3 MID 5L32KAGE 9.9 0.0 9.0 UIST FASTOR 1.0 1.0 1.0 INT 9LGCKAGE 0.9 0.0 0.0

.1089 FLOW = 12.44 SPIZJ = 10192.1 PRESSURE RATIO = 1.341 ISENTRUPIC EFFY = .8630 POLYTROPIC EFFY = .8686 DEL T/T = TEST POINT TIL. = 235220415050

;

178

-----

!

1

ı

ì

I

!

## 3. PHASE II WITHIN - BLADE ANALYSIS (60% SPEED) TEST POINT 208221315260

10.608 515.273 14.696 14.359 1824 0.00 18.57 0.000 18.	Total		
\$15.648 \$15.279 \$14.696 \$14.359 \$1824 \$0.00 \$20.937 \$0.000 \$15.279 \$14.696 \$14.359 \$1.824 \$0.00 \$19.76 \$0.000 \$15.279 \$14.696 \$14.359 \$1.824 \$0.00 \$19.76 \$0.000 \$15.279 \$14.696 \$14.359 \$1.824 \$0.00 \$15.279 \$1.696 \$14.359 \$1.824 \$0.00 \$15.279 \$1.696 \$14.359 \$1.824 \$0.00 \$15.279 \$1.696 \$14.359 \$1.824 \$0.00 \$11.380 \$0.000 \$15.279 \$14.696 \$14.359 \$1.824 \$0.00 \$11.380 \$0.000 \$15.279 \$14.696 \$14.359 \$1.824 \$0.00 \$12.370 \$0.000 \$1.824 \$0.00 \$12.370 \$0.000 \$1.826 \$1.825 \$1.824 \$0.00 \$1.826 \$0.000 \$1.826 \$0.000 \$1.826 \$1.826 \$1.826 \$1.826 \$0.000 \$1.826 \$0.000 \$1.826 \$1.82	1876   1875   1876   1875   1874   1874   1874   1874   1875	V:LOCITILS	V:LOCITILS
2.00 0	510.008	01 0.00 234.	01 0.00 234.
10	110.068   515.273   14.696   14.359   1224   0.00   17.30   0.000     518.068   515.273   14.696   14.359   1224   0.00   13.77   0.000     518.068   515.273   14.696   14.359   1224   0.00   11.36   0.000     518.068   515.273   14.696   14.359   1224   0.00   11.36   0.000     518.068   515.273   14.696   14.359   1224   0.00   11.36   0.000     518.068   515.273   14.696   14.359   1224   0.00   0.000     518.068   515.273   14.696   14.359   1224   0.00   0.000     518.068   515.273   14.696   14.359   1224   0.00   0.000     518.068   515.273   14.696   14.359   1224   0.00   0.00     518.068   515.273   14.696   14.359   1224   0.00   0.00     518.068   515.273   14.696   14.359   1224   0.00   0.00     518.068   515.273   14.696   14.359   1224   0.00   0.00     518.068   515.273   14.696   14.359   1424   0.00   0.00     518.068   515.273   14.696   14.359   1424   0.00   0.00     518.068   515.273   14.696   14.359   1424   0.00   0.00     518.068   515.273   14.696   14.359   1424   0.00   1.516   0.000     518.068   515.273   14.696   14.359   1424   0.00   1.516   0.000     518.068   515.273   14.696   14.359   1424   0.00   1.516   0.000     518.068   514.062   14.696   14.359   14.64   0.00   1.516   0.000     518.068   514.062   14.696   14.294   1.997   0.00   19.60   1.100     518.068   514.062   14.696   14.204   1.900   0.00   1.400   0.00   1.400     518.068   514.521   14.696   14.204   1.900   0.00   1.547   0.000     518.068   514.521   14.696   14.204   1.900   0.00   1.547   0.000     518.068   514.521   14.696   14.204   1.000   1.500   1.500   0.000   1.500     518.068   514.521   14.696   14.205   1.000   1.500   0.00   1.500   0.000   1.500     518.068   514.521   14.696   14.205   1.000   0.00   1.500   0.000   1.500   0.000   1.500     518.068   514.521   14.696   14.200   0.000   1.500   0.000   1.500   0.000   1.500   0.000   0	. 01 J. 03 204.	ui J. Ui Zuk. 9i da 2dk.
\$\text{5.6.86}\$ \times \times \times \text{5.5.273}\$ \text{14.6.96}\$ \text{14.8.359}\$ \text{18.24}\$ \text{0.00}\$ \text{15.2773}\$ \text{14.6.96}\$ \text{14.8.359}\$ \text{18.24}\$ \text{0.00}\$ \text{16.800}\$ 1	\$10.008 \$15.273 14.696 14.359 .1824 0.00 16.10 0.000 15.000 510.008 515.273 14.696 14.359 .1824 0.00 113.77 0.000 510.008 515.273 14.696 14.359 .1824 0.00 113.77 0.000 510.008 515.273 14.696 14.359 .1824 0.00 113.30 0.008 510.008 515.273 14.696 14.359 .1824 0.00 113.30 0.008 510.008 515.273 14.696 14.359 .1824 0.00 0.00 0.000 0.000 510.008 515.273 14.696 14.359 .1824 0.00 0.00 0.0000 0.0	4.01 0.00 204.	4.01 0.00 204.
\$15.279 14.696 14.359 1224 0.00 12.50 0.00 13.50 0.00 0.00 0.00 0.00 0.00 0.00 0.00	\$15.879	•• ul	•• ul
\$15.68 515.279 14.696 14.359 .1824 0.00 12.58 0.000 13.58 0.000 15	15.68         515.279         14.696         14.359         1824         0.00         12.56         9.03         9.03           15.68         515.279         14.696         14.359         1824         0.00         12.56         9.03         0.00           15.68         515.279         14.696         14.359         1824         0.00         9.03         0.00           15.68         515.279         14.696         14.359         1824         0.00         6.76         0.00           15.68         515.279         14.696         14.359         1824         0.00         6.76         0.00           15.88         515.279         14.696         14.359         1824         0.00         6.76         0.00           15.88         515.279         14.696         14.359         1824         0.00         1.50         0.00           15.89         515.279         14.696         14.359         1824         0.00         1.50         0.00           15.89         515.279         14.696         14.359         1824         0.00         1.50         0.00           15.89         14.696         14.359         1824         0.00         0.00         0.00	••••••••••••••••••••••••••••••••••••••	••••••••••••••••••••••••••••••••••••••
\$15.678	1.688	•• 31 0, 09 294.	•• 31 0, 09 294.
2.688 515.279 14.696 14.359 .1824 0.00 9.00 10.20 0.00	2.6.68 515.279 1.6.696 14.359 1.824 0.00 9.00 0.00 0.00 0.00 0.00 0.00 0.0	•• 01 01-9 - 294.	•• 01 01-9 - 294.
\$\$\text{5.6.86}\$\$\text{5.15.2.79}\$\$\text{14.6.95}\$\$\text{14.359}\$\$\text{5.1824}\$\$\text{6.00}\$\$\t	2.0.0.0 215.273 14.096 14.359 1024 0.00 6.76 0.000 0.0	•• 01 0• 00 204•	•• 01 0• 00 204•
15.686 515.279 14.696 14.359 1824 0.00 6.76 0.000 0.00	15.686 515.279 14.696 14.359 .1824 0.00 6.76 0.000 15.686 515.279 14.696 14.359 .1824 0.00 6.76 0.000 15.686 515.279 14.696 14.359 .1824 0.00 2.74 0.000 15.686 515.279 14.696 14.359 .1824 0.00 1.90 0.000 15.686 515.279 14.696 14.359 .1824 0.00 1.90 0.000 15.686 515.279 14.696 14.359 .1824 0.00 1.90 0.000 15.686 515.279 14.696 14.359 .1824 0.00 1.90 0.000 15.686 515.279 14.696 14.359 .1824 0.00 1.90 0.000 15.688 515.279 14.696 14.359 .1824 0.00 1.90 0.000 15.688 514.669 14.300 14.300 1.90 0.000 14.70 -136.435 15.688 514.696 14.297 1997 0.00 14.70 -136.435 15.688 514.696 14.286 .2015 0.00 14.70 -136.435 15.688 514.696 14.286 .2015 0.00 13.47 -68.598 15.688 514.696 14.286 .2015 0.00 13.60 0.00 13.47 -68.598 15.688 514.696 14.289 .2016 0.00 13.60 0.00 13.47 -68.598 15.688 514.696 14.289 .2016 0.00 13.47 -68.598 15.688 514.696 14.289 .2016 0.00 13.60 0.00 13.60 0.00 0.00 0.00 0.00 0.00 0.00 0.00	** 01 0.00 204 • 01 ** 01 0.00 204 • 01	** 01 0.00 204 • 01 ** 01 0.00 204 • 01
EMPERATURES	15.536 515.279 14.696 14.359 1824 0.00 4.64 0.000 15.636 515.279 14.696 14.359 1824 0.00 2.74 0.000 15.636 515.279 14.696 14.359 1824 0.00 1.90 0.000 15.636 515.279 14.696 14.359 1824 0.00 1.90 0.000 15.636 515.279 14.696 14.359 1824 0.00 1.900 0.000 15.636 515.279 14.696 14.359 1824 0.00 1.900 0.000 15.636 515.279 14.696 14.359 1824 0.00 1.900 0.000 15.636 515.279 14.696 14.359 1824 0.00 1.900 0.000 15.636 515.279 14.696 14.297 1824 0.000 19.60 1.900 15.636 515.279 14.696 14.297 1997 0.00 19.60 1.900 15.636 514.659 14.696 14.297 1997 0.00 17.16 1.95.439 15.638 514.659 14.696 14.297 1.900 0.00 17.16 1.95.439 15.638 514.659 14.696 14.297 1.900 0.00 17.16 1.95.439 15.638 514.650 14.696 14.284 2.010 0.00 17.16 1.95.97 15.638 514.650 14.696 14.284 2.010 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 17.16 1.95.97 15.638 514.650 14.696 14.283 2.012 0.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.010 1.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.010 1.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.010 1.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.010 1.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.010 1.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.012 0.00 2.010 1.00 2.71 2.20.97 15.638 514.650 14.696 14.283 2.010 0.00 2.010 2.010 2.010 2.010 2.010 2.010 2.0	•• 01 0• 00 204• 01	•• 01 0• 00 204• 01
156.88 515.279 14.696 14.359 1824 0.00 4.64 0.000 0.00	15.638 515.279 14.696 14.359 1824 0.00 4.66 0.000 15.638 515.279 14.696 14.359 1824 0.00 1.90 0.000 15.638 515.279 14.696 14.359 1824 0.00 1.90 0.000 15.638 515.279 14.696 14.359 1824 0.00 1.90 0.000 15.638 515.279 14.696 14.359 1824 0.00 1.91 0.000 15.638 515.279 14.696 14.359 1824 0.00 1.91 0.000 15.638 515.279 14.696 14.359 1824 0.00 1.91 0.000 15.638 514.706 14.696 14.201 1.91 0.00 19.60 1.35.42 15.638 514.578 14.696 14.201 1.907 0.00 17.16 19.60 1.35.42 15.638 514.578 14.696 14.201 1.000 19.60 1.35.42 15.638 514.578 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 1.000 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.47 10.56 15.638 514.51 14.696 14.201 10.00 13.41 1	••01 0.00 204.01	••01 0.00 204.01
156.8 515.273 14.696 14.259 1824 0.00 3.65 0.0000 0.00	15 15 15 17 1 1 1 1 1 1 1 1 1 1 1 1 1 1	** 01 0. 80 20 4. 01	** 01 0. 80 20 4. 01
EMPERATURES	EMPERATURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURESPRESSURES	•• 01 0• 00 20 •• 01	•• 01 0• 00 20 •• 01
2408 515.279 14.696 14.359 .1324 0.00 1.90 0.000	156.08 515.279 14.696 14.359 .1124 0.00 1.90 0.000 0.600 0.668 515.279 14.696 14.359 .1824 0.00 1.90 0.000 0.000 0.668 515.279 14.696 14.359 .1824 0.00 1.90 0.000 0.000 0.000 0.668 515.279 14.696 14.359 .1824 0.00 0.00 0.00 0.00	0.01 0.00 204.01	0.01 0.00 204.01
15.273 14.696 14.359 .1824 0.00 1.15 0.000 1.566 15.273 14.696 14.359 .1824 0.00 1.15 0.000 0.000 1.566 15.273 14.696 14.359 .1824 0.00 0.00 0.00 0.00	15.273 14.696 14.359 .1824 0.00 1.15 0.000 1.600	*• UL 0• UU 204• UL	*• UL 0• UU 204• UL
EMPERATURESPRESSURES MACHANGLES RADIUS OF STATIC HORD CONVATURE STATIC TOTAL STATIC HORD CONVATURE STATIC TOTAL STATIC HORD CON 19,60 -136,435	EMPERATURESPRESSURES	**************************************	**************************************
EMPERATURES	EMPERATURESPRESSURES	201 - 40 d 50 20 40 40 40 40 40 40 40 40 40 40 40 40 40	201 - 40 d 50 20 40 40 40 40 40 40 40 40 40 40 40 40 40
EMPERATURES————————————————————————————————————	EMPERATURES————————————————————————————————————	FLOW FIELD DESCRIPTION	LOW FIELD DESCRI
AL STATEC TOTAL STATEC "3 WHIRL SLOPE CURVATURE "5.88 514.706 14.696 14.303 .1972 0.00 20.83 -205.758 14.696 14.291 .1912 0.00 19.60 -136.435 14.696 14.294 .1997 0.00 17.16 -95.390 .588 514.578 14.696 14.294 .1997 0.00 17.16 -95.390 .588 514.553 14.696 14.294 .1997 0.00 17.16 -95.390 .588 514.553 14.696 14.294 .2010 0.00 14.70 -76.192 .588 514.551 14.696 14.288 .2010 0.00 14.70 -76.192 .588 514.594 14.696 14.283 .2023 0.00 13.47 -68.2978 .588 514.497 14.696 14.283 .2024 0.00 13.47 -68.2978 .588 514.497 14.696 14.283 .2024 0.00 5.33 -36.77 -47.647 .688 514.510 14.696 14.283 .2024 0.00 5.33 -36.77 -41.896 .588 514.510 14.696 14.283 .2024 0.00 3.82 -28.050 .688 514.696 14.283 .2024 0.00 3.82 -28.050 .688 514.696 14.283 .1998 0.00 3.82 -28.050 .688 514.696 14.298 .2020 0.00 3.82 -28.050 .688 514.696 14.294 .1932 0.00 -2.2 -14.609 .16.696 14.311 .1932 0.00 -2.2 -11.4 -12.154 .588 514.696 14.311 .1932 0.00 -1.14 -2.2 -11.4 -12.154	AL STATEC TOTAL STATEC "3 WHIRL SLOPE CURVATURE 514.706 14.696 14.303 .1972 0.00 20.83 -205.758 14.696 14.297 1997 0.00 20.83 -205.758 14.696 14.294 .1997 0.00 17.16 -95.390 .108.8 514.578 14.696 14.294 .1997 0.00 17.16 -95.390 .108.8 514.578 14.696 14.294 .1997 0.00 17.16 -95.390 .108.8 514.553 14.696 14.294 .2010 0.00 14.70 -76.192 .688 514.551 14.696 14.288 .2010 0.00 14.70 -76.192 .688 514.696 14.283 .2023 0.00 11.00 -53.978 .688 514.492 14.696 14.283 .2023 0.00 11.00 -53.978 .41.696 14.283 .2024 0.00 11.00 -53.978 .588 514.497 14.696 14.283 .2024 0.00 11.00 -53.978 .588 514.497 14.696 14.283 .2024 0.00 3.82 -20.1896 .688 514.696 14.283 .2024 0.00 3.82 -20.1896 .588 514.696 14.283 .2024 0.00 3.82 -20.1896 .688 514.696 14.283 .2024 0.00 3.82 -20.1896 .588 514.696 14.298 .2026 0.00 3.82 -20.1896 .688 514.696 14.298 .2039 0.00 3.82 -20.1896 .688 514.696 14.294 .1932 0.00 -2.28 -14.609 .108 6.13 -20.1896 .688 514.696 14.311 .4953 0.00 -2.28 -14.609 .108 6.13 -2.28 -14.609 .108 6.13 -1.14 -1.28		
8.688 514.669 14.696 14.297 1989 0.00 20.83 -205.758 8.688 514.696 14.297 1997 0.00 19.60 -136.435 8.688 514.696 14.294 1997 0.00 17.16 -95.390 8.688 514.578 14.696 14.286 2010 0.00 14.70 -76.192 8.688 514.553 14.696 14.286 2010 0.00 14.70 -76.193 8.688 514.514 14.696 14.286 2010 0.00 12.24 -60.585 8.688 514.594 14.696 14.285 2010 0.00 12.24 -60.562 8.688 514.594 14.696 14.285 2012 0.00 12.24 -61.562 8.688 514.697 14.696 14.283 2024 0.00 12.24 -61.562 8.688 514.697 14.696 14.283 2024 0.00 3.77 -47.647 8.688 514.697 14.696 14.283 2024 0.00 2.77 -47.647 8.688 514.697 14.696 14.283 2024 0.00 2.77 -47.647 8.688 514.697 14.696 14.283 -2024 0.00 2.77 -47.647 8.688 514.697 14.696 14.283 -2024 0.00 2.77 -41.896 8.688 514.697 14.696 14.283 -2024 0.00 2.77 -7.64.896 8.688 514.697 14.696 14.289 -2004 0.00 2.77 -21.30 8.688 514.510 14.696 14.293 1996 0.00 2.77 -21.30 8.688 514.710 14.696 14.293 1996 0.00 2.77 -21.30 8.688 514.710 14.696 14.311 -1975 0.00 -2.8 -14.009 8.688 514.710 14.696 14.311 -1973 0.00 -2.71 -21.31	8.688 514.505 14.696 14.297 1972 0.00 20.83 -205.758 8.688 514.696 14.294 1997 0.00 17.16 -95.390 8.688 514.6578 14.696 14.294 1997 0.00 17.16 -95.390 8.688 514.578 14.696 14.294 2010 0.00 14.70 -76.192 8.688 514.553 14.696 14.286 2010 0.00 14.70 -76.192 8.688 514.554 14.696 14.285 2010 0.00 14.70 -76.192 8.688 514.594 14.696 14.285 2010 0.00 12.24 -60.562 8.688 514.594 14.696 14.285 2019 0.00 12.24 -61.562 8.688 514.594 14.696 14.283 2024 0.00 12.24 -61.562 8.688 514.697 14.696 14.283 2024 0.00 12.24 -61.562 8.688 514.697 14.696 14.283 2024 0.00 3.54 -41.896 8.688 514.697 14.696 14.283 2024 0.00 2.77 -77.647 8.688 514.697 14.696 14.283 2024 0.00 2.77 -77.647 8.688 514.697 14.696 14.283 2024 0.00 2.77 -77.647 8.688 514.697 14.696 14.283 2024 0.00 2.71 -21.301 8.688 514.697 14.696 14.283 2024 0.00 2.71 -21.301 8.688 514.51 14.696 14.293 2024 0.00 2.71 -21.301 8.688 514.561 14.696 14.293 2024 0.00 2.71 -21.301 8.688 514.690 14.293 2024 0.00 2.71 -21.301 8.688 514.690 14.696 14.293 2024 0.00 2.71 -21.301 8.688 514.690 14.696 14.293 2024 0.00 2.71 -21.301 8.688 514.690 14.690 14.311 -19.95 0.00 -2.71 -12.154 8.688 514.865 14.696 14.311 -19.97 0.00 -1.14 -1.14 -12.154	10- TAM620 101AL 1	AIO TAMSEU TOTAL T
18.638 514.669 14.696 14.310 1131 0.00 19.60 -136.435 18.638 514.656 14.696 14.297 1989 0.67 18.38 -110.078 18.638 514.535 14.696 14.291 2004 0.00 17.95 390 18.638 514.578 14.696 14.291 2004 0.00 17.36 -93.4 18.638 514.532 14.696 14.286 2015 0.00 14.70 -76.192 18.638 514.531 14.696 14.283 2023 0.00 11.00 -76.192 18.638 514.497 14.696 14.283 2023 0.00 11.00 -53.978 18.638 514.497 14.696 14.283 2024 0.00 11.00 -53.978 18.638 514.497 14.696 14.283 -2024 0.00 2.77 -47.647 18.638 514.497 14.696 14.283 -2020 0.00 2.77 -47.647 18.638 514.651 14.696 14.283 -2020 0.00 2.77 -47.647 18.638 514.651 14.696 14.284 2000 0.00 3.82 -24.496 18.638 514.651 14.696 14.284 0.00 3.82 -24.496 18.638 514.651 14.696 14.293 1998 0.00 2.71 -21.301 18.638 514.70 14.696 14.314 -1953 0.00 -2.28 -14.009 18.638 514.70 14.696 14.314 -1953 0.00 -2.28 -14.009	18.638 514.669 14.696 14.310 1.131 0.00 19.60 -136.435 18.638 514.635 14.696 14.297 1989 0.60 13.838 -110.078 18.638 514.578 14.696 14.291 2.004 0.00 17.838 -110.078 18.638 514.578 14.696 14.291 2.004 0.00 14.70 -76.192 18.638 514.532 14.696 14.286 2.015 0.00 14.70 -76.192 18.638 514.532 14.696 14.283 2.023 0.00 11.00 -76.192 18.638 514.544 14.696 14.283 2.023 0.00 11.00 -53.978 18.638 514.497 14.696 14.283 2.024 0.00 13.47 -47.647 18.638 514.497 14.696 14.283 -2.027 0.00 11.00 -5.3.978 18.638 514.497 14.696 14.283 -2.027 0.00 2.77 -47.647 18.638 514.51 14.696 14.283 -2.027 0.00 2.77 -47.647 18.638 514.524 14.696 14.284 0.00 2.77 -2.130 18.638 514.570 14.696 14.284 0.00 3.82 -2.4456 18.638 514.570 14.696 14.293 0.00 3.82 -2.4456 18.638 514.570 14.696 14.293 0.00 3.82 -2.130 18.638 514.70 14.696 14.314 -1963 0.00 -2.28 -14.009 18.638 514.70 14.696 14.314 -1953 0.00 -2.28 -14.009 18.638 514.70 14.696 14.314 -1953 0.00 -2.28 -14.009 18.638 514.70 14.696 14.314 -1953 0.00 -1.14 -12.154	43 0.00 220.43	43 0.00 220.43
18.688 514.578 14.696 14.297 1959 0.07 18.38 -110.678 18.688 514.578 14.696 14.294 1997 0.00 17.16 -995.390 18.688 514.578 14.696 14.298 2010 0.00 17.16 -995.390 18.688 514.578 14.696 14.288 2015 0.00 14.70 -76.192 18.688 514.532 14.696 14.286 2015 0.00 13.47 -68.293 18.688 514.501 14.696 14.285 2023 0.00 11.00 -53.978 18.688 514.492 14.696 14.283 2024 0.00 11.00 -53.978 18.688 514.492 14.696 14.283 -2024 0.00 9.77 -47.647 18.688 514.497 14.696 14.283 -2024 0.00 9.77 -47.647 18.688 514.51 14.696 14.283 -2025 0.00 8.54 -41.896 18.688 514.501 14.696 14.283 -2020 0.00 3.82 -22.495 18.688 514.501 14.696 14.293 19.98 0.00 2.71 -21.301 18.688 514.696 14.293 19.98 0.00 2.71 -21.301 18.688 514.696 14.696 14.293 19.98 0.00 2.71 -21.301 18.688 514.696 14.301 14.301 14.696 14.301 14.696 14.301 14.301 14.696 14.301 14.301 14.696 14.301 14.301 14.696 14.301 14.301 14.696 14.301 14.301 14.696 14.301 14.301 14.301 14.696 14.301 14.301 14.301 14.696 14.301	18.688 514.578 14.696 14.297 1969 0.00 17.16 -955.390 18.688 514.578 14.696 14.294 2004 0.00 17.16 -955.390 18.688 514.578 14.696 14.286 2015 0.00 14.70 -76.192 18.688 514.532 14.696 14.286 2015 0.00 13.47 -68.293 18.688 514.532 14.696 14.285 2013 0.00 11.00 -76.192 18.688 514.492 14.696 14.283 2.023 0.00 11.00 -53.978 18.688 514.497 14.696 14.283 2.023 0.00 11.00 -53.978 18.688 514.497 14.696 14.283 2.024 0.00 9.77 -47.647 18.688 514.497 14.696 14.283 2.024 0.00 3.52 -24.496 18.688 514.501 14.696 14.293 1998 0.00 2.71 -21.301 18.688 514.501 14.696 14.293 1998 0.00 2.71 -21.301 18.688 514.561 14.696 14.293 1998 0.00 2.71 -21.301 18.688 514.561 14.696 14.293 1998 0.00 3.82 -24.496 18.688 514.561 14.696 14.293 1998 0.00 3.82 -24.496 18.688 514.70 14.696 14.314 1986 0.00 -2.8 -14.009 18.688 514.696 14.314 -1993 0.00 -1.14 -12.154 18.688 514.696 14.319 1932 0.00 -1.14 -12.154	.50 0.00 221.53	1.50 0.00 221.51
18.688 514.578 14.696 14.284 2004 0.00 15.15 -55.390 18.688 514.578 14.696 14.284 2004 0.00 15.15 -55.390 18.688 514.578 14.696 14.288 2010 0.00 15.77 -56.192 18.688 514.514 14.696 14.286 2019 0.00 12.24 -56.934 18.688 514.514 14.696 14.285 2013 0.00 12.24 -56.862 18.688 514.694 14.696 14.283 2023 0.00 11.00 -53.997 18.688 514.694 14.696 14.283 2024 0.00 17.33 -36.730 18.688 514.697 14.696 14.283 -2024 0.00 7.33 -36.730 18.688 514.51 14.696 14.283 -2026 0.00 6.13 -72.127 18.688 514.51 14.696 14.283 -2026 0.00 3.82 -24.456 18.688 514.51 14.696 14.293 19.96 0.00 2.71 -21.301 18.688 514.70 14.696 14.293 19.96 0.00 2.71 -21.301 18.688 514.70 14.696 14.304 19.86 0.00 3.82 -24.456 18.688 514.70 14.696 14.304 19.86 0.00 3.82 -14.898 18.688 514.70 14.696 14.311 -4.953 0.00 -2.8 -28 -14.009 18.688 514.70 514.696 14.311 -4.953 0.00 -2.8 -28 -14.009 18.688 514.696 14.311 -4.953 0.00 -2.8 -28 -14.009 18.688 514.696 14.311 -4.953 0.00 -2.8 -28 -14.009	18.688 514.578 14.696 14.284 2104 0.00 15.15 -55.390 18.688 514.578 14.696 14.284 22004 0.00 15.715 -55.390 18.688 514.578 14.696 14.286 2010 0.00 15.77 -56.192 18.688 514.514 14.696 14.285 2010 0.00 12.24 -56.934 18.688 514.514 14.696 14.285 2013 0.00 12.24 -56.852 18.686 514.594 14.696 14.283 2023 0.00 11.00 -53.997 18.688 514.497 14.696 14.283 2024 0.00 17.33 -35.73 18.688 514.497 14.696 14.283 -2025 0.00 8.54 -41.896 18.688 514.510 14.696 14.283 -2026 0.00 6.13 -32.127 18.688 514.510 14.696 14.283 -2026 0.00 3.82 -24.456 18.688 514.560 14.696 14.293 19.86 0.00 2.71 -21.301 18.688 514.70 14.696 14.293 19.86 0.00 2.71 -21.301 18.688 514.70 14.696 14.311 -4953 0.00 -2.8 -14.895 18.688 514.865 14.696 14.311 -4953 0.00 -2.8 -14.895 18.688 514.865 14.896 14.311 -4953 0.00 -1.14 -12.154 18.514 18.514 -12.154 18.514 -12.154 18.514 -12.154 18.514 -13.54 18.514 -13.54 18.514 -13.54 18.554 18.689 -1.14 -12.154 18.514 -13.54 18.544 18.544 -13.64 18.644 -13.644 18.644 1	**I #**********************************	7 5 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
18.688 514.553 14.696 14.288 2010 0.00 14.70 -76.192 18.688 514.553 14.696 14.286 .2015 0.00 13.47 -68.258 18.688 514.514 14.696 14.285 .2019 0.00 13.47 -68.258 18.688 514.514 14.696 14.283 .2023 0.00 13.47 -68.258 18.688 514.497 14.696 14.283 .2024 0.00 9.77 -47.647 18.688 -514.497 14.696 14.283 .2024 0.00 7.33 -32.127 18.688 514.511 14.696 14.283 .2020 0.00 6.13 -32.127 18.688 514.651 14.696 14.289 .2016 0.00 3.82 -24.456 18.688 514.696 14.293 .1996 0.00 2.71 -21.301 18.688 514.710 14.696 14.304 1936 0.00 3.82 -24.456 18.688 514.710 14.696 14.314 .1953 0.00 -2.8 -14.009	18.688 514.553 14.696 14.286 2010 0.00 14.70 -76.192 18.688 514.553 14.696 14.286 2015 0.00 13.47 -68.258 18.688 514.514 14.696 14.285 .2019 0.00 12.24 -60.862 18.688 514.514 14.696 14.283 .2023 0.00 11.00 -53.978 18.688 514.497 14.696 14.283 .2024 0.00 9.77 -47.647 18.688 514.497 14.696 14.283 .2024 0.00 7.33 -36.730 18.688 514.497 14.696 14.283 .2024 0.00 6.13 -32.127 18.688 514.510 14.696 14.286 .2020 0.00 6.13 -32.127 18.688 514.650 14.696 14.283 .2026 0.00 3.82 -24.456 18.688 514.650 14.696 14.293 .1996 0.00 2.71 -21.301 18.688 514.650 14.696 14.311 .1956 0.00 -2.8 -14.809 18.688 514.70 14.696 14.311 .1953 0.00 -2.8 -14.809 18.688 514.865 14.696 14.311 .1953 0.00 -1.14 -12.154 18.688 514.865 14.329 -1997 0.00 -1.14 -12.154	+2.622 DD •D • -2.	+2.5.2.2 00.00 +2.5.5.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.
14.688 514.532 14.696 14.286 .2015 0.00 13.47 -68.258 18.688 514.514 14.696 14.285 .2019 0.00 12.24 -60.862 18.688 514.501 14.696 14.283 .2023 0.00 11.00 -53.976 18.688 514.497 14.696 14.283 .2024 0.00 11.00 -53.976 18.688 .214.497 14.696 14.283 .2024 0.00 8.54 -41.896 18.688 514.497 14.696 14.283 .2024 0.00 6.13 -32.127 18.688 514.501 14.696 14.286 .2015 0.00 4.96 -28.050 18.688 514.501 14.696 14.286 .2015 0.00 4.96 -28.050 18.688 514.501 14.696 14.304 1998 0.00 2.71 -21.301 18.688 514.710 14.696 14.314 1978 0.00 -28 -16.123 18.688 514.710 14.696 14.314 1978 0.00 -28 -16.123 18.688 514.70 14.696 14.314 1973 0.00 -28 -16.123 18.688 514.70 14.696 14.314 1973 0.00 -28 -16.123 18.688 514.70 514.696 14.314 1973 0.00 -28 -16.123	14.688 514.532 14.696 14.286 .2015 0.00 13.47 -68.258 18.688 514.514 14.696 14.285 .2019 0.00 12.24 -60.862 18.688 514.501 14.696 14.283 .2023 0.00 11.00 -53.876 18.688 514.497 14.696 14.283 .2024 0.00 8.54 -41.896 18.688 514.497 14.696 14.283 .2024 0.00 8.54 -41.896 18.688 514.497 14.696 14.283 .2026 0.00 6.13 -32.127 18.688 514.510 14.696 14.286 .2015 0.00 4.96 -28.050 18.688 514.561 14.696 14.286 .2015 0.00 2.71 -21.31 18.688 514.710 14.696 14.293 1366 0.00 2.71 -21.31 18.688 514.710 14.696 14.314 .1978 0.00 -28 -16.123 18.688 514.710 14.696 14.314 .1971 0.07 .65 -16.123 18.688 514.710 14.696 14.314 .1953 0.00 -28 -14.009 18.688 514.70 14.696 14.314 .1953 0.00 -28 -14.009 18.688 514.70 14.696 14.311 .1953 0.00 -1.14 -12.154	. 63 P. 30 224.63	**************************************
18.688 514.514 14.696 14.285 .2019 0.00 12.24 -60.862 18.688 514.501 14.696 14.283 .2023 0.00 11.00 -53.978 18.688 514.497 14.696 14.283 -2025 0.00 11.00 -53.978 18.688 514.497 14.696 14.283 -2025 0.00 6.13 -32.127 18.688 514.497 14.696 14.283 -2024 0.00 6.13 -32.127 18.688 514.510 14.696 14.289 0.200 0.00 6.13 -32.127 18.688 514.501 14.696 14.293 1998 0.00 2.71 -21.301 18.688 514.70 14.696 14.314 0.1971 0.01 0.65 -16.123 18.688 514.70 14.696 14.314 0.1971 0.01 0.26 -16.123 18.688 514.70 14.696 14.314 0.1971 0.01 0.26 -16.123	18.688 514.514 14.696 14.285 .2019 0.00 12.24 -60.862 18.688 514.501 14.696 14.283 .2023 0.00 11.00 -53.976 18.688 514.497 14.696 14.283 -2025 0.00 11.00 -53.976 18.688 514.497 14.696 14.283 -2025 0.00 7.33 -36.730 18.688 514.497 14.696 14.284 .2020 0.00 6.13 -32.127 18.688 514.501 14.696 14.286 .2015 0.00 4.96 -28.050 18.688 514.501 14.696 14.293 1998 0.00 2.71 -21.301 18.688 514.71 14.696 14.314 1971 0.01 6.55 -16.123 18.688 514.70 14.696 14.314 1971 0.01 -28 -16.123 18.688 514.70 14.696 14.314 1998 0.00 -28 -16.123 18.688 514.70 14.696 14.314 1995 0.00 -28 -16.123 18.688 514.70 14.696 14.311 -1953 0.00 -28 -14.009 18.688 514.865 14.696 14.311 -1953 0.00 -1.14 -12.154	25 0.00 225.25	5.25 0.00 225.25
18.688 514.501 14.696 14.283 .2023 0.00 11.00 -53.978 18.688 514.497 14.696 14.283 .2025 0.00 8.57 -7.647 18.688514.497 14.696 14.284 .2026 0.00 6.13 -36.730 18.688 514.510 14.696 14.284 .2020 0.00 6.13 -32.127 18.688 514.501 14.696 14.289 .2006 0.00 6.13 -32.127 18.688 514.501 14.696 14.293 .1998 0.00 2.71 -21.311 18.688 514.710 14.696 14.314 .1956 0.00 -2.71 -21.311 18.688 514.710 14.696 14.314 .1957 0.00 -2.8 -16.123 18.688 514.70 14.696 14.311 -1953 0.00 -2.8 -16.123	18.688 514.501 14.696 14.283 .2023 0.00 11.00 -53.978 18.688 -514.497 14.696 14.283 .2025 0.00 8.77 -47.647 18.688 514.497 14.696 14.284 .2026 0.00 7.33 -36.730 18.688 514.510 14.696 14.284 .2020 0.00 6.13 -32.127 18.688 514.501 14.696 14.289 .2006 0.00 3.82 -26.456 18.688 514.710 14.696 14.314 .1938 0.00 2.71 -21.311 18.688 514.710 14.696 14.314 .1938 0.00 -2.28 18.688 514.710 14.696 14.314 .1938 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.688 514.710 14.696 14.311 -1953 0.00 -2.28 18.689 -514.865 14.319 .1932 0.00 -1.14 -12.154	73 0.00 225.73	5.73 0.00 225.73
18.688514.494 14.696 14.203 .2024 0.00 9.77 -47.647 .886.88514.492 14.696 14.2832025 0.00 8.54 -41.896 -41.896 14.284 14.696 14.284 1.2024 0.00 7.33 -35.730 14.696 14.284 2.020 0.00 6.13 -32.127 14.696 14.284 2.020 0.00 6.13 -32.127 14.696 14.696 14.286 2.015 0.00 6.13 -32.127 14.696 14.696 14.293 1998 0.00 3.82 -28.850 14.696 14.696 14.293 1998 0.00 2.71 -21.301 14.696 14.696 14.314 1996 0.00 3.82 -2.4456 14.696 14.314 1978 0.00 3.82 -14.609 14.696 14.314 1973 0.00 -28 -14.609 14.696 14.314 1973 0.00 -28 -14.609 14.696 14.314 1973 0.00 -114 -28 -14.609 14.696 14.319 1932 0.00 -114 -12.154	18.688 514.494 14.696 14.203 .2024 0.00 9.77 -47.647 .868 .9688 .914.492 14.696 14.283 -2025 0.00 8.54 -41.896 .41.896 .13 -2025 0.00 8.54 -41.896 .41.896 .13 -2021 0.00 7.33 -35.730 .2024 0.00 7.33 -35.730 .2024 0.00 7.33 -35.730 .20.730 .2020 0.00 6.13 -32.127 .10.696 14.284 .2020 0.00 6.13 -32.127 .10.696 514.51 14.696 14.293 .1998 0.00 3.82 -24.456 .10.696 .14.696 14.696 14.393 0.00 2.71 -21.331 .10.696 .14.696 14.314 .196 0.00 3.82 -24.456 .10.696 .10.696 .1971 0.01 .65 -16.539 .10.696 .1971 0.01 .65 -16.539 .10.696 .14.314 .1953 0.00 -28 -14.009 .10.696 .14.314 .1953 0.00 -1.14 -12.154 .10.696 .14.329 .1997 0.00 -1.14 -12.154 .10.696 .14.329 .1997 0.00 -1.14 -12.154	US 6.00 226.03	6.08 6.00 226.08
18.688514.492 14.696 14.2832025 0.000 8.54 -41.896 18.688 514.497 14.696 14.2832024 0.00 7.3335.730 14.696 14.284 2.024 0.00 7.3335.730 14.696 14.286 2.024 0.00 6.1332.127 14.696 14.286 2.015 0.00 6.1332.127 14.696 14.696 14.289 0.00 3.8224.456 14.696 14.293 0.1998 0.00 2.7121.301 14.696 14.696 14.293 0.196 0.00 2.7121.301 14.696 14.696 14.314 0.191 0.6514.893 14.696 14.696 14.3142814.009 0.002814.009 0.00 0.002814.009 0.00 0.002814.009 0.002814.009 0.00 0.002814.009 0.00 0.002814.009 0.00 0.002814.009 0.00 0.002814.009 0.00 0.00 0.002814.009 0.00 0.00 0.00 0.00 0.00 0.00 0.00	18.688514.492 14.696 14.2832025 0.000 8.54 -41.896 18.688 214.497 14.696 14.2832024 0.00 7.3335.730 14.696 14.284 20.24 0.00 7.3335.730 14.696 14.286 14.287 0.00 6.1332.127 14.696 14.286 0.2027 0.00 6.1332.127 14.696 14.696 14.289 0.00 3.82 -24.456 14.696 14.696 14.289 0.00 3.82 -24.456 14.696 -1.14 -12.154 18.516 15.600 11.666 14.696 14.329 11.696 14.696 14.329 11.696 14.696 1	. 23 0.00 226.29	6.43 0.60 226.29
18.688 514.497 14.696 14.283 .2024 0.00 7.33 -356.730 .20.688 514.510 14.696 14.284 .2020 0.00 6.13 -32.127 .32.127 .32.127 .33. 514.531 14.696 14.289 .2015 0.00 6.13 -32.127 .32.127 .33. 514.561 14.696 14.289 .2016 0.00 3.82 -24.456 .18.688 514.696 14.293 .1996 0.00 2.71 -21.301 .18.688 .34.710 14.696 14.311 .4953 0.00 -2.8 -14.893 .18.688 514.782 14.696 14.311 .4953 0.00 -2.8 -14.809 .10.66 14.311 .4953 0.00 -2.8 -14.809 .10.66 14.311 .4953 0.00 -1.14 -12.154 .	18.688 514.97 14.696 14.283 .2024 0.00 7.33 -356.730 18.688 514.510 14.696 14.284 .2020 0.00 6.13 -32.127 18.689 514.531 14.696 14.284 .2020 0.00 6.13 -32.127 18.689 514.551 14.696 14.289 .2008 0.00 3.82 -24.456 18.689 514.560 14.696 14.293 .1996 0.00 2.71 -21.301 18.688 514.710 14.696 14.293 .1996 0.00 2.71 -21.301 18.688 514.770 14.696 14.311 .1953 0.00 -2.8 -14.809 13.686 514.865 14.696 14.311 .1953 0.00 -1.14 -12.154 18.689 18.689 -14.696 14.329 .1997 -0.889 -1.14 -12.154	33	54-33 0 0 226 33
10.646 51.4510 14.696 14.284 .2020 0.00 6.13 -32.12/ 18.658 514.531 14.696 14.286 .2015 0.00 4.96 -28.050 . 18.658 514.661 14.696 14.293 .1998 0.00 2.71 -21.301 . 18.688	10.686 51.510 14.696 14.284 .2020 0.00 6.13 -32.12/ 18.688 514.531 14.696 14.286 .2015 0.00 4.96 -28.050 18.688 514.650 14.696 14.293 .1996 0.00 2.71 -21.301 18.688 -514.650 14.696 14.298 .1986 0.00 2.71 -21.301 18.688 514.710 14.696 14.304 .1971 0.01 .65 -16.123 18-688 514.665 14.696 14.311 -4.953 0.0028 -14.009 18.688 514.665 14.696 14.319 .1932 0.00 -1.14 -12.154 18.689 -514.865 14.696 14.329 -1987 -0.09 -1.91 -18.518	19 5.00 225.19	6.19 5.00 726.19
18.688 514.551 14.696 14.286 .2115 0.00 4.96 -28.050 18.688 514.561 14.696 14.289 .2008 0.00 3.82 -2.4456 18.688 514.710 14.696 14.304 .1971 0.01 1.65 -18.539 18.688 514.710 14.696 14.314 .1971 0.01 18.688 514.70 14.696 14.311 18.688 514.70 14.696 14.311 18.688 514.70 14.696 14.311 18.688 514.70 14.696 14.311 18.688 514.70 14.696 14.311 18.688 514.70 -1.28 -1.28	18.686 514.551 14.696 14.286 .2015 0.00 4.96 -28.050 18.688 514.661 14.696 14.289 .2008 0.00 3.82 -2.456 18.688 514.710 14.696 14.294 .1946 0.00 2.71 -21.301 18.688 514.710 14.696 14.304 .1971 0.01 18.688 514.710 14.696 14.311 18.688 514.865 14.696 14.311 18.688 514.865 14.696 14.319 .1932 0.00 18.688 514.865 14.696 14.319 .1932 0.00 -1.14 -12.154 18.689514-36414-696 14.329 -1987 18.58414.696 14.529 -1987	9. 00 225.85	5* 85 8 0 225 85
10.688 514.561 14.696 14.289 .2006 0.00 3.82 -2.4456 18.688 514.600 14.696 14.293 .1998 0.00 2.71 -21.301 18.688 514.710 14.696 14.304 .1971 0.01 18.688 514.72 14.696 14.3111953 0.0028 -14.009 18.688 514.782 14.696 14.3111953 0.0028 -14.009 18.688 514.065 14.696 14.319 .1932 0.00 -1.14 -12.154	10.688 514.561 14.696 14.289 12006 0.00 3.82 2.21.301 18.688 514.680 14.293 1998 0.00 2.71 2.71 21.301 18.688 514.710 14.696 14.293 1998 0.00 2.71 2.71 21.301 18.688 514.710 14.696 14.314 1971 0.01 65 -16.123 18.568 -514.720 14.696 14.311 -1953 0.00 -28 -14.009 18.688 514.865 14.696 14.319 1932 0.00 -28 -14.009 18.688 514.865 14.696 14.319 1932 0.00 -1.14 -12.154 18.689 -18.514 -18.514	0.00 22	5.28 0.00 22
18.568 51.500 14.696 14.293 1996 0.00 2.71 -21.301 18.688514.659	18.668 51.680 14.696 14.293 1996 0.00 2.71 -21.301 18.668	. 00 ° 0.	25 00 00 55
18.688514.659 14.696 14.298 1386 0.888 1.66 -18.539 12.688 514.710 14.696 14.304 1971 0.87 0.87 0.65 -16.123 18.589 1.658 -514.70 14.696 14.311 1.4953 0.8028 -14.009 18.588 514.865 14.696 14.319 1932 0.80 -1.14 1.2.154 1.658 514.865 14.696 14.319 1932 0.80 -1.14 1.2.154 1.698	18.688514.650 14.696 14.298 1386 0.888 1.66 -18.53 . 18.688 514.710 14.696 14.314 1971 0.87 .65 -18.123 . 18.688514.865 14.696 14.3111953 0.0028 -14.809 . 18.688 514.865 14.696 14.319 .1932 0.88 -1.14 -12.154 . 18.689514.96414.696 14.329 .19870.888 -1.91 -18.518 .	0.40 22	3.40 0.40 22
18.688 514.710 14.696 14.304 .1971 0.07 .65 -16.123 . 18-68851.782 14.696 14.311 .44.953 0.0028 -14.009 . 18.688 514.865 14.696 14.319 .1932 0.00 -1.14 -12.154 .	18.688 514.710 14.696 14.304 .1971 0.07 .65 -16.123 . 18-68851.8782 14.696 14.3111953 0.u028 -14.009 . 18.688 514.865 14.696 14.319 .1932 0.00 -1.14 -12.154 . 18.689514.96414.696 14.329 -19870.00 -1.91 -18.518 .	<del>0.00</del> 22	25 94 9x 94 25
18-688514-782 14-696 14-3111953 8-0028 -14-889 18-688 514-865 14-696 14-319 -1932 8-00 -1-14 -12-154	18-588514.865 14.696 14.3111953 8.u028 -14.889 . 18.688 514.865 14.696 14.319 .1932 0.00 -1.14 -12.154 . 18.689514.865 14.529 -19878.89 -1.91 -18.518 .	0.00 22	0.00 22
14.665 14.665 14.665 14.819 .1932 0.00 -1.14 -12.154 .	10.688 514.065 14.696 14.319 .1932 0.00 -1.14 -12.154 . 10.609514.36414.696 14.329 .19870.00 -1.91 -10.510 .	12	82
	18-688514-36414-696 14.329 -19878-88 -1.91 -18.514 -	•JI 0•00 Z16,	6.J1 0.00 216,

	S RADIUS OF SPECIFIC SLOPE CURVATURE WEIGHT	-63.631	197-001 - 197-001 - 017	95 1152,952 .07	78 1032.811 .87	43 -3025.278 .07	13 -358.653 .07	70	100 CC0 CC0 CC0 CC0 CC0 CC0 CC0 CC0 CC0	76 -47.848 -87	36.936 .07	02 -29.476 .87	65 -24.089 .07	28 -20.041 .07	92 -16.914 .07	42 -14.451 .87	74 -12.480 .07	-10.096 -17	TO TO THE TOTAL TO	10. 069.8- /*			R	URE	12 -388.854 .87	3 -195.022 .07	16 -126.887 .07	76 -94.628 .07	75.957	10 - 070 - 0	100 Th: 100 10	00.00 00.000 00.000 00.000 00.000	56 -33.856 .07	16 -30.760 .07	59 -28.460 .07	19 -26,366 .07	56 -24.355 .U.	100 C/2022 CO	12 - 14 BX7 - 12	3.56 -17.111 .07	
	HAIRL S	0.00	<b>.</b>	20	00	00	00	200	<b>9</b> 0		0	00	00	c <sub>3</sub>	00	00	00	00	<b>9</b> (	00			SLE	NHIR. S	0	00	00	00	90	9 0	<b>3</b> 6		000	00	00	00	9 0	ء د	2 6	90	
	HACH NO	.2141	v	S	· 0	~	.2215	N	No	u v	1 0	. ~	~	N	N	N	~	∾ (	.2116	N			MACH	0	2	230	233	235	3G	7	) ·	1 to 1 to 1 to 1 to 1 to 1 to 1 to 1 to	247	3	248	240	200	7 6	0 C	3	
	SSURES STATIC	14.235	14.230															٠	÷.	;			SURES	ST	7	: =	•			;	# ·	14 - 096			3	3	•		•	7	
	- TOTAL	4.69	14.696	700	. b3	4.69	4.69	69*4	60		4	69.4	69**	4.69	<b>*•</b> 69	4.69	4.69	<b>69°</b>	4.69	<b>*•</b> 69			235d	TAL	4.63	69.4	4.69	4.69	4.63	<b>4.6</b> 9	69.4	14.696	9	69 *	69.4	į	69.4	69.4		060**T	
	PERATURES STATIC	14.0	513,953		13.7	13.7	13.5	13.6	13,5	72.0	44.5	13.5	13.5	13.5	13.6	13.7	13.9	13.9	14.1	14.2			TURES.	STATIC	X . X		13.1	13.0	12.8	12.7	12.5	512.595	100	12.4	12.3	12.3	12.4	12.4	12.5	10.7	
	TEMPER! TOTAL	18.68	518.688	18.50	18.50	18.68	18.58	18.63	18.68	18.50	200	18.68	13.68	13.68	18.68	18.65	18.08	18.68	18.68	18.68			7	TOTAL	4	0 · 0	18.5	18.6	18.5	10.6	10.6	518.568		13.6	18.6	16.6	18.6	10.6	13.6	0 7	
SCRIPTION	TOTAL	39	2+0-+2	, ,	, ,	9	47.	.0	6	9	• • •		5	20	.,	45	42.	39.	36.	32.	P		•	TOTAL	- :	: :	•			:	<u>.</u>	272.74	: .:	•		~		ċ	:		•
FILLS DES	LOCITICS	0	0.03	<b>~</b>	9 0	0	0	Ç	0	9	•	<b>-</b>	0	0	0	0	C	0	c	Ξ,	t.) us		CTTT	TANGEN	4	Þ≂	, =	0	0	0	0	0.00	<b>&gt;</b> =	•	0	Ф	'n	•	0	p c	,
3 FL3#	45 K I D	239.23	2+0+2	241.73	20 mm 1/2 .	246.07	247.35	240.45	24.5. 37	250.03	14.000	25.0.40	249.57	244.53	247.05	245.13	242.72	23 4, 42	230.42	232.55	-+ FLOW	,	, N	AIU	4 	25.40	3 3 3 3 3 3	26 3. 27	255. 35	2000.47	27 0 . /4	272.74	27 5 73	27 0 0 05	27.7.20	27 7. 32	276.99	276.15	27 ** 30	27.2.53	
STATION	4ADIJS	9	6.7259	# C	<u>ה</u> כ	; ;	33.	Ť.	ご	5	n c	היה	? ~	53	1	Š	9	79	91	5	A710		SUTGAG	Š		<b>~</b> 3	9 0	<b>,</b> 0	·N	m		7.5396	40		יס נ		*	<b>F</b>	3	un v	9
	STREAH -LINE	-	N	∾ .	. t	۰ د		80	o ·		, H (	۷ ۲ ۲ ۲	) <u>1</u>	12	91	17	0	13	20	21			HARONS	- LI R	•	н п	y 1º	<b>.</b>	'n	•	٧.٠	en (	<b>7</b>	o +	15	P.T.	14	15	16	7,	•

POLYTROPIC EFFICIENSY	1.6000	2 :	2 :	2 :	::	2 2	2 :		2:	2 :	: :	3 2	:	2 :	3 :		3	8	5	8	:																										
ISENTROPIC P	1.0300	9		9 (		D (			9	50	3		3	9 (						9	5				MEIGHT		•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	1620.	•	•
DELTA T	0.000	8	8	9	8	5	8	5	8	8	2 8	3 ;	3	ם פ	3	8	8	8	8	8	8	,		PADTIIS OF	CURVATURE		6.199	6.519	7.079	7.955	9.271	11.214	14.154	19.040	28.741	56.808	793.747	-72.565	-37.102	-26.628	-22.272	-20.666	-21.034	-23.657	-38.504	-52.456	-1665.883
PRESSURE RATIO	1.000	9	1.000	8	3	3	8	8	1.000	8	5	5	3	3	1.000	9	9	9	e.	9	1.000	:		,	יי		22,32	21.07	19.70	18.24	16.70	15.11	13.48	11.81	19.12	8.42	6.72	5.03	3.35	1.68	• 05	-1.60	-3.17	-4.71	-6.25	-7.80	-9.38
ELATIVE MPERATURE	591.165	2.531	£*004	\$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	966.9	26+-8	0.017	1.549	3.097	296.4	747.0	7.555	004.6	1.150	2.844	4.375	6.348	8.166	0.342	1.976	3,382	,		- CNA	Ξ		28.95																		. 26.07		
G 10																								20	2	:	.3075	.3114	.3151	.3186	, 3221	.3257	.3293	.3326	.3357	.3385	.3411	.3436	.3+6	.3483	.3505	.3522	.3536	m	135°	.3543	2555
RELATIVE PRESSURE	19.369	19.54	19.72	19.91	20.09	25.28	20.47	20.67	20.87	21.07	21.27	21.48	21.70	21.92	22.14	22.39	25.62	22.86	23.12	23, 39	23.67			00000	STATE	)	15.757	15.744	15,728	15.712	15.695	15.678	15,664	15.652	15.643	15.639	15.640	15.644	15.653	15,667	15,685	15.707	15.734	15.763	15, 793	15-825	15.856
RELATIVE Jelocity	•	•	789.35	٠	•	•	•	•	•	•	•	•	٠	٠	927.55	٠	•		•			•		11302.00	,																		7.152				17,283
RELATIVE	. 6835	6460.	2002	ζ.	. 72.84	. 7393	. 7501	. 75 07	.7711	. 7914	. 7915	. 80 17	. 9117	• 3215	. 3314	. 3412	. 45 69	. 60 05	. 57 03	30.00	80 47	•			STATE	•	29.0	20.	28.8	28	28	28	2	28	28	28	528.284	2	2	29	2	30	31	31	532.348 .	33	7
BLADE SPEZD	719.5	731.9	7 * * • 1	756.2	766.2	7.80.1	791.9	603.7	915.4	827.0	938.7	850.3	962.0	873.7	645.2	4.768	686	921.5	933.9	4	0 1			. 40. 50	£		•					-	-	-		•		-	İ		_	-			1		46.971
1055 30EF	0	0.0000	0.000.0	0	9	0	00	8	0.000	8	9	0	9	2	9	00	3	0.0013	3	2		3	NOTE				61.	.93	1	6	- 69	OF.	26		340.12 5				:						ļ		402-16 .54
CVIATION (NCIDENCE		-3.022	-0.110	•	÷	÷	-6.295	÷	-3.340	÷	-3.446	-3.25+	÷	-4.721	-3.922	- 3.132	-9.370	-3.621	- 4. 873	-11,114	7417	:	41508.50		FOF 21		8+8 60	33	٠	_	20	368	372	31	•	0	•	_	:	30	ķ	99	6	•	1	10	38 - 402
F.034		~	70	-70.9.5		-71.310		71.255	-71. 593	-71.552	- 52.24-	-	72.150	7213	-72.570	72.374	43,444	73.253	40.00	~ * * *		****	D# Field	,	-T > O J - A -	•	166	10%	165	163		1 100.7	- 15		3 157.	157.		158	1	101	164.	167	172	175	123-	179	##
% '*	245 -7		5.450 -7	_			0.334 -7				•	6.137 -7				3,4	ķ	23	2	; ;	4 4	000	FLO4		9	4	- 30 ** 93	31.0.75	51 be 3	321.03	326.05	35 2. 11	34.7.17	341.01	340.83	•	352.01	355.4	4	350.34	ď	362.67	å	i N	t,	35.0.95	4
BLADE-ANGLES	1 200	598 1	601 1	2 0 2	736- 1	-	-				•				į	į	Ŧ	m	178	, o c	127		S14110N		44010s		4269	6.00.7	.7.4183	7.2143	7.3170	7.4135	7.5191-	7.6137	7.7177	7.8153	7.9140	6.0133	100	8.2111	0-3106	8.4111	4.5127	8.615b	66.7	8.8259	100
LOCAT BL		2 -02.	•	2	ı				9 -53.059		44								4					, ,	SIREAR	2 4 4 5	1						į	•	!		;	15		*		16		91		50	-
1											1						•		1	8:	1		ı	٠.		•	ì				1		١		i				١		:		i		١		Ì

4
-
~
~
.,,
Ç,
⋖
_

EFFICIENCY	1.0010	1.0004	9666.	.9993	6966.	9866.	9866.	<b>*266*</b>	6966.	9066.	7496°	.9788	.9713	. 9641	.9531	. 9322	.9121	.9010	. 6915	.8610	.8688	. 045
EFFICIENCY	1.0010	1.0004	9666.	.9993	6966.	9966	6266.	<b>4266</b>	6966*	9066.	.9845	.9783	.9707	.9633	.9521	.9307	.9101	.6988	0699.	.8783	*8657	1 NO
- NO	.039	.039	040.	0 70 •	. 040	040	. 040	.041	. 041	. 041	. 042	• 043	**0.	. 045	950.	. 048	640.	, 051	. 052	. 053	• 055	DELTA T
RATIO	1.145	1-146	1.146	1.147	1.247	1.148	1.149	1.150	1.151	1.152	1.153	1.155	1.157	1.159	1.152	1.154	1.157	1.170	1.172	1.174	1,176	955
TE 4PERATURE	552.341	554.323	565.705	557.390	558.+77	569.368	571.263	572.364	574.374	575.497	576.930	578.394	579.372	531.374	532,302	534.+01	546.158	537.594	559.374	591.101	5 32 , 3 8 3	PO.Y. EFF.
PRESSURE T	-	-	19,939	20.103				20.809											22.593	22.773	256.52	EFF.= .954
VELOCITY	643.44	14.759	671.46	685.27	693.88	712.23	725.19	737.77	749.93	764.70	771.12	791.15	750.08	799.75	817.92	913.87	319.64	927.12	334.96	942.74	359.41	I SEN.
4454 40	7265.	58.02	. 5925	6700	. 5169	62.49	.0403	. 15 15	. 2523	. 27 17	. 23 98	. 2895	1260.	. 7355	. 71.25	.1172	. 7215	.7273	* 7 3 4 4	.7+09	. 7479	PYFSSURE DATIO = 1.129
3660	7 35 . 3	7.00.7	757.9	769,3	700.0	7.30.3	301.0	912.1	822.1	333.2	3+3.7	80.4.2	904.7	872.3	6359	3.00	907.4	110.4	6.6.5	940.0	9:2.3	SSURE
1384 108 FF	9.0 0.5	ii ii	, –			.9132		. 1411							. 3 2 0 2				06.40			
LANTICE				-1-303	-1.272	-1.221	-1.133	-1.1.7	-1.137	-1-173	-1.122	-1,127	-1.1.1	-1.163	-1-143	1.5.1	-1.331	-1.4.5	-1.235	-1.773	-1.373	INT OEAFORMANDE
AND INTERNET	-51.712	F 6. 7 1 4.	-21.432	-52.133	-52.115	CL5.26*	*6.5.5.	7( * * * * * *	-52. 22		96	-52.131	4/1 - 2	u 2 c	-53.572	50000	-53.7.50	- 5.5 C . 2.5 C .	654 . 40	-34 . 133	+60.00-	INT . CHAT
1.45.1.2 J	10.432	679.5	9.00	7.00.43	9.622	24	107.4	.130	3.755	3.3.0	6.0.5	2.6.36	2,031	1.0.19	to by Jo	1.0 25	1.7.3	1.029	1.350	1.743	1.5.24	STATIUN >
3c40c-1NGc23 section can	5e5.b		10000	0.c.	4-6-0	- 1.333	1.103	- 11 - 2 - 2	1 - 305		6.44.1	2 (1 . 1 . 1 . 1 . 1 . 1 . 1 . 1 . 1 . 1	-51.934	7 - 2 - 2 - 7	- 2.17+	2 . 247	404.2.	. 2.333	1,2,031	2. 305	-55.350	SIAT
-10N	•	۰,	,	,	٠.	2	٠.	· •c	T		: :		1:3				17	÷	6		;;	

F SPECIFIC RE WEIGHT	6090. 2	2080. 9	•	4080.	•	•	•	•	•	•	•	•	•	Ī	•	•	•	•	•	•	•
RADIUS OF CJRVATURE	4.30	5.65	7.61	11.598	19,90	51.73	-148.03	-35.69	-22.34	-17.37	-14,94	-13.64	-13.01	-12.85	-13.11	-13.94	-15.76	-19,34	-25.90	-50.34	1665.88
LES SLOPE	27.37	25.21	23.02	20.81	18.59	16, 39	14.23	12, 10	10.00	7.96	5.96	4.03	2.16	. 36	-1.37	-2.98	-4.45	-5.80	-7. OE	-8.25	-9.38
ANGI	33,37	32.24	31,30	34.51	29.84	29, 28	29.84	20.49	28.21	28.26	24,35	28.50	28.75	29, 02	29.51	30.56	31.65	32,27	32.82	33,42	34.12
A P C I	.3653	.3698	.3740	.3776	.3 80 7	.3936	. 3 965	.3493	. 1917	.3937	.3954	.3970	. 3984	1865.	. 1003	.4014	.4013	.4017	.4019	3336	.3977
STATIC	16,154	15,099	10.354	16.019	15.991	15,971	15,959	15,953	15,955	15.962	15,975	15,993	16.014	15,038	10.064	16.092	16, 122	15, 153	15.183	16.212	15.238
P3c5S TJTAL	17.711	17,691	17.630	17,673	17,570	17,67	17.688	17.798	17.733	17,759	17,790	17.825	17,862	17.901	17.940	17,979	19.010	10.049	19.075	13.093	14,104
TURES STATIC	532.795	532,397	531,909	531.591	5 31 . 3 45	531.172	531.081	531.055	531.031	531.429	531.817	532.264	532.824	533.414	534.235	535.647	5 37 - 1 21	538.144	5 35 - 0 99	5+0-120	5-1-25
T_ 4PEKA T ) TAL	926.945	246.778	3+b.700	5.6.057	5 40.554	540.709	0-0-0-0	6+0-2+5	5+7.259	547.746	240.344	543.938	549.535	550.352	551.203	552.801	524.352	355.39n	550.314	557.251	138.264
10126	415.24	( ) ( ) ( ) ( ) ( )	42.50.13	429.33	-45.44	435.07	+33.91	**2.03	56.0400	4+7+2)	449,35	.51.35		17.000	126.47	457.31	10.000	454.14	4.3dete	437.53	435.92
_3ulff=3- TA 40_19	223,53	22 m - 5.5	22.30.34	217.79	21.50.15	21.3.07	211.71	210.34	213,30	211.74	213.40	215. 1/	213.01	220.71	22 4 4 3	232.90	2-1-73	245.17	2.40.53	251.40	2
72.410 TA32.4	367.31	5.5.5	36.5.22	35.9.0+	\$75.12	30 u 01	334.47	300.21	392,00	39.30	395. **	39.00	547.43	54.7.75	* * * * * * * * * * * * * * * * * * * *	394.20	6048	100.00	34 20 45	47.45	27.7
2A 01 Js	7.0734	7. 17-1	7.7671	7.3579	7.4433	7.53.2	7. 6211	7.7050	7.7920	7.877	7. 3520	4.0474	4.1333	4.21.40	4.5072	4.397.4	3,4837	4.5747	3.673.	4. 75 35	7 / 57 - 7
STREAM -LINE		• ^	a e-1	, ,	· rc	v ve		. 40	o	* 67			, ~ , ~	) <u>1</u>	. u		, ,	· «	6		; ~

POLYTROPIC EFFICIENCY	1.0014	•	*****************	4866	9266	.9978	.9962	. 9955	.9863	- 9776	.9687	4/46		P 0 0 0				424	6900	्र जू •्						•				•		;								,	
SENTROPIC P	1.0015	•	J O	1066	• •		ູຕ	T	.9860	.9770	σ,	,	,,	,,,,	, .	,			.8811	# # # # # # # # # # # # # # # # # # #	SPE	•••	•	•	8	. 1828	9	3	2	2	2	::	3 5	. 2638	3	3	2	2 :	2 5	3	
DELTA T IS	. 054	*	Ç	1 10 10 10 10 10 10 10 10 10 10 10 10 10	5	• 054	9	.055	. 056	5	.058	2 :	2	9	9 5	9 5	3 2	120	076	DELTA T	RADIUS OF	CURVATURE	_ ≿	•	2	7	2	#	Ω.	2!	` :	7	2 5	-8-913	9	*	≥!	14.95	2 4	2 4	146.24
PRESSURE RATIO	25	2.	25.	֚֡֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	2	20	20	.20	•20	5	2	5	7	22.	֭֭֓֞֜֞֜֓֓֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֓֡֓֜֓֓֡֓֓֓֓֡֓֡֓֡֓֡	, ,	"	, ,	1.232	N. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10	LES	,	26.61	23.83	21.17	18.63	16.19	13.86	11.62	9.48	7.42	7.5	1.74	- 01	-1.67	-3,25	-4.69	-5, 95	- / - 03	16.36	0
ELAFIVE MPERATURE	565.285	Š					•	-	m	'n	6.3	-	4. 6	•	u .	۸.	-4 .	۰.	067-1	PO.Y. EFF	AMG	HHIRL	37.9	37.7	37.6	37.6	37.5	37.5	37.5	37.5	37.5	25	2000	39.07	39.5	40.3	41.9	43.5	4	U . U .	0 0
LATIVE RE ESSURE TEM	192	40	661	101	200	98	962	117	624	365	96	200	28	523	2 1	, i		Ø (	0 C	. 931	Ą	ပ	1 . 480	14.61	*****	9 .4.83	787.	184.	78 T	+6+·	76.7°	303	3 4 4	.4842	464.	. 4.63	.483	5.483	29 <b>*</b> *	7774	1040
TIVE REL	11		23	n c	ם ינ		5.2	78	23	m	<b>~</b>	m	7.	œ (	36	? ;	. م		200	SEN. EFF.	:	STATI	15.62	16.54	.65	16.69	16.73	15.77	16.91	15.85	10.59	16.93	10.9	5 17.062	17 - 10	17.15	17.19	17.24	17.29	17.55	24 • 71
VE RELA 0 VELO	630	949	662	9 4	707	713	723	733	741	748	10.0	76	760	770		21	773	27.5	787	1.215 IS	20	TEL	13.45	19.43	19.5	19.59	13.64	19.68	19.73	19.77	13.83	19.87	19,92	20.02	20.07	20.12	20.17	20.22	20.28	20.55	6.0.03
E RELATI	. 55	יטי					. 63	***	. 65	. 65	ć.	. 53	/c ·	٥.	)ç.	9	\c_3	0	25.00.0	AATIO E	.,	STATIC	37.1	37.3	37.0	37.9	38.2	38.5	33.0	39.4	39.3	0.0		543.185	1	45.4	47.6	6.64	51.5	53.1	20000
HLAD SPEE	75.	764.	7.4.	7 33	20.00		821.	8 30.	639	9.9	857.	867.	876.	* C	8 95	• • • • • • • • • • • • • • • • • • •	916	726	39 434	PAESSURE	- TEMDE	•	40	20	2	55	5	53.	ô4.	•	<u>ښ</u>	92	פרק	206.134	69	5	73.	75.	۲,		5
10N LOS.	3 8	0	200					00.	00.	5 .01	2 .01	59 . 65	90 .03	*0 · 0 ·	11 .05	20. 02	20.07	60. 77	01.	FORMANDE CRIPTION		0 TA	40	6	; ;	ď	*	~;	;	;	;	<b>.</b>	י א	556.07	٥	Ġ	:	÷	•	ŕ	ŕ.
DH JEVIATION	3 -1.	3 -1.	-1	1	1			7	·1-	0 -1.	.1.	-1.5	I.5	2 -1.0	4 -1.7	D . T .	F-1-0	7 -2.1	****	T40 Per	11.5	7 VI 17	7.65	2/19	333	7. 10	7.37	0 * • .	2.49	7.04	7.33	۵. <del>ق</del>	5, 75	3: 0.01		0.05	2, 25	5.03	24.49	9,43	43 72 43 72
RLL FLOW	· • • • •	-50.0	-50.7		2.7.	117		-57.7	-57.0	-50.1	-53.3	-58tz	-53.7	£. 06-	-59.5	-54.5	P. (F) (F)	-50.3	E/-00- 4	INTGG&A	7	278	2, 53	3	2	· 宋 :	8, 43	9.35	9.58	9. 3ú	0.11	8 - 5 - 3	6. 43 5. 43	464444 434444	8, 93	. 35 3	E 72:	6. 49 3	00.0	1.80 3	? ?
L-ANGL-S	7	~	*	•	•					•			•	•	; *	€.			2 2 0 +4	ATEOM 2	307.6	5010												1637					5.244 ·		
CAT 3LAD	·	7.41-	6.44.		5 17 1		6.00	15.50		7.00-	->5.7	9:00-	-,7.1	5.76-	2.7.	7.74-	7.9	1.86-	0 4	# 1	AT HERE	r	~	` `	. ~	`	_	~	_	_	•	•	•	12 0.	7 44	70	4	<b>1</b> 07	T .	77)	
100.	#1		~,	<b>-</b> (	n V		- =		10	=	1,2	7	<b>4</b>	4	7	#	ã		.83		213	7										7			-		Ī	-			100

4
-
⋖
Ć.
냋
×
٦,

POLVTROPIC Efficiensy	1.0014	1.000	2666.	. 9991	3966 *	.998	. 9972	1966.	.9950	.9872	: R_6.	<b>.</b>	9636	. 5495	.9337	.9837	6748	. 8586	. 6445	. 8293	.8121	
ISENTROPIC P EFFICIENCY E	1.0015	1.0816	2666	1666	1966*	.9979	.9971	.9963	9656*	.9867	- 976	.9691	.958	.9472	.9307	.8993	. 1691	. 8528	.8372	. 8212	. 6832	1 ON T = . 496
DELTA T	. 003	.084	. 084	. 085	. 886	.087	. 088	. 088	. 089	. 091	- 092	• 00	• 636	• 098	.100	. 105	. 109	.113	.116	.119	. 122	DELTA
PRESSURE RATIO	1.324	1.326	1.330	1.333	1.336	1.340	1.343	1.346	1.349	1.353	1.356	1.359	1.363	1.366	1.369	1.373	1.377	1.380	1.384	1.388	1.391	935
RELATIVE TEMPERATURE	568.409	569,357	570.304	571.251	572.204	573,164	574.135	575.1.8	575-116	577.132	578.172	579.236	530.328	561.450	582.507	593.312	535.176	536.+01	537.778	589.211	590.708	2 PO_Y. EFF.=
RELATIVE PRESSURE	20.254	20,399	20.514	20.630	20.746	20.868	20.987	21.109	21.234	21.310	21.389	21.467	21.532	21.600	21.628	21.538	21.445	21.457	21.489	21.511	21.511	EFF.= .932
RELATIVE VELOCITY	618.43	625.64	632 - 14	638.18	643.95	649.60	655.03	660.47	665.96	60.699	679.36	672.56	573.85	675.33	674-11	665.05	655.40	652.63	651.17	649.02	645.49	ISEN
RELATIVE	. 5416	.5478	. 5533	. 55 34	. 56 33	. 55.80	. 5726	.5771	.5817	. 5831	. 5847	. 5862	. 5865	. 2875	.5858	. 57 56	. 5572	5540	. 55.20	. 5593	. 5553	24110 = 1,358
8LA0E SPE E 3	779.4	786.8	794.2	801.4	909.0	6.15.9	823.1	4.05.8	837.7	845.1	852.6	860.2	867.3	875.8	893.8	892.1	9.006	4.606	918.9	926.4	938.2	PRESSURE 24
L033 30£ FF	0015	00 35	.0003	. 3013	. 0015	. 0020	.0027	. 0034	.30.43	. 01.29	.0195	.0272	.0363	10+0.	ch 20.	. 3 \$ 92	11177	1335	1.72	1021	.1795	
DEVIATION INCIDENCE				-2.687	-2.200	-2.465	-2.405	-2.3-3	-2.293	-2.204	-2.25	-2.201	-2.287	-2, 333	-2.405	-2.51+	-2.070	-2.936	-3.201	-1.355	4,903	INTESTATES PEPFORMANCE
RLL FLOW DEVIATION ANGLE INCIDENCE	-+5.221	0000	-46.3+0	-+1 72	-47.342	0+1.2+-	648.74-	D 62.04-	-40.635	860.64-	-69.530	-+4.753	-20.150	-50 - 359	-50.987	-51. +13	-51.392	-52.423	-53.010	-5.3 co+3	-54.339	INTESANT
ANGLES	-5.902	-5-8+5·	-5.634	-5.437	-5.243	937	-4.3.12	-3.954	-3.219	- 2. t. 30	-2.0+3	-1.0 Jb	-1.227	907	404	100	797	1.473	7.150	2.72B	3.033	STATION 7
SLABE-ANGLES SECTION LEAN	-42.577	-43.085	45.537	-+3.935		4.925	C++ - C+-	-42.910	5.341	** 7 * 6 * *	-47.127	7.502	-47.874	3.237	-+8.582	606.6	-+3.215	4.516	6 60 464-	560.0.	-53.376	STAT
-ION	-	~	m		· w	··c		. •0	œ	10		12		*	15		17		5		Z	

FLOW FIELD DESCRIPTION	
STATION O	

•

SPECIFIC - WEIGHT		. 484	****	. 1847	6498.	. 8852	.0853	. 8855	.1856	. 8657	. 1857	. 4857	. 1856	.0856	. 8854	いかのは、	0480.	. 0847	. 0846	. 1846	. 1845
RADIUS OF SURVATURE	-1. AB3	-2.23	-2.684	-3.292	-4.148	-5.397	-7.437	-11.281	-21.009	-82.230	59.701	25, 321	17.462	14.059	12.412	11.985	12.743	15.805	20.686	40.551	316564.766
ANGLES MMIRL SLOPE	16.55	14.88	13.28	11.77	10.31	8.89	7.51	6.14	4.79	3.44	5.09	. 73	64	-1.99	-3.32	-4.62	-5.81	-6,9	-7.89	-6.74	-9.37
ANGL	42.57	42.99	43,33	43.57	43.74	43.83	43.87	43.85	43.76	44.02	44.25	44.48	44.82	45.15	45.83	47.57	49.49	50.61	51,65	52.91	54.51
MACH	.6257	.6198	.0149	.6109	•6076	.6047	•6022	.6000	.5980	.5952	.5927	9065.	.5836	.5867	.5644	.5808	.5776	.5751	.5728	.5713	.5704
OTAL STATIC	16.933	17.047	17.146	17.233	17,308	17,373	17.429	17.477	17.516	17.549	17.577	17,600	17 . 622	17.641	17.660	17.682	17.710	17.745	17.788	17 - 640	17.902
PRESS TOTAL	22,036	22.079	22,121	22.161	22,199	22.234	22.201	22,282	22,298	22,291	22.284	22.277	22,269	22.252	22.246	22,213	22,193	22,194	22,211	52.249	22.111
TURES STATIC	539.343	541.021	541.362	542.780	543.438	544.099	544.043	545-117	545.513	546.349	5+7-139	547.935	548.877	549.517	551.200	553.678	556.550	558.569	560.423	562.553	565.077
TCHPERA TOTAL	531.921	2 32 - 2 95	532.058	333.004	5 83.324	543.610	563.872	384.082	584.241	584.775	535,305	555.881	536.624	537.391	588,564	593.911	533,505	595.225	536.918	394.57b	511.544
1 OT AL	710.37	710.35	705.33	701.27	69.760	695.05	692,52	530.25	588.13	030.40	033.14	661.19	579.43	577.35	675.93	073.43	671.41	669.69	co 3 . 12	667.24	Uo7.97
VELOUITES	40 04	64.40	43.5.43	433.43	+3.2,52	.01.32	47.3° 30	473.14	475.92		476,03	+77.24	473.87	+0 0.24	4d+ 33	16.16	514.43	517.40	523. 35	232.47	5+3. B3
7ERI J	527.55	519.57	513.13	÷0.95	504.21	501.33	444.22	497.79	497.02	49 2, 87	+8 9, 33	+80.02	+0.1.94	47 9 0 07	47 U. 95	45 4 34	+30,13	42 4 95	+14.75	462.23	367.77
RAUIUS	7.4732	7.5275	7.57.33	7.5275	7.6732	7.7319	7.7837	7.8404	7.8932	7.9532	3.0110	5.0716	3.1331	d. 19b2	3.2613	5. 3304	3. 4:13.3	8.4005	8.5614	8.6403	9.7359
STREAM -LINE	-	۰ ۸	s e+7		· •	•	~	. 0	•	4	11	12	1 3	4	1 2	91	17	9	19	20	21

OL AUE DATA

.

POLYTROPIC Efficiency	1.0013	1.0005	9666.	.9991	9866 •	-9985	<b>4266.</b>	9966*	0966	.9877	96.46	.9709	.960	.9492	.9326	9006	.8697	.8515	. 6357	.8191	. 8008	3
ISENTROPIC P EFFICIENCY E	1.0014	1.4005	9666*	.9991	.9985	.9981	.9972	<b>4966*</b>	.9957	6986.	.9783	.9691	•9576	.9461	33285	6460.	.8619	.8426	. 6259	. 5033	.7838	0N T = .134
DE TA T	.122	.123	.123	.124	.125	.125	.126	.126	.126	. 127	. 126	.130	.131	. 132	.135	.139	. 144	. 148	.151	.155	.150	DELTA T
FRESSURE RATIO	1.499	1.502	1.505	1.50 A	1.511	1.513	1.515	1.516	1.517	1.517	1.516	1.516	1.515	1.515	1.514	1.511	1.510	1.510	1.511	1.514	1.518	£6. =•.
RELATIVE	2570.707	571.380	572.374	572.788	573,523	574.278	575.053	575.348	575.263	577.302	578.369	579.264	590.191	591,151	582.151	583.207	584.341	535.550	536.330	568.187	589.233	1 PO.Y. EFF.=
RELATIVE PRESSURE	20.577	20.656	20.738	29.824	20.914	21.007	21.100	21.196	21.296	21,330	21.368	21.404	21.421	21.440	21.404	21.209	21.010	20.950	20.915	20.869	20.793	ĒFF.= .931
RELATIVE VELOCITY	613.21	609.16	69.904	605.56	605.94	607.40	90.609	612.93	617.11	617.14	617.91	618.91	618.77	618,38	615.19	599.36	581.93	574.45	568.26	563.95	248.07	I SEN.
RELATIVE	• 5355	. 5315	+ 5283	. 5275	. 5275	. 52 85	. 23 92	. 5323	. 5362	. 2359	. 5361	• 5365	• 23 69	. 5358	. 5318	. 5169	• 50 05	. 4933	. 4872	. 47 92	• 45 80	RATIO = 1.513
SLADE SPcto	5.767	8 02 . 4	8.07.7	813.1	918.5	524.2	829.9	835.0	8+1.7	847.9	85.0	860.4	867.0	973.7	880.7	888.0	895.8	0.406	912.5	921.7	931.2	PRESSURE RI
.035 50c FF	9921	00,3	. 0003	.0013	.0020	.0025	. მ მ პა	• 00 •	.0053	.0159	. 0259	.0353	16+0.	.0015	.0303	.1191	.1571	.1703	.1905	.2103	.2353	
DEVIATION INCIDENCE	-5.420	-5.303	-4.792	-+. 593	412	-4.254	-* 122	-+.017	-3.941	-3.335	-3.980	-3.390	-3.342	123	-4.149	-** 339	-4.660	-5.018	-2.527	-0.135	-0.034	INTEGRATED DERFORMANDE
ACL FLOM	-30.249	-3100	-32.244	-32,430	-33.293	-3363	-35.331	-35.294	-35.351	-37.090	-37.535	-39.2-9	-38.343	-34.434	-40.043	-40.799	-41.458	-42.203	-43.123	-44.030	-44.35.0	INTEGRATE
ANGLES - LEAN	-6.276	-5.831	-5.378	-4.728	-31939	-3.222	-2.438	-1.697	947	345	. N.	.7 96	1.138	1.450	1.751	2.074	2.339	2.715	2.930	3.210	3.347	<b>6</b> -₩07
LOCAT BLADE-ANGLES FON SECTION LEAN	-25.429	-26.466	-27.452		-27.0-65-					-33.104	-33,755	-34.353	-34.981	-35.411	-35.894	-35.369	-35.838	-37.271	-37.026	-37.895	-38 -132	STATION
LOCAT	-	~	m	•	- 5	٠	~	•	σ	10	##.	15	13	*1	15	16	47	18	61	2 8	ี 5	•

SIATION 9 FLOW FIELD DESCRIPTION

SPECIFIC Weight	6490.	.8852	• 1854	• 1855	. 0857	. 1858	.3860	.0861	.0862	.0862	.8862	. 8862	.0861	.0862	.0858	.0854	6790.	.0847	****	-0842	. 8640
RADIUS OF CURVATURE	-5.625	-7.200	+06.9-	-11.034	-13,824	-17.827	-24.471	-38.527	-93,119	171,739	40.630	21.868	14.706	11.071	8.877	7.497	6.746	6.471	6.595	7.718	20.749
ANGLES HIRL SLOPE	8.54	8.18	7.75	7.27	6.72	6.13	5.50	4.83	4.12	3, 37	2.56	1.71	. 81	13	-1.11	-2.15	-3.26	64.4-	-5.80	-7.24	-8.95
ANGI	45.89	45.97	45.99	45.98	45.93	45.85	45.77	45.67	45.54	45.96	46.35	46.73	47.17	47.59	4.8.47	50.68	53, 17	54.64	56.00	- 57.72	00.12
HACH	.6630	.6585	.6543	.6503	.6475	.5445	.6416	.6390	.6366	.6374	.6383	•6382	.6327	•6275	•6222	•6166	.6105	6589	.6 913	.5956	.5879
ESSURES STATIC													17.787								
P2ESS TOTAL	23.230	23.229	23.22A	23.227	23-226	23.226	23.224	23.22	23, 221	23.275	23,329	23,358	23.291	23.202	23,120	23.032	22.937	22.878	22,823	22, 761	22.683
TURES STATIC	543.273	543.919	544.496	545.012	545.473	545.384	546.325	546.711	547.062	548.012	548.941	549.892	551.125	552.140	553.792	-557.000	560.427	562.669	564.795	-567 42 33-	570.253
TEMPERA Total	590.688	590.746	590.799	590.8+6	590.805	590.919	590.978	591.031	591.078	592.204	593,339	594.344	534.813	595.287	596.344	599.055	6 U 1 · 867	603.651	695.296	507.145	509.338
TOTAL	761.44	756.73	752.47	7+8.0+	7.5.15	741.35	738.9+	730.13	733.67	- 735.1+	730.07	737.33	731.31	726.43	721. **	717.01	712.04	-708.12	703.97	6-38.81	691.50
LOCITIES TANGEN	546.76	544.03	5+1.22	930,34	53=.33	532,30	529.51	525.01	523.65	- 523.45	533.13	535.88	536.65	<b>536.37</b>	240.04	- 55+e-74-	569.95	-944246	543.65	59 64 40	533.67
YERIO	529.94	- 525.55	522.77	-554455·	518.28	-216.79	5152	514.45	513.05		508.61	- 565.39	497.54	44 9-32	478.37		426.73	- 40 9 at	393.01	-37-34-22	344.43
-RADIUSVelocifics	7.5439	7.59+0	7.6390	-5+89a2-	7.7316	7.7791	7.8273	7.8752	7,9259	7.9762	5.027>	- 44644-	8.1333	-60444	6.2451	94964	8.3690	844376	8.5100	8+586a	6. 66 39
- STREAM	-	ru	m	*	5	9 ::	~	· · · • · · ·	<b>~</b>		11	-15	13		15	*	13		19		2.1

FICIENCY	.0014	000.	666	999	966	997	166	99.7	565	CA S	077	9	ď	600	200	200	֓֞֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֡֓֜֜֜֜֜֓֓֡֓֜֜֡֓֡֓֜֡֓֡֡֓֜֡֡֡֡֡		2	3 6	מ מ	8																						
FICIENCY EFF	1.0015 1	.0006 1	266	9666	9984	8266	9966	9959	0951	9852	2755	9652	200	9386	64.00	3076	20.10	7740	1010	200		ın.		SPECIFIC	I HOTEN	.0850	8	•	2	ю.	9 6		8	8	8	8 8	9 6	3 6	. 8635	3	8	8	Ě	D
04 T EF	.139	₩) ₩	∾	2	13	13	13	133	7	. 1			1 4		ų	1	1	9 ;	::	01	<b>~</b> 1	►		RADIUS OF	28	•	3	7	9	3	7 6	68	.80	. 87	23	5	9 6		62	.01	.27	33	8	
RATIO	1.581	• 58	58	58	• 58	.58	5.5	. 58	, G	3	4	ű	, x	7	ï		ה	ָ נוס	ָרָ הַיִּ	֓֞֞֞֜֞֜֞֜֓֓֓֓֓֞֜֜֟֜֜֓֓֓֓֓֟֜֜֟	4	54			ž	7.82	7.72	7.66	2.05	D9 • 0	11.0	5, 07	4.54	<b>6.</b> 00	3.46	2,91	K. 55	36.	52		-1.74	•		•
ELATUP	¥6¢*	31	35	2	27	35		3,1	0	1			ם ט	, ,	9 0	r	<b>-</b>	<b>7</b>	2	- 1	٠ د د	9		ANGLE	WHIN	9.	5.4	5.0	9			9 6	2.7	3.0	3,50	3,57	֓֞֜֞֜֜֜֜֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֜֜֜֓֓֡֓֜֜֡֓֓֡֓֜֜֝֓֡֓֡֓֡֓֜֜֡֓֡֓֡֓֜֡֡֓֡֓֜֡֡֡֡֓֜֡֓֜֡֓֜֡֜֡֡֜֜֝֜֜֡֡֜֜֝	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜	47.17	9.5	1.2	2,8	, ,	
URE TEMP	05 571.	ß	'n	ß	w	w	· w	, ft	Ľ	ی ۱	٤. ١		י ע	· u	, u	n u	י ר	n L	v	ΛI	<b>v</b> 1	ß		HACH	25	. 5514	.6:318	.0630	.6643	υ.	6 6 6 7	6659	. 5693	•6722	6420.	.6761	PA	6666	.6536	.6452	.0374	.6291	6440	
PRESS	20.7	$\sim$	40	თ	0	0	-	ın	1 1	١ ٢	۰,	۰ ۲	) M	) M	"	u c	٠,	ο.	* *	₩, (	N	_		AES	_	. 32	• 32	30	80	52.	ŝ	12	. 20	• 20	. 20	200	7,6	S	17.295	34	. 41	649	n 1	
VELOCITY	589.42	7	۲.	٠	٣.	٠,	4		٦		, ,	, u	, ,	, ~	• נ	۰	• •	•	٠.	<b>.</b> .	•	٠,		PRESSJ	UI AL	3,239	3,229	3,228	3.227	3.226	3.22.5	3,222	3,221	3.275	3,329	3.356	3,281	7.420	23.032	2,937	2.878	2,823	376.6	
4A 24 40	.5132	7	. 5130	3	155	.5177		1256	:	;;	2010	ij	;	10 47	1 6	3 9	1000		7	145+	• +2 15	. 4923		'URE S	4116	43.479	43.4.85	43.393	43.229	#3.0 <i>6</i> 2	CT 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	42.962	42,795	43.445	+4.129	206.44	10.435	P = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 =	210	55,951	58.518	61.239	124 4 24	
SPEED	3	6	7	ដ	₹	29	2		3		3	``	26.2	56		9	0 8	7	χ,	6	12	ž		JCHPERA 1	- A-	.688	.7+6	•799	940	• <del>4.85</del>		2 2 2	.078	.204	•339	446	. 41.5	107	0.26	.367	.651	.29.	11.7	
SOFFE		3	9	00	90	0	2	2	3	;		; ;		2 5		⊋ .	* (	,	γ,	11	~	S.	<u> </u>	1:	ت ت	73 53	23 23	45 54	00 59	71 53	14 29	34	37 53	17 59	FC +/	59	24		73 53	30	0.0	33	4	
GIDENCE	14.14	13.35	13.52	13.15	12.69	12.51	12.40	12.27	12.2	, ,	, ,		10.57			70.01	200	*****	12:01	Ξ.	1 > 11	10.32	•		4101 K	d 759.	\$ 700.	0 /01.	7 755.	3 70te	7.55		3 7öå.	3 772.	6 775.	2 771.	0 //3.	7.00	750	7 749	2 742.	0 734.	1	
NOT THOM	. 301	. 731	. 60.	400.	021.	0/00	7000	: :	600		772			? .	, ,	210	F	0 .	171	•	7,6	• 233		, , ,	ş		42.0	3.9.0	30.0	ر در ک ر	50.1		21.3	20.3	31.8	32,3	ال ال ال	, n	554.4	73.5	7 300	35.2		
AN A	₹ <del>-</del> 5€	33	<b>?</b> - <b>*</b> ?	3e -2	, 96	5- 50	£	100		֓֞֜֝֞֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֡֜֝֓֓֓֓֡֜֝֓֡֓֡֝֡֡֡֜֝֓֡֡֡֜֝֡֡֡֡֜֝֡֡֜֜֜֡֡֜֜֝֡֡֜֜֡֡֡֡֜֝֡֡֡֡֜֝֡֡֡֜֝֡֡֡֜֜֡֡֜֡֜֜֡֡֜֜֜֡֡֡	֓֞֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֡֓֡֓֡֡֓֡֡֡֓֡֡֡֡	77	? •	? ~	7 6	? .	; ;	; ;	? '	٠ -	36 -	17 -4			15.41.0	ď	÷	۲.	'n.	ຕໍ່ເ	÷,	: -		;	;	m.	٠.		514.42		:	÷		•
CTION LE	16 2.	29 2.	53 2.	65 3.	43 3.	52 3	7 2 2	7	4	0 0	35	, ,	;	, ,	• : • :	r c		•	÷ .	· · ·	30	°¢ 3°		RADIUS		.57	. 52	99.	.7	2	45.4	0 0	95	. 4698	å	60.	1		A. 3204	35	45	48	2	
TON SEC	-11.	-12.	-14.	-15.	-15.	.17.		7	0	120			•				2	••>-	***		-54.	1 -24		STREAM	z										4	، ب	<b>"</b>	<b>.</b>	n 4	۰ ۸	. 10	σ		•

i

	•	POLYTROPIC EFFICIENCY 1.0014 .9991 .9991 .9995 .9970 .9970 .9970 .9974 .9974 .9770 .9770 .9770 .9770 .9770 .9770 .9770 .9770 .9770 .9770 .9770 .9770
SPECIFIC MEIGHT		EFFICE EFFICE CONCYC
RADIUS OF CJRVATURE	26.367 -26.367 -26.327 -21.527 -21.527 -21.527 -21.527 -21.527 -21.337 -34.337 -34.337 -34.337 -34.337 -34.337 -34.337 -34.337 -34.337 -34.337 -34.337 -34.337 -37.337	DELTA T 00 I 1 39 1 39 1 39 1 39 1 39 1 39 1 39 1
SLOPE SLOPE	2000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PRESS
ANGLES	5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	### ### ##############################
A CA	6698 71029 71029 7109 7451	11VE REL 230 590 228 590 228 590 228 590 228 590 228 590 228 590 339 594 220 596 231 594 231 594 231 594 231 594 231 594 231 594 231 594 231 594 231 594 231 594
SSURES	17.204 16.947 16.710 15.519 16.270 16.190 16.190 16.100 16.110 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 16.100 17.170 17.170	
PRESS TOTAL	223, 223 223, 223 233, 223 233, 223 233, 223 233, 233 233,	4EL41IVE 768.63 768.63 786.80 803.37 815.64 833.74 833.74 833.74 842.02 842.02 842.02 843.84 851.59 851.59 851.68 851.68 851.68 851.69 851.69 851.69 851.70 873.46
PATURES STAILC	540.417 540.417 535.300 535.300 535.300 535.300 535.000 533.033 533.033 533.033 535.23	RELATIVE AAGA 40 .0598 .0598 .0598 .7222 .7322 .7450 .7419 .7472 .7472 .7472 .7472 .7476 .7414 .7476 .747
-TEMPERAT	300 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	11
۰ پر	**************************************	100 S S S S S S S S S S S S S S S S S S
I = 5	74 75 76 76 76 76 76 76 76 76 76 76	DEVILATION CIDENCE 1 1 4 4 0 0 0 3 1 1 4 4 0 0 0 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		ALL TARK WAS A CONTROL OF THE CONTRO
AE AI U	24 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
440105	7.6514 7.77.47.77 7.77.47.77 7.90.77 7.90.77 7.90.77 9.00.17 9	1100. 1100.
STREAM -LINE	またろい ちらた ちらじまえきん ちらん けんりん	100A1 100A
	187	, i

STATION 11 INTEGARED PERFOAMANCE PAESSURE RATIO = 1.573 ISFN. EFF.= .921 PO.V. EFF.= .926 DELTA T ON T = .149

STATION 12 FLOW FIELD DESCRIPTION

ı		FO
SPECIFIC WEIGHT	00110 0010 00110 0	INTERPRETATION OF THE PROPERTY
RADIUS OF CURVATURE	13.000 13.000 13.000 13.000 13.000 13.000 14.000	DELTA 1 1 39 1 1 39
ANGLES HIRL SLOPE	0.4888999444444444444 0.48694644444444444 0.486946444444444444666	PRESSURF RESSURF 11.55.1 11.55.2 11.55.3 11
ANG WHIRL	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	PRATIVE CO. 10 C.
NO NO		
SSURES STATIC	13.775 14.093 14.093 14.093 14.093 14.093 14.093 15	PRELATIVE 23.004 23.0073 23.0073 23.0073 22.992 22.992 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946 22.9946
PRESSU TOTAL	23.084 23.073 23.073 23.073 22.085 22.092 22.092 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093 22.093	VELATIVE VELATIVE 992.78 992.78 993.1148 9915.29 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78 9915.78
rures static	510.0 0 0 110.	75.14 TIVE 69.00 69.20 69.20 69.20 69.20 69.20 69.20 69.20 69.30 69.20 6
-TEMPERATURES- OTAL STATI	99000000000000000000000000000000000000	
1 AL 1	5.3.3.4.3.5.4.3.5.4.3.5.5.4.0.6.4.6.4.6.6.4.6.6.4.6.6.4.6.6.6.4.6	000 000 000 000 000 000 000 000 000 00
IES	44 43 43 43 44 44 44 44 44 44	ACTIDA ACTIDA ACTIDA ACTIDA ACTIONA AC
VELOCITI TANGE		C
#E AID	4327.74 927.74 927.74 937.16 937.16 937.16 775.03 775.0	
RADIUS	7.7150 7.7548 7.63943 7.63943 7.63943 7.63914 7.99114 7.99114 6.15120 6.1514 6.1514 6.32647 6.32647 6.32647 6.32647 6.32647 6.32647 6.32647 6.32647 6.32647	ADDE-ANGLOS OF STREET OF S
STREAM -LINE		100 A 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

STATION 13 FLOW FIELD DESCRIPTION

. <del>.</del>	20.5		20	n P	e e	<u> </u>	*	وِ	و.	<b>.</b>	ب م	9 4	M	•	Ņ	•	10		•	POLYTROPIC PEFFICIENCY	.9742	02/6.	7505.	6.706.		9556	.9487	. 9450	2556.	6126	4116	2969	.8826	. 8587	. 6191	. 6001	-7835	• 7654	7444
MEIGHT	.0822	280.		7 4 5	460		. 0.85	. 885	. 065		.050			180	100.	. 883	.000	.082	. 862	ISENTROPIC EFFICIENCY	.9726	2016.	96/8	7696	120C ·	.9515	.9455	.9415	1626*	.9178	9000	8888	.8752	.8414	.4879	.7878	.77.02	.7511	7203
CJRVATURE	-5.196	-5.854	-6.666		-16,704	-12,731	-15.175	-18.824	-21.158	-24.406	-27.534	24.727	-37.589	-33,392	-35.281	-40.630	-59,363	-223,782	76.314	DELTA T	.139	.139	139	P C P V	- F0 -	.139	.139	. 140	241.	***	. 1 40	94	.150	.155	.160	.164	.167	.171	176
SLOPE	-2.23	-2.39	-2.51	00.00	-2.56	-2.45	-2.28	-2.05	-1.77	-1.47	-1.15	6	100	. 10	.36	•63	. 82	• 91	. 88	PRESSURE Ratio	.56	92	1.559		ָ טַ טַ ע		.54	\$2	•	1.547	1.747	1.044	ķ	1.539	.53	53	53	1.528	E S
WHIRL SLO	17.58	17.	,,		17.	17.	17.	17.	17.38	17.	17.	:,		17.	17.	18.	18.	18.	19.	RELAFIVE TEMPERATURE	590.566	9*.40	9,49	D 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000	0.978	1.331	1.976	702.2	3.339	****	5.287	248.0	9.32.6	1.867	3.551	5.296	7.145	27.0
Şç	96	.6838	.6714	0000	6367	5.550	. £ 166	.6094	•6065	•6046	.6031	o u	5,5975	'n	S	.5963	.5995	.6040	•6098																		1		
STATIC	16.596	16.775	16.945	17.103	17.381	17.495	17.589	17.664	17.721	17.763	17.793	17.010	17. 811	17.795	17.765	17.718	17,651	17.560	17.446	RELATIVE PRESSURE	22.944	22.9	22.9	***	2000	22.7	22.7	22.6	22.7	22.7	7.52	2000	22.6	22.6	22 • 5	22.5	22.4	22.4	3.00
TOTAL STA	22.944	22.	22,911	260.22	27.823	22,773	22.722	22,689	22,769	22,729	22.739	22 600	72,554	3 3	22,561	Ñ	22.434	ñ	Ħ	RELATIVE VELOCITY	756.90	783.39	770.36	107.00	743.92	722.26	712.15	704.51	761.97	700.59	699.55	695.23	694.67	694.45	695.15	697.65	8	8	1
STATIC	38.749	40.555	42.266	770004	45.31	48.320	49.561	50.493	51.913	53.208	554.333	55.1 UI	77.1.1	50.00	62,371	63.473	65.020	66.175		RELATIVE MACH NO	. 69 <b>68</b>	. 6638	• 67 14	65.65	. 0463	. 62 60	. 6165	· 68 94	• 60 65	• 60 46	.6031	. 50 e	5265	. 5959	. 5950	. 5963		. 60 40	80.60
OTAL STATE	590.688	97.0	662.3	010	6.00	870.0	1.031	1.078	12.204	13,339	サナ かっかっ	510	7020	9-0-6	1.967	3.651	15.296			BLADE SPEED	0.0	0.0	9	•	•	9	0.0	0.0	0.0	0.0	9		0.0	0.0	0.0	0.0		ت. •	ć
AL FO	36		e d	6 6	26	3.5					9.59									LOSS		3	200	5 6	Λu	9	6	6420.	9	9 (	9 6	10 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	•	0	.0583	. 0565	0552	• 0545	57 116
N - 10T	79.0	9	22	2		7,	. 2	9 70	70	o 79	<b>5</b> 9			יי פר פר	. 69	3 69	4 79	2	9 71	DEVIATION ENCIDENCE	1.351		1.364	1.383	1.416	1,495	1.524	1.561	1.595	3,	1.651	1.680	1.682	1.677	1.672	1.671	\$	1.688	1 3 40
D TANGEN	2+0-7	٠	231.9	ė į	221.5	;	ં તં	210.	20	209.	209	ָ פֿיל פּיל	2 6	210	4	216.	221.	227.	235.	FLOW DE	47.585	7.539	6.523	2000	0001	4.4.0	7.378	7.358	7.385	96+	1754	07	7-550	7.033	7.788	16.839	16,378	8.782	920
-#5.210	759.65	740.93	734.61	٠.	7111627	F. 0. 0. 0.	679.64	672.42	06 9. 90	66.6.43	667.31	<b>;</b> ,	00 3: 03	; ;	: 4	66 3. 35	٥	;	675.70	N X	j	921	361	* 5		1		-3,273 17			801	İ	1-150 - 1		1		ı	.935 1	KA2
50 <b>104</b> 2	7,7230	757	162	2	7. 9015	7.9467	7.9801	5.0212	8.0633	<b>ð</b> . 1402	6.1500	0 1 7 6 0	3. 246 t	A. 7343	.6, 3612-	8.4295	8.4798	9.5289	8,573€	BLADE-ANGLE	ا خ	ا د	φ.	! 		15.955		1	_	7.5051.		ĺ	, ni		•	•	1	٠	
LINE			m).			, , !	. •0	. 6	10		12		: • •			1.0	19			LOCAT 3L	*	2 16.				15	8 15.		•	-	12 15.	i	1		T	18 15.	T	20 17.	

<b>∴</b>		٠.		•	•	*	•			<b>.</b>		Ď.	97	·	•	m	Ŧį.		. ŗ	J (	<b>10</b> (	ō	<u>ر</u>	•		POLYTROPIC	EFFICIENC	.9687	5786	9537	. 9501	*946*	.9393	.9316	.9237	9186	9089	. 8935	.8827	8778	6730	86.22	8326	. 8033	7455	6607	7523	7264	7 6 7 .
SPECIFI Weigh	-			9		8	-			9	0	8	800.	8	8	2	8			3	•	2	8	•		SENTROPIC	FICIENCY	.9582	5756	9056	0276	8E76	9355	.9274	.9191	9137	-9442	8878	.8755	4783	M. C.	45.4	A 2 2 5	7015	7736	7554	100/-	7000	7017.
RADIUS OF CURVATURE	10 34	747.07	11.0520	18.345	19.651	21.170	22.967	20.400	301.62	*1.7.72	20.636	34.545	38.476	42.553	47.407	54.841	63.374	77.350	444	****	145.502	263.	1070.660	-610.607		LTAT	# NO	.139	140	0 11	139	139	139	139	55.1	1160	142	144	44.5	147	41.	-	7.7	64.	1	101.	,101	1	•1/2
SLOPE		67.	7	-3.90	-3.69	-3.47	3.22		20.30	-2.00	-2.34	-2.00	-1.66	-1.32	- 99	68	95.4	12	4 4	•	• 39	. 63	. 86	1.06		PRESSURE	RATIO	55	L	1	25	7	53	53	5	2	3	5	5	, 5	, 0	, :			֓֞֜֝֝֜֜֜֝֓֓֓֓֜֝֟֜֜֜֓֓֓֓֓֓֓֜֜֜֜֓֓֡֓֡֓֜֜֜֡֓֡֓֡֡֡֡֡֡֓֡֓֡֡֡֡֡֡	,,	1,514	ij	ĭ
ANGLE WHIRL	•		•	ż	ผ้	2,5		•	ָ ה	•	? 5•	٠ ۳	4	1 5.	3	e.				ň	ķ	ŝ	ž	3 6.33			MPERATURE																				605.296		
C NO	į	9 .	<b>+</b> 90.	.532	.530	5.78	500		• > 10	.514	.511	.511	.512	.513	.513	.514	4 1		0.00	*176	.513	.513	.512	.512		IVE	RESSURE TE			f -	• •	Jal	σ		. 0		9 -	. 4	9 0	•	<b>+</b> 1	0.9	٠.	<u>0 L</u>	n :	5 :	22.340 6	<u>~</u> :	0
SSURES STATI	:	9	15.	18	87	4		•	18.	18.	÷	18.	10,	18.	18.	15.	•	•	9	13	97	18.	7			a	FLOCITY PRE	đ	3	<b>,</b>	T 0	מי	2 +	•	15	1 0	U +	. 0		0 4 - 4	0 0	<b>9</b> 0	r c	2.5	2 !	ι .	22 94	ω.	
PRE TOTAL		. 0.7	2.17	2.74	2.71	67		00.0	2.53	2.45	2.41	2.45	2.42	2.42	2.43	2.43		? .	040	2,37	2,35	2.33	2.30	22,279		•	_			• 220	• 629	270	610					200			100	200	\$ D C	000	500	605	909		
TURES STATIC		28.7	29.0	59.3	59.5	0.00		* * * *	61.0	61.5	6119	65.3	63.9	64.9	65.2	10		•	9	7.1.3	73.5	75.2	77.0	579.207		Ç	14C+ 40	7	3 !	50.	•	. נ	200			ָה ה ה	16.	7	10.	10.	ָּהָ בּי		יין		10	. 51	. 5133	.51	.51
-TEMPERA Otal		90.6	90.7	90.7	9.06	1	2 0	5.0		91.0	91.0	32.2	93.3	94.4		26.2	•	0.0	93.0	01.8	03.6	9.50		000330		10 A 19	SPEED	•	•	• •		• •	•	• 6	•	•	<b>.</b>	•		ė	<b>.</b>	ה	•	Ď	ė	ċ	0.0	ċ	Ö
TAL		£9.	• 2+	3.31	.63		200	10.0	5.51	1.21	66.0	3.17	649	0,70	0	2.2	9 (		.23	5.53	5.85	9	0	7.31		-	CE SOEFF	Č	•		•	•		•	•	•		1 .	.12	7			60.	60	. 0	80.	00	•	· 0 ·
ITIES			ታሪ	23	7		ר י	0	ም	\$	91	-	~	1		+ 4	2 :	ž.	30	93	93	7	. ~	00 CE CE		11010	INCIDEN	ſ	•	۰,		•	٠,٠	in	<b>.</b> (	•	· .	• •	i	•	N.	۲,	٠ ن	N.	٠.	ດໍ່	2.705	~•	~
VeLOC		.05	909	9 26	77		22	55	59 5	.35 5	4 61	5	73				? :	ر د .	47	55	38 5	4	7 (	,		<b>.</b>	ANGLE	•	:	Ç.	Ť.	, i		•	, (	,		2	,		5	5	2	7	, J.	٠٠,	5.319	۵,	. 32
US TERI		3 521	910	•	2	•	210	0 007	3 002	196	594	or or	, 5				00	2	0.00	200	300		3 5		E DATA	e. Q	LEAN	,	- I. 024	375	922		(51	* O C I	5 db	510	1004	0 m + . I	354	295	1.38	1 41	157	255	421	031	833	+16	
RADI		•	۲.	^		• 1	•	70	ີ	٠,	•	. =	? =	. •	; •	• (	•		٣.	٣.			, 4	0000	- 51	,	SECTION	7	\$	.83	2	5	ţ.	3	77	7	£ ;	2	.33	.78	.3	۲.	2	.81	8	38.	3.112	3	ŝ
STREAM -LINE		-	2	M	4	<b>†</b> 1	^	•	~	<	σ	•	? + • •		1 .	? .	*	15	10	17	*	•	4 (	90		6	-10'A			~	m	\$	<b>"</b>	ا م	_	<b>4</b> 0	σ	10	11	15	13	7.	1	16	17	18	19	20	27

FLOW FIELD DESCRIPTION	
STATION 15	

	; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	POLYTROPIC	.99472 .99472 .9374 .9379 .9185 .9983 .9919 .8916 .8548 .8516 .8516 .8516 .8516 .8516 .8516 .8516 .8516 .8516	7406 7234
SPECIFIC NEIGHT		. 8869 SENTROPIC FICIENCY		
RADIUS OF CURVATURE		-33.90 DELTA T ON T	*********************************	.171
ANGLES HIRL SLOPE	111111111	v 20	11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500 11.500	1.507
MACHANG NO WHIRL	64926 0000 64917 0000 64917 0000 64918 0000 64795 0000 64717 0000 64717 0000 64775 0000 64775 0000 64775 0000 64775 0000 64775 0000	3 0.0 CLAIIVE PERATUR	5990 5990 5990 5990 5990 5990 5991 5991	607.145
10	110 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OOG SELATIVE	22, 661 22, 577 22, 573 22, 573 22, 573 22, 148 22, 129 22, 129 22, 129 22, 129 22, 133 22, 129 22, 133 22, 133 23, 13	-
TOTAL STATE	22.666 22.666 22.666 22.666 22.666 22.667 22.667 22.667 22.667 22.667 22.667 22.667	22.144 22.144 RELATIVE VELOCITY	577.29 577.29 577.20 577.20 577.20 577.20 567.20 567.20 567.30 567.30 567.30 567.30 567.30 567.30 567.30 567.30	
TJRES STATIC	563 563 563 563 563 565 565 565 565 565	Season Andrew An		474.
TEMPERAT	500 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	. m		000
OTAL	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~			
ALLOCITIES TANSEN T		DEVIAT TRICIDE	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
RIO	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	ν α 10		0.00
RADIUS	7. 6409 7. 7139 7. 7139 7. 7139 7. 6635 7. 6635 7. 6635 7. 6635 7. 6635 7. 6635 7. 6635 8. 6633 8. 1734 8. 1734 8. 1734 8. 1734 8. 1734 8. 1735 8. 173	LAGE BATA		69 61
STREAM &		THE RES		77

SPECZTIC	P. OF	2060	.0901	. 6961		5000		J. 10	40.0	2644	1683	. 689	.0838	. 1666	. 86 84		. 1877	.1675	. 1572	. 8369			SPECIFIC		2068	-9902	1860°	3068		\$ <b>6 6 6</b>	2688	9688	1698	2691	1691	620	8688.			7000	5200		. 6669
RADIUS OF CURVATURE		1160.356	622.714	448.557	366,245	321,255	292.469	200.000	248.555	385, 371	333, 857	374.766	.35.512	524.789	661.887	689.227	1310.289	2251,112	5418.267	0.00			CIDYATURE			90.0						0	0.00	9.88	0.00		9.0						0000
ANGLES		- 03	. 65	08	60 •	. 11	- 12	10.14	12			50	90.1	07	- 05	- 04	03	02	01	00.0		(	.ES		00.0	-	60	- 00	60			- 01	01	81	01	91	10.	87	In .	5			00.0
H P P P P P P P P P P P P P P P P P P P		0000	•	0	0	-	-	<b>&gt;</b> •	<b>9</b> C	•	, C	Э Ф	•	0	0	•	0	0	0	•			WHTD! SID	1	0.0	00.0	0	0.00	00.00	) )		9 9	0.00	00.0	0.00	0.00	0.00	5 C	0.00	00.00			
A CH	t v	.5044	.5015	. 4987	• 4956	9684·	6294	10/5	7,4,7	5524	7074	4729	4.750	.4772	.4764	.4754	54250	.4738	.4733	.4728			2 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2	• 5 0 8 0	.5053	• 5 025	.4995	1961	2054	7.454	4725	.4719	.41.33	.4710	.4731	4752	.4773	+92+	*6/5	0224	. 732	.4720
URES	0 0 0	19 020	•	•		•	•	•	•							•	_		•	_			RESTA	-	9	9.00	9.00	9.00	8.6	بر 19 م	90.00	6	9.08	9.00	9.00	9.00	9.00	200	9.00	00.6	3 6	,	19.000
PRESSURES	22.66.1	22.620	22.577	22,533	25.487	22,394	22.299	23 463	22.145	22,124	22.120	22,150	22,179	22.209	22,136	22,182	22.167	22,160	22,152	22.144			TOTA, ST		99	.62	57	53	3	7	,	1	13	12	. 12	. 15	17	20.	13	2	2 +	1	25.144
TURES	462.012	562.362	£2.7	63.0	63.4	64.1	96		900	,	9	5.69	69.7	70.5	73.2	76.0	77.8	79.5	581.327	83.4	•		UREST	31.4	561.912	562.262	562.616	562.371	563.338	564.030	104.10 104.10	566.004	567.147	568.300	569.289	569,525	569.763	570.557	573.221	576.045	5// •665	564 252	583.485
TEMPERATURES-	10-11	590.746	90.7	9006	8. 8.	6.06	7°07	7	200	2 6	2 4	9446	35.2	96.3	0.66	11.8	03.6	05.2	97.1	09,3			TOTAL STATES		598.668	590.746	590.799	590.846	590.885	990.919	594.034	591.678	592.204	5 3 3 3 3 3 9	194.344	534.613	595.247	596,344	599.026	581.867	3 (3,651	107.475	509.338
SCRIPTION		589.24	ø	n	~	► •	Ωı	n u	Λu	ΛĽ	۱ u	٠.		···			ംവ		'n		CRIPTION		1014.	5	7	•	~	רים	0,	• 7		) m	•	m	m	D	•	• •	-	N	551.6	• •	562.57
IECU DE	ון 1	000	9	0	0	0	· •	<b>5</b> 9	<b>-</b>	> €	2 0		•		0	0	0	0	3	0	FIELD DES		LOCKTIEN-: TAMESE	25	Ф	9	O	0	0	0 1	7 C	ď	0	0	0	<b>¢</b>	0	0	0	Θ:	00.0	<b>&gt;</b> <	0 • 0 • 0 • 0
16 FLJW F	2 3	589.24	ė	ò	Ġ	å	<u>،</u> ۱	٠,	, ,	, w	, ~	, ,		4	: -:	d		-	å	å	17 FLOW (	•	**************************************	2	'n	÷	ċ	÷	•	÷.		5 ~	M	m	ĸ	ċ	'n	å,	÷	Ň.	: .	• •	362,57
STATION	4	7.6738	.718	. 753	. 901	344	900	•	100	6 0 6 7		177	227	278	330	302	430	463	544	600	STATION		340195		2	• 67	7.	. 75	8	5	•	7 6	20.	. 07	. 12	.17	25	23	۳. ۳	9	7 4	, u	6.6030
STREAM	-	• ~	m			•	<b>►</b> 1	<b>5</b> 6	•	2 + 4 +	• •	1 F	9	. 6	10,	17	18	-1	<b>9</b> 2	~			STREAM	2 N T 1	41	~	m	3	<b>S</b>	۰ م	- 1	o 7	10	11	12	₩¥ ···	7 7	<b>5</b>	16	2.	01		2.5

· J
7
ž.
å
Ö
Ŀ
Y
T.
_
~
0
-

-ANGLES OUTLET			ANGLES		
LEAN-A	17.00 17.00		LEAN-AI Inlet	- 89.941 - 35.794 - 33.475 - 33.475 - 35.786 - 25.788 - 25.788 - 25.788 - 25.788 - 25.788 - 25.788 - 26.788 - 26.788 - 26.788	-13.537 -9.867 -2.126 -2.126 -2.126 -6.699 14.395 28.926 36.926 46.652
N-ANGLES OUTLET	- 11.016 - 112.929 - 15.163 - 16.243 - 17.263	1119 1119 1119 1119 1119 1119 1119 111	ON-ANGLES	77.74.844 77.844 77.844 77.844 87.844	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
SECTION-ANGLE	-62.667 -62.601 -62.601 -62.736 -62.736	- 6 6 3 3 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	SECTION	46.617 47.273 47.273 46.736 46.315 45.364 45.641	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
36LTA . H/U**2	44666666666666666666666666666666666666	0.000000000000000000000000000000000000	DELTA H/U**2		
REL V RATIO	8 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6692 6692 6694 6694 6694 6694 6694 6694	REL V Ratio	. 7311 . 7325 . 7160 . 6925 . 6603 . 6695	65527 65527 65527 65527 65527 65536 65536 65536 777 777 777 65536 65536 777 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 65536 77 77 77 77 77 77 77 77 77 77 77 77 77
DELTA P ON A	<b>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</b>	00000000000000000000000000000000000000	DELTA P ON 2	98789	
3-0 D FACTOR	# G G G G G G G G G G G G G G G G G G G		3-0 D FACTOR		
2-3 D FACTOR	50 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	64444444444444444444444444444444444444	2-3 D FACTOR		. 5119 . 52159 . 5220 . 5220 . 5220 . 5309 . 5499 . 5455 . 5455 . 5456 . 5456
LOSS		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	LOSS	. 0946 . 0970 . 0999 . 1089 . 1195 . 1466	. 1520 . 1594 . 1594 . 1591 . 1553 . 1156 . 1110 . 1110 . 1110
UE VI A	113.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	11.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	DEVIA -TION	7 . 2 3 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
INCID	66 111 112 123 133 133 133 133 133 133 133	100.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	INCID		DOMESTICATION OF THE PROPERTY
I VLET M. MO	3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2000 2000 2000 2000 2000 2000 2000 200	INCE INCE INCE INCE INCE		
OUTL_T KASIUS	0 10 0 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	OUTLET I	7.0460 7.0792 7.7193 7.7512 7.512 7.465 7.4912	7.34 c.134 c.134 c.136 c.136 c.146 c
INLET	7 9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		STATOR INLET RABIUS	20 20 20 20 20 20 20 20 20 20 20 20 20 2	4 6 7 2 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
LOCAT		72444444444444 193	L00AT -10N	まちまみららてめ	

MAKE AND BOUNDARY LAY R BLOCKASES (PERCENT)

	14 15 16 17 9.0 11.9 12.8 12.9 1.0 1.0 1.0 9.0 11.0 12.8 12.9	
	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	7.0	12 1
	4 6 4 4 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ASS
	7.00 7.00 7.00	6.0
	24. 3. 3. 3. 3.	V = R S
	7.0 7.0	(S C)
•	5.7 6.9	ION
	0.0 11.9 9.2 b.7 7.6 1.3 .2 .5 .3 0.0 0.0 12.2 9.3 0.9 7.8	CULAT
	4 . S	f CAL
	0.0 1 1.0 1	-
	040	0
	0 . 0 0 . 0 0 . 0	SUMMARY POINT NO. 1 THE CALCULATION IS CONVERGED PASS 21
	4000	744
	STATION - HID BLUCKAGE U DIST FACTOR 1 INT BLUCKAGE 0	ENDS

TEST POINT TITLE = 203221315260

FLOW = 14.08 SPLEU = 12214.9 PRESSURE 2ATIO = 1.514 ISENTROPIC EFFY = .4387 POLYTROPIC EFFY = .8478 DEL T/T = .1493

!

-

## 4. PHASE II WITHIN - BLADE ANALYSIS (70% SPEED) TEST POINT 208240215670

-LINE	21.7.7.0		STATE OF THE		1040	7.10EC-	11333CG	2000	MACH	STA	F. C	PANTIIS OF	SPECIFIC
1	3	HERID	TANGEN	2	TOTAL	STATIC	TOTAL	STATE	2	WHIRL	SLOPE	SURVATURE	MEIGHT
	. 068	ૄ	-	232.71	18.6	14.2	4.69	5	.2084	•	26.93		1970.
۱ ۲	6.2267	232.71	9.00	232.71		514.233	14.636	14.2.48	-2084	e e	19.79	0.00	-
m .	303	ů,	•	232.71	9:0	14.0		Si	1000	<b>&gt;</b> c	10.03	2 2	, .
e u	700	: .	•	232.71	18.5	14.2	69.4	2 0	2084	9 6	16.30	: 2	44.0
<b>.</b>	847	: .:	9	232.71	10.6	14.2	4.69	25	.2084	0	15.13	2	. 0741
~	999		•	232.71	18.6	14.2	69.4	25	.2004	•	13.96	2	. 0741
•	151	å	•	232.71	18.6	14.2	<b>4.</b> 63	52	.2084	0	12.78	2	14.0
•	303	å	•	232.71	18.6	14.2	69.	25	.2004	9	11.61	2 :	1940
0 7	453	å	•	232.71	18.6	14.2	69.	52	1902	8	10.44	2 :	K#\D.
	603	សំ .	•	232.71	10.6	7.67	600	52	****	<b>P</b> •	7.6		74/0
	753	ů,	9 0	232.71	0.01	7.41		C K	****		7. 67	2	10761
	306	٠.	, D 6	222.71	0 4		F 63	, ,	48000	•	5.97	2	19.41
		: .		242.71	8 4		69	) K	2000		4. 87	2	. 8742
91	366	: .:		232.71	18.6	14.2	69	23	.2084	0	3.86	2	. 8741
•	964		9	232.71	18.6	14.2	4.69	25	.2084	•	2.91	2	. 6741
	645	: *	9	232,71	18.6	14.2	4.69	25	.2084	•	2.04	2	.8741
-1	. 793	å	•	232.71	18.6	14.2	4.69	25	.2004	•	1.25	9	.0741
20	941	å	•	232.71	18.6	14.2	4.69	25	.2064	0	. 56	2	.0741
<b>21</b>	. 896	å	•	232.71	19.6	14.2	4.63	. 25	.2084	0	90.0	2	.0741
	STATEON	2 FLOW	FIELD DE	SCRIPTION									
,	 												
STREAM	RADIUS	;	ELOCITIES		TEMPERA	ATJRES	PRESS	SURES	HACH	ANG	LES	RADIUS OF	SPECIFIC
***		MERIO	TANGE	TOTAL	OTAL	II	TOTAL	Ľ	2	MHIRL	SLOPE	CURVATURE	EICH
-	6.3746	250.93		_	18.6	13.5	14.696	=	.2249	•	29.83	Ñ	. 1731
~	514	å	•		18.6	13.4	4.69	18	.2259	•	19.64	3	. 1731
m	653	'n	•	_	10.6	13.4	4.69	7	.2268	•	16.46	io i	90 LO.
•	190	•	9	_	18.6	13.3	4.69	4	.2277	•	17.23	<u> </u>	98/80
· •	927	٠.	9	-	18.6	13.3	60	7	48224	•	10.03	2 0	
م ۵	200	٠,	, q	-	10.01	700	, 60 J	9 ¥	2224	<b>,</b> 4	13, 71	. 2	82.4
. «	MM	: .:	0		18.6	13.2	69.4	9	.2305	0	15.51	Ñ	.0738
•	194	: .:	9		10.6	13.2	4.69	16	.2309	•	11.30	ሟ	. 6737
10	691	ċ	Ö	-	18.6	13.2	4.69	12	. 2313	•	10.09	N,	1878.
#:	\$ .	ė.	Ö (	•	9.0	13.2	4 . 69 6 4 69	14.156	22315		0000	₽ ≤	0737
71		: .				700		;;	6.66	•	9	2	. 8737
? <b>.</b>	7	: .	9		18.6	13.2	69	19	.2309		5.30	*	.0737
<b>15</b>	268	•	•	_	18.6	13.2	4.69	97	.2303	•	4.14	١٠	9069
16	402	ķ	9	•	16.6	13.3	69.4	9:	.2293	å (	9° 00	ŭί	67736
	537	٠,	•	_	10.6	13.3	69	7	1922*	- (	1.91	2 4	
<b>5</b> 0 0	8.6736	25.65		252.65	516.555	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14.696	14.161	2245			\$24.41-	6220
) C	9	: .	2 0		18.6	13.5	69.4	20	-2221		-1.07	2	.0739
- 21	9	244.63			16.6	3.7	5	12	.2193		-1.91	#	. 8739

; į .0731 SPECIFIC - HEIGHT . 0735 . 0735 . 0735 . 6730 0727 0727 0727 0727 0727 0728 CURVATURE... NEIGHT RADIUS OF S -63.621 -126.728 -236.261 -236.261 -1812.623 -1853.337 -1853.337 -131.673 -131.673 -131.673 -131.673 -131.673 -131.673 -131.673 -131.673 -131.673 -131.673 -131.673 -14.942 -16.942 -16.297 -16.297 65.587 39.284 32.261 30.173 30.173 36.793 36.793 36.793 44.917 59.223 44.344 143.444 . 19.55 19.55 15.59 20.54 110.38 1112.23 112.24 112.24 112.24 113.24 11 --- ANGLES---HHERL -SLOPE HHIRL **|** HACH MACH ---PRESSURES---13.996 13.996 13.996 13.996 13.996 13.996 13.996 13.696 13.696 13.696 13.696 13.696 13.696 13.696 13.696 13.696 13.696 13.696 ---PRESSJRES---14.696 512.653 512.553 512.553 512.6615 512.09 512.09 511.99 511.966 512.516 512.52 512.52 512.52 511.032 511.032 511.032 510.057 510 --TEMPERATURES----TEMPERATJRES--TOTAL STATEC 516.688 518.688 518.688 518.688 DESCRIPTION 295.15 295.15 300.72 300.72 300.72 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 312.65 2271.02 2772.03 2772.03 2772.03 2772.03 2773.0 FIELD DESCRIPTION TOTAL TOTAL ----VELOCITIES-----VELOCITIES-FIELD FLOH 205.00 20 271.91 272.91 272.93 272.93 272.93 283.93 285.93 28 # REO ~ \*\*\*\*\*\*\*\* \$07441G STATION 6. 6016 6. 7270 6. 9515 6. 9515 7. 2207 7. 4634 7. 9639 7. 9636 7. 9636 9. 9236 9. 6701 9. 9213 6. 8667 7. 3256 7. 3256 7. 3256 7. 5498 7. 7711 7. 9919 7. 9919 7. 9919 8. 4318 8. 4318 8. 6524 8. 6524 RADIUS RADIUS į STREAM STREAM \*\*\* 3\$2 # 16 **\$24** 

RELATIVE TEMPERATURE 576.563 5502.723 5502.723 5504.967 5504.967 5501.197 5503.341 5503.341 5503.341 5503.341 6605.393 6611.400 6613.322 6613.322 RELATIVE PRESSURE RELATIVE VELOCITY 889.99 904.43 933.47 947.92 947.92 947.92 947.92 1006.34 1108.04 1108.70 1108.70 1108.70 11110.76 11110.76 RELATIVE MACH NO . 7392 . 6122 . 6825 . 6845 . 6645 . 6915 . 9152 . 9275 . 0840.0 0854.9 0854.9 0853.4 0912.3 0912.4 DEVIATION INCIDENCE -70.953 -71.9659 -71.671 -71.6 REL FLOM ANGLE DATA 3LADE-ANGLES SECTION LEAN Br. ADE LOCAT ----i

POLTTROPIC EFFICIENCY

ISENTAOPIC EFFICIENCY

\_

DELTA ON T

PRESSURE Ratio

SPECIFIC MEIGHT RADIUS OF CURVATURE 6.199
6.251
122.0562
136.951
136.951
14.069
-1.16.069
-7.069
-7.069
-7.069
-7.069
-7.069
-7.069
-7.069
-7.069
-7.069 222.32 221.13 110.13 110.13 111.15 11 ---ANGLES---WHIRL SLOPE 2002 2002 2002 2003 .3058 .3069 .31415 .31416 .31416 .3150 .3150 .3150 .3150 .3160 .31 ---PRESSURES---116.917 116.932 116.932 116.9932 117.0117 117.0117 117.117 117.222 117.446 117.446 117.633 117.633 117.633 117.633 117.633 --TEMPERATURES--TOTAL STATEC 5540.121 5540.121 5540.122 5540.122 5540.122 5540.122 5540.122 5540.122 5540.122 5540.122 5540.123 5540.1 346.13 3359.00 3359.00 3359.00 3359.00 3359.13 3379.00 3379.00 3379.00 3379.00 3379.00 3379.00 3379.00 3379.00 3379.00 3379.00 TOTAL -----Velocities-Merio tangen STATION 5 RADIUS STREAM -LIME 

DESCRIPTION

FIELO

FLOR

ı

ļ

197

POLYTROPIC EFFICIENCY	7696	. 9895	2686	2000	1000	1414	9886	3616	1116.	9998	. 9543	224	9329	.9817	****	.0670	- 1877	. 6478																					
ISENTROPIC PO	***		- 3696		1000	1010	2616		.9795				9515	.8992	!			428	* 1246	* **	SPECIFIC	HEIGHT		7					700	4444		7			•	. 1107	- 0867	-	
DELTA T 13 ON T -EF	. 041	. 842	245	7	200	7 4	1	. 645	970.	****	. 053	851		0.00	. 061	. 063	. 065	• 067	690.		RADIUS OF	CURVATURE	4.382	5.328	6.710	N78.0	16.349	25.669	49.313	215.527	27.74	-37.784	044.00-	-24.736	-24.194	~	-31.954	100 000	742428
PRESSURE RATEO	1.151	1.152	1.153	•110	- 00101	1110	1.162	1,165	1.165	1.172	1.176	1.160	1.105	1.195	1.200	1.205	1.209	1.213	1.216		ANGLES	SLOPE	27.37	25.13	22.66	77.12	15.53	13,28	å.	5. 71 6. 55		2.51	. 65	-2.74	. ~	-5.54	-6.67		
relative Temperature	9.229	561,268	3.164	55155		900	12.354	16.21B	16.393	. 299.90	10.593	2.323	576.403	150	1.284	613.452	15.554	7.591	20.168		ONF	WHIRL	7	31.	ģ	*	28.	27.	27.	27.	27.	27.	2.5	28.	=	31.	32.	35.	
RELATIVE RE PRESSURE TEM													24.936 60								MACH		3 .3799	•	3858	•	• •	•	•	•	• •	•	5 .4633	• •	•	•		•	****** 7
																					PRESSURES	STATI	16.68	16.53	16.48	16.45	16.36	16.	16.	16.	4	16.	16.31	7 1	16.37	16.	16.43	16.40	10.4
E RELATIVE VELOCITY		788.	883.54	919	920		872.25	48.5	969	903	911.97	920.	928	9670	948	955,57	964	972.	988.			TOTAL	18.340	18.298	16.253	18-230	18.180	18-169	19.167	18-172	18.196	18.218	18.247	10.40	19.90	18.413	18.462	18.511	16:330
RELATIVE MAC4 40	.6612	. 6953	. 70.69	. 7219	665.	00416	7697	77.07	7882	. 7955	. 80 27	. 88 95	. 3164	8274	8318	4354	. 6432	6649	. 85 65		URES	STATIC	537.477	536.891	536.364	535.346	536,257	535.011	534.832	534.717	535.852	536.612	537.409	756.640	546.930	542.867	544.403	è٠	247.147
BLA0E SPEED	•										_	_			•	-	_	_	_		-TEMPERA	OTAL STATIC	52,913	52.563	52.271	51.996	51.572	51.480	51.464	51.504	52.932	53.846	554.663		100 to 000	61.046	62.780	54-154	42.144
N LOSS E COEFF	9		00.	0		-		•		.01	10.	• 05		9 4	8	.05	90.	. 06	. 87	PTION		OTAL T	29	••••	••••	., .		• •••	-				466.31 5			16	11		*
DEVIATION INCIDENCE	ė		2	6. 00		3 8		3 2	-6.000	2	8	:	000		9	9	9	8	. 00	DESCRI	TIFS	-	6.46 433	8	69	₽ :	<b>.</b> .				218.83 45						2	9 .	42.2
REL FLOW AMGLE	-66,251	56	-66.525	-66.691	-56.846	976.00-		107.75	57.569	-57.693	-57.631	-57.963	-5d . 087	-56.205	•	9	•	~	ሙ	FLOW FIELD	WF1 OC 1	ED TANGEN	67 23	95 23	22 14	2	. 55 C16.	7 7	2	<b>3</b> 8	<b>7</b>	3	20	<u> </u>	e e	2	.98 251.	2	2
NGLES			8.963	7.698	6.455	12.6	75000	1001	3,054	2.79	2.356	2.018	1.740	1.000	1.779	1.834		~	•	2	St	A W	36.3.	8	37	200	707		60			7	7	9 1	; ;	3	7		
3LADE SECTIO	-68.252	-60.376	52	69	9	-60.378	-61.106	162910-	1	3	-61.832	2	-62.087	182.29	7	5	72	8	5	STATIO	SULUY		7.87	7.1768	7.27	7-36	7.50	7.62	7.71	7.88.	200		0.1454	52 40	10.5	A. 69	33	99	
LOCAT	-	N			1					- 1			14		Ì		4		7	!	CYDEAN	-LINE		· ·	m	1	n d	~	•	σ (	=	7	PT:		2	11	#	6	+

ISENTROPIC POLYTROPIC EFFICIENST ; 9865 9865 9859 9859 9859 9853 9853 9853 9712 -----SPECIFIC WEIGHT EFF.= .496 OELTA T ON T ï 25.51 23.77 21.06 113.41 11.06 1 CURVATURE DELTA DELTA ON T PRESSURE RATEO ---ANGLES---WHIRL SLOPE RELAFIUE Temperature • 693 ¥ S ¥ S RELATIVE 222.0 220.0 200.0 117.673 117.693 117.693 117.751 117.936 117.938 117.938 117.938 118.938 118.118 118.118 118.118 118.589 118.589 118.589 EFF. \* TOTAL STATIC RELATIVE VELOCITY 740.20 779.33 793.41 793.41 809.33 809.65 865.63 865.12 865.12 865.12 8674.11 8974.11 897.99 894.71 900.23 900.23 911.15 1.246 RELATIVE MACH VO .6466 .6557 .65616 .7260 .7446 .7575 .7573 .7735 .7735 .7735 .7737 × -- TEMPERATJRES--TOTAL STATIC RATIO PRESSURE 576.33 5776.53 5776.53 577.40 5777.40 5777.40 5777.60 5779.60 5779.60 5779.60 5779.60 5779.60 5779.60 5779.60 5779.60 5779.60 COEFF PERFORMANCE DESCRIPTION NERID TANGEN TOTAL DEVIATION INCIDENCE INTEGRATED FIELD REL FLOW ANGLE -50.757 -50.757 -51.1694 -51.620 -51.620 -51.620 -52.060 -52.647 -52.647 -53.186 -53.1 FLOH 452.69 455.69 4556.58 4557.61 4557.61 4557.63 STATION 7 T SLADE-ANGLES --- SECTION LEAN 9 BLADE DATA STATION RADIUS -54.590 -55.757 -55.1691 -55.1691 -55.655 -55.656 -55.656 -55.666 -55.656 -55.666 -55. -STREAM すりらりょうらかをこす 事らりょうらゃらごでんこう ちょうちょうちょうしょう 

OLADE DATA

į			:																			,	
POLYTROPIC EFFICIENCY	- 9662	. 9880	. 9476	.9678	. 9677	.9877	- 2116.	.9877	- 2296.	.976	2636	. 9435	. 9287	.9145	1116.	.8716	-5249-	. 8241	. 8330	. 7957	.7793	-131	!
isentropic Efficiency	9876	.9873	.9672	.9671	9871	.987	.9478	1286.	1216.	9426	-9578	1946.	.9246	9606.	2569*	. 8648	. 9336	.8134	7667.	.7848	.7653	. H . H.C	
DELTA T ON T	.111	.112	. 112	. 113	. 113	. 114	. 114	.115	. 116	.118	. 121	.124	.124	. 131	. 135	.142	• 150	.156	.161	. 167	. 174	DELTA T	, , , , ,
PRESSURE Ratio	1.442	1.444	1.446	1.448	1.451	1.453	1.456	1.456	1.462	1.466	4.479	1.475	1.481	1.487	1.494	1.502	1.512	1.522	1.532	1.542	1.552	606. =	
RELATIVE P TEMPERATURE	586.7.88	588.832	589.346	590.562	- 926 - 165	743,382	594.536	535.384	597.347	596.733	688-153 · ··	601.512	503-111	604.554	696+246	507.505	649v311	511.412	513,276	615.201	517.195	30.Y. EFF.	
RELATIVE !	22,561				!	23.460			•											23,977		EFF 904	
RELATIVE VELOCITY	692.72	702.65	711.75	720.27	728.42	736.34	744.96	751.66	759.14	760.69	759.45	758.31	757.36	756.51	755.71	743.57	730.07	722.33	719.22	714.77	707.06	I SEN.	
RELATIVE !	.6015	. 61 40	.6179	. 6250	. 6313	. 6385	143·	.6513	. 6575	. 65 82	· <b>65</b> 62	.6543	. 6525	. 65 88	1649.	.6369	• 6235	.6154	. 6116	.6865	• 59 65	RESSURE RATIO = 1+463	
BLADE SPEED	910.4	919.2	927.9	936.5	945.8	953.5	962.0	970.5	979.1	927.7	4.966	1005.3	1014.4	1023.6	1633.0	1042.7	1052.7	1063.1	1073.8	1084.7	1095.6	SSURE RA	
LOSS	. 11.35	.0134	.0132	.0130	. 0126	.0125	. 0123	.0120	.0118	. 0228	. 0386	6. 35	.0577	.0812	. 0942	.1247	.1555	.1773	. 1916	, 20 51	.2203	•	10N
DEVIATI V	-6.616	-6.631	-6,583	-6.567	- 5.552	-0.539	-6,530	-6.523	-6.519	-6.517	-6.519-	-6.523	-6.529	-6.537	-6.547	-6.560	-6.576	-6.595	-6.621	-6.654	-6.700	D PERFORMANCE	FLOW FIELD DESCRIPTION
REL FLOW Angle	-49.195	-49.697	-50.146	-50 • 59%	-51.87¢	-51.577	-52.058	-52.538	136.	-> ,345		-54.075	-54.432	-54.782	-55.113	-55.425	55,733	-56.048	-56,373	-56.711		STATION? FNFEGRATED	FLOW FIEL
	-5.962	-5.442	-5.688	-5.474	-5.103-	-4.888	-4.345	-3.790	-3.174	-2.559	-2.11	-1.582	-1.233	879	432	.143	110	1.517	2.188	2.7.0	3.00%	7-10	<b>60</b>
LOCAT BLADE-ANGLES		2 -43.896		050-44-		6 -45.03B	15.530	4 -45.007	9 46.436	•	- 967024	12 -47.552	+80-24-08-			16 -48.865	757-64	18 -43.452	\$	S 28 -58.857	9/2-15-12	14419	STATION

DESCRIPTION	
FIELD	
- 8 FLOM	
TATION	4. 40000

1 ,	1	1	1	:																
•	SPECIFIC MEIGHT	. 1874		2983		76 4 G	- 1000	. 1961		0060.	11614	6610	******	2698		86 × 8 ·	-19-92	. 1887	- 9886	1000
	RADIUS- OF CURVATURE	-1.863	-2-156	-2.493	-3.459	25.289	6.764	-9.383	26447	-27.542	111-877	74.883	31.066	964-22	78-85	21.404	- 78*487·	51.451	27.0.067	9.37*816564.766
	SLOPE	16.56	14.64	12.61	\$ .	•	4.60	6		動車・	-24-1	-2.86	4.26	-5.68	7	-7.96		-9.40		-9.37
•	WHIRL SLOP	4.3, 15	200	23	44.17	- 44 . 26 . 44 . 45	4.36	44.33	100	45.78	- 46.64	47.49	100	22.64	***	54.15	-26-14-	57.64	44.65	61.72
	NO NO	.6732	9999	.656	•6524	<b>- 5491</b>	1779	.6487	.627.1	.6335		.6275	- •6251	9229	14.00	.6211		.6225	188	•629
1	PRESSJRES	17.995	18.132	18,365	18.465	18.537	18.718	18.774	\$24-93:-	13.465	10-934	18.982	19.020	19.076	-13-45	19.188	-132-61-	19,342	19.424	19.535
	TOTAL	24.371	24-417	24-517	24.568	24.619 - 24.665	24-784	24.735	- 54.739	24.734	-24.733 -	24.739	24.751	24.765		24.879	24.93	25.106	- 25,276	25.507
	-TEMPERATURES	550.378	551.573	553.617	554.483	999.000 999.000	556.545	557.139	- 229*975 -	560.544	562-454	564.352	一一一一	322.996		· · · · · · · · · · · · · · · · · · ·		583.843	- 614-36	590.542
	TEMPER TOTAL	599.937	600.242	607.109	F01.378	502-067	.602.350	502.577	643.664··	6 05.225	606.832	006.487	97.8.2.0		20000	524.765	424.49	37.1.50	- 2	536.999
	TOTAL	777.42	770.67	764.20	756.22	749.05	747.06	744.40	- 741-23	738.21	735.73	733.74	192.00	736.65		. 34.01	736.98	739.74	- 744. BI-	753.25
	MERIO TANGEN TOTA	531.68	530.45	524.12	526.94	524.15	522.33	520.14	523.25	529.05	534-95	26.146	· · · · · · · · · · · · · · · · · · ·	223.65	- 1000	594.92	<b>611.96</b>	624.84	64 16 11 -	663.32
4	HERIO	567.13	559.06	333	542.40	536.23	534.11	532.52	444	514.85	505.11	495.70		20114		\$ .6.2±	***	395.97	17.54	356.91
	RADIUS	7.4792	7.5283	4629	7.6806	7.7050	1629-2	7. 8938	7. 94.92		1999	0.1263		2000		3650 · 0		8.5568		<b>8.</b> 7359
	STAGAM -LINE	-	-	,	<b>.</b>	-	-	<b>o</b> ;				7 -		67		<b>\</b>		61		21

	OLYTROPIC FFICIENDY	9886	. 9887	- 3005	\$0.5	めたいか。	. 9863	- 9862	.9881	19881	.9765	0707.	. 460	• 3670	6216.	6769	2000	9000	1219.	7/6/	.7629	<b>•</b> 1			•											•					
	ENTROPIC P FICIENCY E	9996	.9876	.9876	.9875	.9874	.9874	.9873	.9872	2/96.	1476.	1966.	3886	• 325	5406.		1669.	.623.1	7.67.	410/	.7440	N T = .17			SPECIFIC WEIGHT	8680.	.0901	1068		9064	. 1910	.0910	• 6911	7060	<b>+060</b>	0050	7680.		.0879	.0874	•
	DELTA T IS	. 157	.157	.158	. 159	. 159	• 160	. 161	.161	.162	.164	.167	17.0	.1.3	•176	100	100	197	*0Z*	117.	. 228	DELTA T O			RADIUS OF SURVATURE		-8.363	E.	; .	53.	22.476	•	٠.	7.145	6.117	5.360		7.00	3.826	3.848	•
	PRESSURE RATIO	•65	ş	•66	99	•67	•67	•67	• 68	99	.58	. 65	8	9	9	8	8	60	?:	2	1.736	F.= .987			SLOPE	A. 54	7.94	7.29	6.61	5.42	10 to	3.65	2° 99	10.01	.36	1.54	-1-6	*****	-4.51	-5.69	,
	E, AT I VE MPE RATURE	ď.	``	•	~	, I	<u>.</u>	~	Ť.	<u>ښ</u>	9	Ŋ.	٠.	ŭ,	Ţ.	ď,	٠.	'n.	~'	٠.	613.392 615.726	PO.Y. EF!			ANGLE	E. 8.4	46.3	48.2	+ 0 ·	40.4	47.5	47.3	67.0		6.6	49.7	50.0	51.78	56.6	50.0	
	LATIVE R ESSURE TE	959	185	14	848	99	257	772	)21 -	7.4	191	121	996	/16	573	933	50 E	52	787	2	22.629 6.	636. =•			IC NO	.,	96	55	4.1	2	100	7.0 0.2	20	90	70	05	00	or d ⊷ n	7.		
	ELATIVE RE ELOCITY PR	• 75	.43	.39	.53	.74	.92	<b>.</b> 94	• 29	. 45	.28	50.	9:	2.	* S.	<b>.</b>	١	. 65	6.		<b>.</b> 9	ISEN. EFF			OTAL STATE	213 18.3	194 16.7	175 18.8	157 18.9	140 10.9	096 19.0	064 19.0	033 19.0	19.0 19.1	959 19.1	1.61 229.1	779 19.1	651 19.0	552 19.3	501 19.1	
	LATIVE R	60	91	55	5965	60	5963	52	6035	6072	6037	Œ:	59.05	<u>.</u>	5791	57.36	<b>.</b>	69	.c :	*	54845 54845	IO * 1.686			ES	201	124	067 2	578 2	2003	639 2	859 2	013 2	326	185 2	0.84	2 866	70.915 26.	100	459 2	
	BLADE REI SPEED MA	31.2	3	43.5	69.8	56.2	62.7	69.3	76.0	85.8	89.7	9.00	0.04-1	011.7	019.5	027.7	0.35.2	045	052	9	1076.1	SSURE RAT			-TEMPERATJRE	251 556	153 551	.056 554	966 556	780 550	616 559	425 55÷	232 56	436 261	271 565	.817 567	323 568	1682 570	504 580	392 564	
	1 .08S	-	-	5	5	5	-	5	0	5	8	5	20	5	-	2	φ,	20	23	n 1	3053	IANCE PRE	NC11		,	915 61	56 519	.60 519	.32 518	919	25 610	•29 618	.78 518	74 524	69 523	.37 624	•49 526	126 19.	56 537	45 541	
	DEVIATION Incidence	•	•	•	•		•	•		•	•	•	•	•	•	•	•	5	9	֓֞֞֜֞֜֜֞֜֜֞֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֡֟֜֜֓֓֓֡֓֓֓֡֓֡֓֡֡֡֝	-11.151	ED PERFORM	DESCRI	• • • • • • • • • • • • • • • • • • • •	ITTES	14 47	91 86	29	42 65	10 01	16	28 84	90 65	12 04	92	96 83	75 63	7.45 555 7.45 654	45	23	
	REL FLOW ANGLE	•		•	•	•		•	•	•	•	-42.256	•	•	•	•	•	•	•	•	-48.931	INTEGRATE	# FIE		RID TAN	ď	49 66	55 64	59 63	20 20 30 30 30 30 30 30 30 30 30 30 30 30 30	9	17 62	61	20 22	63	95 64	72 64	1.43 650	23 69	32 71	•
ADE DATA	E-ANGLES ON LEAN	9 -6.2	4 -5.8	2 -5.3	2 -4.7	6.8.	1 -3.2	3 -2.4	3 -1.7	9 -1.0	P .	•	•	n•.	* i	1.7	0 · 2	2 2 3	9.0		3,211 2 3,347	ATION 8	1		OIUS	85	51	340 57	782 57	675 575 575 57	134 57	597 57	066 57	242 20 047 56	540 55	073 54	628 53	2187 521	59 554	152 43	
<u>.</u>	LOCAT BLADE	-25.42	-23.52	-27.55	-29.51	23.40	-30.24	31.02	-31.76	-32.45	-33.10	133.71	-34.27	0/ - + 5 -	-35.25	-35.70	41.05.	155.50	40°-25-	***	-37.77	SI	-	•	STREAM RAI	2			ن. د د		7	<b>~</b>	<b>:</b> ,	: «		•	<b>.</b>	15 8.5	•	•	•
	3	***	. •			1	_			Ĭ	ā :	F'	7	Ä:	÷ :	# :	<b>=</b> :	<b>.</b>	ä		ន <b>ដ</b>	ı	1	1	17				•						, <del>, , ,</del>	4	<del></del> •	7	• •	**	

POLYTROPIC EFFECSENDY	9006	. 9165	7985	. 9881					0340	DECO	9396	9224	6486.		. 0516	1574	• 7893	47785	6647																						
ISENTROPIC		.9875	24963	.9578		7000.		2005	2006	9886	9350	-9165	. 8965	. 6760	.6366	1995	.7714	-7548	.7287	-7825 ·-		31 41394	I METEN	060	•		i			•			;					:	• •	' !	Ì
DELTA T	*64.	.194	. 194	• 193	501.	251.	. 193	196	101	400	282	502	.208	. 210	.219	229	.237	.242	.249	.257		RADIUS OF	CORVATOR	9.349	10.38	11-62	14.188	14.743	14.867	14.622	14.032	12,297	11.341	10.454	9.549	770 0	200	700.7	6.346		
PRESSURE RATED	1.852	1.050	-1.849	7.848	1.0047	1.040	****	1.046	,	920	1.634	1.629	1.822	. 81	1.811	ę	1.803	8	۲.	•79	:		LOPE	7.82	7.66	7.38	7 · 6 · 6	6.19	5.74	5.30	4.05	1 0 0	W 45	2.92	2, 35	1.72	· ·	40.4	-2,55	16.24	7301
at Ive Erature	1.200	2.006	2,334	8,563	41551	~?**	245	*		100	501.204	2.286.	3.415		5.350	7.227	•	۳.	'n	4.268	,		MHIKL	<b>6</b>	9	,	• •	46	45	45		F. 5. 2.7	46.83	47.58	48.36	49.21	51.75	54.79	59,36	64.06	10 070
ATIVE RELISSURE TEMPI	115	222	333	9		70.	710	7	273	1	101	316	185	357	376	99	144 60	163 64	545 61	49 61		MACH	2	.7478	5242	27478	4947	2469	7647	2642	.7485	747	•		.737	.732	827.	-	602		70.
PREL	23.	23.	23	23.	23	2	82	52	2		23	23.	23	23	22	2	25.	21.	21.	•		SSURES	Ë	18.788	٠.	ŗ	16.736	59	18.672	• 65	•	10.044	18.643		9	SO 1	``	18.766	•		:
RELATIVE VELOCITY			ř	5.							6467.83					•	544.41	•	•	•		2	OTAL	12.	27.194	27,175	27.157	27.124	27.096	27.064	27,033	76.043	26.959	26.875	26.779	26.681	26.617	26.552	75.462	101.00	VT++0V
RELATIVE MAC4 40	æ		. 56 40	. 5624	. 5657	. 55 99	2	66.26		2 :	55.54	35		Š	. 5159	. 4819	. 4576	. 44 24	.4198	. 3961		JRES	STATIC	57.3	57.3	57.1	56.9	56.5	56.4	56.4	55.3	27.27 50.2	61.2	63.2	65.2	•		577.573	- 4		ĭ
BLA02 SPEED	7	945.2	50	52	961.5	9	22	2	8	3	4.000	600	1016.2	023	030	038	041	057	67	1079.4		-TEMPERATURES	TAL	-	_								-		-			37.504			1000
COEFF	N	0	N	~	8	Ν.	20	-	5 6	3 ;	200	; ;	13	15	20	5	ጥ	Q.		•	<u> </u>	•	At. 70	ND M	, ,	20	167 4	7.2	52 6	85 5	66	2 4		11	35	26	92	2.	E) 1E		đ
EVIATION	-14.539	7	-	7	<b>70</b>	=	=	2	3	v	112 207	, ,	12	w	ò	å	-13,565	;	-16.283	19.		SS	101	998	998 998	16 868	82 869	34 870	74 870	698 40	37 868	52 GBG 51	? C	· ~	21 663	35	38 857	32 854	929 /4	***	7
EL FLOW D ANGLE I		27.			58.	30.	•	31.	32.	9	-000.066	7 4	;	Š	-35.957	5.68	37.77	-39.128	1.07	•50		VELOCITIE	0	65	<b>+9</b> E0	40 641.	50 63	200	24 62	10 61	55 614.	19 67 3:	12 02	3 26	99	65	29	82 698.	72	. :	
GLES REI	96	527	2.895	130	£	791	060	288	924	629	76.74		926	926	669	692		271	3	517	: !		ÆRI	576.	581.	586.	595		60 7	61 1.	614.	19:	0 C	504	573	56 1.	530.	492	45.5	?	4
3LADE-AN S: CTION	1.816		3.935	066	ιŅ	988	688				******											SOTOY		574	619	7.6645	7,7035	7. 7001	7.8437	7.8887	7.932,	7.64	0. U.S.S.	8.1189	-6,1686	8.2203	6.2745	<b>Ø</b> (	•	•	444
LOCAT				•	i						:					ı		19		な	1	STREAM	-LINE	. <del></del>	~	m	+.	n 4	~	•	o	:	1	13		15			•	C 4	

.

----

:

•

•

SPECIFIC WEIGHT		.6578	***************************************	6856	- 4856		.8852	18852	,6650	0400	9489		2004	2400	.0837	8	*****	8	<b>3</b>	* 6054	OPIC POLYTROPIC ENCY EFFICIENCY	- 87	. 9885	*		•				6426.	i			!		-	.•			
RADIUS OF SPEC	6.367		:	30.405		;		•	-79.670	:				23,597		:		i	599	!	DELTA T ISENTROPICON T EFFIGIENCY	#194 · 4987	194	6.	5	193	193		192	.194 .9727		202		210	219		•	1	•	•
SLES	90.6									ì				3,79		•	+	i		•	PRESS'IRE RATIO	6	8	49,	. 9.	1.4847 1.4847	6	9	. 83	. 63	563		8.5	10.	.81	. 68	8	1.004	5	5
NO - WHIRE	712 46.	852 44.	40.	10 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	182 41.	204 41.	211 40.	207 40.	197 40.	174	42.	45.	048 43.	976 . 44.	910 46.	164. 929	703 51.	545 545	322 58.	018 64.	RELATIVE TEMPERATURE	619,251	19.15	5	36	618.373				n	2	2 1	: :	9	9	37.50	41.39	46.37	647.501	21.26
NTIC	18.373 .7	112 .7	1001		1682	425	392	379	380	. 393	416 .8	644	9. 464.	. 551 .7	627 .7	. 741 .7	. 606	154 .7	506 .7	. 985	RELATIVE PRESSURE	27,213	27.194	27,175	27.157	27.148	- 70 V 20	27.064	27.033	27.007	26.953	26.959	26.779	26.681	26.617	26.552	26.501	•	ġ,	ċ
TOTAL ST	27.213	194	2113	17.	124	960	490	033	200	.983	959	675	.779	681	617	.552	501	794	417	361	RELATIVE VELOCITY	893 . 34	•	•		936.79	•			•		•				•	•	Ġ	871.94	
IJRES STATIC	53	51.5		ċ	9	Š	Ś	5	46.4	4.64	50.	52.6	54.9	57.4	62.5	56.5	73.8	78.9	85.3	594.134	RELATIVE MACH 10	•		•	•	•	•	•		•	•		•					•	. 7322	.701
TEMPERAT Total	19.	6	· ·	• •	6	10.	18	18	19	21.	23.	? •	<b>5</b> 9.	27.	32.	37.5	41.3	£ 6.3		52.1	SS BLADE EFF SPEED		•	ė	ė	00	•		0	•	ċ					•	ċ	÷	ċ	•
TOTAL	893.34	907.71	37.0	936.79	941.23	943,36	943.90	943.34	943.22	943.07	942.30	936.32	933.16	927.14	923.46	917.67	908-14	893.51	871.94	841.79	SVIATION LOS	00.00	109 0.00	0.00	913 0.00	194 0.00		645 0.00	713 0.00	167 0.00	346 0.00	277 0.00	372 0.00	775 0.00	311 0.00	. 601 0.00	.735 0.00	.187 0.00	434 0.00	.479 0.00
VELOCITIES O TANGEN	49	641	9 2 4	627.	623	619.	61.4	610.	614.	6229	631.	636.	642	648.	671.	697.	715.	727.	741.	758.	FLOW D		932 -3	.742 -3	797	2.052	700	527	303	30	. 321	. (143 753	513	348	.657	. 438 3	9696	512 7	235 9	.293 1
ÆRI	3	2 4 5			705	711.	716.	719	715.	700.	669	689	676.	663.	633.	596.	523	518	459	365.	GLES REL	9.941	600.	3.64	0.667	7.407 42	0.10	. 829	.613	1.122	7.293	3,399	56.	369	2.551 4	9:398	7.146	4.732	1.456	6.652
* RADIUS		9:	,,,		60	96	36	96	• 02	.07	.11	• 15	. 20	. 24	. 29	ž.	3	\$	. 53	. 61	3LADE-AN S≅CTION	.617 -3	.041 -3	.276 -3	.710 -3	256 -2	566 -2	272 -1	1- 910	- 609	- 299.	• 029		5.124	5.346 1	.637	5.234 2	7.326 3	9.801	0.814 4
STREAT	<b>+</b>	<b>~</b> •	n 4		Φ.	~	•	6	10	***	12	10 11	**	12	-	£4	<b>4</b>	<del>,</del>	03	N	LOCAT		~	**)	3	un u	, 0 A	- 40	•	97	#	12	3 4	15	16	17	10	61-	20	5

.

!	ŀ			:				r		•						: ]						LYTROPIC	EFFICIENCY	.9683	.9683	- 3681	.9676	- 3996	.9651		r 0	9476	-9556-	.9119	1962	. 0000		.6316	77.57	2860	.7363	2123	
SPECIFIC HELGHT	999	619	.0826	1299	. 1845	. 8852	.0656	• • • • • • • • • • • • • • • • • • • •	.0868	. 878.	2/98.					P	•		• •			ISENTROPIC PO	FICIENCY EF		•	.9651	.9647	- 6296	.9621		2000	0424	9234	.9043	.6473	.6785	.8541	.8176	7540	7166	7143	6885	
RADIUS OF CURVATURE	-3.688	-3-512	-3.494	-3.526	-3.595	-3.691	-3,803	-3.925	-4.072	-4.270	-4.538	4.00.4.	175.57	10.650	7/10/-	; :	\$000 E	100.00	2000	***	•	DELTA T	+ *0		194	-	.193	. 193	.193			- •	194	.202	585-	. 208		. 219	622*	24.2	542	257	
SLOPE	5.21	n 0	3.00	2, 92	2,52	2.23	2, 05	1.96	1.95	1.97	2.03	2.10	2.17	20 C	77.7	. 68 W.		Ď,		•	;	381135300	RATEO.	4.424	1.827	1.026-	1.825	1.623	1.820	1.516	1.812	- A-00-4	406	1.802	1.794	1.793	1.789-	1.786	10/01	10/07	1.779	1.775	
WHIRL	32.61															!					•	, 77	EAPERATURE -	10.254	19.153	613-158-	19.966	18.873	18.780	18-516-	18.425	262.44	21.31.00	23.271	24-647	26.323	27-362	632.463		265.140	100	52-128	
S HACH		251 .5	776	8- 628	265 .0	662 .S	ø	966 .7	023 .7	170 .7	303 .7	15. 17.	524	.616 .7286	675	712-	. 507	631	•	. 254 - 465	•		PRESSURE TE	950	~	•	26.814 6	٠,		•					- 1				1		•	•	
PRESSURE OTAL ST	26.869 15	153	0 4	6.787 17.	745	592	336	585	55.0	51.7	6.485 18.	***	355	6.285 18	252	- 9 T	5 E	17	2	.p.89* 18			VELOCITY		1802,74	48.549	970.66	955 • 83	939.62	-924+75 ··	910.75	597.92	907.57	873.65	- 664 - 46	853.52	61.646	843.69	-963-16	845.04	4000000 44	- :	:
STATIC T	50	2	. F	3 5	162	90	32	35	99	99	145	6.5	528	\$6 I	153	9	119	123	90	569.268			MACH 40			00 TO		. 6317			.7886	. 7763	(65)	75.67	727	. 72.85	7296	.7154	.7116	. 7112	Ċ	-7335	***
-TEMPERAT	151	619.153	5 4	23	0.8	16	52	32	90	241	171	117	123	251	63	404	41.392	92	47.801			•	SPEED		•					1	•	<b>a</b>	- ·	<b>)</b> C	•	0		9.0		-		9 d	;
TOTAL	017.51	002.35	5.7		29		22		57	29	3,65		25	. 15	69.	•	5.04	50.69	61.37	876.34			TON COST		# P		886 .036	920	. 039	. 041	740.	40.	200	* 4	74	.045	240	0.40	.037	. 035	•		•
VELOCITIES O TANGEN	551.31		526.04	561.20							447.21	443.36	å	438.17	439.47	. 443.7B	451.61	463.68	•	4, 7, 39	:		LOW DEVIATION		•		• •	5635	•	•	•	•	.i .			: :	1	•	-	÷	류 . ;		:
MERIO	855.20	844.77	634.63	-842.04	: :	10	77.8.95	76.A.92	760, 42	753.83	747.02	739.88	731.18	723.65	720.13	716.95	714.12	713.22	715.95	721.71	DATA		AN ANGLE		2	2 5	3 2	M		95		295	241		466	25					1	2 :	
RADIUS	•	7.7539	•	•	• •	•	7.987A	, ,	8,0687	1	8, 1523	195	8.2387	- 6. 2630	0.3281	- 8x3748	8.4209	8.4692	519	573	4		BLADE-ANGLES -Section Lead		γ'	1./86 -25.	31.054 -19.125	8.258 -16.778	30.527 -14.5		•	•	•	29.492 - 5.		"	130			31.288 15.	1	725	
STREAM	<b>~</b>	~	M	• •	. «		. <	•	, a		12	-	14		16	-	10	- 67-0	<b>02</b>	-55			LOCAT			N 1	l	- (		1	•	1		2 - 11					1		\$		

<b></b> ن	.c. 02	•			~	•	ю (	<b>.</b>	•	عب	•	<b>-4</b>	6	~	•	~		n •0		POLYTROPIC EFFICIENCY	.948	.9478	.9471	1946.	0440	9386	.9354	. 9329	.9200	.9817	9698	. 8568	. 8423	. 8108	16//	7442	7218	+669
SPECIFIC E WEIGHT	.0345	•	•	•	•	•	•	•	•		•	•	7	•	•	•	•	•		SENTROPIC	6246.	.9433	.9425	.9414	1946.	AMM C	9388	. 9273	M	9869		. 8 4 4 2	.6294	.7953	.7611	44.00	6004	.675
RADIUS OF CURVATUR	-5.196	-6.526	-7.450	-6.607	-10.05*	-11.864	-14-113	-16.696	-241162	-28.575	-33.159	-37.318	-40.745	-43.689	-47.268	-55.063		76.314		DELTA T 2 ON T E	*19*	.194	.134	193	56.1	2 6	.192	. 192	.194	198	2020	.208	.210	.219	622.	. 242	340	.257
SLOPE	-2.23	-2.46	-2.53	-2.55	-2.52	-2.43	-2.27	78.5-	1.00	1.22	68.	•• 56	23	60.	en.	**	m 6	260		PRESSURE Ratio	1.806	1.804	1.602	1.800	1.798	10.79	1.783	1.779	1.776	1.773	10//01	1.764	1.761	1.756	1.76	1.756	750	1.757
WHIRL	9 17.58	17.	17.	17.	17.	17.	17.	<b>.</b>	1		7	17.	17.	17.	17.	18.	•	6		ELATIVE MPERATURE										621.342								52.128
IC NO	107 - 7019 308 - 5896	9	9	9	9	9	9	φ,				ູ້	,	r.	'n	.596	. S. G. G.	. 602		ELATIVE RE RESSURE TER																		25.816 69
ESSURES-	5 19.	. 65	19.	19.	19.	5 20.	2	200	. ה ה		20.00	20.	9 20	1 20.	50.	20.	ຂໍ	20.00		RELATIVE REI PELOCITY PRE	.4		و	7	<b>=</b>	2 1	ي د	*	2	*	2 :	4 19	*	96	2	<u>.</u>	<b>.</b>	2 +4
12	26.53	26.48	26.45	26.42	26.36	26.28	24.28	26. #	20.03	20 000	25.93	25,92	25.87	25.87	25.66	25.86	25.85	25.84		4 >																		69 736
RATURES STATIC	564.069																			DE RELATIVE ED MACH 40	-		•	•	•	•	•		•	•	• •	•			•	.0 .59	70. 0.	99.
ICHPERATU Total	619.251	•		•	•	•	~	•	.,	v	~ ~	,,,	, ,,		г,	-	-	~ .		SS BLADE	4:	20	0	0 04	C+	93	07	52	0	69	0 16	ב ה	92	200	9.	245	D 42	2 62
TOTAL	820.54	764.55	782.41	770.91	758.93	747.55	737.16	728.54	723.05	**************************************	712.01	710.43	708.54	711.05	18	10	723.01	728.80		DEVIATION LOS INCIDENCE CC.		357	369	383	417	255		• •	296	625	649	627	• •	671	• +99	•	299	719 .07
-VELOCITIES- D TANSEN	247.90	240.01	235,66	232.23	228.28	724.15	2207	217.41	216.04	215.54	21.4.77	21 2. 64	213.54	215,26	218.11	222, 32	227.75	234.50		FLOW DEVIA NGLE INCID	4 4 4	1	526	529	532	206	7	363	385 1	1 +24	٠ . د د د	<b>~</b>	4 +	. ~	-	~	~ ·	
MERIO	782.19	•	: 2		m		÷	ŝ	<b>.</b>	٠,	67.0	÷ ~		: ~		83.	86.	6.5	•	REL		925 17	573 17	145 17	17.	208 17	R	152 17	416 17 ·	567 17.	655 17	254 17	104 17	016 17	055 17.	195 18.	100	91 275
4ADIUS	7.7230			96	33	.93	.97	. 11	. 05	2	*:		2 6	88	.37	. 42	. 47	.52	LADE DA	LADE-ARGLES CTION LEAN	•	186 -8	157 -6.	240 -7.	.115 -7.	.054 -6.	100	800	789 -2	.804 -1.	.613		- 06.4 - 06.4	.951 2.	.110 3.	.362 4.	.699	510 6
STREAM -LI WE	₩;	v •	0 4	· •	٠.۵	~	•	•	9	# (	21	? .	, v	10	17	9 1	61	20	:	LOCAT 3		•		,c   #	45	÷.		0 0		1 4	13	i	7 -	: ::	57	4	7	21 12

														1								POLYTROPIC EFFICIENCY	.9281	• 9256	- 4251	*226	9169	0125	0006.	*******	. 6914	7.72	. 0220	6311	6193	.7901	7687	0044.		5999
SPECIFIC	+260	5 · 5 · ·	9269.	5760.	246			9909	9966	2966	8958	9667	. 1953	4668	. 0943	5260A	. 8930	• • • • • • • • • • • • • • • • • • • •	. 6920	•6914		ISENTROPIC EFFICIENCY	. 9226	.9205	.9186	9116	- 5145	2506	.9005	. 8967	.8826	. 16530		A176	8046	.7734	97416	.7193		+6645 ·
RADIUS OF CURVATURE-	16.241	17.147	16.156	19.286	26.05	618.22	. KO - CO - CO - CO - CO - CO - CO - CO -	28.154	000000	35. 45p	30.736	65.230	52.732	63,351	79.297	185,387	155, 765	289	1305.219	910		DELTA T	.194	<b>*67.</b>	•194	.193	× 10.	193	.192	.192	.194	198	202.	880	210	.219	. 229	.237	242	.257
ANGLES Hirl Slope	-4.29	•	-3.91	-3.70	- No. 48	-3.24	95.2	- 2. 43	10.01	-2.0	26.4	11.00	66	300	04	. 23	. 40	. 70	. 90	1.06		PRESSURE RATIO	1.783	1.780	1.778	1.775	1.772	1.750	1.753	1.748	1.744	1.741	1.738	10131	1.734	1.735	1.737	1.738	1.739	1.738
17		• •	'n	<b>.</b>	:				•	25.24						· .	5.	5.	9 6	1 6.3		RELAFIVE	9.5	3.	Ţ,	18.366	18.573	1000	18,425	18.232	19.438	521.342	23.271	710-42	27.362	32.463	637.504	141.392	44.376	52-128
RES MACH STATIC NO	. 292	. 259 .5	• 526 • 5	.252	. 246 .5	242	. 236 .5	23.0	. 223	. 412.	000	101	182	172	162 .5	153 .5	. 144 .5	.136 .5	.129 .5	.123 .5		RELATIVE R	203	166	128	187	# # # U	74	766	585	635	586	539	200		100	202	543	551	2 4 2 4 3 4
PRESSJRES	6.203	6.166 21	6.128 21	6.087 21	6.044 21	5.957 21	5.864 21	5.766 21	5.685 21	655 21	2000000	7,000	5.500 21	5,441 21	5.500 21	5.528 21	5.543 21	5.551 21	5,553 21	5.548 21		RELATIVE VELOCITY	è59.94	657,95	655.88	653.70	651.40	040.00	6.35.61	630.93	628.98	627.40	626.02	22. 529	24.020	631.07	035.62	3	3	547.04
INGES STATIC	83, 569	63 67	83.8.5	83.957	64.110	84.532	64.923	85.325	85.628		07.040	31.16	96.033	20.00	99.857	0 to 10 3 to	07.901	10.615	13.795	17.883		RELATIVE MACH 40	. 5551	6	150	3	iV i	7	9 M	5,0	52	N	52	3 5	7 0	. 52.36	52	S	O	5283
TEMPERATU	-	•	*	-	•	~	•	•	•	-	v۲	• •	v	,,,	y r-	, [7]	, 4		•	552.128		BLADE	0	c		0	•	-	<b>3</b> C	. 0	•	0	0	<b>-</b>		<b>•</b>	71 0.0	0	0	
OTAL	59	57.95	55.88	53.70	51.46	*6.56	41.24	35.61	30.93	628.94	27.40	20.02	22.02	26.27	31.07	35.62	3	•	3	Ş		ON LOSS	.11	.11	11:	.11	11.	-12	21.	113	* # •	.14	• 1 4	*1.		112		.11	• 10	2:
ITIES NGEN I	1.0	9.50	6.03	6.75	5, 65	4.42	3,25	2.13	1.21	0.67	9.27	5 ° °	٠ • • •		7.7		3.07	4,92 6	7.62 6	1.30 6		OEVIATION INCIDENCE	2.21			•	•	•				•	•	•	•	• •	2.682	•	•	•
RID TA	~	27	. 34 6	29 65	9 €0	34 0	11 6	•	95 6		50	٠ •		00.	60 4 40 4	. 63		93	11.	. 10		REL FLOM Angle	. 18	٠.	95	.36	.78	7;	0 1	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֡֡֡֓֜֜֜֜֡֓֡֓֡֡֡֡֡		.51	64.	<b>6</b>	5	ה ה ה	5.572	0.0	. 80	20.
;	7,	35	65	92	ŶĢ	ģ	63	53	8	26	29	26	20	2 5	3 3	9 4	3 6	9	9	E 90 006	E DATA	ANGLES	-	9	924	842	755	œ٠	166.		- 413	m	N	204	M# 1 .	1,24	1.416	629	6 32	974
M RADIUS	47	•	٦,	٦.	•	٠,	٠.	·	•	٠,		•	7,	• •	•	, ,			·	, 40	9t A0	3LADE-A	46.5	A . A .	3.705	3.579	3.459	44m.m	*****	3.11.6	2.917	4.842	2.787	2-754	2.747	001.0	2.630	2.984	3r114	3.291
STREAM	-	۰ م	m	*	4	9	^	•		10					- 17		-	•	20	2 4	;	LOCAT	+	۰ ۸	, ro		'n	ا و	: *- •	0 0	` e	=	15	+	# L	ë.	2 2	: 2	+	ຂໍ

OF SPECIFIC	1960 429		202	1	172	120	•	•	574		131	. 269	713	969	6/	139	•	•			F ISENTROPIC POLYTROPIC	Ì	.8975	6469*	. 8922	•	. 4266	80.00	. 0655	.8516	.8321	- 6133	9062°	. 7.96	. 7516	. 7212 · ¬	.7088		260.
RADIUS OF CURVATURE	10.6	11.0	12.21	12.9	13.6	15.1	16.8	19.0	28.57	n	59.	118.	1932	-151	-77	101	21	37			E DELTA T	.194	.194	.194	• 193	. 193	261.	1499	. 192	.194	.198	202	208	. 210	. 219	. 229	.237	.242	642.
SLOPE-		i		Ť	7	ï		i	22.1	•		•	i	•	•	•	•	•	•		PRESSURE RATIO	1.760	2	.75	•75	* 1	?;		7	.71	2	2:	1.786	7.0	2	7	7	ž;	1.719
MACHANGLE NOWHIRL	9	921	156	143	0 960	0.40	966	952	106	200	992 6	898	901 0	926	951 0	974 0	993	989			RE.ATIVE TEMPERATURE	619,251	619,153	619.158	618.366	618.973	616.750	010.010	618.232	619.438	621.342	623.271	626.323	627.862	632.463	637 . 584	641.392	644.376	647.501
1 0	546	. 516	C1 099 17	ME ST	407	.384 .5	. 362 4	345	350		3 E62	288	. 286 .4	. 287	. 291	4. 765.	. 305	.315 .4			RELATIVE PRESSURE	- ur		N LOT	L.		un I	en u	1 E	. 67	w	un I	25.670		1 61		เลา	41	w
PRESSURES	5.870	5.820	<b>.</b>	5.662	5,553	5.439	5.322	5.227	7.1/4	5.057	5.070	5.074	5.977	5.119	5.164	5.209	5.233	5.257	•		RELATIVE	61A.57	: :	ف	i	'n	ė.	٠.	•	ď		Ġ,	587.99	e Pe			3	07.	609.93
TURES STATIC	67.9	67.3	567.925	88.0	9.60	88.8	89.2	39.5	5.00 5.00 5.00 5.00	2 4	5.5	9.76	99.3	03.4	07.9	11.4	14.1	17.3			RELATIVE MACH 40	•		51	.51	. 5143	8		• •		E# *	94		* 4		9	67	64.	3
-TEMPERAT OTAL	19.251	19.153	0179.056	18.873	18.780	18.616	18.425	16.232	19.438	24 274	24.817	26.323	27.562	32.463	37.504	1.392	44.3	7.8	7 • 7		BLADE SPEEJ	9	• c	•	0	0	0	<b>.</b>	<b>-</b> c	•	0	0	<b>9</b> 6	<b>ə</b> c	9 63	•	0	•	9
TAL T	4.57	7.59		3.75	9.0	2.83	6.52	1.64	9.92	7	7.77	22	2,0	5.44	0.63	5.11	7.54	9.93	60.		N LOSS												.1915						
TANGEN TO	0	00	<b>.</b>	9 0		00	00	00	-	200		, «	000	00	9 00	00	00	9 00	•		DEVIATION INCIDENCE		֓֞֞֜֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֡֓֓֓֓֡֓֜֓֓֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֡֡	5,5		9	• 05	. 22		29	8	8	9° 469	3 6	5 5	9	8	12	16
V EL 0	25	53	<b>.</b>	2.5		63	29	*	<u>6</u>	200	ה ה ה	2		*	63	11	74	93	50.0		REL FLOM	Č	9 6		00.	.00	. 30	90.	•		00.	• 00	0000	9 6	9 6		8	.00	00
S	61	01	910		909	502	966	65	589	000	000	o «	2.6	595	600	00 5	209	609	1	5 ;	S S	90.0	900	9.0	010	.015	.014	.012	70.0	200	. 005	.003	1001	100				0 24	£ 0.0
RADIUS		vo.	7.7191				ு	or.		<b>,</b>			, ,	_	~,	- 8	-	٠.	9.00.0	70476	SLADE-ANGLE SECTION LEA		7 403	٠.	7.72	7.39	9.05	9.22	5.50	-4.67A	9.80	9.90	B) (	30	3.65	3.06	5	9. t2	4

TION
DESCRIPTION
FIELD
FLON
10
STATION

	973		1 <b>v</b>			Š	•	, L	10	- -	•	, ,	No.	- 15	÷ i	:	<u>N</u>		2.	-	!	!	·	•		2	,	<del>بر</del>	· •	•		<b>=</b> 0 (		n •	· ·			51	•		32		m	<b>7</b>
SPECIFIC WEIGHT	•			60	•	168	0	<b>968.</b>	•	<b>161.</b>	66.	668			9 (	:		9759 ·	760		;	SPECTETC	HOLDH.		492	. 197	161		-0971	. 197	6969	8960.	# 50 C	969	7000	304	900	560*	460.	6	5	692	.092	. 891
RADIUS OF CURVATURE	0 - 0	1216.203	55C 4CO	363,335	336.063	309.439	296.320	293,734	300.792	- 217.947-	347.417	392.87	460.980	564.693	•	•	.,,	-2787.579			;	of affice of	CUPVATURE		0.666	0.00	0.00	0.0	₽•00 <b>•</b>	0.00	000.0	0.800					900,0	0.00	000.0	0.000	0.000	94440 .	0.00	0.00
SLOPE	•			6		11	12	-, 12	11		10						02	10.	. 6			- Care			9.00	00		0	•	00	•	01	. 61	19.							80		- 00	*
WHIRE SLOP	0.0	00.0			0.00	9.00	0.00	09 • 9 · -	00.0	0.0	00.0	0.0	ċ	å.	ċ	•	ė		•	•	•		d	-		0.00	00.0	0.0	00.00 -	0.00	00-0	0.00	9	9 0				0-0	00.00	00.0	0.00	- 84 86	00.0	ĕ
A CH	.5321	.5294	6250	5207		- LD	E	-3	•	4	.4863	• 4865	. 4 868	.4871	2684.	• 4925	* 952	.4964	1264	• 4 995			5 c	2	.5334	.5303	.5275	.5246	215	.5153	.5088	.5019	2964		\$ 4	* 4	1	4872		•	*	4	.4981	\$
PRESSURES OTAL STATIC -	21.341	•								•			•	•	-	•	•	•	•	•		010000	-03400 -0447	•				•	•		•	•		•	•	•	24 . 127							•
TOTAL	5.87	5. 82	25.769	99.5	5.55	5.43	5.32	5.22	5.17	5,11	5.06	5.07	5.07	5.07	5.11	5.16	5.20	5.23	5.25	5.28		360	70761	5	5.87	5.82	5.76	5.71	5.66	5.55	5.43	5,32	5.22	5.17		7. 10. 10.	25.074	5.07	5.11	5.16	5.29	5.23	5.25	5.28
TURES STATIC	86.3	86.5		24.0	6.78	99.4	89.0	4.69	90.9	93.1	95.3	96.8	98.2	99.6	03.7	98.2	11.6	14.3	17.4	21.4		0	1275311	1	86.2	86.4	86.5	96.9	87.2	87.8	88.4	88.3	4.68	6.06	1.5	֓֞֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֡֓֡֓֜֜֜֜֓֡֓֡֓֡֡֡֓֜֜֡֓֡֡֡֡֡֡	506-113 506-107	200	03.7	08.2	11.5	14.3	•	1.4
TEMPERAT: TOTAL	19.2	19.1		4.04	18.7	18.6	16.4	18.2	19.4	21.3	23.5	8.42	26.3	27.8	32.+	37.5	41.3	M. 44	6. 7.	52.1	t		TOTAL	5	19.	19	19.	18.	18	18.	÷	10.	8	6.	Ċ	,	100434-	7	32	37.	7	į	47.	52.
TOTAL	3.	630.96	627.73	621.82	613.97	606.53	598.71	592.28	589.28	586.49	583.83	584.85	585.87	585.68	592.04	597.60	602.61	605.74	608.97	612.63	CRIPTION		101	5	**	631,99	•			•		Ġ	-	å,	<b>.</b>	i.	505613	5 %				ŝ	608.97	ö
ELOCITIES- TANGEN	3.00	0		•		0	0	•		•	0	•	ø	0	0	æ	0	•	0	õ	FIELD DES				•	•	0	0	0	0	•	a	0	0	9 4	<b>,</b>		3 6	• •			•	0.00	
HERIO	634.10	630.95	627.73	52 4 52	613.97	60 6. 53	596.71	592.28	589.28	566.43	583.83	58 4. 85	505.87	ė	592.04	ċ	'n	605.74	ė	612.63	17 FLOW	3		2	635.14	+	8.7	ŝ	÷	614.82	:	÷	592.33	å,	28 0 35	764.15	. 96 % 13	: .	59.74			i	60 8, 97	125
RADIUS	7.6400	7.6785	7.7179	7007-7-	7.8422	7.8859	7.9310	7. 9773	8-0248	40×4-4-	6.1231	•	N	6,2769	~	ייי	₹.	9.4902	ŝ	9	STATION	2012.0	201047	,	2.64.04	7.6784	7.7179	7.7582	7. 7996	7.8420	7.445	7.9308	7-9772	2420 - 9	4. 1732	6271 0	22	8-22ek	8.3293	45.45	8.4360	484	8.5448	
STREAM	## :	~	M .	•	•	À	. 🔹	+	10	#	12	21	<b>7</b> F	12	16	+	10	-67-2	<b>5</b> 80			, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	111111	- · <b>3442</b>		~		•	•	٠		•		<b>0</b>	#	21		4	16		10	4	20	

w
DRMANCE
Z
•
z
œ
0
PERF
ï
w
Æ
_
~
×
Y
T
•
ROTOR
_
٠

		,				•		i	i	į	į			2
TALET AADEUS	- RADIUS	INLET M. NO	INCID	AIVEO - NCIT-	COEFF	FACTOR	FACTOR	DELTA P ON Q	REL V	0ELTA H/U**2	INLET	N-ANGLES OUTLET	INCET	ANGLES OUTL!
75.00	ķ	799	=	4.53	. 0221	•	N	.6430	.7285	.6938	å	5	17.205	
1998	53	. 0122	3	4.36	. 0219	425	.4335	.6321	.7177	.6855	å	2	16.450	
9020	.63	825	25	4.18	. 0217	435	<b>.</b>	.6199	. 7065	.6772	٠i	2	15.428	
	3	.8385	Ž (	\$ F . F	• 0214	\$ 4 \$ 1	n 1	5000·	6907	.0003		7 -	140.131	
7.1256	7.7676	0100	1000	13.030	2000	4254°	1040	4078	1000	65.24	-62.713	-16.988	11.400	, ,
4		977	) M	N. F.	0203	46.2	œ	5652	.6852	6437	ċ	2	10.254	•
8645	85	2069	2 2	2 · E	0199	465	an c	.5507	.6813	6349	Š	2	9.335	_
2099	8	905	2	3.10	. 0195	45.8	•	. 5361	.6795	.6262	m	3	0.501	•
77.11	95	915	2	2.31	. 0379	582	3	.5213	. 6671	.6262	ņ	=	7.633	_
4612	8	.9275	2	2.37	. 0542	N	50	.5 <del>86</del> 6	.6562	.6302	ŕ	٤	6.883	•
99 09	. 05	939	~	2.29	. 0832	521	5,7	.4920	.6342	.6348	m	33	6.120	•
1007	. 10	951	2	2.31	. 1128	536	m	.4775	.6192	.6350	ň	2	5.601	<b>.</b>
2105	91.	963	2	2.44	. 1354	554	w	.4632	. 6043	.6355	'n	ゞ	5.214	J
3205	2	975	7	2.55	. 1573	570	56	0644.	. 5903	.6357	m	8	4.896	₹
4310	27	987	2	2.59	. 2083	611	9	.4353	. 5543	.6530	m	35	4.550	•
-545	*	966	2	2.58	. 2599	658	5	.4225	. 5145	-6714-	m	2	4.187	•
6544	7	.010	~	3.50	. 2957	691	89	.4110	. 4845	.6817	;	2	3.575	•
7678	5	.021	2	4.60	. 3201	715	7	.4006	. 4633	.6857	\$	22	<b>5.96</b>	4.271
8828	.57	.033	젊	6.28	+ C + E •	743	2	.3916	. 4371	8069.	į	2	2, 383	m
0000	99	1.0446	2	3.54	. 3815		•	.3853	. 3993	.6966	\$	96	1.836	m
STAT0	OR PERFORM	ANCE							1					
	•	ų	2	5	0 00	9	-	7.00	2	AT 124	CECTIO	N-AMELES	- 644	SHUME
ALE 1	0011.51			OF TANK		66.10	0 0 1 0 E		DATTO	17:040	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TECT OUTLES	13 #1	STITE OF THE STATE
•	5	2 •	•	2	5	;		2 2 2		, }				}
6199	-7.64-80	.7712	-2.490	7.239	. 1529	. 4501	. 6254.	.3589	• 695	0.5400	46.617	-7-239	- 290 062 -	;
6727	7.6791	785	-3.109	7.393	. 1513	. 4737	.4736	.3749	.6604	2.0000	48.041	-7.393	-37.889	
7229	7.7191	797	-3.535	7.557	. 1513	. 4877	.4878	.3666	• 66 93	0.0066	47.278	-7.557	188 - 88-	
7704	7.7600	. 8070	-3.913	7.724	. 1524	<b>4664</b> •	9664.	.3975	.6613	0000.0	46.710	-7.724	-30.667	
0157	7. 80 17	913	-4.194	7.891	. 1544	. 50 69	เก	- 9694.	. 6552	0.000	46,256	-7.891	-27.417	
18597	7.8445	518	904.4-	8.058	. 1530	. 5205	•5206	.4071	.6463	000000	45.892	-8.058	-24.152	•
-21-	-7 66 64	828	-4.558	8.223	. 1713	. 53 07	S.	4684.	- \$6399 -	0.000.	45.565	-6,223	-25-35-	į
9451	7.9336	821	-4.645	8.384	. 1602	. 5401	n.	. 4104	.6321	0.0000	45.272	-6.384	-17.829	•
9872	7.38.88	820	-4.713	8.538	. 1871	. 5471	.5471	.4105	.6272	900000	45.816	-0.530	-14.613	I
0293	8. 0275	819	-4-167	8.678	. 1904	. 5527	N.	8604.	.625	000000	44.809	-8.678	-11.122	•
8718	6. 6759	818	-3.346	6.602	4461	. 5590	-	- 4-866-	- 46237	0600-0-	44.667	-6.582	262-2	1
44	6.1254	A15	-2.577	8.106	1983	. 5545	· UT	. 4070	6223	0000-0	44.620	-8.906	-3.399	٠
4		:	- 4464		1915			6-67 Z		0000	44-646	-6.949	-217	!
M. 200	8.2267		-1.372	N 40 6	1837	5612	.5610	4086	6315		44.885	-9.863	3.568	٠
210	A. 27 A.3	707	775	K-76-0	1756	5.5.A.4.	u	1001	4.364		45 - 124	-Q. B53	7.369	•
2066	A. 33.06	. 6		9.0.0	1567	55.6		4071	6448		45.346	-9, 059	12,551	١
27.36		4 6	1 6	4	4676	F 2 2 F	۱ų	45	777	4444	77 77	P. 0	40. 204	1
	P7 D7 • D	100	7 7 7 7		100+	6137	n u	2072	7759		45.034		27.146	
	0000	200	700	2000	* P. 7 * *	2000	2000	2000			200	424		-
1200	CACAGO		181.0	03716		2000	, ,	2615	2003		03514	044-01	1011	•
1726	F##0.0	7757	# 0 P - P -	F 0 1 0	1001	2010	7916	1000			10000	F 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	207 77	•
,														

WAKE AND BOUNDAY LAYER BLOCKAGES (PERCENT)

STATION	-	~	m			۰0		•	σ	10	11	12	13		15		17
: MED BLOSKAGE		0.0	0.0	1.0		1.5	2.0	2.5	2.5	1.7	3. B	5.0	7.0	⇒.6	12.3	13.3	13.4
DIST FACTOR		1.0	4.4			ŵ		m	. 2	1.0	1.0	1.0	1.0		1.0		1.0
INT BLOCKAGE	0.0	0.0	0.0		1.0	1.5		5.	5.5	1.7	3.0	5.0	7.0		12.3		13.4
NHOS	IARY	POINT	0 7	NUMMARY POINT NO. 1 THE CALCULATION IS CONVERGED	HE CAL	COLA	TION	IS CO	4VERG		PASS 2	23 :					

TEST POINT TITLE = 208240215670

FLOW = 16.92 SPEED = 14266.8 PRESSURE RATIO = 1.722 ISENTROPIC EFFY = .7957 POLYTROPIC EFFY = .8106 DEL T/T = .2101

## WITHIN - BLADE ANALYSIS (82% SPEED) POINT 208241115882 PHASE II Ŋ

## TEST

Color   Colo	01.05	CS CS CS CS CS CS CS CS CS CS CS CS CS C		A THE STATE OF THE	1.0		A A C A C A C A C A C A C A C A C A C A	X X X X X X X X X X X X X X X X X X X	ESS. SCOT. 110. 110. 110. 110. 110. 110. 110. 11	ACCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	THE COORDINATE OF COORDINATE O
Section   Sect	2267 250.15 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	25500000000000000000000000000000000000		- NO 10 10 10 10 10 10 10 10 10 10 10 10 10	mmmomommmomommomomomom uuuuuuuuuuuuuuuu	- + + + + + + + + + + + + + + + + + + +	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	00000000000000	200 113,57 1		
250 20115 0100 250125 110000 511379 14.650 14.191 22.22 0100 115.77 01000 511.59 14.650 14.191 22.22 0100 11.59 01000 511.59 01.650 14.191 22.22 0100 11.59 01000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.000 511.59 01.000 511.59 01.650 14.191 22.22 0100 11.59 01.000 511.59 01.00	2557 250.13 0.00  53835 250.13 0.00  6937 250.13 0.00  9949 250.13 0.00  9535 250.13 0.00  9535 250.13 0.00  9525 250.13 0.00  9527 250.13 0.00  9647 250.13 0.00  9747 250.13 0.00  9447 250.13 0.00  9447 250.13 0.00  9450 250.13 0.00  947 250.13 0.00  947 250.13 0.00  947 250.13 0.00  947 250.13 0.00  948 250.13 0.00  948 250.13 0.00  948 250.13 0.00  948 250.13 0.00  948 250.13 0.00  948 250.13 0.00  958 250.13 0.00  968 250.13 0.00  968 250.13 0.00  968 250.13 0.00  978 250.13 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00  978 270.20 0.00	CX		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~			\$	2000000000000	2 4 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		
6472 250.15 0.00 250.15 510.600 513.50 14.666 14.191 2282 0.00 15.77 0.000 15.70 0.000 15.70 0.000 250.15 510.600 513.50 14.666 14.191 2282 0.00 15.77 0.000 15.70 0.000 15.70 0.000 250.15 510.600 513.50 14.666 14.191 2282 0.00 15.77 0.000 15.70 0.000 15.70 0.000 250.15 510.600 513.50 14.666 14.191 2282 0.00 110.35 0.000 15.70 0.	6937 250.15 0.00 6947 250.15 0.00 3029 250.15 0.00 4535 250.15 0.00 4535 250.15 0.00 6035 250.15 0.00 6035 250.15 0.00 6035 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6040 271.42 0.00 6529 272.54 83 0.00 6659 272.54 63 0.00 6661 277.53 0.00 6461 277.23 0.00 6461 277.23 0.00 6461 277.23 0.00	CA 55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	+   -   -   -   -   -   -   -   -   -	: 4		l # # # # # # # # # # # # # # # # # # #		000000000000	1117 1117 1117 1117 1117 1117 1117 111		
\$25.15 0.00 250.15 510.668 513.56 14.191 2222 0.00 15.50 0.000 15.	8472 250.15 0.00 8472 250.15 0.00 1518 250.10 1518 250.15 0.00 1518 250.15	CS CS CS CS CS CS CS CS CS CS CS CS CS C					\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	8009000000	11111111111111111111111111111111111111		
9457 250.15 0.00 250.15 510.06 513.54 14.656 14.191 22242 0.00 13.97 0.000 13.99   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 13.70 0.000 13.70   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 12.71 0.000   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9515 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 11.55   9516 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 0.00 11.20   9517 250.15 0.00 250.15 510.06 513.54 14.650 14.191 2242 0.00 11.20   9518 250.15 0.00 250.15 510.06 513.54 14.650 14.191 2242 0.00 0.00 11.20   9519 250.15 0.00 250.15 510.06 513.54 14.650 14.191 2242 0.00 0.00 11.55   9510 250.15 0.00 250.15 510.06 513.54 14.650 14.191 2242 0.00 0.00 11.55   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2242 0.00 0.00 11.55   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2242 0.00 0.00 11.55   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2245 0.00 0.00 11.55   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2245 0.00 0.00 11.15   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2245 0.00 0.00 11.15   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2245 0.00 0.00 11.15   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2245 0.00 0.00 11.15   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191 2245 0.00 0.00 11.15   9510 250.15 0.00 250.15 510.06 512.55 14.650 14.191	8472 250.15 0.00 3029 250.15 0.00 4535 250.15 0.00 4535 250.15 0.00 6035 250.15 0.00 6035 250.15 0.00 1999 250.15 0.00 6047 250.15 0.00 6047 250.15 0.00 6040 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 250.15 0.00 6041 270.20 0.00 6041 270.20 0.00 6041 277.23 0.00 6041 277.23 0.00 6041 277.23 0.00	250 250 250 250 250 250 250 250 250 250						000000000	21 24 24 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	000000000	
1519 250.15 0.00 250.15 510.06 513.54 14.650 14.191 22242 0.00 12.79 0.000 12.	1516 250.15 0.00 1518 250.15 0.00 1529 250.15 0.00 17531 250.15 0.00 1993 250.15 0.00 1994 250.15 0.00 1995 250.15 0.00 1997 250.15 0.00 1990 250.15 0.00 1991 250.15 0.00 1991 250.15 0.00 1992 250.15 0.00 1991 250.15 0.00 1991 250.15 0.00 1991 250.15 0.00 1991 250.15 0.00 1991 250.15 0.00 1991 270.20 0.00 1972 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00	2500.115 2500.115 2500.115 2500.115 2500.115 2500.115 2500.115 2500.115 2500.115 2500.115		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	• • • • • • • • • • • • • • • • • • •			00000000	1112 1112 1112 1112 1112 1113 1113 1113		
151. 250.13 0.00 250.13 510.08 513.549 14.696 14.991 .2242 0.00 11.27 0.00 15.20 0.00 15	1516 250.15 0.00 1529 250.15 0.00 6035 250.15 0.00 9023 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1999 250.15 0.00 1990 250.15 0.00 1990 250.15 0.00 1990 250.15 0.00 1990 250.15 0.00 1990 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00 1977 270.20 0.00	25500000000000000000000000000000000000						9000000	11.2 11.1 10.0 10.0 10.0 10.0 10.0 10.0		
250 251.13 0.00 250.13 510.00 511.140 14.696 14.191 .2242 0.00 11.151 0.00 51.151 0.00 250.13 510.00 511.140 14.696 14.191 .2242 0.00 11.151 0.00 51.151 0.00 250.13 510.00 511.140 14.696 14.191 .2242 0.00 5.940 0.00 511.140 14.696 14.191 .2242 0.00 5.940 0.00 511.140 14.696 14.191 .2242 0.00 5.940 0.00 5.94	3029 25 0.15 0.00 5035 25 0.15 0.00 7531 25 0.15 0.00 9023 25 0.15 0.00 9023 25 0.15 0.00 1999 25 0.15 0.00 4966 25 0.15 0.00 9417 25 0.15 0.00 9417 25 0.15 0.00 9417 25 0.15 0.00 9417 25 0.15 0.00 9417 25 0.15 0.00 9417 25 0.15 0.00 9417 25 0.15 0.00 950 25 0.15 0.00 971 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00 927 27 0.25 0.00	CA CA CA CA CA CA CA CA CA CA CA CA CA C		W IV W W W W W W W W W W W W W W W W W W				000000	11. 12. 13. 14. 14. 14. 14. 14. 14. 14. 14. 14. 14		
\$25.15 0.00 22015 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.00 6.00 0.00 0.00 0.00 0.00 0.0	4635 250.15 0.00 7531 250.15 0.00 9023 250.15 0.00 9023 250.15 0.00 1999 250.15 0.00 4966 250.15 0.00 9451 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 9500 250.15 0.00 971 271.42 0.00 7914 271.42 0.00 7914 271.42 0.00 7914 271.42 0.00 7914 271.42 0.00 7915 271.42 0.00 7917 271.53 0.00 3322 276.73 0.00 3322 276.73 0.00	CA Part of the control of the contro					\$	00000	2000 000 000 000 000 000 000 000 000 00		
1943 250.15 0.10 250.15 518.608 513.543 14.696 14.191 2242 0.00 6.94 0.00 8.95 0.00 8.	7531 250.15 0.00 9023 250.15 0.00 0512 250.15 0.00 0512 250.15 0.00 0413 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.15 0.00 0417 250.20 0.00 0417 250.20 0.00 0417 250.20 0.00 0417 270.20 0.00 0417 270.20 0.00 0417 270.20 0.00 0417 270.20 0.00 0417 270.20 0.00 0417 270.20 0.00 0417 270.20 0.00 0417 270.20 0.00	CALPTIO					\$	9000			
9973 250.15 0.00 250.15 518.608 513.543 14.696 14.131 .2242 0.00 6.97 0.000 6	7551 250.15 0.00 1993 250.15 0.00 3434 250.15 0.00 3434 250.15 0.00 7934 250.15 0.00 9417 250.15 0.00 0900 250.15 0.00 0900 250.15 0.00 374b 270.20 0.00 5143 271.42 0.00 7946 273.58 0.00 7967 275.53 0.00 73661 277.23 0.00	250-15 250-15 250-15 250-15 250-15 250-15 250-15				4 <del></del>	\$	9000	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		
9912. 250.15 0.00 250.15 510.688 913.548 14.696 14.191 .2242 0.00 5.09 0.00 0.00 0.00 0.00 0.00 0.00	9023 250.15 0.00 1999 250.15 0.00 3434 250.15 0.00 4966 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 3745 250.15 0.00 3745 250.15 0.00 3745 271.42 0.00 5529 272.54 93 0.00 927 274.93 0.00 927 274.93 0.00 927 275.39 0.00 927 276.79 0.00	250-15 250-15 250-15 250-15 250-15 250-15 250-15					\$	000	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		
1999 250.15 0.00 250.15 510.688 513.548 14.696 14.191 2242 0.000 5.05 0.000 0.	1993 250.15 0.00 3434 250.15 0.00 4966 250.15 0.00 6451 250.15 0.00 7934 250.15 0.00 7934 250.15 0.00 7947 250.15 0.00 7940 2 FLD FELD DE 7945 271.42 0.00 7945 272.54 93 0.00 7957 275.53 0.00 3322 276.73 0.00 3322 276.73 0.00 3322 276.73 0.00 3322 276.73 0.00 3322 276.73 0.00	250.15 250.15 250.15 250.15 250.15 250.15 250.15 250.15			4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		\$\$\$\$\$\$\$\$\$ \$\$\$\$\$\$\$\$\$\$\$	00	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		
1999 250.15 0.00 250.15 516.686 513.549 14.696 14.191 .2242 0.00 3.80 0.000 0.	3434 250.15 0.00 3434 250.15 0.00 5451 250.15 0.00 9417 250.15 0.00 9900 250.15 0.00 0900 250.15 0.00 3745 270.20 0.00 5143 271.42 0.00 5143 271.42 0.00 5143 271.43 0.00 3322 276.39 0.00 3322 276.75 0.00 5907 277.53 0.00	250.15 250.15 250.15 250.15 250.15 250.15 250.15		######################################	444444 ••••••• •••••• •••••		**************************************	0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9	• •
334 250.15 0.00 250.15 518.680 513.543 14.696 14.191 .2242 0.00 2.85 0.000 0.0	3434 250.15 0.00 4966 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 9417 250.15 0.00 9710 2 FLJM FIELD 0E  ATION 2	250.15 250.15 250.15 250.15 250.15 250.15 250.15	111111111111111111111111111111111111111	######################################	44444	A A A A A A	\$\$\$\$\$\$\$ \$00000		3.80	8	•
950 1550-15 0.00 250-15 518-58 513-549 14-696 14-191 12242 0.00 2.05 0.000 0.0	6451 250.15 0.00 0.00 0.494 0.25 0.15 0.00 0.00 0.00 0.00 0.00 0.00 0.0	250.15 250.15 250.15 250.15 250.15 CRIPTIO	11125	E E E E E E E E E E E E E E E E E E E	4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		22222	0	•	5	
14.69   14.191   12.242   10.00   10	7934 250.15 0.00 7934 250.15 0.00 7900 250.15 0.00 7917 250.15 0.00 7918 271.15 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00 7918 271.45 0.00	250.15 250.15 250.15 250.15 CRIPTIO	18.68 18.68 18.68	133.00	4 4 4 6 6 9 9 9 9 9 9 9 9		**************************************	0	2.65	=	•
7314 250.15 0.00 250.15 510.600 513.540 14.696 14.191 .2242 0.00 .55 0.000 659 0.000 6900 6900 6900 250.15 0.00 250.15 510.600 513.540 14.696 14.191 .2242 0.00 6.00 6.00 0.000 6900 6900 6900 250.15 0.00 250.15 510.600 513.540 14.696 14.191 .2242 0.00 6.00 0.00 0.00 0.00 0.00 0.00 0.0	7934 250.15 0.00 0900 250.15 0.00 0910 250.15 0.00 010 250.15 0.00 010 2 FLOM FIELD DE 01	250.15 250.15 250.15 CRIPTIO	18.68 18.68 18.58	13.5	69°4 69°4 69°4	<b>ન</b> ન ન	22¢ 22¢ 22¢	8	00°2	8	•
99.17 250.15 0.00 250.15 510.608 513.549 14.696 14.191 .2242 0.00 0.00 0.00 0.00 0.00 0.00 0.0	9417 250.15 0.00 0900 250.15 0.00  ATION 2 FLOW FIELD DE  1746 270.20 0.00 51+3 271.42 0.00 6529 272.54 0.00 1977 276.39 0.00 1977 276.39 0.00 1977 276.39 0.00 3322 276.79 0.00 3322 276.79 0.00	250.15 250.15 CRIPTIO	18.68 18.58	13.5	4.69 4.69	ਜਜ	35	0	1.22	8	•
ATION 2 FLUM FIELD DESCRIPTION  ATION 3 FLUM FIELD DESCRIPTION  ATION 3 FLUM FIELD DESCRIPTION	0900 250.15 0.00  ATION 2 FLOW FIELD DE  OLUSVELUCITIES  HERID TANGEN  3745 271.42 0.00  5143 271.42 0.00  6529 272.54 0.00  7904 274.93 0.00  927 274.93 0.00  927 276.73 0.00  4661 277.23 0.00  4561 277.23 0.00  7331 277.63 0.00	250.15 CRIPTIO	18.58		<b>4.69</b>	-	54	0	. 55	8	•
## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD DESCRIPTION  ## FILD TANGEN 1074L	ATION 2 FLOW FIELD DE DIUSVELUCITIES HERID TANGEN 17904 273.59 0.00 0927 274.93 0.00 0927 275.49 0.00 0927 276.70 0927 276.70 0927 2	CRIPTIO		13.5				0	0.00	9	•
01USVELUCITIESTEMPERATURESPRESSJRES MACHANGLES QADIUS OF SPEC	01US #ERIO TANGEN 3746 27 0.20 0.00 0.00 0.00 0.00 0.00 0.00 0										
OLIVIS  VELUCITIESS   FIRPERATURESS   FIRPERATURESS   FIRPERATURESS   FIRPERATURESS   FIRPERATURESS   FIRPERATURESS   FIRPERATURESS   FIRPERATURESS	01USVELUCITIES #ERIO TANGEN 374b 27 0.20 0.00 51+3 27 1.42 0.00 55+5 27 5.5 7904 27 3.5 7904 27 5.5 7904 27 5.5 7904 27 5.5 7905 27 6.7 731 27 7.23 0.00 5997 27 7.23 0.00 5997 27 7.5 7331 27 7.5 7331 27 7.5										
#ERID TANCEN TOTAL TOTAL STATIC TOTAL STATIC NO WHIRL SLOPE CURVATURE NE S143 271-42 518-686 512-592 14-696 14-113 .2435 0.00 18-63 -143-697 58 514-3 271-42 518-686 512-597 14-696 14-113 .2435 0.00 18-63 -143-697 58 514-3 271-42 518-686 512-597 14-696 14-113 .2435 0.00 18-63 -143-697 58 518-686 512-597 14-696 14-113 .2435 0.00 18-63 -110-946 512-597 14-696 14-1	3745 27 0.20 0.00 5143 27 1.42 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	1	- TEMBEDA	->36111	7 d c d	1260	HO W	SNA	A	PADTUS OF	•
374b         270.20         0.00         271.42         518.688         512.592         14.696         14.108         .2425         0.00         20.83         -205.758           51.43         271.42         518.688         512.537         14.696         14.103         .2435         0.00         19.63         -143.697           6529         272.54         0.00         272.54         518.686         512.541         14.696         14.096         .2445         0.00         17.23         -117.285           9270         273.58         0.00         273.53         518.686         512.549         14.696         14.096         .2445         0.00         17.23         -117.285           9270         273.59         0.00         274.635         518.686         512.459         14.696         14.086         .2477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.00         14.642         -82.477         0.0	3746 270.20 0.0 51.3 2710.20 0.0 55.9 272.54 0.0 7904 273.56 0.0 9270 274.53 0.0 1977 276.19 0.0 3322 276.79 0.0 4661 277.53 0.0	TOTA	OTAL	STATE	OTAL	STATI	20	WHIRL	SLOPE	CURVATURE	HEI
3745 270.20 0.00 270.20 518.688 512.592 14.696 14.103 .2435 0.00 19.63 -143.697 .558 .543 271.42 0.00 271.42 518.688 512.587 14.696 14.103 .2455 0.00 13.43 -143.697 .573.59 0.00 271.42 518.688 512.541 14.696 14.094 .2455 0.00 17.23 -1401.946 .573.59 0.00 271.42 518.688 512.541 14.696 14.094 .2453 0.00 17.23 -1401.946 .575.33 0.00 275.33 518.688 512.425 14.696 14.086 .2477 0.00 17.23 -1401.946 .575.33 0.00 275.33 518.688 512.425 14.696 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 -52.371 .569 14.087 .2483 0.00 12.40 .569 14.080 .2477 0.00 12.40 .569 14.080 .2477 0.00 12.40 .569 14.080 .2477 0.00 12.40 .569 14.080 .2477 0.00 12.40 .569 14.080 .2477 0.00 12.40 .569 14.080 .2483 0.00 12.40 .569 14.080 .2483 0.00 12.40 .569 14.080 .2483 0.00 12.40 .569 14.080 .2483 0.00 12.40 .569 14.080 .2483 0.00 12.40 .569 14.080 .2483 0.00 12.40 .569 14.080 .2483 0.00 12.40 0.00	3746 270.20 0.0 51+3 271.42 0.0 5524 272.54 0.0 9270 274.53 0.0 1977 275.33 0.0 3322 276.73 0.0 4661 277.53 0.0 5997 277.63 0.0						•				•
51+3         271,42         518,688         512,537         14,696         14,103         22435         0.00         19,63         -143,697         -143,697         -143,697         -143,697         -143,697         -143,697         -143,697         -143,697         -14,946         -14,094         -2445         0.00         17,23         -113,697         -143,697         -14,094         -2445         0.00         17,23         -113,697         -14,096         14,096         14,096         14,096         -2445         0.00         17,23         -14,193         -91,183 <td< td=""><td>51+3 271-42 0.0 6529 272-54 0.0 7904 273-58 0.0 9270 275-53 0.0 1977 276-15 0.0 1977 276-15 0.0 4661 277-23 0.0 5997 277-63 0.0</td><td>270.20</td><td>18.68</td><td>12.5</td><td>j</td><td>4.10</td><td>.2423</td><td>0</td><td>20.83</td><td>202</td><td>=</td></td<>	51+3 271-42 0.0 6529 272-54 0.0 7904 273-58 0.0 9270 275-53 0.0 1977 276-15 0.0 1977 276-15 0.0 4661 277-23 0.0 5997 277-63 0.0	270.20	18.68	12.5	j	4.10	.2423	0	20.83	202	=
6529         272.54         910.640         512.547         14.696         14.096         2445         0.00         17.23         -117.285           7904         277.58         0.00         273.58         516.646         512.541         14.696         14.094         2245         0.00         17.23         -101.946	6529 272,56 0.0 7904 273,58 0.0 9270 274,53 0.0 1977 276,19 0.0 3322 276,79 0.0 4661 277,63 0.0	271.42	18.68	12.6	÷	4.10	.2435	0	19.63	143.	•
7904 273.58 0.00 273.59 518.646 512.541 14.696 14.094 .2454 0.00 17.23 -101.946 9270 274.53 0.00 274.53 518.668 512.499 14.696 14.089 .2463 0.00 15.03 -91.183 .915.18	7904 273,58 0.0 9270 274,53 0.0 1977 276,13 0.0 1977 276,79 0.0 4661 277,63 0.0 5997 277,63 0.0	272.54	18.58	12.5	÷	<b>60 • </b>	N	0	18.43	117.	•
9270 274.53 0.00 275.53 518.688 512.499 14.696 14.089 .2463 0.00 16.03 -91.183	9270 274.53 0.0 1977 275.33 0.0 1977 276.15 0.0 3322 276.73 0.0 4661 277.23 0.0 5997 277.63 0.0	273.58	18.54	12.5	;	<b>60 • </b>	N	0	17.23	101.	•
1977         275.39         10.06         .2471         0.00         14.62         -82.371           1977         276.15         0.00         276.15         516.688         512.425         14.695         14.069         .2477         0.00         13.61         -76.442           3322         277.29         0.00         277.29         516.588         512.373         14.696         14.007         .2483         0.00         12.60         978           4661         277.29         0.00         277.29         518.588         512.357         14.696         14.077         .2483         0.00         11.19         -59.87           7331         277.73         0.00         277.74         0.00         277.74         -518.688         512.357         14.696         14.075         .2492         0.00         9.97         -53.135           7331         277.74         0.00         277.74         518.688         512.357         14.696         14.077         .2489         0.00         7.56         14.688         14.696         14.077         .2489         0.00         7.56         14.688         14.696         14.077         .2489         0.00         9.97         -53.135         14.696         14.077 <td>1977 275,33 0.0 1977 276,15 0.0 3322 276,73 0.0 4661 277,23 0.0 5997 277,63 0.0</td> <td>274.53</td> <td>16.68</td> <td>12.4</td> <td>j</td> <td>4.08</td> <td>.2463</td> <td>ø</td> <td>16.03</td> <td>-91.183</td> <td>•</td>	1977 275,33 0.0 1977 276,15 0.0 3322 276,73 0.0 4661 277,23 0.0 5997 277,63 0.0	274.53	16.68	12.4	j	4.08	.2463	ø	16.03	-91.183	•
1977         276.15         0.00         276.15         518.686         512.425         14.696         14.082         .2477         0.00         13.61         -74.442         3322         276.79         0.00         276.79         0.00         12.40         -66.976         -66.976         14.086	1977 276,15 0.0 3322 276,79 0.0 4661 277,29 0.0 5997 277,63 0.0	275.33	18.58	12.4	j	4.08	.2471	0	14.82	-82.371	•
3322 276.79 1.00 276.74 518.666 512.395 14.696 14.080 .2483 0.00 12.40 -66.978 4.661 277.29 0.00 277.62 518.588 512.373 14.696 14.077 .2483 0.00 11.19 -59.870 .59.870 277.63 0.00 277.62 518.688 512.357 14.696 14.077 .2492 0.00 8.76 -41.080 .53.135 .518.688 512.357 14.696 14.077 .2492 0.00 8.76 -41.080 .53.135 .577.45 0.00 277.77 518.688 512.352 14.696 14.077 .2489 0.00 7.56 -41.080 .512.359 14.696 14.077 .2489 0.00 6.37 -35.682 .5996 277.45 0.00 277.74 518.688 512.859 14.696 14.077 .2489 0.00 6.37 -35.682 .518.688 512.82 14.696 14.077 .2489 0.00 2.93 -25.862 .518.688 512.82 14.696 14.696 14.070 .2484 0.00 2.93 -25.862 .518.688 512.82 14.696 14.696 14.070 .2484 0.00 2.93 -25.862 .518.688 512.82 14.696 14.696 14.08 .2477 0.00 2.93 -25.862 .518.688 512.82 14.696 14.696 14.13 .2477 0.00 1.84 -19.587 .518.688 512.859 14.696 14.13 .2477 0.00 1.84 -19.587 .518.688 512.859 14.696 14.13 .2452 0.00 1.84 -19.587 .518.688 512.859 14.696 14.13 .2452 0.00 -380 -16.750 .518.688 512.859 14.696 14.13 .2453 0.00 -380 -16.750 .518.688 512.8574 14.696 14.13 .2453 0.00 -3.00 -1.91.697 .518.688 512.8574 14.696 14.13 .2453 0.00 -3.00 -1.00	3322 276,79 0.0 4661 277,29 0.0 5997 277,63 0.0 7331 277,79 -0.0	276.15	16.68	12.4	j	4.08	N	0	13.61	-74.442	•
4661         277.23         518.586         512.373         14.696         14.077         .2485         0.00         11.19         -59.870           5997         277.63         0.00         277.75         37.665         512.357         14.696         14.076         .2491         0.00         9.97         -53.135         -55.135         -55.23         -55.23         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.33         -55.492         0.00         0.00         27.77         -516.68         512.35         14.696         14.077         -2499         0.00         7.56         -41.089         -45.95         0.00         7.56         -41.089         -55.20         -35.682         -55.662         -55.	4661 277.23 0.0 5997 277.63 0.0 7331 277.73 0.0	276.73	18.65	12.3	÷	4.08	N	0	12.40	-66.978	•
5997         277.63         0.00         277.63         512.357         14.696         14.076         .2491         0.00         9.97         -53.135           7331         277.73         -0.00         277.74         0.00         277.74         -46.622         -46.622         0.00         7.56.22         -46.622         -6.622         -75.46         -75.46         -75.46         -75.46         -75.46         -75.622	5997 277.63 0.0 7331 277.73 0.0	277.29	18.58	12,3	÷	4.07	N	0	11.19	-59.870	•
7331 277.79 -0.00 277.79 518.688 512.350 14.696 14.075 .2492 0.00 8.76 -46.829 . 9665 277.77 0.00 277.74 518.688 512.355 14.696 14.077 .2489 0.00 7.55 -41.080 . 9996 277.45 0.00 277.74 518.688 512.355 14.696 14.077 .2489 0.00 6.37 -35.682 . 913.2 276.92 0.00 276.92 518.688 512.358 14.696 14.079 .2477 0.00 5.27 -35.682 . 901.2 276.92 0.00 276.92 518.688 512.489 14.696 14.088 .2477 0.00 2.93 -22.862 . 901.2 274.91 0.00 274.91 518.688 512.480 14.696 14.094 .2452 0.00 2.93 -22.862 . 901.2 274.91 0.00 273.39 518.688 512.480 14.696 14.103 .2477 0.00 1.84 -19.587 . 901.4 259.09 518.688 512.549 14.696 14.113 .2432 0.00 1.84 -19.587 . 901.4 269.09 518.688 512.541 14.696 14.113 .2432 0.00 -1.84 -19.587 . 901.4 269.09 518.688 512.841 14.696 14.113 .2433 0.00 -1.84 -19.587 . 901.4 269.09 518.688 512.841 14.696 14.113 .2433 0.00 -1.84 -19.587 . 901.4 269.09 518.688 512.841 14.696 14.113 .2433 0.00 -1.84 -19.587 . 901.4 269.09 518.688 512.841 14.696 14.113 .2433 0.00 -1.84 -19.587 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.587 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.587 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.587 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.587 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.587 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 2433 0.00 -1.84 -19.588 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.113 . 901.4 269.6 14.1 269.6 14.1 269.6 14.1 269.6 14.1 269.6 14.1 269.6 14.1 2	7331 277.73 0.0	277.63	18.68	12.3	j	4.07	N	0	9.97	-53.135	•
8663         277.74         0.00         277.74         515.688         512.352         14.696         14.075         .2492         0.00         7.56         -41.088         .           996         277.45         0.00         277.45         518.688         512.355         14.696         14.077         .2489         0.00         6.37         -35.682         .           2671         276.92         0.00         276.92         516.648         512.828         14.696         14.077         .2489         0.00         6.37         -35.682         .           2671         276.92         0.00         276.04         512.828         14.696         14.07         .2477         0.00         4.06.621         .           4016         276.93         0.00         276.96         14.696         14.08         .2466         0.00         2.93         -22.862           4016         277.93         518.686         512.49         14.696         14.08         0.00         2.93         -22.862           576         27.45         0.00         27.46         0.00         27.69         0.00         1.86         -19.587           677         27.45         0.00         27.47		277.79	18.68	12.3	;	4.07	w	0	8.75	-46.829	•
9996 277.45 0.00 277.45 518.686 512.365 14.696 14.077 .2489 0.00 6.37 -355682 . 1332 276.92 0.00 276.92 518.686 512.459 14.696 14.079 .2484 0.00 5.20 -30.898 . 4016 276.03 0.00 276.09 512.428 14.696 14.079 .2487 0.00 4.03 -26.621 . 4016 274.91 0.00 275.99 518.688 512.459 14.696 14.08 .2452 0.00 2.93 -22.862 . 5368 273.39 0.00 273.39 518.688 512.549 14.696 14.103 .2452 0.00 1.84 -19.587 . 6730 271.45 0.00 271.46 518.688 512.549 14.696 14.103 .2435 0.00 .80 -16.760 . 8104 259.09 0.00 271.46 518.688 512.8741 14.696 14.113 .2413 0.00 -1.09 -1.09 -1.09 -1.2.274 . 8104 259.09 0.00 265.23 1.00 265.23 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	8663 277.74 0.0	277.74	16.58	12,3	.;	4 • 07	w	0	7.56	-41.000	•
1332 276.92 0.00 276.92 516.546 512.390 14.696 14.079 .2464 0.00 5.20 -30.898 . 2671 276.03 0.00 276.06 512.428 14.696 14.083 .2477 0.00 4.05 -26.621 . 276.03 0.00 2.93 -122.808 512.490 14.696 14.080 .2465 0.00 2.93 -22.862 . 25.856 14.696 14.696 14.094 .2452 0.00 1.04 -105.03 -22.005 . 25.85 0.00 1.04 -105.05 . 25.85 0.00 1.04 -105.05 . 25.00 . 10.00 27.00 27.00 0.00 27.00 0.00 27.00 0.00 27.00 0.00 27.00 0.00 27.00 0.00 27.00 0.00 27.00 0.00 1.04 -105.00 0.00 27.00 0.00 1.00 1.00 1.00 1.00 1.00 1.00	9996 277.45 0.0	277.45	18.68	12.3	į	4.07	N	0	6.37	-35.682	•
2671 276.03 0.00 276.08 512.428 14.696 14.083 .2477 0.00 4.05 -26.621	1332 276.92 0.0	276.32	16.60	12.3	•	4.07	N	0	5,20	-30.890	•
4016 274.91 0.00 274.91 518.686 512.480 14.696 14.088 .2466 0.00 2.93 -22.862 . 5368 273.39 518.686 512.549 14.696 14.084 .2452 0.00 1.84 -19.587 . 673 25.635 0.00 2.71.45 518.688 512.549 14.696 14.103 .2435 0.0080 -16.760 . 810 2.69.09 518.688 512.741 14.696 14.113 .2443 0.0018 -14.338 . 671 256.23 0.00 2.543 0.0018 -14.338 . 672 256.23 0.00 26.243 0.0018 -14.338 . 672 256.23 0.0018 -14.338 . 672 256.23 0.0018 -18.548 . 672 257 0.001.011.011.011.011.011.011.011.011.011.011.011.011.01	2671 276.09 0.0	276.08	18.58	12.4	;	4.08	N	0	4.05	-26.621	•
5368 273.33 - 0.00 273.39 518.686 512.534 14.696 14.094 .2452 0.00 1.84 -19.587 . 677 271.45 0.00 271.46 518.686 512.635 14.696 14.103 .2435 0.00 .80 -16.760 . 681 4.5760 . 681 4.696 14.113 .2435 0.0018 -14.3760 . 681 4.696 14.113 .2413 0.0018 -14.338 . 681 4.696 14.113 .2413 0.0018 -14.338 . 681 4.696 23 0.0018 2.6568 512.74 14.696 14.135 .2357 0.00 -1.09 -12.274 . 681 4.696 14.135 . 2357 0.00 -1.09 -1.09 -12.274 . 681 4.696 14.139 . 2357 0.00 -1.01 -1.01 -1.01 -1.01 -1.01	4016 274.91 0.0	274.91	18.68	12.4	;	4.08	.2466	0	2, 93	-22,862	•
6730 271.45 0.00 271.46 518.688 512.635 14.696 14.103 .2435 0.00 .80 -16.760 . 80 40.950 0.00 .80 1.6.760 . 80 80 80.00 . 80 1.6.760 . 80 80.00 . 80 80.00 . 80 80.00 . 80 80.00 . 80 80.00 . 80 80.00 . 80 80.00 . 80 80 80 80 80 80 80 80 80 80 80 80 80	5368 273,39- 0.0	-273.39	18.68	12.5	;	<b>60 • 4</b>	N	0	1.84	-19.587	•
8104 259.09 0.00 259.09 518.688 512.741 14.696 14.113 .2413 0.0018 -14.338 9433 256.23 0.00 266.23 518.588 512.867 14.696 14.125 .2387 0.00 -1.09 -12.274	6730 271.45 0.0	271.46	18.68	12.6	;	4.10	N	0	. 80	-16.760	•
9433 266.23 0.00 266.23 518.688 512.867 14.696 14.125 .2387 0.00 -1.09 -12.274 . Noon 285.88 6.00 262.83 -448.888 613.016 14.696 14.139 .2357 0.00 -1.91 -10.518 .	8104 259.03 0.0	269.09	18.68	12.7	÷	4.11	.2413	0	18	-14.336	•
NOTE 25.25 R. D. D. 252.47 14.48.68 413.616 14.439 2357 D. D. D. 2110.518	9493 2b6,23 0,0	256.23	18.58	12.8	;	4.12	.2387	0	-1.09	-12.274	•
	26.2.4. DE 26.2.4.	269.44	48.68	14		7	2357		10.1	-10.518	

STATION 3 FLOW FIELD DESCRIPTION

i

					100	֡֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֜֜֜֜֜֓֓֓֓֓֓֜֜֜֜֜֜֜֜֜֓֓֓֓	<u></u>	ししていること	5					
-LINE		FIU	TANGEN	TOTAL	TOTAL .	AL STATIC	TOTAL	TAL STATIC .	0	WHIRL	HIRL SLOPE	CURVATURE	· · #E16HT·	,
+	•	2	9	292,59	- 0	11.5	÷	_	.2627	0.00	20.54	2	. 1732	-
~	6.7266	29 4 . 25	00.00	94.2	518.688	511.575		14.001	2492	0.00	19, 35	-122.112	.0731	
m	•	•	0	•	•	11.4	÷	on.	.2058	0.00	18.17	<u>N</u>	.0751	
\$	6.9741	297.73	0	۲.	Φ	11.4	j	₽	.2674	0	۰	<u>بر</u> ۱	16/0.	
ķ	7.0967	6	0	299.56-	Φ	##	j	S.	•2690	0	ŝ	Ž,	90/9°	:
9	7.2187	30 1. 28	0	4	۰	11.2	14.696	ത	N	0	÷	<u>.</u>	.873	_
~	7.3400	302.83	0.00	40	Φ	11.1	÷	or.	.2721	0	13.27	2	. 6730	_
•	7.4607	;		304.34	Φ	11.0	j	gr.	.2734	0	'n	2	.0729	_
•	7.5811	305.00	0.00	305.60	S	11.0	14.696	5	~	0	10.71	<u> </u>	. 6729	_
10	7.7011	ġ	0	9	Φ	10.9	÷	o	N	0	9.41	-81.121	62/0	_
	-7- 8669	- M - COT	00.0		۵	10.3	÷	œ	.2761	0	6.10	-624632	6729	-
15	2046.7		0		Φ	10.3	4	ס	.2765	0	6.77	-48.842	.0729	_
) M	A. 0606	307.83		307.63	۰۰	10.9	14.696	σ	N	0	5.44	-39.219	.0729	_
) <u>4</u>	0000		· a	307.50	۰	10.3	4	o	.2763	0	<b>60 •</b>	-31,865	.0729	_
	770		, c	396.74	•	4.0	3	σ	~	•	2.74	-26.067	. 1729	_
n u			, c	306.43	) u	1 1 2		. 0	<b>N</b>	0	1.36	-21.421	. 1729	
9 1	1000	•	9	14.6.00	ď		14.696				. 81	17.671	8730	_
  -  -	School.	å.	9	֓֞֜֜֜֜֜֜֜֜֓֓֓֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֜֜֜֜֜֜֓֓֓֜֜֜֜	Dυ			ם י		) C	72.4-	-14.639	02.20	
0	6. 5555	<b>:</b>	<b>-</b>	7.5	0 ،	7	•		9 6	Э С	100	42.404	12.34	
13	8.7940	9	٠	96	٥	11.	•	,	1000	<b>9</b> (		16464	7666	
20	8.9209	÷		34.0	മ	11.5	14.696	•	ž	3	71.	70701	40.00	
21	9.0500	289.28	00.0	289.28	•	11.5	9.	0	23	0	-5.47	-8-69	25.184 .	
ï	STATION	* - FL3#	FEELD DES	GRIPTION	•								:	,
1	91110	7	7		CHEL	ÿ	P2FS	- !	HOTH	ANGLE	ES	RADIUS OF	SPECIFIC	
0 7 C A C	20104	010		TOTAL	TAL	STATE	)	STA	2	HHIRL	SLO	SURVATURE	MEIGH	
1					•	•	•							
+	-6.7598	- 31.7. 14 ··	0.00	317.14	-518.68c	510.427	14.696	13,891	.2651	0.0	20.32	-388.054	. 8727	_
~	5.8661			9.9	ø	0.	;	13.876	.2877	0.00	19,31	151-167	.0727	
: PF	F. 981.3	М.	9	3.0	80	9	;	13,861	.2904	00.0	16.23	85.997	. 8726	
<b>.</b>	7.0957	326.12	00.0	···	ല	6	į	13.845	.2933	00.0	17.09	66.084	. 0725	
u	2000	42 0 43	•	-		6	j	13.630	N	0.00	15.90	60.373	. 1725	
٠ ١	7. 2240	33.14	•	! -	•	6	14.696	13.614	.2988	0.00	14.67	61.039	. 1724	
, ,	7.644	224,00	4	3	•	6	j	13.800	~	0.0	13.38	68.416	- 6724	
. •	7 54.00	74.7	•	337.44		2	;	13.787	77	0.00	12.04	85.639	. 0723	
9 6	1000	77 022		35 022		g		13.775	17	00.0	10.67	26.	6723	-
r	00000		•	26.4.62	•	٥	٠.,	13.765		00.0	9.27	285.037	.1722	
<b>3</b> (	1007	76 74 76	9 6	747	Э 0	9	٠.,	13, 757		00.0	7.86	048.	. 0722	
; H (	2010.	24.00	9 0	243.6	9 2	, 0		17.751	, ,,	0,0	9 6	-279,655	. 0722	٠.
21	1.9061	34 4 9 15	•	244010	3 0	9		14.7.7	7 17	9 6	6	156	- 4722	
-	1060-0	CD 24 00	•	- FP - L - F	0 0		•	17. CT	"		7, 5,	192	. 0722	
7	5.2063	34 5. 32		242466	0 .	9	;	130140	7 6	•			4722	
-61	6. 5169	ň.	•	040.00		ġ	14.050	177 AT	יו כ		<b>4</b>	-40.335	4722	
91	8.4279	344.91	•	344.91			•		2010			,	664	
44-	4.5397	ë.	•	343,93	₽ .	8	<b>.</b>	13.752	95050	•	11.15	֓֞֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֡֓֡֓֓֓֡֓֡֓֡֓֡	2000	
97	8.6525	342,28	0	342.28	518.588		14.696	13.761	1000	•	0 1 2 1			
+	\$	ŕ	•	300		Š	j.	134774	00000	•	1004	•		
20	8.8822	226.25	0,00	346.25	œ	104,004	46.696	13.793	• 3 0 2 5	00.0	-b. 55	192.41.	ry/n•	•
		;	>	,			•						1000	

•

⋖
<b>b-</b> -
⋖
Ö
w
0
⋖
S)

POLYT20 EFFICIE	1.000	7-000		1.000			1.0	1.1818	1.100	1.000	1.00																																
ISENTROPIC P EFFICIENCY S	1.0003			= 5			:=	=	=	' =	2								9 (	1.6966		SPECIFIC		. 1777	. 0777	. 1776	.0775	.1776	.1776	.1776	.8776	6777		.8778	. 1779	.0760	.0761	.0752	2918	40.00	70/01	07.00	) ) . > >
DELTA T	0.00	2	2	2	2 6	3 5		2	8	8	2	2	2 2	2 2	2 2	2 2	3 2	3 8	3 3	8		RADIUS OF	SJRVATURE	•	7.865	10.896	18.179	56.410	-54.300	-19.138	-11.963	-7.24	-6.253	-5.654	-5.316	-5.186	-5.251	-5.549	-6.186	354.7-	700 BT -	-1665-883	****
PRESSURE Ratio	1.000	8	6	8	9			8	8	9	=	5	3		3 6	•	3 6	3 6	3	6		SLES	SLOPE	22.							11.21									92.4-	0 1	0 M · 0 I	7
REL AF IVE EMPERATURE	600.9																	?•	•	•		ANGLE	MMIRL																			74.45	24.00
-	598.																	-	•	Φ		MACH	<b>Q</b>	.3251	.3284	. 3313	.3338	.3363	.3391	.3417	.3441	1047	3648	3513	.3531	.3550	.3569	3588	.3606	3621	22020	35050	2000
RELATIVE	24.236	2	2	2	8 8	2 6	2 %		2	28	2	2	3	ה ה	5	3 ;	÷ ;	č	3	ž		JRE S	STATIC	15.280	15.265	15, 255	15.248	15.247	15,251	15.261	15.279	17.504	15.5.5	15.420	15.469	15.522	15.577	15.633	15.688	15.741	15.769	15.569	17.000
RELATIVE VELOCITY	1033.25	1050.22	1067.14	1083.96	1100-66	1117.21	1153 - 60	1165.91	1181.83	1197.61	1213.28	1228.88	1244.41	1259.90	1275.35	1230.78	1500-18	1361.90	1330.98	1352.37		PRESSJRES+-	TOTAL	16.439	16.443	16.457	w	16.486	w	vo	16.581	D 4	3 W	16.791	16.059	œ	17.009	17.086	17,161	17.232	17.24	17.347	100°
RELATIVE MAC4 VO	98 26	2946.	g,	<b>7</b> (	Ē	1.0050	36	3	0	1.0780	1.0922	1,1063	1, 1203	1, 1342	10 14 01	7:	4	9 6	Ю.	1.2165		URES-	STATEC	525.143	525.127	525 .143	525.204	525.301	525.447	525.692	526.073	770.77	328.843	29.620	30.773	31.855	32.954	34.244	35.576	36.573	57.553	538.455	22.0
BLADE	983	1000	1017	1033	1050		2001	1115	1131	1147	1163	1179	1195.5	1211	1771	7	1260	1771	1294	1311		EMPERAL		36.183	36.400	36.613	36.849	37.125	37.470	37.912	38.468	23.00.07	53.500 b1.241	42.625	43.940	45.191	46.464	47.931	49.432	50.679	51.554	52.654	22000
LOSS	00	8	8	8	9 6	0.0000			30	8	00	8	00	9	8	3	3	9 6	8	8	PTION	•	AL T	•	41			· w	10	ď	ın (		1 14	, 41				'n	in.		~ .	6.15 5 7.36 6	
DEVIATION INCIDENCE	9.459	2	. 791	2		\$	0.014	1.028	1.044	10.075	1112	1.157	1. 224	. 320	2445	1997	65.	550.	1 • 081	***	SCRI		TOT	366.	370	373	376.	379.	382	385.	338.	391	, 40 to	396	<b>+00</b>	403	405	40 P	410.	413	• • • • • • • • • • • • • • • • • • •	416	17.
		•	•	•	•	1	7 7	•	' ï	7	7	7	7	7	7	ï	7	7	ï	7	30 073	CITIES	TANGEN	9.0	05.6	0.5.3	1 2 1	15.2	05.6	06.7	0.9.3	7 • n •	) 4 0 1 1 1	24.5	29.8	34.6	39.4	45.0	50.6	6 ÷ 6	900	9	030
REL FLOM	-72.1	-72.2	-72.3	-72.4	-72.5	-72.7	-72.0	-73.0	-73.2	-73.3	-73.5	-73.7	-73.9	2.4	2.		2.5		-12.	-75.8	FLOW FI	VEL	RIO	1.14	'n	9.6	1.65	4.62	:	0.75	3.15	27.6	01.0	8.02	8.87	9.93	÷	1.74	å	2.85	74.5	3.73 2.83	60.0
-ANGLES	17.205	16.455	15.442	14.158	12.172	11.442	10.233	1 K K K K K K K K K K K K K K K K K K K	7.673	6.838	5.146	5.620	5.227	906*	4.501	4.116	3.586	166.2	2.386	1.636	TON S	15	¥		35		36	38	35	2 37	37	200	3 6	'n	5 37	2 37	38	38	7 38	38	50 C	96	97
BLADE-A	-62.567	53	23	5	۲,	Ž:	9 6	2 2	5	2	3	ķ	9	3.77	90	95.50	90	02.4	4.35	64.476	STATIO	RADIUS		-			~	7	٠,	r.	91	•	•		٠.	~	٣.	₹.	'n	8		9 4 3 3 3	;
LOCAT						•											<b>9</b>		20	- 12		STREAM	-LINE	-	۰ ۸	J PT		· w	•	۰	•			1 7						•	: 61	<b>8</b> ;	12

4	
Η.	
Š	
21	
3	
5	

ROPIC IENGY-	90		, K	2	9	57	32	5	<b>9</b> 9	:	<b>#</b>		• •	::	22		72	<b>.</b>		33			:																	•			
POLYTROPIC	. 9616	1			.93	.926	.916	.91	5	•		7		Ñ		•	.75	. 75	*	, 73	•																	•					
ISENTROPIC P	9612	3240	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	9362	9315	9255	9168	9686	6969	. 1199	8381	1616	1000	000	77.75	1010	7516	7457	7379	7269		4	MEIGHT	90	•	8	8	9		9 (	2 :		•	98	8	3	•	2	8	. 5823	۰ ٥	5290.	•
ISEN	•	•	•	• •	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		u		25	•	= :	9	5	e :	2 9	<b>.</b>	! :	. 5	7	33	6	2	2	<u>m</u>	40.	<b>u</b> :		2
DELTA T	980.			486	.036	. 037	. 038	. 039	. 041	n de u	• 040	* to *	100.	* 00 *	• 026	660.	. 062	• 06 4	• 066	. 067		9116	CURVATI	F • 3	2.5	6.5	8	11.0	15.9	• • •	100	18 18 19 E	-28.8	-21.5	-18.0	-16.2	-15.5	-15,6	-17.0	-24.4	F	-51.3	I 000 + 0
RESSURE RATIO	1-119	;;	7 6	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֡֓֓֓֡֓֡	12	12	.12	.13	.13	•13	\$	:	::	ij	919	• 15	•17	• 17	55	.13		ć	SLOPE		;	å	ċ		15.17	ů.	••	1 4	3, 77	1.80	03	-1.70	ņ	•	Š.	40	•	•	•
TIVE P	518	•	00	4 4			m	-	-	m	σ,	an ı	м (	ю (		•	-	ın.	m	►		- 3	MHIRL	'n	å	ċ	÷	÷	ċ	÷,	, ,		; ;	: 4	å	ņ	m.	;	ů,	36.18	٠,	٠,	:
E RELA	601.5		, u		, w	· ·	w	w	Ψ	ų,	u		υ.			ψ,	w	w	w	w		•	E 0	1	13	15	17	.4183	56	7	6124	100	3 5	4 28	.4310	33	32	• 4 38 0	7	4426	‡ !	Ĵ.	. 4453
RELATIV	24.030	*	0 A			•	•	٠.	~	Λ.	in.	•	<b>N</b> 1	Λ.	~	Aı.	•	_		മ			STATIC	. 32	• 25	• 19	. 13	• 09	. 05	S O	50.	9 6	2 -	92	.05	• 07	11.	• 15	5	17.234	?	.32	. 35
RELATIVE JELOCITY	20.596	•		200		057.	070	083.	94.	103.	111.	120.	150.	139	143	156.	165.	178.	183.	200.			OTAL S	465	407	359	314	274	243	/ 22	422	163	27.8	319	369	456	684	561	638	9.710	111	0 7 0	69.6
VE 0																							; <u>≃</u>	-	-	+	-	-	-	-		→ •		•	-	-	-	-			-	₩,	-
RELATI	. 3553	7	c d	1000	. 6	. 9367	ま	35	36	97	. 3911	6	3	9	1.0091	5	• 02	33	<u>*</u>	95		1	STATIC	6.44	44.5	44.2	44.0	43.8	43.V	43.		• u	1 (	48.7	50.4	51.9	53.4	55.4	57.6	559.353	2009	62.2	94.0
BLADE SPEED	1004.9	מינו מינו	200	100	90	260	111	125	141	155	70	1 8	199	213	228	242	257	272	86	0		1	I E H P = K &	~	•	ď.	٠,	۲.	٠,	91	ຕຸ	• •	: `	. 60	~	2	W.	ŝ	7	1.129	۰	w, i	۳.
33S 0EF=	0105	٠,	٠.	٠.	٠.	. 4	~	N	N	m	4	S	9	9	~	œ	œ	•	T	ኍ	, , , , , , , , , , , , , , , , , , ,		12	in O	i,C	J.	ņ	96	910	2	. O.	0 11	יי מ	9,10	5.5	5.7	57	2	2.0	10 i	U .	ים ים	7
TION C	410	• 565	•		330	325	•	305	. 762	. 062	584	273	. 672	275	275	•	•	•	•	•	CAIPTIO		TOTAL	r,	'n	:	÷	÷	<b>.</b>	ů	፥.	ė.	• -			ċ	:	÷	å	515.25	:	å.	•
DEVIA	•	0	ה ו	0 1	7	•	100	10	7	T	~	p	20	e e	ກ	10	70	ř	n	n	3 03S		IIIIS-	ľ	თ	70	G	*	3 1	S	┥(	Vu	١ ١	•	۰	~	9	ď	۵	4.20	*	∾.	-
FLON		9 1			35	*	9	. 7.3	36	£.	• 12	- 24		*	3.0	.70	*	3.	٠1,	. 35	FIEL	9	TA TA	٠,٥	10	S	'n		4	.*	\$.	* :	• 4	۱ vo	۵، ۱	~	~	n	σ	364	_	<b>+1</b> .	-4
α 11 <b>14</b>	5.	Ç,	ָרְי וּ	1	U		i.	+	,C	Ĵ	~	-7	-	-	-7	~	~	-7	-	-	F. C.F.		RID	ň	÷	ň	2	;	;	:	å.	÷.	, -	: 6	6	6	÷	å	ۀ	9, 88	å	;	.2.73
NOLES	10.492	ָי יַ	٠, د	•		٠٠	7	~		10	۳.	•	`•	۰	`•	۲.	8	20	~	ŝ			, ,		۵	٥	_	,	4	'n	"ი.	·	0 15	٠.	ຸດ	~	•	٥	0	T* *	_	다. 6	7
SECTION	252	קי	Ü	23	2	1	23	7.	50	2	83	9	3	£ :	8	4.5	55	7	33	50	STATIC		44 UIUS	. 1073	. 172	. 264	. 354	. 443	.530	.017	. 703	F 0		740	134	. 223	. 312	<b>~</b> 00.	. 493	3,585	6/9.	.772	.00.
LOCAT	í H								0	+		m	,	s.	ø	_	so.	19	0	7			SI AEAR	-	~	m	•	'n	ه ه	•	<b>10</b> (	7 (	> + + +	15	F 1	4	15	• 16	17	<b>€</b> 0 (	<del>1</del> 3	20	21

BLADE DATA

POLYTROPIC EFFICIENSY	9896*	. 9635	.9577	1256	6946.	.9419	. 9355	6076	6716	87.4	56.45	. 8215	. 6043	.7883	.7683	4842.	.7349	.7261	.7161	.7034
SENTROPIC !	.9683	.9621	• 9560	5 B C C C	9446.	•9396	9330	0000	#16.	8668	.6374	.8144	.7964	1611.	.7587	•7379	.7237	.7145	.7039	.6905
DELTA T IS	•	•	80	9	8	8		3	9 6	2	9	=	=	10	끆	_	12	12		200
PRESSURE RATIO	.32	. 32		?	5;	3	1.308	,	2	×	31	31	.32	.32	.33	.33	.34	.34	.35	.35
E AFIVE MPERATURE	505.303	2.00	1001		7:	17.05			. ייי טער	60	31.3	33.3	36.3	38.5	41.4	1.55	46.3	ξĐ.	52.3	55.
LATIVE R	28	157	757	00.0	200	500	700	2 6	124	316	989	114	183	360 6	172	570	757 6	119 6	9 59	9 99+
LATIVE RE	6+	•	.33	67.	T (		200	1		.51	10.	. 91	• 02	.14	. 86	.01	96•	. 33	.18	.75
111 VE 2E 1 10 VE	69	21	0.00	2 6	V 8	D (	2 5	1 3	, M	1 06	35	35 1	76 1	17 1	33 1	ί,3 1	81 1	다 강	97 1	39 1
LAUE RELI	31.2	·	56.3		• • • • • • • • • • • • • • • • • • • •		22.3	4.4	2.74	59.7	72.4	85.1	. 0.86	11.0	24.1	37.4	50.8	68. 4.49	78.1	91.9
JEFF S	0215 10	1620	0282 10	7700	1 0000	17 6050	11 6290	04.84	0569 11	0764 11	0948 11	1095 11	1212 11	1324 12	1473 12	1627 12	17.51 12	1795 12	870 12	968 12
IDENCE C	4.295	212.0	3.555 3.50	243		1000	8.395	F 0 4 . 8	3.40	5.415	8.419	8.421	8.42	8.42	3.42	8.41	d.412	Q . 40	3.40	8.40
AGE INCI	986		551	100	3 6	0		701	980	.072	.24	.413	.546	672.	.910	• 384	.283	, .	2+1	.00
EAN KE	3.782 -52	100	אר אר		2 7		7.86	851	23	778	.95		609		137	£24	0 31		0 2 0	366
SECTION L	590		77.	2 6 1 4	7 2	900	115	298	431	658	828	966.	164	327	491	. 568	.871	660	345	508
NO H										+	N	m	3	w,	۰ م	i.	•		20	

	POLYTROPIC EFFICIENCY	.9701	C406.	9356	.9500	.9457	.9461	. 9318	. 9239	0016.	25.00	. 8321	.8150	1990	1790	.7591	.7456	.7366	.7267	.7144	~ 1																					
	ISENTROPIC P Efficiency e	.9683	4296	9518	6946	.9424	.9363	.9275	0616.	2000	C448	6211	8028	7856	.7640	.7425	.7278	.7180	.7072	.6938	0N T H .15		SPECIFIC		•	•	4000	•		•	•	•		-	•	•	•		•	•	•	•
	DELTA T IS	.133	\$ 7 F *	136	.137	.138	.140	.142	• 144	. 147	101	164	173	179	.187	.196	. 203	. 208	.214	. 221	DELTA T (		DIUS OF	CURVATURE	-1.883	-2.146	-2-473	44.4	-4.115	-5.086	-6.519	-14.012	-21.564	-48.509	-1501-015	67.505	30.00	40.680	86.583	-365,485	-86.797	816564.765
	PRESSURE Ratio	1.531	•	• •		•	•	•	•	1.552	•		1.58.	•	•	•	•	1.632	•	1.653	60 H 60 H 71 H		į	SLOPE	16.56	14.57	12.66	200	7.31	5.61	3° 94	6.36	. 83			-5.00	-2.25	-6.21	-6.92	-9.45		37.
	RELATIVE TEMPERATURE	611.744				-	_	~	•		Α.,		•			-	-	~		•	PO_Y. EFF		ANG	WHIRL	40.	41.	41.55		2	43.	ř.	2 4	46	48	50.	51.		52,	5.8	60.	629	63.
	tel 141																				827		MACH	0	26	16	.7084	5 U	3	6 85	51	770	? 2	699	8	699	27.0	: 2	686	35	• 6 995	3
	RELATIVE PRESSUR	25.911	26.103	26.4.49	20.703	26.91	27.107	27.26	27.436	27.51	7.00	27.12	27.11	27.107	26,999	26.871	26.87	26.588	27.07	27.095	EFF. H		SS	STATIC	18.722	16.875	19.012	13.133	19,345	19.435	19.517	19.591	19.724	19.790	19.857	29.928	20.00	20.187	20.302	20.432	20.574	20.725
	VELOCITY	836.57	3 ,	2 5	8	75	31	ŝ	8.	891.95	o i	? ?	; ;	3	22	43	39	7	841.37	38	75 ISEN.		P2ESSU	TOTAL ST	676	565	26.55d			265	609	629	55.1	701	788	30.5	4.0	. 0	916	125		9.6
	RELATIVE	.7217	.7269	74.45	7474	. 7530	.7579	.7510	. 76 42	1540	N C / C	444/·	7424	.7277	. 71.85	73.87	. 70.35	. 7035	.7022	.6983	ATIO = 1.5		JRES	STATIC	395	212	573		110	4.85	0 93	7 4 6	137	4 95	4.25	1964	24.4	8 9	963	.557	711	19.585
	BLADE SPEED	1065.3	1075.1	1004	1106.1	1113.3	1123.4	1133.2	1143.0	1153.0	1103.2	1113.7	11001	1205.9	1218.7	1230.6	1243.2	125b.0	1269.0	1282.3	ESSURE &		TEMPERAT		.861	346	865		50.00	381	478	0.00 to 10 t	) M	118	359	745	200	037	756	.557	N	1.3
	105S 30EFF		.0382	ייכ	9 0	0	.0585	0	C	. 1853	~ .	4 T	4 +	• •	• •		•	N	80	. 2352	• !	N I	•	-	10	177	53	n ·	o ve	•••	יחי	.n	, 10	y y	٠,	יחי	0 (	, ·r	שיר		so .	.0
	STATION INCIDENCE	_	9 6	מ מ	500	100	3	37	ğ	32	2 5	2 6	5 6	3	5	53	51	72	10	8	7. 0.1	SCRIPTION		TOTAL	4	35.	•	,	2 6	, m;	66	9 6		3.	96	66	•	22	32.	.;	353.4	59
	LONT 3									· · · · · · · · · · · · · · · · · · ·											4 (51	20 577	CITI	ANGEN	43.4	48.8	20 f	P ( )	7 . 4	48.0	50.3	2 7 7	76.6	95.8	13.1	26.7	45.0	ה מי מי	17.6	34.3	54.1	80.2
	Ret FLS Avge	-53.290																			NTEG	FLOW FI	VEL		25	33	30	<b>.</b>	1 15		E :	7 1	0 10	, ic	•	<u></u>	<b>n</b> 6	2 2		65		93
DATA	NGLES	5.962		ָ ער יי	, ,	10	4.4	3.9	3.3	2.7	7.7	0 M	2	'n	۰.	~		•	. ~	3.033	2	en 1	;	Å.			618.										4 4	7 1	40.0	Ŧ	39	38
BLAUE	SECTION	- 115	- 611	1000	573	920	55.5	. 025 -	+34	509	e e	704	4 .5		796	10	2	7	. 05	33	TATIO	STATIO	RADIUS		3	40	7.5709	יע		7.7666			י ס		•	•	~ .	, r	, ,	u,	Ψ	
	LOCAT - TON									01								19		;;;			ST46. '	-LINE	71	~	ო.	<b>P</b> U	n ve	~	•			15				-	0		50	

ď	
A	i
ã	į
ä	ì
BLA	į
Ø	

쏦ᄎ					:											•			,													:											
POLYTROPIC EFFICIENCY	.9721	.9658	.9618	.9569	4266.	9460	7746	4676	9116	1000°	. 8515	.8284	.8195	.7920	.7702	. 1691	.7350	.7264	.7175	.7870	•		; ** <b>-</b>	-	_										_	_							
ENTROPIC	1696.	.9640	. 9585	.9532	5840.	. 4460	2000	6816	9032	.8699	.6367	.6134	. 7929	.7736	1641.	.7263	.7106	.7008	° 5905	,6783	7 · · · · · · · · · · · · · · · · · · ·		SPECIFIC	.0928	•		•	-	2500	, ,	, 0	•	•	•	•	63	•		о (	Pe	7000	.0858	
DELTA T IS	.189	.190	19	. 192	13	12	194	; 5	2	.212	22	22	.236	2	• 256	• 269	.280	.289	.300	.314		;	CURVATURE	2	ž	2	2	3	5 4	i u	1	9	9	3	3	'n	დ :	4	2 :	Z !		20.749	
PRESSURE Ratio	.80	.83	.80	99	5		1.610		. 81	18	. 61	• 82	. 83	• 8	.85	.87	.83	•	46,	.97		!	SLOPE	•	σ	N	•	თ∘	5.15	• •	<b>)</b>		S	₽	S.	4	31	m,	<b>3</b> 1	S o	9 6	-8.95	
Af I VE IPERATURE	0	NI.	•	.0 (	70 (	NI .	25.146	٠.4	•	'n	-	m	•		•	C		J.	.0	*			HHIRL	45.	<b>4</b> 6.	<b>*</b> •	46.	• 9	•	4	9	*7.	6.4	51.	53.	54.	200	200	• • • •	20.5	•	69.74	
IVE RE URE TEM	•	•	Q	Φ,	۰ م	י פ	51 62	2	40	ο.	ø	Φ	ø	ဖ	ø	۰	ø	ø	Ø	ø			N O Y	2	7	2	9	800	5 6	1 5	7 80	3	772	69	3	6	2	3	8 :	# ;	ì	, 6286	
RELAT	3	ñ	ø	•	Ď.	'n.	27.1			٠.	*	ᅻ	σ	Ċ	3	9	ڻ	Ġ	ø	<u>`</u>			STAILC	9.70	9.79	9.85	9.91	9.95		00	6.6	9.97	9.95	9.93	9.91	9.90	9.69	. 6	,		? .	20.286	
RELATIVE VELOCITY							825.52															1	TOTAL	3.76	0.65	0.57	n. 48	0.39	0.51	מים בי	9.85	9.71	9.59	9.47	9.42	9.42	9.43	29 6	0.33	2.5	7967	51.794	
RELATIVE MACH NO	72	• 7159	77	, 70 94	2 5	25	2007 •	2	6	2	• 65 65	Ś	8	5	3	ŝ	ŝ	ů,	25	53		:	SiATIC	67.1	68.5	69.7	70.9	71.7	77	7 2 7	75.3	77.9	82.5	87.3	91.5	95.5	99.5	0.50	11.5	10.0	יייי אינייייייייייייייייייייייייייייייי	631.6°	
BLADE SPEED	1089.6	1095.2	1103.0	1109.3	1110.9	1124.1	1139.0	1146.7	1154.5	1162.5	11711.5	1180.7	1190.3	1200.3	1210.8	1222.1	1233.9	15.46.4	1259.2	1272.7			-TEMPERAT OTAL	446	341	133	:15	230	D C C	) M	200	366	254	326	333	365	919	5 C	69.	160	0 0	17.312	
L388 33EFF	*	ŝ	S	96	מ מ	٠,	0.0973	6	=	13	•	2	24	56	5	30	Ĵ	3	5	39	TEON		. <u></u>	·U	(1)	•••	ď		., .,	, .	, (1)	Ψ,		Œ.	****	ω,	,		υ,	<i>D</i> F		25 7:	
VIATION	j	•	÷	:	• .	<b>:</b> .	13.860			'n	÷	÷	÷	'n.	÷	ň	÷.	÷	÷	:	DESCRIPT		N TOTA	966.	958.	955•	. 946	941	937	926	921.	917	917.	917	920	924	928	9020	973	• P 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1001	7 1024	
FLOW JE	- 560	015		637	0 P	13/	415 -1	900	574	119	6+2	142	534	124	533	171	714	216	563	132	FIELD		TANGE	-4	•	**	•	∙ .	<b>*</b> a		۰.		- 70	ın	·n	~	о.	-	N 4	о ::	•	961.17	
RÉL	1	Ť	7	5	2	<b>+</b> 4		1	94	74-	-47	84	-+8	•	<b>.</b>	-50	יי	-51	-51	ţ			ERIO	73.51	LD.	Φ.	O.	oo ⋅		, .		· OT	w	•	or (	N	т.	Ν.		-	, ,	354.75	
-ANGLES N LEAN	N	5.9	5.4	∞ •	•	9 6	1.934	1.2	ം	0	. 47	σ.	m	1.65	œ.	۳.	۰	٥,	ņ	٣.	ATIGN 9	,	) E	19 65			-															0 f	
SECTION	25.42	25.48	27.47	23.40	77.67	20.00	3 6	32.22	32.86	33.45	34.02	34.55	35.05	35.54	35.02	35.52	37.00	37.43	37.78	39.13	STAT		NA OLO	•	•	•	٠	•	7.7		•		•	•	•	•	6		٠	•	•	8.66	
LOCAT	٠	•	٠	•	•	• •	- 00	٠	•	•	•	•	•	•	•	•	• •	19	20 -	•		0	-LINE	-	~			'n,	۸ م	. «	•		11	- 12	M ·	*	12	01	71	n d		21	
																•		23	٠ (				•				•					•											

	<b>υ</b> >				ţ						,					1						:					i				,		1							
	POLYTROPIC EFFICIENSY	.9727	.9673	9206		9472	9646	. 9313	.9219	9329	-8725-		1004	7744	7482	7261	.7105	6669.	. 5885	.6754					-														_	-
	SENTROPIC FFICIENDY	.9697	.9638	. 47 V.	976	9415	5486	.9241	.9138	.8962	• 659¢	.6241	1774	77.	7223	6973	.6797	.6675	.6544	.6393			E WEIGHT	•	•	•	•	• •	•	•	•	6888	•	•	•	• •	•	•	•	•
	DELTA T I	.241	. 241	242	244	243	243	.244	. 244	.247	. 256	592.	****	200	308	328	343	354	. 367	.383		RADIUS OF	CURVATUR	9.349	11.318	13.086	16.484	15.679	15.643	15.296	14.696	13.010	11.979	10.952	10.02	6.565	7.994	7.417	6.73	5.523
	PRESSURE Ratio	• 09	• 08	80.	•	9 6	5.0	74:02	•03	• 02	50.	8	3 6	3	3 6	90	5	1	13	•16		GL E S	SLO	•	7.67	7.45	7.19	90.90	6.27	5.94	5.60	4.85	4.41	50°E	3,27	1,68	. 62	•	•	-4.06
	ELATIVE HPERATURE	7.385	8.371	06.6	146.0	37.1.26	300	5.+60	625.9	2.343	9.275	0.701	057.20	000	00000	894.6	85.4.4	100	6.563	49.+13		NV	2	**	4.4.	4 4	*		43	43.	÷ ÷		40	6		50.00	58	60.	62.	٠
	ω H	w	J.	Ψ.	D Y		. u	, ,,	•	w	•	·5 (	, ע			, u	, 11	, Œ	Ψ	368 64		MACH	0	3	35	34	\$ 18 0	3 K	831	26	822	.8142	810	807	000	3 5	827	Ř	35	÷
	RELATIVE PRESSURE																			22.3		PF 0.=	STATIC	້	6	ė	å,	•	. 6	÷	တ်ဖ	19, 154	6	ö,	٠. م		. 6	Ġ	19,637	19.809
	RELATIVE VELOCITY	85.	83.	200	2	ָ מַמַ מַמַ	3		87.	81.	55.	27.	50	• •	•	87.	֝֝֝֝֝֝֝֡֝֝֝֝֝֡֝֝֝֝֝֡֝֝֡֝֝֡֡֝֡֡ ֓֓֞֓֞֓֞֞֞֞֓֓֓֞֞֞֞֓֓֓֓֞֡֓֡֓֡֓֡	, ,	6	63		((S)460		30.751	30.667	30.575	30.485	50,399	30.200	30.032	29,864	29,535	29.476	29.425	29.428	29.827	30.338	39.738	31.03+	31,373
	RELATIVE HAC4 40	. 67 12	. 6578	. 6557	1200	c d	65.74	ġ. S	3	ò	.0357	8	, 50 10 10 10 10 10 10 10 10 10 10 10 10 10	ŭ i	۲. نا د	4000		6470	4 5 4 5 5	.3767		3F (a	TATEC	335	200	808	0.25	15.54 15.54 15.54	063	290	160	575.834	784	2.84 2.84	397	+ ic	473	.21.	000	101
	BLAUE SPEEJ	1099.3	1105.4	1111.0	1116.6	112201	1146	1141.2	1147.7	1154.4	1161.5	1169.0	1176.9	1185.4	1134.0	1243.0	1221.0	1236.7	1249.2	1263.1		TAGGGM	OTAL S	779	841	.033	.215	3.90	.780	.103	* 25	51.524 5	326	933	.365	, 4 14 17 4 4	699	.551	.385	CE W
	LOSS	0.5	90	20	2	9 6	9 0	, 0	12	7	19	23	27	20	9,	2 4	) r	7 4	7	4921	NOI		-	ינו	94	·0	22 9	787	23	15 5	ຄຸດ	לל הינ	999	62 6	**	61. 6.4	99	13 6	55 7	
	EVIATION NCIDENCE	·	÷	÷.	÷.	•		, ,	18.035		17.543	17.315	٠,	ءُ	٠.	•	; ,	•	, ×	תו ל	DESCRIPT				977	977	977	976		970	465	901.		961	963		1002	1016	1022	1020
	FLOW DE	130 -	935 -	- +0.2	500	137	7007	261 -	016 .	615 -	971 -	200	618	- +26	366	6,63	200		528	399	Fice	7 7 7 7	TANGE	8.0	8.0	5.6	2,3	9.5		3.0	1	<b>γ</b> . τ	. 2	5.9	:	, ,	. 60	4.0	9.8	4
	ZEL AN	-31		-32		40.4	1 (		-37	-37	-37	-36	-38	£ 1	ا ا ا	2			2 2	1	FLOW	1	RIO	٠,	: :		÷	å,	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		÷.	65.37	: :	÷	å.	ė i		m	å	
E DATA	ANGLE S LEAN	2,399	2.63:	2.03	3.10	2000	000	30.44	4.35	4.53	4.67	4.73	φ. φ.	ý	•	100	N 11	200	000	3.617	10N 15	ĺ	) <del>) '</del>									1531 08								
BL ADE	SECTION	1.81	2.75	3.71	£ 4 .	20.0	0 0 0 0 0	2 2 3	96.8	9.57	0.32	6.0	1.55	2.14	2.70	3.5	1		700		STAT	10.40	ř	L.F.	o.	S.	•		• •	•	or o	7. 45	. 0	0	(	v	u m			ш
	LOCAT		2 -1				0 ^					~	m	<b>.</b>	σ.	0 6	٠.	9	n c	.8		***************************************	- INE	-	• ~	m	•	w.	۰ ۸	•	σ (	<del>-</del>	121	13	# L	12	17	<b>.</b> #	19	6

FLOW FIELD DESCRIPTION	
STATION 11	

<u>.</u> ⊢	95	<u>.</u> .	iù	Ņ	6,		Ü	*	<u>,</u>	*	<u>,</u> (	<u>, , , , , , , , , , , , , , , , , , , </u>			23	Ši	9	ż	ñ			. POLYTROPIC	***	.9727	967	962	. 9569	700	1	931	921	905	872		910	771	748	726	.7105	669	. 5885	•679•
MEIGHT	80		0 60	80	8	9	80	8	8	9	8 8	0 4	3 6		9	9	•	•	•			ENTROPIC	FICIENC	2696.	.9638	.9579	.9523	1000	. 1410	19261	.9138	.8962	. 6594	19261	. 7 9 3 0	7481	.7223	.6973	.6797	.6675	4624	.6393
CJRVATURE	26.367	2 5	0 N	3	7	3	3	5	\$	36	6	2 :	3 3	15	2	26	1.24	9.35	• •			DELTA Y IS	- E	.241	2	'n	ž	v	2 4	200	2	.247	. 256	200	ï	. 202	38	32	546.	.354	.367	.383
SLOPE	9, 05		8 . 17	7 - 86	7.57	7.31	7.10	6.93	6.79	6.64	9.44	0.10			3.60	2* 55	•	•	•			PRESSURE	ATI	• 09	.08	8	20.	9	9 6	1	.03	• 02	. 31	96	9 6	200	.03	.06	• 09	11	2.135	•16
WHIRL	<b>.</b>			9	9 40	3 40.	3 40	.0.	3 41.	9 42.				51.	0 54.	2 56	2 58.	\$ 62	2 67.			AT IVE	PEZAT	, Û.	3.		12.				7	. 36	5.5	32	7 ·	0 7	10	. 55	. 55	38	709.332	31
E S	73	3 8	0 0	8	06 3	883	883	877	72	67	863	200		86.0	877	880	22	9	Ç.			×	<u> </u>	61 6	67 6	•	φ,	56	<b>*</b> C	2 0	1 37 1 40	2	32	9.0	27	0 20	22	9	30	JE.	73	Į.
STATIC	18,727	נינ	ח פ		8.1	8.0	8.0	0	8.1	8.1			40		8	8.5	8.8	N	€0			4EL	PRE	0.7	9.0	້	4.	7) I	3.6		6	9.1	e.	<b>.</b>		, ,	9		6.0	2	31.3	1.7
TOTAL	30.751	9 2	• •	9.39	0.31	0.20	0.03	9.85	9.71	9.53	9.47	,	7		0.33	0.73	1.03	1.37	1.79			RELATIVE	ELOCIT	015.5	023.9	0.59.6	033.2	0.34.0	1 24 · D	027.7	022 • 3	017.9	017.1	0.26.2	010		36.6	055.1	1064.4	63.6	1057.61	6.9
STATIC	•	57.3	26.7	56.5	56.8	57.4	58.5	59.8	62.0	66.3	71.9	٠ و و و	• • • •	7.06	97.5	63.9	6.60	17.7	27.8			ELASI	5	. 6733	. 5905	. 88 61	. 4895	6966	C	2 M	. 87.77	. 37 23	. 8579	. 8534	20 50 °	26 CO .	8565	.8770	. 4802	36.46	. 8545	. 84 92
-iemperai Otal	m	D (	• •		.0	4.7	5.1	5.4	6.8	1.5	6.3	ים ים	2 0		8.6	6.5	7	9.0	7.3			4	SPEED		•	•	٠	•	•	•	•	•	•	•	• c	•	•	•	•	•	0.0	•
# 	51 5	6	22	90	.0	'n	n	'n	۰.0	n	21.	n .		יי ט	,	9+	65 7	61 7	2 2			(A	SOEFF	0	.00	8	00	8	0.0003		0	00	.00	00	þ	3 6	000000	200	00.	00.	0.0003	6
N TOT	1 7	201 4	1029	1034	8	~	2	10 1022.34	۳ ۳	۳ ۳	1016	1016	0101	1036	1055	5 1054	6 10o3	2 1057	5 1046			EVIATION	GIDENCE	-6.315	16	8	.63	3;	7 8	, ,	: 2	5	8	8	3	<u> </u>	5.714	: 2	=	5	13, 325	<b>.</b>
TANGE	636.7	200	50 U.		672	609	607		570.	690	711.	7.3	2 4 4		355	88	910.	935.	966			0 10	MGLE IN	•	•	•	985	*0.	•	•		-	•	•	•	•					. 220	•
4ERIO	749.42		: -	764.48	٥	Š	÷	ŝ	ۀ	ė	'n.	<b>.</b>	•	**************************************			ċ	ò	0.1.	TA	;	ES REL	4 7:4				562 40										3 5			ģ	1.518 52	25
SOTORY.	619	. 666	7.7575	807	. 843	. 885	.927	.969	.012	. 055	. 099	. 145	5 T T C	25.	440	. 401	. 462	.532	. 619	BLADE DA		LADE-ANGL	ECTION LE	. 917 - 3	. 056 -3	.252 -3	.617 -3	114 -2	2- 527.	2000	.861 -1	.682 -1	- 075.	•		25.5	521	615	.401	N- 444.	, 995	. 914
-LINE	#	יא	7 .	· w	٠	~	•	σ	10		75		1 .	15			+	0 2 19	8			=	-10H				2		:			J	•			•				1	20 43	

																							POLYTROPIC	FFICIENCY	60%6.	.9367	.9324	ייט	סייט	2110	, 0,	•	. 8795	<b>40</b>	60 1	_	•	2304		.6903	.6788	.6653	40	
	SPECIFIC WEIGHT	.0853	8	5 6	9 6	, 6	֚֓֞֜֞֓֓֓֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֡֓֜֜֡֓֓֡֓֡֓֜֡֓֡֓֡֓֡֡֡֡֡֡	່ດ	6	g.	5	5	ייס	5	5	בי ספ	5 6	? <b>.</b>	0 4		D		SENTROPIC >		.9347	.9301	.9254	• 9205	.9153	,,		•	•	. 8329	• 1	•	•	∿ r	6758	9000	·	.6305	w.	
	RADIUS OF CURVATURE	-3.688	•	•	•	•	•			•	•	•	•	•	٠	•	ė	•		• • u	•		DELTA T IS		.241	5¢	.242	Š	242	2 0	5	.244	4	• 256	56	27	. 283	2, 5	2 5	0 7 M	35	35	80	
	SLOPE	5.21	4. 61	4 t	4.03			3,21	3.21	3.25	3,35	3.42	3.47	87.	M+ *M	3.25	20.5	5.24	1.69	00.0	*C• 03		PRESSURE	RATIO	•	• 03	• 03	.03	102	5 6	5	98	•98	• 97	96.	96	.97	. 6		7 · 0 · 0	900	80.	101	
	4HIRL	32.8	32.	32.1	) 1. ¢		7 * * *	31.	30.9	30.8	30.8	30.9	31.0	31.1	31.3	31.0	32.0	32.6	25.6	200	4.0			EZATURE	3.0	184	. 33	7	۳.	, ,		.+	36	32	32	W.	œ.	Ξ.	2 4	מַייַ	. ~	3	33.	
	C NO		Φ,		•	•	•				٠.	9.	9.	٠.	9•		٠.	~ ·	· ·	` ·	,		$\alpha$	JZE TE	23	29	9,6	820	739	\$ (	368	226	109	020	938	923	95*	988	320	120	o m	800	876 717	
	SSURES STATI	17.67	18.05	18.43	13.31	13.10	19.00	20.10	20 35	20.57	20.78	20 • 96	21 - 12	21.26	24. 18	21.47	21.52	21.50	21.39	71.12	20.84		8	a.	08 30	61 29	39 29	63 56	93 29	52	55 23	3. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	74 29	50 29	53 28	24 28	88 28	08 28	62 60	89 29	30	300	a7 30	
	TOTAL	0.02	3,95	9.89	9.82	200	, c	23,368	9.22	9.10	9.05	8.97	8.92	3.95	3.94	9.32	9.75	0.10	0.34	0.59	1.37		VE RELATIVE	O VELOC	1049.	1026.	1004.	981.	959	938.	917 895.	877.	869.	648.	837.	630.	325.	823.		בי בי בי	000	927	961.	
	TURES STATIC	53.5	57.5	61.4	200	70.4	,,,	579.309	82.4	86.2	92.5	98.9	34.5	69.5	14.5	21.2	28.5	23.00	36.2	38.5	41.3		RELATI	アナウサビ	90	. 08	. 85	. 53	. 61		77	73	. 72	• 70	ęċ•	. 68	, 57	.67	60.		7.		• •	
	TEMPERA Total	43.6	43.3	0.4	2*4	9	֓֞֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֜֜֜֜֓֓֓֓֓֜֜֜֓֓֓֓֓֡֓֜֜֡֓֡֓֡֓֜֜֡֓֡֓֡֓֡֡	544.760		0	51.5	50.3	÷0.9	55.3	6.60	79.5	83.6	30.5	02.3	0.66	17.3		8640	: SPEE		ċ	•	•	ċ	•	<b>.</b>			•	•	0	ċ	•	•	•	• =	• -		
CKIPTION	0.TAL	48.63	26.01	04.39	81.93	24.43	384	, 	77.31	20.74	6.50	37.53	30.24	25.48	23.03	38.03	59.49	30.01	00.00	27.41	61.97		N L.35	35 33EF	. 0.	- 15	. 05	• 03	.03	60.			.00.	50. 1	• 0•	<b>*0.</b> ~	<b>†0.</b> 6	€	<i>*</i>	***	ייי טינ			
AC 356 CJ-	OSITIES TANSEN I	67.34 1	1 69.16	3+.43 1	17.13	P 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	95.67	12.13	51.17	+1.43	35, 35	30.31	27.48	27.63	23.23	39.27	55.43	74.14	3.55	7.30	5. oJ		1420 4	INCIDEN	•		•		•	•	•	• •		6		0 1.	2 1.	ند این	 	• •		• ~	· ~	
FLOW F.I.	410 KI	6 90 5	5.77 5	0.37	e 62.4	W 689	5 . S3	7.44	2.28	9.52	9.31	8.53 4	1.43 4	b.57 +	2.43 +	·. 75 4	*	3	₹ 30.2	ν.	2.15		FL 0	ANGLE	32.00	32.59	32.15	31.77	31.45	31.23	31.12	40.00	30.43	30.86	39.91	31.03	31.18	31.35	31.60	32.01	34.50	23.63	34.55	
ATION 12	9195	150	31	914 &	\$ . 56	566	6/0	34/5 /8	200	707	134 7	570 7	015 7	455 7	21 7	378 7	8	23	752	229 7	730 7	AUE DATA	 - ANSLE	ON LEAN	9 -24.8	5 -23.3	4 2 3 0 4	3 -19.2	9 -15.8	1 -14.5	4 - 1 C - 4		.5.3	-3.7	6 -1.5	3.	3 2.9	5.7	9.9	12.5	700	, c	8 28.225	
STI	EAH &A	7.		۲.	~	•	<b>:</b> ,		: 4		ź	÷	ø	9.	•	÷	ė	÷	÷	20	ė	31,	AT 31.AD	N SECTI	31.95	31.64	31.27	50.69	30.53	30.30	30.10	30.00	29.37	29.62	23.87	69.62	30.13	30.30	30.56	30.99	51.50	32.25	33.47	
	SIR																				~		2	9-	-	~	, ~1	•	S.	Φ.	~ •	0 1	10	: =	12	- 13	7.7	15	91	7	01	61	3.5	

STATION 12 INTEGNATED PENFORMANCE PRESSURE RATIO = 2.013 ISEN, EFF.= .777 PO.Y. EFF.= .798 DELTA T ON T = .283

FLOW FIELD DESCRIPTION	
STATTON 13	1 1 1 1 1 1

					•										•									TOCATA	EFFICIENCY	7000	9696	5605.	1206	- 6982	. 6939	.5555	. 9112	.8733	0000	.8534	• 5236	. 7956	. 1733	****	. 7303	917	1074	0/00.	1660.	. 5412	7429•	:
MEIGHT	.0971	. 0977	2960	D (		0	•	0	•	0	•	•		.0971		Э С	9000	Э (	ь.	. 1930	8	.1912		. Cleonary	FICIENCY			*069	. 8923	800	. 8633	.8774	2018	6098	.5550	.8392	. 8066	.776,	.7516	5867	./118	7000	1469.	****	*029*	9400	1496.	•
CURVATURE	-5.196	2	-6.438	9	3	Ď.	ž	2	z	2	3	3	: 6	2	7	4 6	? :	2	8	7	36	꿆		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	- EF	į	142	192.	242.	• 242	.242	.243	. 243	**2*	**2.	.247	• 256	. 265	4.20	.283	262.	505.	• 328	7	. 354	.367	. 333	
SLOPE	-2.23	-2.29	-2.33	-2.34	-2.31	-2.25	-2.12	-1.94	-1.72	-1.47	-1.20	. 91	. 6	3.5		•		7.	•	- 82	.91	. 88		Č	RATIO		. 5	66	98	96	.97	.97	• 96	95	ţ.	9	93	93	. 93	6.9		5.65	98	3	50.	2.026	ś	;
WHIRL		:	17.53	:	:	:	:		2			2			٠,	٠,	٠,	٠.	ů.	ė	÷	6			ALLVE ERATURE		ň	*	M	7	39		2	=	.+	9	Š	<u>س</u>		<u>م</u>	Ξ:		9	Č	M.	9.032	31	
E 0	87	ž	.6621	2	38	2	15	20	95	5 88	5 83	5 79		: 5		200	* 1	9	20	8	38	56			SSURE TEMP		25	e 9	12	51	81	<b>3</b>	69	ţ.	80	21	26	Ü,	25	20	23	26	53	٠,	<b>\$</b>	78 709	98	ı
STATIC	38	53	2	95	1	.5	.36	.45	525	57	9	4		3		֚֭֭֭֓֞֜֞֓֓֓֓֓֟֜֜֓֓֓֓֓֓֟֜֓֓֓֓֓֓֓֓֓֓֓֓֓֡֜֜֜֓֓֡	9	Ď	• 69	.68	99	22.589		i	7 9 1 9		~	Ň	Ň	₹	ö	ຕຸ	Ď.	<u>`</u>	ó	ū	*	3	•	3	י הי	٠.	7	7	r.	•	σ.	
TOTAL	9.32	9.56	9.21	9.15	9.08	8.98	3.86	5.72	5.60	8.52	8.45	A. 40				26.00	3.6	3.12	3,39	3.58	9.77	•			VELOCITY		•	٠	•	•	•	•		•	٠	•	•	•	•	•	•	•	•	٠	•	804.70	•	
JRES STATIC	4.68	90.5	92.5	4.46	96.1	97.9	99.7	31.5	03.0	15.3	10.4	15.1	10	7 7 6 7	,	5.72	200	41.7	47.3	51.5	56.2	662.109			MEC4 11 VE		. 6877	• 67 45	. 6621	. 55 01	.6387	95	5	. 6043	. 5953	38	. 58 32	. 57 92	2	Š		0.5940	• 608	• 62 03	. 6289	. 63.87	. 6503	
-TEMPERAT OTAL	43.6	43.8	44.0	44.2	M.++	44.5	44.7	45.1	. 5	46.8	51.5	26.4	90	,	•	5.00 10.00 1		38.6	96.5	02.3	09.0	17			SPEE		ċ	•	ċ	ċ	•	ċ	•	•	•	•	•		ċ	<u>.</u>	•	<b>.</b>	•	•	0	0.0	ċ	
- <del>-</del>	50	8 9	.15 6	÷	ģ	63	21	T		) M	2	: 2	3:	1 2	<b>.</b>	<b>.</b>	2	7	35	55	20	2.96 7		7	COEFF	}	-	-4	-	0	0	2	-4	2	2	2	σ	9	8	9	•	80	10	-	Ħ	.1319	'n	
EN 101	5 82	2 80	2 73	0 78	2	1 75	<b>5.</b> 5	2 72	7.	7.7		7				2 71	2	3 75	ė 77	3 73	90	04 822			EVIATION		35	. 36	.38	9.	. 43	. 47	• 50	. 54	• 58	.61	.63	• 65	• 67	• 67	.67	99.	• 65	• 65	• 65	1.674	.73	
Velociti TANSE	9	43,	38.	35	31.	27.	25.	13	3		2 2		<u>.</u>				23.	31.	;	<b>6</b>	59.	271.0		;	FLOW DEN	• !	ţ.	.54	3	.53	.53	.50	*	.38	• 36	• 39	3	۲٠.	. 40	• 50	. 55	.0	8	• 05	• 39	8.789	• 22	
A RIO	۰	÷	ؿ	ď.	÷	6	ė	۵	ď	ď	3		:	• e	•	;	÷	÷	'n	å	;	77.04	¥ F	,   ;	א אר אר		414 1	925 1	371 1	7 39 1	015 1	133 1	256 1	271 1	277 1	325 1	1 19	758 1	148 1	1 264	2.58	234 1	275 1	3 36 1	631 1	020 1	542 1	
RADIUS	.723	.750	. 791	. <b>3</b> 26	. 863	. 903	.939	979	. 021	290	107		201.	- 1C		. 293	.341	. 383	• 430	+84.	.531	8.5795	9LADE DA		CTION LE	:	234 -	190 -	149	128 -	- 660	035 -	939 -	\$	788 -	- 482	803 -	815	819	835	299	980	151	604	739	115 7.	10	
STREAM -LINE	-	~	m		r	•	~	. •0	σ													21			LOCAT 3L		15	15	15		15	15	13	15	15	15	15	15	13	15	+	1.0	15	15	<b>\$</b>	20 1.7	÷.	

DESCRIPTION	
FIELD	
FLOW	
#	
VOIL	
STAT	

		POLYTROPIC EFFICIENCY	
SPECIFIC HEIGHT	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ENTROPIC P	
RADIUS OF CJRVATURE	110 110 110 110 110 110 110 110	DELTA T IS	######################################
LES SLOPE	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	PRESSURE RATIO	1.947 1.944 1.946 1.946 1.946 1.935 1.935 1.909 1.909 1.954 1.954 1.954 1.954 1.954 1.954 1.954 1.954 1.954 1.954 1.954
HHI RL		ELAFIVE H MPERATURE	66643399666643399666643399966643399999999
MACH	, , , , , , , , , , , , , ,	TIVE R Sure te	66666666666666666666666666666666666666
SSURES	23.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.	VE RELA TY PRES	2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
P2ES TOTAL	22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	RELATI	66579 66579 66579 66579 66579 66579 66579 770 770 177 177 177 178 178 178 178 178 178 178
URES STATIC	50000000000000000000000000000000000000	RELATIVE MAGH 43	5438 5349 5349 5349 5369
-TEMPERAT OTAL	10000000000000000000000000000000000000	BLADE SPEED	A K S S S S S S S S S S S S S S S S S S
٨.	\$	1055 005F	44.000
TES		EVIATION	2. 2. 4. 4. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.
-VELOCII	W + 10 B & B & + 10 B & B & B & B & B & B & B & B & B & B	L FLOM J	######################################
+ERIO	DA 100 100 100 100 100 100 100 10	GLES RE	11.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930 1.0930
440IUS	7. 70 70 70 70 70 70 70 70 70 70 70 70 70	BLADE-AN	8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
STREAM -LINE	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	LOCAT	40m 400 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

		POLYTROPIC - 6444 - 6440 - 6376 - 6376 - 6376 - 6376 - 6376 - 6376 - 6410 - 7985 - 7728 -	
SPECIFIC WEIGHT		IENTE ENTE ENTE ENTE ENTE ENTE ENTE ENTE	1 = .263
RADIUS OF CURVATURE	10.624 11.0624 13.008 13.008 14.157 15.640 17.662 20.498 33.777 52.549 123.456 123.456 113.906 -173.906 -173.906 -173.906 -173.906 -173.906	T	DELTA T DN
SS	2014 W G G G G G G G G G G G G G G G G G G	PRESSOR A SECTION A SECTIO	. z . 721
WHIRL		EMPE ATINE 643.544 643.341 644.391 644.391 644.391 644.391 644.391 646.391 646.361 655.361 655.361 656.361 666.381 702.382	PO_Y. EFF
A A CA		S S S S S S S S S S S S S S S S S S S	969. ≖.
ESSURES STATE		11VE R 386 386 557 78 551 118 551 552 552 552 553 553 554 554 554 555 557 557 557 557 557 557	SEN. EFF
101AL	22. 890 22. 890 22. 890 22. 890 22. 890 23. 890 23. 890 23. 890 23. 890 23. 890 23. 890 23. 890 23. 890 23. 890 23. 890	7	1.883 I
RATURES		4 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +	E RATIO =
TEMPER TOTAL	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SSS BLADE 373 PEECO 313 00.0 2313 00.0 2255 00.0 2255 00.0 2	PRESSURE
TOTAL	- ֏ԿԾԱՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵՐԵ	วิธี ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผู้ผ	PERFORMANCE
LOCITIES- TANGEN		LECT 10	EGRATED" PER
4F 7 1 3	4 E A L C C C C C C C C C C C C C C C C C C	20 20 20 20 20 20 20 20 20 20 20 20 20 2	
KADIUS	7.5400 7.6803 7.76803 7.76803 7.76803 7.88504 7.88504 7.9844 8.0877 8.1868 8.18	A A A A A A A A A A A A A A A A A A A	ST ATTON-1
STREAM	, 40m3m9r9pot0t0t0t0t0t0t0t0t0t0t0t0t0t0t0t0t0t0t0	100 A T T T T T T T T T T T T T T T T T T	
· ·	, 223	- · · · · · · · · · · · · · · · · · · ·	i

	SPECIFIC WEIGHT	.1821	.1020	19201	41019	01010	1101.	. 1017 1017	4847	1010		966	6964	1000 ·	8764	9960	4560	4460		0000	9	4			SPECIFIC	HEIGHT		1281	9701.	8767	-1016	.1016	*1915	.1013	.1012	2101.	2000		-	87.00	9968	4660.	**60.		. 1929	5
	RADIUS OF CURVATURE	8	50	677.157	5	11	. d	, ,	. 5	7	1		7	5	6	28	47A.25	E84.00	, ,	F. 00.		•			RADIUS OF	2		•	3 6		9	.00		.00	. 69	8		•					.00		00000	•
	ANGLES HIRL SLOPE	00.0	- 03	. 65			) ·	D +	1	10	-			- 0.0		- 0.0	× 4		1	1	•	•			ES	SLO		ф ·		•		00	01	01	01	01	100		T • • • • • • • • • • • • • • • • • • •	1 6		00.1	- 00	00	6.	ø
	WHIRL	0.00	•		•	•	•	9 5	•	9 0	9	2 6	•	2	9	•	, ,	•	•	•	•	•			ANGLE	HAIRL		ф с	<b>7</b> (	<b>5</b> C	•	•	0	0	Ф	0	9 (	<b>3</b> C	<b>,</b>	<b>,</b> c	•	, 0	0	Φ	0.00	•
	MACH	.5085	.5060	.5035	v 1	100 P.	3.	3	7 4	,	4564		7.4		104	ľ	١u		n u	1010	71700	.565			AACH	2	, !	ומו	2000	nυ	× × × × × × × × × × × × × × × × × × ×	• 3	+4814	. 4813	.4783	. 4777	2225	* -	7 .	14	1000	5075	.5147	.5182	.5217	.5253
	SURES	4.0	40	23.400	5.5	3.0	33		2 6	א כי	7 6	2 6	ָר מ מ	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֓֡֓֡		9 6	2 6	9 6	2 6	9 6	2 6	5			Sures	TI		. 23. 387	5	9 6	) N	10	38	. 38	.38	() ()	9	? !	900	2 6	9 6	8 M	300	.38	23,387	3.38
	PRESSI TOTAL	8	3	27.812	2 :	9	9	200	2 5	\$ F	? 6	2 6	3 5	1 5	1 5	3 %	2	5 6	2 4	9:	36	₹			P2ES	TAL			3	7 7	2 5	. 9	20	33	ŧ,	33	32	35	¥ :	7 9	2 5	2 6	20	9	13	2
	TJRES	~	~	513.241	~ (	SI (	<b>~</b> (	D o	0 11	•		• 0	,	- 4	2	JU		$\cdot$	hε	<b>,</b>	יו ת	<b>7</b>	•		.,	STATIC	•	612.192	12.0	4004	515.176	614.937	515,813	616.910	517.453	618.903	623.432	024.410	021.10	520.487	5010100 546.507	655.322	661.959	567,861	672.327	86.3
	TEMPERATJRES fotal ·Static	43.6	43.8		44.2	りゅぎ		46.	# 10 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		0 0 0	C • T C	0.0	65.4	9 0	78.5	4	ם פרו	70.0	200	֓֞֜֝֜֜֜֝֓֜֝֓֜֜֝֓֓֓֜֝֜֜֜֝֓֓֓֓֡֓֜֝֓֡֓֜֝֓֡֓	17.5			- 1546	TOTAL		3.64	\$8°5.	クコ・ナナ	77044	44.55	44.78	45.10	42.45	46.86	4	75.00	9.00 B.C	00.00	78.58	88.50	96.55	82.38	09.03	17,31
DESCRIPTION	TOTAL.	619.13	-	613.57	┥′	<b>~</b>	0	თ თ	0	ю :	0 4	9	0 0	2	<b>,</b>	40	u r	nι	N U	Λ,	o i	•	CRIPTION			10		620.11	617.30	24.410	6041.00	601.31	595.13	588.19	584.78	584.76	586.18	564.55	55.25	64.2 40	65.010	639,25	651.23	.658.20	665.56	673.72
FIELD DES	LOCITIES- TANGEN	0	•	0.00	•	•	~	•	•	•	•	•	•	•	•	•	•	•	•	• ·		•	FIELD JES		11.	NA NA NA NA NA NA NA NA NA NA NA NA NA N		₽ 0 ° 0	0	9	<b>5</b> C	0	0	C	Ф	C	0	9	Ф (	9 0	9 0	9 0	0	Ф	0	Ф
16 FLJM	-HERIO	9.1	ġ	÷	•	:	÷	13.466	:	;	•	i c	•	•	• •	2 u				έ.	٠,	÷	17 FL3#	!	. A !!	ER10	•	₽,	ᆞ.	:.		; ;	'n	÷	÷	j	586.13	·,	ċ.	٠,			; ;	÷	'n	73.
STATION	RADIUS	4	2	- 7.7203	3	5	3	5	2 5	2	2 4	6	3 q	9 4	2	0 6	2 9	P :	¥ 6	† ! ? :	÷ (	5	STATION	!	PANTIIS			7.6480	Ψ.	•	•		•	· · ·	3.	٦.	•	7	Έ,	•	•		•	1.	•	¥
	STREAY -LINE			m		į		~ •				н (	<b>,</b>		<b>.</b>	ח ע	ا 9 ج	1.1	9 0	F (	,		i		MARGIC	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	) : 4	1 41 1	~	n.	<b>+</b> 4	ص ۱		•0	σ	10	स स	12		# L	6 4	9 6	- ec	67	20	2.

	NGLES OUTLET	2.339	93	=	8	9 0	12.5	36	23	3	CE	46	95	91	79	25	9 t N	7	7			MGLES	_	2	2:	# :	1 =	: =	걸	# 1	2 5	9 0	2	2	2 2	2 5	2 =	1 #	2	032
	LEAN-A	17.205	5.	;	2.7	4 C	9.6	'n	9,	•	7	. ~	5	r.	╗	ri,		?•	•			LEAN-A	ii)	-39.941	۳.		, 4	. 10	2.2	4.6		, ,			<b>~</b> ⋅	٥ م د د	, 6	້		41.518 46.652
	ON-ANGLES OUTLET	-11.816	12	8	2	מים	2 M	98	3	2 2	1 1 1 1 1 1	3	2	23	7	<b>:</b> :	7	2 2	0			I-ANGLES	41	23	7,33	2.50	. 6	8.03	8.24	8.41	9.20	2 6	8.92	9.00	9.05		9.05	80	9.12	-9.171 -9.213
	SECTION INLET	-62,667	62.5	62.5	62.7	7.50	62.9	63.1	63.1	5.5	# 15	63.5	``	٠,	ď.	9	Ņ٠	? -	•			SECTION	الا	ø	0 (	N٠	۰.	• ~	m	0	<b>10</b> U	o u	S	ø	9	NU	<b>^</b> ≪	•	3	48.395 50.814
	0ELTA H/U**2	.6302	, o	ø	w,	ט פ	.5973	N.	un v	Φ.	<b>D</b> 4	, o	ס	.6738	.7045	.7241	.7339	*****	010/•			JELTA	ŧ	• 00	00.	00.	•	00.	.00	. 00	9	•		• 00	9	900		000	• 00	0.0000
	REL V	.7615	733	721	711	202	.6843	575	.0613	530		550	527	493	424	• 4255	6404.	1165 •				לבר N	Ï	.5953	. 5902	5.585.5		.5765	.5723	. 5701	.5713	.5772	.5817	. 5895	. 5963	.6037		. 6139	.620+	. 5402 . 5435
	DELTA P ON D	.5619	Š	.5231	w.	* :	.4639	3	3.		440.59	או כ	m	m	.3429	ומו	. 3255	ייי	6010.			DELTA	ö	5	414	423	7 7 7	437	4	446	450	4 7 7 Y	5	461	450	454	100	32	369	.3387
	3-0 D FACTOR	.3740	3	-	3	9 3	t v	9	4 1	, 10 10	v v	61	 	.:	72	u (	. 38 . 4	<b>-4</b> L	r.			3-0 0	5	4.5	3	90	- ^	. 5	93	00	9	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֡֓֓֡֓֡		7	60	98	9=	80	00	.5879
	2-3 D FACTOR	3654	120	411	5 i W	4 4	£10 t	454	490	516	55 C	611	637	619	727	O I	<b>س</b> .	<b>.</b>	0			2-5	c C	542	554	55.0	2, C	595	593	630	603	1 0	613	612	610	909	2 2	9	0	.5881
	LOSS	. 0540	6	င	8	200	1089	2	# :	5	25	3034	33	36	3	64840	• 4505	1807	1764.			L 05S	6	237	231	0.0	220	22,	N	220	<b>.</b> +	V €	•	177	01	103	4 4	תו כ	2	. 2675
	) = VI A - T I D M	19.314	3.33	9.75	8.50	* · ·	3.02	8.03	46.7		7.07	2.40	5.55	5.34	3.34	3.23	3.53	, t	•••			DEVIA	2	.23	939	96.	. 7	.09	2	1 + 1	90.	. 6	92	• 0 0	• 0 5	9 0	֓֝֝֝֓֜֝֝֓֜֝֓֓֓֓֓֓֓֓֡֝֜֝֓֓֓֡֓֡֓֓֡֓֡֓֜֝֓֡֓֡֓֡֓֡	.03	.12	9.171 9.213
	CIONI -ENCE	9.459	7.3	. 83	80		.02	3.02	3.04	20.0	11.0	0.22	0.32	77.0	0.53	0.73	683	1.03	***			CIONI	N N	.31	5.16	5.87	0.1	21	4.94	4.57		1000	.03	.33	24.	.65		11.	1,38	13.325 10.614
1 E	INCET M. NO	. 9288	53	426	500.		7.2	640	. 153	876	992	120	134	.148	.161	.175	139	.203	• 110	NCE	1		2	73	90	936	ה ה ה ה	, 0	333	083	377	2 5	363	360	859	857	*77	80	875	.4648
PERFORMAN	UU TL ET RAJI US	7.5499	2 2	5	2	: t	2 2	3	2	7	20 6	, M	13	25	33	9	φ (	č	ç	PE QF 02MA		OUTLET	בנ	0 40 •	680	.21	2 6	450	. 395	. 341	989	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	136	. 187	. 238	288	3 6	2 4 4 5	464.	8.5471
2010R	INLET	5.7500	.981	• 095	502	. 521		. 655	.766	.876	935	200	.316	.427	.539	. 552	•766	288.	•	STATOR		INCET	AOI	.619	• 666	2.7		843	.885	.327	969	uu	660.	.145	193	.241	444	401	.462	3.5325 8.6199
	LOCAT -ION	<b>↔</b>	m	3	so .	م م	<b>.</b> 60	6	07	# :	21 2	3	15	16	17	91	(	25	3			LOCAT	2	#	2	m.	t u	۰ ۵	^	<b>6</b> 0	σ,	3 ;	15	13	<b>3</b> 1	517	1 10	. 07	-19	22

MAKE AND BOUNDARY LAYER BLOCKASES (PERCENT)

STATION 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 MIO BLOCKAGE 0.U 0.0 0.0 1.0 1.0 1.5 2.0 2.5 2.0 4.2 3.0 5.0 7.0 9.0 11.0 12.1 12.1 0.ST FACTOR 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 10 10 10 10 10 10 10 10 10 10 10 10 10	
1 2 3 4 5 6 7 8 9 10 11 12 13 15 13 15 15 15 15 15 15 15 15 15 15 15 15 15	
1 2 3 4 5 6 7 8 9 10 11 12 12 0.0 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.5 2.9 4.2 3.0 5.0 0.0 1.0 1.0 1.0 1.5 2.0 2.5 2.0 4.2 3.0 5.0 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.6 2.0 4.2 3.0 5.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	
1 2 3 4 5 6 7 8 9 10 11 10.0 0.0 0.0 1.0 1.0 1.5 2.0 2.5 2.9 4.2 3.0 1.0 1.0 1.0 1.0 1.0 .5 .5 .7 0.0 1.0 1.0 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.6 2.0 4.2 3.0	
1 2 3 4 5 6 7 8 9 10 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.5 2.0 4.2 1.0 1.0 1.0 1.0 1.0 .5 .5 .2 0.0 1.0 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.6 2.0 4.2	25
1 2 3 4 5 6 7 8 9 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.5 2.0 1.0 1.0 1.0 1.0 1.0 .5 .5 .2 0.0 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.6 2.0	PASS
0.0	
0.0	VERSE
0.0	NO. (5
0.0	NO
00.0	CULATI
00.0	CAL
00.0	H
00.0	-
0.0	Z
0.0	2
TION BLOSKAGE T FASTOK BLOSKAGE	¥
AID OIS INT	Y ARELON

FLOM = 18.12 SPEEJ = 16694.3 PRESSURE RATIJ = 1.883 ISENTROPIC EFFY = .6353 POLYTROPIC EFFY = .7214 OEL T/T = .2831

TEST POINT TITLE = 203241115882

## 6. PHASE II WITHIN-BLADE ANALYSIS (90% SPEED) TEST POINT 208300315990

1	,	FLOCITIES-		T_MPERATJRES-	1755-		P < L SSU < E S	HACH	ANGLE	2000	RADIUS OF	SPECIFIC
9636 3639 5391 6937	NERTOT	TANGEN	יטיאב	LOIME	STRIC	LOTAL	SIAILC	2	14 14	בר ה ה		
5267 5391 6937	1 141	111111111111111111111111111111111111111	19.78	916.556	166.216	360.41	14:138	.2353-	- 0. 00 · ··	-20.93	000.0	
5539 5931 5937 6937	262.60	000	252.00	510.588	512.337	14.690	14.138	.2358	00.00	19.77	0.000	•0739
' :	292:00	90.0	19.292	919-916	120.32	260.41	14:138	5222	0.00	12.00	- 000°0	•0133
' :	52.0g	00.00	262.00	516.688	512.397	14.636	14.138	.2358	0.0	17.42	000.0	5570.
:	32: 50	99.00	19.292	918-658	\$12:397	14.696	14.138	5222	0.00	16.24	000.0	Sera.
:	25.2.00	0.00	262.00	510.688	512.397	14.636	14.138	.2353	00.0	15.05	000.0	かりとつ・
	32:60	00:00	262.60	518.665	166.516	14.696	14:1:38	.2358	00°	13.67	0000-	66/00
7.1517 2	26 2 • 60	0.00	262.60	518.588	512.397	14.696	14.138	.2358	0.00	12, 69		.0739
Ĺ	282.80	00.0	262.80	918:318	166:216	14.096	14.138	6664	20:0	11:31		60100
	16.2.60	3.00	252.63	516.688	512.397	14.630	14.138	.2353	0.00	10.34	000.0	•0739
	287.55	00-0	262.60	915.568	166-216	14.695	14.138	.2353	00.0.	9.18		66.00
	25.2.63	0.00	262.63	513.060	512,397	14.690	14.138	.2358	00.00	8.04		.0739
	1	11.4	267.60	+	- 512.337-	T4.596"	- 140-138	2353	00.00	5.92		640.
0512	26.2.60		262.50	210.028	512,997	14.630	14.130	.2358	00.0	5.84		.0739
į	00.70		505.00		4000	- W-W-	48-1-84	- 22.58	0.00.	196.	i	66.40
	00.70	•	00.000		E 1 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	464	14.133	2000	00.0	3.80		.0739
2040.	19 5 9 1	•	60505	210000	715 527			945		2.46		9844
:	•	6 <b>0-0</b> -	09.292	213.555	166*216	260.4T	14.150	0000	•			07.40
	26.2. 60	00.0	252.03	518.684	512.397	1+•695	14.150	. 6353	0.0		•	
	63	00.0	D0:292	\$18.508	-512:337	14.635	ñ	- 2322	. 00. ກ	1.22	nn•n	66/0.
8.9417	25.2.60	0.00	262,64	518.538	512.397	14.690	14.138	.2353	0.00	. 55		かっ しつ・
I	\$2.50	00.0	252.50	- 919 0 0 0	166.516-	14:09E-	14.138	2395		-00:0	0.000	100
								3	, •	į	1 0000	21310300
- Spins	VELOCITIE	CITIES-		TEMPERA	A41 URES	3	5.745.5	13 A E	ないしに シー・・	F 5-1-1	בסדסאצ	
ı	# 620	TAMBEN-	197AC	- LOTAL	-31416-	10141	-SIATEC	0x	HIER	StoPE	-0.5×××±0.0-	
7166	20.5.05	-	100	444	- 44 9 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	14.696-	14- 346 -	.2551	0.00	29 - 63	-205-758-	
D r		•	2 1		544.374	404	14,040	2 11.3	0.00	19.62	-141.303	.0735
2116	CT -C 07	•	CT • CC 2	0000010		200	1	9117		44.40	をはないなっても	
9259	28 65 34 ···	00.0	200.24	210.000	726°II6	360°+1		0 0 0	3 0	17.0	-08.513	0735
7902	287.43	0.00	287.43	518.500	211.373	14.095	14.030	+ 00.00	3 6	***		į
	204.43	9.00	4.00%	118.008	25.115	14:032	14:025	2533	•	10.01	T - 1 - 1 - 1	2 1
0624	28 9. 32	0.00	269.32	518.088	511.780	14.696	14.021	.2601	0.00	14.80	-79.188	
40.0	11.60		- 11-11-22:	-515.385	541.742	4.695	14-018	.2003	0	13.59	-71,632	•
2218	20 0. 22	0,0	75.066	34 2 5 5 2 3	511.710	14.696	14.014	•261→	0.00	12,37	-64.022	
	40.00		1	4 4 4		- + ta. tak	44-012	9449	9.00	11.15	766:25	
0 0	27.76		204 62	9 4 4	111111111111111111111111111111111111111	14.596	14.011	2622	0.00	9, 95	-51.637	.0734
****	231.03	•	50.163	0000010	2000	7	4	2624	9 6	A . 74	-6-5-4-6-	
1.7327	131.73	B :	610162	900.016	205.116	169	0 1 0 0 1 7	25.22		7.54	-40.265	
8660	291.72	0.00	231.12	218.586	211.502	260*+7	010.41	000		1	-25.404	
*666	291.41	: B	- 691:41	-214.503-	711:588	E	14.016	יייייייייייייייייייייייייייייייייייייי	00.0	000	101000	
1330	290.82	00.00	290.42	518.600	511.703	1+,696	14.014	.2615	00.0	5.13		
9230	7	00.0	- 66.000	-518.508	- 511-730	14.695	14, 018	.2607	8	-F # -	-56,434	100
4045	28 A. 20	0000	288.73	514.688	511.909	1+•696	14.024	•2535	0	2.95		
4 96 9	7		i	***		4.59	14: 831	.2551	00.0	- 1- 04-	19,535	•
1000.	20.00	•	200		****	969.74	170.01	C 4 R C .	_	. 60		.0735
<b>.</b>	28 5. 07	000	782.07	210.000	211.501	9	110011	4.00	-	#	·	
. 6164		00.00	١.	210.016	- 5.E.C. 0.23.6-	260.41	74007					.0736
*6*6*	27 9, 57	0000	279.57	518.686	512.23/	14.095	14.002	21620	•	00 4	111111	

SPECIFIC 0731 0730 0730 0730 0730 0729 0729 0728 0728 0728 0729 0729 0730 SPECIFIC .0724 .0725 .0723 .0723 .0721 .0721 .0721 .0720 .0720 .0720 .0720 .0720 RADIUS OF RADIUS OF -83.031 -115.355 -159.083 -216.681 -235.631 -173.631 183.76. 95.883 75.683 68.258 68.751 77.77 99.170 153.301 401.500 897.211 -258.350 -156.816 -53.004 -58.317 -27.765 -19.937 -14.356 -10.317 -309.094 WHIRL SLOPE 19.27 17.01 17.01 14.57 13.28 11.95 10.56 9.19 7.79 2.50 2.01 2.50 2.01 2.50 3.50 2.01 SLOPE --- ANGLES---00.00 WHIRE 2755 2862 2863 28613 2863 2867 2867 2867 2910 2910 29113 291 HACH NO MACH TO W 13.935 13.926 13.927 13.997 13.89 13.851 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 13.856 TOTAL STATIC 13.784 13.784 13.784 13.767 13.718 13.688 13.665 13.665 13.644 13.644 13.644 13.646 13.646 13.646 13.646 ---FRESSURES---STATIC 14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.690
14.690
14.690
14.690
14.690
14.690
14.690 14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696
14.696 TOTAL 510.575 510.784 510.784 510.403 510.403 510.115 510.054 510.054 510.054 510.054 510.054 510.054 510.105 510.105 510.105 510.105 510.105 510.105 510.105 510.105 510.105 509.291 509.291 509.291 508.594 508.594 508.283 508.283 508.283 508.283 507.993 507.993 507.993 507.993 507.993 --IEMPERATJRES--STATE --TEMPERATURES--518.588 518.688 518.588 518.588 518.588 518.588 518.688 518.608 518.608 518.608 518.608 518.608 518.608 518.608 916.686 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 518.688 FLOW FIELD DESCRIPTION 309.46
313.20
313.20
313.20
315.02
316.33
316.43
322.33
322.33
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44
323.44 4 FLOW FIELD DESCRIPTION 337.43 346.74 349.72 349.72 356.92 357.23 357.23 351.64 361.64 362.93 362.93 362.93 362.93 362.93 362.93 362.93 362.64 362.64 ELOCITIES-----TANGEN TOTAL HERID TANGEN TOTAL \*\*\*\*\*\*\*\*\* NE RIU 309.45 311.32 313.20 315.05 316.63 316.63 312.27 322.30 323.44 323.43 32 337.43 340.52 340.52 340.72 350.72 350.65 350.66 351.73 352.53 352.53 352.53 352.53 352.53 359.97 359.97 353.71 348.50 STATION 6. 7264 6. 8504 7. 2180 7. 2180 7. 2180 7. 4599 7. 4599 7. 7003 7. 7003 7. 7003 7. 9601 8. 1804 8. RADIUS STATION 6.8657 6.8657 7.20946 7.3207 7.3207 7.5437 7.5437 7.5437 7.5437 7.5435 8.1055 8.4276 8.4276 8.5395 8.6524 8.6524 8.6652 RADIUS STREAM STREAM 202

	SLADE-ANGLES	INGLES	38 1	JEVIATION		BLAD.	RELATIVE	RELATIVE	RELATIVE				DELTA T I		POLYTROPIC
2		2	1000	TACIDENCE	G	21.2	मस्त्र ६०	VELOCITY	1	₽.	E-HPE CATURE-	KATTO		EFFICIENCY	<u>eppendency</u>
	2.557	17.205	06.1.21	1	0.000	10801	1:018/	1130.62	569.92	ı	06,	1.000	-0.000		8000
	-62.595	16.458	-72.325		0.0300	10 93.5	1.0355	1149.18	27.205		13	1.000	0.00	1.0000	1.0006
	+02.654	14.150	-73.045	164 • 01 •	5050	6.9111	1.0525	1167.65	27-725	ŀ		1.000	0.00	•	1.0000
•	- 1	12.736	3.200	48.01	9.0000	71133	1. 33 92	1185.05	23.25	ı	:	1.000	0.000	1.0000	1.0000
9		11.456	-73.376	-10.623	0.0003	1171.3	1.1024	1222.40	29.368	544.544 541.545		1.000	0.000	1.0000	9999
	!	10:303	-73:488	10.01	0.00.0	2:69.11	1811-1	1240.35	146.62	1	:	1.000	0000	: 1:	• •
	-62.411	9.381	-/3.508	-10.597	0.000.0	1207.0	1.1349	1258 . 14	30.525			1.000	00000	1.0000	1.0000
	-63.161	7.683	-73.876	-10.715	0.000.0	154571	1.1510	17.6721	31.126	i		1.000	0.000	6.	1.0000
	63.583	8.848	820.44	1	60000	1200-0	: [:	1910-60	32.37	- [	i	1.000	0.00	1.0000	1.0000
15	-63.412	6.151	-74.190		0.0000	1277.5	1.1983	1327.85	33, 923			1.000	0.030	1.0000	1.0000
	103.243	2.023	2000		0.000	1295.5	1.21.35	10	169.55	1		1.000	0.00	1.0000	1.0000
	-63.771	7. 9.08 F. 9.08	174.040	-10.001	0.000	1312.3	1.2293	1362.16	34.380			1.300	0.00	1.0000	1.0000
10	-53.867	4.562	8+6-14-	-11.082	0.0000	1348.4	1.25.01	13/9:26	35.030	ı	,	0000	00000	1.0000	•
	-65.960-	4.119	175:275	-11.215	0.0000	1366.3	1.1755	1415.58	36.384	í	:	0000		0000	1.000
	690 • + 9 -	3,587	-75.425	-11.355	0.0303	1384.4	1.2907	1+30.42	37,372	676.	. ×	1.000		1.0000	1.0000
	707.40	166.2	-75.704	-11.497		£05.	B	\$	38.192	680.	- 29	1.000	0.000	1.0000	1.0000
	0 No. 40	11.9.00	-76-164	0/0-11-	0.000	1421.2	1.3210	1464.51	39.047	\$0°	<b>3</b> 0	1.000	0.00	1.0000	1.0000
•	STATION	n i	fedit freed	FLOW FILLD DESCRIPTION	¥62				! ! !	:	:	!			
STZEAM	RADIUS	. '	S=1113014A		'	TEMBELAT ISEC.			;	,		:			
-LINE		£	TO TAN	1	+	346	1	TOTAL STA	110	NO N	**************************************	St.0PE	SURVATURE	SPECIFIC	
+	fr. 8474	4 24.A. G.	54-4-4 · - 44	2		. !	ļ	,		;	- 1				
~	7.0061								· · · · · · · · · · · · · · · · · · ·	1	17.73	22.32	5:199	•	
<b>P</b> )	7.1129				İ	,	527.767	, K	0.4400 4.460	10.4 10.4 10.4	17.46	12.12	5.384	ļ	
<b>.</b>	7.218					5+0.715	527.759	<u>o</u>	15.390	3509	16.96	18.33	10.484	• •	
۸ ۷	7.5227	285.19 285.19		114:91399:43	1	ï	527:155	- 664.	5.374 .	3533	۵	16.79	15.005		
۰,	7. 528	ŧ	1	3	į	ī		. :	363	560	16.55	12.18	27.312	•	
•	7.629								350		10.40	13.41	-150:105-	•	
•	7.7291			1	İ	- !			0 40 00		ċ	11.79	. 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	00/00	
0 :	7.829	394.52						1	388			8.25	-11,440		
#:	7.929			1	İ	1	1	1	115			6.50	-9.006-	֓֟֝֟֝֓֓֓֓֓֓֓֓֓֓֓֟֟֓֓֓֓֟֓֓֓֓֓֟֓֓֓֓֓֟֓֓֓֓֟֓֓֓֡֓֡֓	
	8.1295	5 595, 65 9- 306, 74	74 126.98	98 416.34	-		7.30	16.958 1	15,451	.3672	18.05	4.78	-7.375	6220	
<b>*</b>	8.229*						534-073	Ì	5 7		ė d	٠.	5.00		
15	9.3294			!	+	.005	350000	1	) e	_	13,78	1.47	1000	•	
9 ;	8.4294	399.85			5,0	•608	36.619		557		20.31	-1.76	-5.691	• •	
	•	:		10 426:93	1	151	7.985·	٠	17		20.91	3.30	15:085	.0763	
•	100000		156.95	1			39.111	407	. 92	3777	21.35	-4.62	-7.037		
20	. 832			37 434.32		555.535 5	40.004	17.537	330	:	21:66 2:	:	-9.233	-98786	

BUNDE DATA

:

-

!

ŧ

i

ì

ادا	1	!	1		i			ļ			1		i	١		1			Ī	I			1	١		İ	1			١		1			1	
POLYTROPIC EFFICIENCY	9221	• 9065	.3994	.8875	. 8883	. 8701	1100.	. 6163	. 7945	2111.	7537	.7412	66210	.7240	21505	1705																				
STNT-ROPIC PEFFICIENSTER	. 3207	2506.	.8975	.8854	.8780	.8076	+ 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	.8146	.7903	. 2277	77:77	.7353	.7236	.7173	7080		5 <b>5</b> 0:. = 1 M		-cecifer i	WEIGHT	6480	. 0843	0340	.0838	.0836	-0835	1834	. 0033	. 1829	.0827	.0825	479D*	.0822	2290.	1827	; ;
05_TA T IS	.041	. 042	240	. 043	***6	240	045	. 020	. 053	• 0.00 0.00 0.00	1.50	.063	. 056	.069	1/0.	17.1	DELTA T ON		30 OF	SURVATURE	4.302	3.176	. 12:933	26.557	-41.757	-22.023	-16.521	-13.521	15,131	-13.722	74.995-	-21-156	-28.477	-63.395	1665-861	,
PRESSURE RATIO	1.147	1.140	1.140	1.140	1.142	1.1+3	1.145	15	1.154	2.			• 17	91.	1.159		.= .793		16000	SLOPE	27.37	22,78			13, 30	1	1	0 to to	2 . 35	۲.5°	72.67	15.0	-5.59	-6:71-	-8-61	) ) • P
ATIVE SERATURE	613.345	5.384	3.565	1.360	3.171	1,390	544.344	. 526.	176.150	366	001-100	3.398	1.367	675.586	3.250	0 #	PO_Y. EFF		And Anticon	NHIRL	31.89	30.42		29.41	29,03	28.78	28.80	30,04	30,95	31.71	32,36	33.77	34.56	35.07	35.88	3000
10,47											٠.٠	, ω			:	c 1	788		2	200	.4137	.4223	4258	.4289	4353	. 4388	4:421	0644	.4503	.4534	4577	. 13	4664	• 4603 • 4591	1/540	200
RELATIVE PRESSURE	27.504	27.35	29.43	28 92	29-89	30.37	30.852	31.63	32,090	32,50	36.90	33.889	34:357	34.839	35.467	20.04.04.0	EFF. =	!		STATIC	17.321	17.24U 17.173	17:121	17.081	17.053	17.031	17.036	17.049	17.098	17.129	17-163		17.276	17.315	17.394	•
AELATAVE VECUCITY	1052:47	1038.64	1100.33	1140.70	1155.92	1172.17	1200.32		1221.67	1232.64	1243.02	1265.58	1275.18	1288.07	1300.95	1314.64	60 ISEN	; ; 1 ;		TOTAL	į	19.441	265		19,554	i		19.550			19.737	1	·	20.050		
RECATIVE	9313		. 97 95	1, 10 39	1,0241	1.0373	1.0612	1.0012	1.3775	1.0861	1.0943	1.1113	16 11 -1	1,1284	1.1387	1.1495	<pre>&lt;4TIO = 1:163</pre>			STATIC	46.375	546.404 546.404			546.565	547.134	547.775	546.914 551.067	553.255	555.240	557.075 558.325	554 : 1174	63.183	564.851 566.195		
BLADE SPEET	1103.7	1138.1	1154.3	1188.1	1204.5	1220.7	123543 4252.8	16.26.5	1284.7	1300.7	13100/	1346.7	136407	1380.8	1397 0	1413.1	PRESSURE R			TOTAL	5.528	5.555	900.9		67.207			5 176.076	l		500.105			549.948 5	062	32.577
1.088	.0233	.0273	.0290	0317	1333	.0365	1650	11333	.0525	1690	-12 84	.0873	2+60.	ጥ	0001	103/	;	Z.1			56	9 c	۲	10	יי ח	1	56		T		   	1	1 10			Λ
i ;	-3.251 ·	-3.268		-3.272	i	3.270	9, 26 g	ļ	-9.258	692.6	-9.270	-9.272	212.6-	-3.272	112.6-	-3.210	INIEGRATED PERFORMANCE	FIELD DESCRIPTION		TOTAL		480.55	1		45.064 45.006	-		66.516 516.41			01.025	20.4.4	537	537.01	535.33	536.33
REL FLOW DEVIATION				_				١		i	1		1		; !	į	KATED P			MERIO TANSEN	251.29	248.13	76.5.64	241.96	240,36	16.2.2	245.04	249.48 258.81	568.19	276.06	283.00		304.68	311.30	313.77	317.16
REL FL	1	1		711.07-			-70.654	- 1					ł		:	27-	INTEG	FLOW		MERIO	403.89	41 1.56 41 8. 49	92:424	42 3.27	433,43	12.244	445.71	447.47	7.00	446.77	446.57	440.03	44.2.33	440.14	١.	6.23
NGLES	10.432	.20.6	7.796	5.515	4.706	4-140	3.717	SACT	2,396	2.136	36	1.705	1:73	1.833	1.632	3	ON S	9 NO	ĺ			١														ž
T 3LADE-ANGLES	-60.252	-60.526	0.690	-60.845	1.105	1.246	-61.335	-01.244	-61.825	-61.955	-62.079	-62.310	624:29-	-62.563		-62.879	STATION	STATION		מאסומא	7.0764	7,2683	7.3596	7.4495	7.5377	7.7107	7.7960	7.9617	1250.8	8.1386	8.2259	0 + TC + C	6.4933	8.6777	8.77.9	0000
LOCAT	 	1		6 4		•	b c	ļ		13 -6		16 -6	1	1.8 -6		9- 02				-LINE	 	<b>7</b> ×		w	9 ~	. 8	o i	P :	121	13	14.		17	200	2	12
1				I !			!	ļ		•					123	30	l	'		, ,		!			,	1			į		İ					

	LYTROPIC FICIENCY	0220	.9197	.9122	• 9052	-8968-	.8931	. 4857	.8754	. 8559	10201	0170	7744	7574	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	07474			0000	. 2073	1770	* 600 *		ı							!		1							!						1	
	FICENCY SFF	9	. 4165	99	7	6468	9388	3811	9704	22	D##0	5155	1001		74.0	7.23	2277	1000	<b>.</b>	4 0	ŝ	<b>†</b>	34 T = .112				0111771170	24	8	0 :	0 4	) oc	90	0.8	8280	9 6	9 0	. 469.	8	98	9	Ф	so (	Ф (	å:	. 4646	
	DILTA T IS			.091	60	Š	60	93	660.	60	61	7	7.4.	- -	7 7	 H ,	71	4:	۲; ا	137	<b>.</b>	. 143	DELTA T				49 0105 OF	( ) - ( ) -	٠,		TU	,	3.9	-	31	``	⇒ .	-5.303	י תי	~	-7-+03	N	i.			3.4	
	PRESSURE KATIO	,	1.323	32	.32	.31	.31	.32	.35	32	32	, t	200	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	ָּבָּי נְי	ç,	٠ د د د د		ŝ	š,	ş,	3	F.= .795				565.5	2 2	å	÷,	•	÷ .;	٠.		•	•	•	7 ° ° 1			-5.09	-5.26	-7.20	17.96	-3.53		
	1 AT IVE MPERATUPE		527.343	. 6	90		+1	V.	75	٠ د د	9	* *	٠ د د	1		2,	• •	,	ية. در	2,	30.76	34.51	PO. Y. EF				T P N C L	Ē	7 32.1	35.1	0.00 0.00 0.00 0.00	35.4	35.5	3 35.8	30.2	30.7	30.00	20.04	42.0	7 43.3	10.44	1 40.9	47.4 E	1	49.2	-	
	LATIVE 4 ESSURE TE	į	77.25% n	337	720	103	500	37.3	211	55,0	823	912	012	1/1	2,5	5.00	762	111	235	5 ll S	) . (of	2%1	F.= .775			,	HOW	<del>د</del> د	275. 9	745. 75	r 0 .			5+3	9 .550		56.00	*	11 .553	095. 66	.552	495. 564	5 . 265	59 •567	51 •567		֡֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֡֓֜֓֓֓֡֓֜֓֡֓֡֓֡֓֓֡֓
	RELATIVE REL	,	77.65	7	0.	4.5	25	.53		.92	16	, 20 !		13.16	25.53		69.	5.24	. 95	200		20 • 2	INT SEE			,	37) 4 111 F	3. 51.0	18.	57 15.	19.	. e	15 10.	552 13.	18.	735 18.	944 19.	175	18.	390 18.	31 18.	33 19.	19.	1 13.	.53	1	
į	1411Vc 54-40		25.45	00 d d	3328	- 52.64	9213	3532	3+35	75.7		!	↔ .	⊶ ·	-	-	. 37.71	-	-	3343 - 1	00 15 1	11111111	7 = 1.340				1 :	<u>-</u>	2	61	\) (	v	, ,	2 1	22	25	25	570.293 22.	SS	23.	23	7	^1	۴,	2. T		١
; ,	31475 45 SPEPT *#		1132:5	•		1	•	1	•	!								,		¦•	+	•  -	SSURE RATIO	i	ļ		10.KATUR			3±8	247		<u>.</u>	2.5	2	el i	알.	O #	9 6	57.5	182	65	000	i	.072	400	
i	.033 .03 <u>E</u> FF		14/4/5					i	1 6270.								1753 1	•					410 - 2708		<u> </u>		† :	4L 131A	5 39	77.0	25 590	146	ı	100	5	7.5		.03 535.15 22 136 E	**	41.0	53 521	3.	95 53	73 53	કુદ 18		
. ; !	DEVIATION THOTOENDE	1	÷,		17		-19	-13	•	6	7	6	Ť	7	ŕ		.4.493	-	- 3.600	Ť	Ť	-15	) PE4F044A		LO DESEMIPT		Seeees	NOT NOTE	1 334	.935	3 636	100	000	90	2 541	1 543	. nag	651	400	2 1	900	200	57 677	633	54 691	•	
,	REL FLOM	1		220.460	100		FF. 2.50-	-0.5.8.1	-55 . 945	-56.027	-56.121	-52.22	-56.3+0	-26.472	-20.05-	-66.736	-55.330	?	2	~	3	າ	IMTEGRATE		FLD4 FIEL		#EL 9C	RIO TAN						374.7				5.28 410.52					4	50	51		•
DE DATA	-ANGLES		3.782	v		CT C	7,1,7	200	7 36	851	819	778	735	P 343	800	563	134	*2*·	1.025	1.594	2.054	2.356	TION S		ATION 7		1	۵ ایا ۲	51	*	51	ξ, ;	ָרְאָרָ מי	Z is	. 22	51	51	9906 505	ar 0	r 4	7 3	ì	- 3	*	. <del>T</del>		
BLADE	3LAJE SECTIO			. t	֓֓֓֓֓֓֓֓֓֓֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֡֓֓֡	1 5	2	4	90	23	4	\$	82	8	17	333	ŝ	5	87	53.10	34	53.60	STAT		STAT		AH -RADIUS	Ā	۲.	~					-7	~		~ (	e •			1	e d	sŏ	ď		
	LOCAT		⊶ ·	<b>~</b> •	n -	* 4	٠.	<b>~</b>	. #0	σ	10	##	15	2	1,	15	16	11	18		<b>%</b>						STREAM	-118	4	?	m	•	rc 1	<b>.</b>	. 60	ð	#	11	77	7	7 -		17	7	19	. 1	

T ISENTROPIC POLTTROPIC .9273 .9199 .9132 .9132 .8953 .8539 .8539 .8539 .7773 .7773 .7773 .7598 .7598 .7598 .7598 1 .9129 .9179 .90179 .6899 .6899 .6899 .7159 .7159 .7629 .7629 .7629 .7629 .7629 .7629 .7629 .7629 .7629 .7629 .7629 .7629 100 DELTA DELTA - DW T PRESSURE 1.514 1.515 1.517 1.523 1.523 1.536 1.547 1.562 1.592 1.592 1.592 1.592 1.612 1.612 1.645 1.645 RELATIVE TEMPERATURE" 633.554 633.554 635.576 633.3767 646.236 646.234 656.234 657.356 657.263 657.263 657.263 657.263 657.263 657.263 657.263 657.193 667.176 12. RELATIVE PRESSURE 28.537 29.621 29.102 29.353 29.011 29.011 29.011 30.268 30 EFF. X VELOCITY 957.55 966.75 983.23 990.92 1008.75 1008.79 1015.18 PRESSURE RATIO = 1.576 RELATIVE HACH NO . 83 35 . 84 53 . 85 83 . 8 BLAGE 1169.9 1180.9 1202.6 1213.3 1213.3 1274.0 1274.0 1274.0 1275.3 1276.5 1377.3 135.3 135.3 135.3 135.3 135.3 LOSS STATION - 7 - INTEGRATED PERFORMANCE **DESCRIPTION** DEVIATION -14.375
-13.921
-13.921
-13.921
-13.634
-13.634
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659
-12.659 -57.170 -57.170 -57.510 -59.040 -59.040 -59.040 -59.040 -59.040 -59.040 -59.040 -59.040 -59.040 -59.040 -59.050 -59.076 -59.07 FIELD FLOW FIE -5.962 -5.862 -5.867 -5.867 -6.861 -6.861 -6.862 -6.862 -6.862 -6.863 -6 DATA 3LADE-ANGLES SECTION" LEAN • STATION 8 BL A DE -43.135 -44.119 -44.119 -45.129 -45.129 -45.617 -45.616 -47.510 -47.51 LOCAT 

232

SPECIFIC WEIGHT 1.883 -2.124 -2.417 -2.417 -3.212 -3.259 -4.457 -5.359 -5.359 -12.855 -12.652 -15.625 SURVATURE 16.55 14.44 12.39 10.43 6.58 6.68 7.12 1.40 SLOPE 338,79 339,29 349,384 40,39 40,39 40,39 46,10 46,10 46,10 46,10 50,09 50,09 50,09 51,82 51 7253 7173 7173 7101 7011 6979 6953 6913 6913 6914 6915 6914 6914 6914 6914 6914 7143 7143 7143 AB CH 18, 909
19, 055
19, 055
19, 456
19, 456
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 566
19, 56 FOTAL STATIC 26.827 26.852 26.834 27.034 27.079 27.326 27.326 27.326 27.326 27.415 27.326 27.415 27 TOTAL 564.051 569.117 569.117 571.557 571.557 573.272 573 TEMPERATURES -- TOTAL STATIC 523.067 525.179 525.179 527.532 530.354 534.471 537.539 534.471 537.539 549.172 554.908 554.908 557.537 650.693 630.693 630.693 846.72 832.97 823.99 823.99 823.99 815.52 816.52 818.05 818.05 818.05 825.74 831.43 831.43 855.74 831.43 855.74 831.43 MERIO TANGEN 10TAL 529.38 531.31 533.46 533.42 545.26 557.89 557.89 557.89 557.89 637.73 680.16 734.39 774.87 660.82 623.75 623.75 623.75 623.75 623.75 601.18 917.97 950.38 950.38 950.38 951.46 951.63 951.46 951.63 95 HERIO 7. 4792 7. 5252 7. 5252 7. 6690 7. 7187 7. 8742 7. 8742 7. 8742 7. 8742 8. 1079 8. 1178 8. 117 RADIUS -LINE ŧ

1.00   1.00		NOT I			DEVIATION		SS	31405	RELATIVE	RELATIVE				PRESSURE	DELTA T	ISENTROPIC	POLYTROPIC
25.51.25.51.26.010 - 13.409 - 1.020   1.	יוויייייייייייייייייייייייייייייייייייי			THOCE	INCIDER			SPEEJ	האכז עם	ייייסטניי			E CATURE	RATEO	-	EPFICIENCY	
1.00   1.00	4646	624		612:6:-	19:8			1.96.1	. 3043	939:13	146:82	₽P i	.53	28.	- 102	826	9346
1.25   1.25	460	. 517	:	6.010	-13.40	į		204.0	1964	934.95	29.03	Φ.	•	. 62	.203	.9214	.9277
11.52	ų.	• 7 C		190.04	11.6I.		Ĺ.,	6.611.2	7354	26.156	21.62	<b>,</b>	1.574 ·		202.	2416	2126
10.177 - 1.177	ì	100	]		10.00	-		22.5	. 1323	930.01	73.64	۱	7	1.055	61.5	5,06.	9250
12.527 -1.594 -49.1160 -17.556 -114-3 12.514 -7775 -974-25 5-36.515 11.664 -7.565 -1.594 -49.1160 -17.556 -114-3 12.514 -7775 -974-25 5-36.515 -1.665	ĩ	2 2		-+8.314			٠.•	235.6	7893	929.12	20.00	0 4		1.850	. 212	6706.	0700
11.552   1.1594   477.559   177.565   177.59   975.750	ភ	32.7		-48:735				1000	1374	926		i i		- 45.00	-215	5488	6967
1.00	ñ	535		-49.168	-17.53		•	251.4	. 79 32	924.92	3		3000	1.854	.219	.8761	. 6863
\$2.51.000.0	7	- 262	'	-49:55B	22.4		į,	253.3	:7795	955.38	62		285	1.859-	-223	-3695	.876*
38.13	7	909	11	-49.936	-17.02		7	268.5	• 77 05	914.06	53		161.	1.865	• 259	.8472	859
1985   1985	7	194	i	#05°65	ŀ	<b>.</b>	١.	1:42	485	46.168	N.	ı	.188	200	-540	1916	6629
1.0   1.0	2		202	-50.658		<b>5</b> 0 k	m i	287.2	• 7255	869.30	2		.100	1.882	.252	.7648	-8022
1.00   2.2.31   1.0.2.20   1.30.2   1.30.2   1.30.3   1.30.2   1.30.3   1	, ,			201016	ĺ		٠.	297:3	560.	82.949	61.82		. 231	1.895	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1594	-
1.00   2.010   2.011   10.020   130.	7 6		,	-21.410	10.5	į	إ	507.5	• 668	339.52	27.90		\$ (0 t)	1.909	: 273	.7387	. 511
1.132   2.687   2.132   2.142   1.144   2.142   2.14	, ,,			-52.311	110.32		<b>-</b> .,		6076	783 04	29:12		295	526-1	622.	1134	7262
17.77   2.795   2.795   2.795   2.795   2.775   2.775   2.79	5		1	-52-550		į		1 K. C.	10 10 1	109.00	340:36	i	1000	C+C+T	2620	1050	.,636
13.21   2.395   95.396   16.526   16.07   13.05   13	30			-53.428	13.44			355.7	60.00	) T	25.77		75.5	1,990	100	. 66.68	6704
STATION   STATE   ST	3	.412		99	20.03	1	١	169.2	- 20.00	739. 64		223	, a	2.015	100		
\$1AITON 9 FILTON FIELD DESCRIPTION  RADIUS FIELD FIE	-33	.770	213	. 53	-15.75	•			.5994	729.28		673	١-:	2.043	367	6645	6826
STATION 9 FLOW FIELD DESCRIPTION  RADIUS 9 FLOW FIELD DESCRIPTION	*	.132	347	-251:66-	17.00	•  -			-57723			67.3	•	2.076	198	ż	6736
7.5699 702.05 727.34 1011.45 563.330 579.223 33.133 20.564 .0551 45.96 8.54 -5.825 7.556 8.669 8.36 7.75 -5.825 7.569 702.05 727.34 1011.45 563.330 579.223 33.133 20.564 .0551 45.96 8.56 7.75 -22.629 7.625 687.35 725.71 1002.47 565.231 562.523 33.066 20.534 6.5734 .0451 46.77 7.02 -21.629 7.76 7.02 -21.629 7.76 7.02 -21.629 7.76 7.76 7.76 7.76 7.76 7.76 7.76 7.7			1 2	¥€£\$	200	0101	TOTAL	IPERATU		7		HACH .	S. W. C.	LE Summer		8	
2546 697.35 725.71 1002.47 565.22 33.105 20.564 .8551 45.96 8.56 -55.825 .8546 697.35 725.52 1002.47 565.22 33.105 20.566 .8551 45.96 8.56 -55.825 .8525 .8527 1002.47 565.22 33.105 20.566 .8459 46.37 7.02 -22.629 .8527 .8527 1002.47 565.22 565.52 33.065 20.74 .8459 46.37 7.02 -22.629 .8527 .8527 1002.47 565.22 565.52 33.065 20.82 .8357 47.25 6.42 15.02 100.435 .8528 .8357 47.25 6.4527 1002.47 565.32 .8357 47.25 6.4527 1002.47 565.32 .8357 47.25 6.4527 1002.47 565.32 1002.47 565.42				. '	•			, ,	3 1 1	ָרְ אָרְ	;	2	HUTER	SLUFE.	_	1	
667.6 67.35 7.29.7 1000.47 554.231 562.522 33.066 20.504 46.97 66.27 7.79 -999.723 567.02 1000.47 554.639 37.066 20.734 66.97 66.27 75.75 20.21 66.97 66.27 75.75 20.65 67.85 747.25 66.27 75.75 20.65 67.85 747.25 66.27 75.75 66.27 75.75 67.27 73.75 73.7		•	20/		i	11.45	563.1	י חט	79.223	139	56	•	ů,	र १५ १०	-5.82	.00	4
10.12 676.15 731.16 997.23 567.02 53.000 20.734 0495 46.97 6.244 157.532  17.03 675.02 731.57 995.02 957.23 567.02 546.395 20.855 47.15 6.44 18.432  17.03 675.02 731.57 995.02 957.23 567.02 32.95 20.857 47.26 4.62 10.1229  17.03 675.02 731.57 994.91 569.069 567.70 32.962 20.857 47.26 4.62 10.1228  17.03 675.02 731.57 994.91 569.069 567.70 32.96 20.853 48.351 47.49 3.80 7.806  17.04 662.90 741.77 994.91 572.458 591.136 32.752 20.853 8326 48.21 2.11 4.507  17.05 652.90 741.77 994.91 572.458 591.136 32.752 20.853 8326 48.21 2.11 4.507  17.05 652.90 741.77 994.91 572.458 591.136 32.752 20.853 8326 48.21 2.11 4.507  17.05 652.90 774.77 994.91 572.458 591.136 32.752 20.853 8326 48.21 2.11 4.507  17.06 652.90 774.77 994.91 572.458 591.136 20.749 .8249 53.1953 3.007  17.07 994.91 572.458 591.136 591.136 52.255 20.674 .8240 53.1953 3.007  17.07 994.91 572.458 510.379 56.34 56.34 56.34 57.26		•	687		i	100.43		ן היי	51-020	2014	61	ю (	ġ,	7.75	25.6-	460°	
7032 678.15 731.16 997.23 557.023 557.023 55.035 4.055 4.035 47.28 4.62 10.122.  7032 678.12 731.57 995.62 567.024 586.385 32.995 20.857 47.28 4.62 10.122.  7035 675.02 733.41 994.99 562.06 69 57.705 32.916 20.853 8351 47.49 3.80 7.086 10.122.  7035 675.02 733.41 994.99 56.06 69 567.705 32.916 20.853 8351 47.49 3.80 7.086 10.122.  8010 657.11 737.67 994.99 56.06 591.135 32.916 20.844 8335 47.88 2.916 2.91		7.6634			1	0 C . 4 /	2020	!	220.29	990	? .	•	46.71	7.02	29-12-	• !	
7436 675.02 731.57 995.02 -967.894 -586.365 32.916 20.853 .8351 47.25 4.62 10.122 10.122 10.103 73.41 994.99 569.069 567.705 32.916 20.853 .8351 47.49 3.80 7.066 5.495 -87.10 17.10		7. 7032	678		י ס	27.28	167.0		45.244		. 6	דס	10.37	71	15/65/21	•	
7854         672.33         733.41         994.99         569.069         587.05         32.916         20.853         .8351         47.49         3.60         7.066           871d         b67.11         73.62         994.91         569.069         587.05         32.916         20.844         .8356         47.49         2.96         5.96		7.7438	675.1		,	- 64 C		1		0 - 330 9 - 449	3 4	3 €	11.00	4.4	7000	!	
8210 662.93 741.77 994.91 572.458 591.136 32.732 20.844 .8359 47.88 2.96 5.495 .8371 652.93 741.77 994.91 572.458 591.136 32.732 20.823 .8326 48.21 2.11 4.507 994.94 91 572.458 591.136 32.732 20.823 .8326 48.21 2.11 4.507 994.94 92 1.229 49.829 49.8299 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.8299 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.829 49.82		7.7854	672.				569.0	. 0		916	85	9	64.24	3.80	7.06		
9114 662.93 741.77 994.91 572.450 591.136 32.732 20.823 .8326 48.21 2.11 4.507 9149 652.92 774.77 995.34 675.534 592.574 20.789 .8312 49.82 1.25 -1.5832 9159 652.03 774.77 995.31 31.155 7.99.523 32.511 20.789 .8242 1.25 -1.5932 9150 652.03 774.77 995.31 996.93 5.233 32.511 20.789 .8243 2.337 3.737 9150 6597.30 7961.19 996.93 5.228 510.879 32.515 20.674 .8247 55.13 -1.43 2.832 9150 6597.30 7961.19 996.93 5.101.60 593.228 510.879 32.337 20.674 .8275 56.91 -2.33 2.8772 9150 6526.37 869.28 1076.15 705.99 621.284 32.377 20.659 81.07 -1.13 2.659 9150 9150 9150 91 1020.99 717.297 627.770 91.026 91.07 -1.12 20.910 9150 9150 9150 91 1020.93 72.949 91.07 -1.1097.31 72.089 91.07 72.08		7.8260	290	!	•	1	570.7	1	i	640	6	Ð	47.08	2,96	64.5		
952.62 151.62 195.74 675.534 1531.155 195.54 -32.674 1812 1812 1813 1813 1813 1813 1813 1813		7.8716	-				572.4	•		732	82	ø	48.21	2.11	4.50		
9543 026.33 774.77 99f.31 531.155 549.527 32.511 20.749 .0245 53.19 -553 7.357 3.357 3.156 -597.30 796.19 -597.165 -597.165 -32.31 20.874 .0245 53.19 -553 7.7327 3.156 -597.30 796.19 -597.165 -397.165 -35.23 -2.836 3.127.5 557.65 82.176 1016.15 705.91 621.284 32.377 20.628 .8299 58.80 -3.23 2.658 3.27.7 56.95 597.914.54 1016.15 705.91 621.284 32.377 20.628 .8299 58.80 -3.23 2.659 3.27.7 476.17 954.28 1076.33 723.85 634.305 33.787 20.658 .8695 63.62 -5.12 2.722 3.27.7 476.17 954.28 1076.33 723.85 634.305 33.787 20.658 .8695 63.65 -5.12 2.722 3.27.7 476.17 954.28 1076.33 723.85 545.345 62.867 65.45 -6.41 -2.346.11 1020.3 1100.3 7.46.385 545.342 34.801 20.813 65.78 58.50 -6.41 -2.346.11 1020.3 1100.3 74.6.385 545.342 35.301 20.813 65.78 58.56 -6.73 4.421 -2.821		7.9169					g The L		i		7.8	ø	49.82	1,25	3+83	-	
1276 576.63 821.76 1001.60 593.226 510.879 32.235 20.674 8247 55.13 -1.43 22.836 10.879 532.65 821.76 1001.60 593.226 510.879 32.235 20.674 824.7 55.13 -1.43 22.836 10.879 57.82 87.82 10.674 82.827 56.91 -2.33 2.836 10.876 52.836 10.876 51 1001.60 51.86 51.86 51.87 20.689 82.99 58.80 -3.23 2.659 10.96 52.836 10.85 52.837 20.629 86.99 81.07 -4.15 2.659 10.83 51.879 51.87 51.87 51.629 86.99 81.07 -4.15 2.659 10.83 51.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 72.836 10.83 80.86 72.836 10.83 80.86 10.83 72.836 10.837		7.9643	950				581.1	۰۵.		511	7	æ	÷	.37	7.35		
2.635 20.674 851.0 1001.00 394.514 35.235 20.674 8247 55.13 -1.43 2.635 -1.645 851.0 1001.00 394.514 31.0 1001.00 394.514 31.0 1001.00 394.514 31.0 1001.00 394.514 31.0 1001.00 394.514 31.0 1001.00			•			,	19761	i i	- 264	P. 334	2	•	mi 1	w.		ļ	
1896 526.37 869.21 1003.03 3373.74 32.377 20.628 6299 56.80 -3.23 2.656		•	_			ï	343.6			2,235	6		ů,	* 1	<b>•</b> 1	ω (	
2360 509.57 914.54 1044.95 717.297 627.778 20.629 61.07 41.15 2.659 3273 478.17 964.28 1076.33 723.836 534.305 20.659 68.95 63.62 5.12 2.725 ************************************							7.05.0		16.	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Š	<b>D</b> 4	å.	70	<b>~</b> u		
3273 478.17 964.28 1076.33 723.836 534.305 33.787 20.658 .8695 63.62 -5.12 2.722 .4841 455.93 998.11 1020.53 1110.93 746.385 545.342 34.801 20.813 .8903 66.78 -7.09 3.308 .9730 411.21 1046.97 1124.82 -754.831 20.949 .8975 68.56 -6.73 4.421			500	i	Ì	o un	4 L	-		1.491-	2 6	• ≪	• +	u ÷	0000		
**************************************					. 60		723.8	. 49	34.905	787	5 6	•	i	4	2.72		
<4857 438.01 1020.53 1110.93 746.385 545.342 34.801 20.813 .8903 66.78 -7.09 3.308 .9730 411.21 1046.97 1124522 7754.939 7650.998 7733 41.21 1046.97 58.56 -6.03 7424 75.424 75.48		•	ķ	•	##	•	-739.1	T of	}	36.0	*	•			96.2-		
•9/30 411.cz 1046.97 1124:52 754.939 7 560.998 7 751.301 20.949 69.96 56 66.56 66.03 4:421 20 60		9 (	÷.	-	P) (	m	746.3	٠o٠		801	81	•	ġ	-7.09	3.30		
			ä			-	ļ	-	-	•	į	•	•	•			

DELTA T ISENTROPIC POLYTROPIC ON T EFFICIENCY EFFICIENCY 7494 7282 7096 6925 6809 6725 6638 7974 345 £ PRESSURE ( 2,255 2,255 2,255 2,225 2,225 2,225 2,227 2,227 2,200 2,200 2,233 EFF RE\_ATIVE TEMPERATURE 6443.96443.06443.06443.06443.064443.064443.064443.064443.064443.064443.064443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.06443.064443.064443.064443.064403.06443.064404 655-324 655-323 557-300 650-321 657-305 657-305 671-305 671-305 .757 RELATIVE PRESSURE 29.028
29.035
29.035
29.035
29.035
29.038
29.058
29.058
29.058
29.058
29.058
29.058
29.058
29.058
29.058
29.058
29.058
29.058 PRESSURE RATIO = 2.262 INCHESTER RELATIVE 847.04 847.04 847.04 843.07 643.07 643.07 740.40 740.40 714.52 643.62 64 RELATIVE - HAC-T-VO 1213.3 1213.3 1223.1 1223.1 1239.0 1245.7 1255.5 1255.5 1255.7 1265.7 1265.7 1265.7 1265.7 1265.7 1265.7 1275.7 1275.7 9LA05 SPEC3 1371.7 1183 11645 11645 11571 11663 11939 11939 2180 2180 2180 2180 3783 4473 LOSS LOEF-FLOW FIELD DESCRIPTION "9"INTESTATED PERFORMANCE INCIDENCE REL FLOW -34,366 -34,951 -34,951 -36,004 -36,007 -36,910 -36,910 -36,910 -37,990 -38,274 -38,274 -39,031 -39,553 -39,966 -38,799 -37.236 -37.257 -38.298 -40.101 4.137 4.340 4.555 4.756 4.951 4.955 4.955 4.592 4.297 3.958 2,597 2,697 2,630 3,086 3,552 3,636 3.617 SECTION LEAN STATION 10 DATA STATION BL ADE į 234

STREAM	KADIOS	A GIN SK	WEERENTELOCITIES - TOTAL	TOTAL	TOTAL	ATJRES STATIC	TOTAL	OTAL STATE	. KON	MHIRL SLO	SLOPE	RADIUS OF CURVATURE	SPECIFIC WEIGHT
						Ι,		!		;	,		2006
	7.5746	716.75	754.97	1019.46	563.330	577.582	33.159	20 • 398	. 8 62 8	45.55	79.	T+0.7	0.00
. 2	7, 6139	DX - 127	726.03	1023.23	564.289	578-203	33.102	- 20,311	. 8658	45.20	7.70	9.676	2560.
M	7.6537	725.95	726.94	1027.35	565.231	578.462	33.066	20.219	.8691	45.04	7.53	10.002	.0937
	1989	75 0 - 98	727.64	1031.41	555.144	378.591	33.030	821.02	\$228	44:87	7.31	- 102.71-	5660.
· un	7.7348	735.90	728.17	1035.27	557,029	578.922	32.930	20.041	.8754	44.70	7.07	10.193	8260.
	7:1158	760.45	728.56	1038.73	- 364-196	579.190	32.962	-13.961-	.8782	44.54	6.82	19:038	3260.
۰ ۸	7.8172	742.70	730.4+	1041.70	559.069	579.973	32.916	19.892	-8802	44.52	6.56	9.794	.0920
	7.8590	781.57	134.77	1043.30	570.764	581-194	32.849	19.834	.8810	44.74	. 82.9	9.494-P	.0919
• •	7. 9815	72.9.75	738.98	1045.63	572.458	532.598	32.782	19,785	.8814	44.97	6.00	9.147	.0911
	5886	731.52	748.98	1040.94	57.5.384	589.510	150.25	19:745	- 6 805	- 29.69	5.70	3,786	4060
11	7.9900	708.10	772.28	1047.77	591.155	590.364	32,511	19.715	.6770	47.48	5.37	3,352	<b>1690</b>
21	8.0378	651.65	795.93	1047.93	537-105	596.314	32.334	19:696	-8725	24.64	4.95	7.890	. 0995
1 1	8.0883	65 8. 31	819.84	1051.44	593.228	502.461	32.235	19.689	.8717	51.24	64.4	7.406	.0876
15	8.1415	636.55	843.95	1057-11	\$14.99c	507-793	32,330	19:69	9218	52.97	3.90	5.938	.1869
15	5.1977	611.24	864.33	1061.89	7 05.990	613.463	32,377	19.729	.8725	54.86	3.19	6.507	.0862
100	8. 2572	587.73	914.39	1087.00	182911	20 30 029	33.021	19.789	5885	57.27	82.2	221.5	.0895
11	6.3208	556.83	965.02	1114.17	729.935	528.095	33.797	19.888	6406.	60.01	1.15	5.791	6480.
81	8.3895	528.02	999.85	1150.69	739.199	634.469	34.360	20.03	9133	- 91.29		- 25426-	1,0847
6	8.4639	5000.77	1023.56	1139.49	746.386	540.063	34.801	20.220	.9159	63,93	-1.89	5.107	.0847
- 02	8.5659	45 4 95	1050.28	1158.55	754.539	196.949	35,301	054.02	.9196	56.12	-3.83	4.519	• 1545
	A. 6.499	416.25	1383,69	1150.33	764-642	554.403	35,921	20.711	.9239	68.99	-6.18	3.053	6480.

## 1	######################################
FLOM FIELD : 02  FROM FIELD : 02  FROM FIELD : 02  FROM FIELD : 03  FROM F	RADIUSVL_DCITIES   7.6199 020:39 721.02   7.7129 020:39 721.02   7.7599 020:39 721.02   7.7599 020:39 7721.02   7.8646 047.52 7721.02   7.8646 047.52 7721.02   7.8671 -979.39 7721.02   7.8671 -979.39 7721.03   7.8716 047.75 7721.03   8.10575 047.75 7732.43   8.10575 047.75 7732.43   8.10575 047.75 7732.43   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25 0439.33   8.2445 7760.25   8.2445 7760.25 0439.33   8.2445 7760.39   8.2446 7760.39   8.2446 7760.39   8.2446 7760.39   8.2446 7760.39   8.244
- ΗΙ ΙΣ ΒΟΦυβουσουσουσκικικουσουσ ΚΙ ΝΣ ΣΙΟΝΑΝΑΚΗΨΟΝΗΦΟ	A

	,		クリインインク	ï	•					5		,		į	
	띭		TANGEN	TOTAL		TOTAL	STATIC	TOTAL	STATIC	0	WHIRL	SLOPE	CORVATORE	<b>x</b>	
•	_		504.65	1115.97	10		560.303	32,375	17.947	• 9546		2.21	- 7.633	1000	
7,753	•		586.79	1092.33	'n	N	506.103	32,352	•	σ (	•	29.	13.440	2/00.	
7. 7929	90 4.24		557.76	1057.73	ļn į	55.231	571.497	32,325	18.943	שית	36.16	***	-3.104	1060	
7.832	_		540.05	1046.3	2	30.144	5/00/41	32.21	13.440		• .	1	-3.017	6	
7.871	ı		36.056	1013.43		620.70	077-106	30.40	20. 177	) I	31.22	3,49	-2,959	.0931	
2.5.0		2.5	513.00	13463/	•	940.0	500000	12, 121	20.781	•	31,11	3,31	-2.947	2460	
100	0	P 0	26 • 20 •	10.00 TE		7.00	395.05	32,040	21-141	~	31.04	· N	-2.941	.0951	
444		n s	431.00 LR1.45	975.73	1	377.458	5.111.523	31.968	21.462	. ~	30.96	3,20	-2.947	8560.	
30.00		2.0	472.25	610.43		75.336	605.879	31.482	21.747	7	30.89	C	-2.964	• 0962	
3,116	5 777	י פיי	454055	1	1	15155	513.845	31.743	22, 900	.7437	30.67	•	-1.019	1960.	
6.163		.*	45 8. 62		ታ	17.135	521.727	31,612	22.221	.7 285	30.92	₩:	-3.120	• 0958	
5.204		2	¥56.75	88	10	13.228	528.541	31.63%	72.413	.7191	31.04		-3.755	9660.	
6.249	755.	æ	457.61			19.514	635.475	31.677	22.576	~	31.19	# 1	-3.537	. 0953	
8, 295		32	459.8T		1	- 066.31	542:001	31.750	22,735	.7093		∽ .	-3.932	\$ . 5 . 5 .	
8.340		10	475.34			17.297	246.249	32.238	75.794	~ 1		- •	020.4	0 460	
8.386	;	100	24.964	ı	1	9.836	658-027	. 226.25	. 22* 822	.7433		n,		2000	
-2		7.	518.73	752.		19.199	563.375	33.497	22.787	/	ů	- 1		1760.	
		53	542.13	988.5	- 12	16.335	20	33,752	22.617	1611.	m,	N .		2020	
8.5237	848	.71	570.+0	1022.2	ň	i4.539	559.014	34.13+	22,303	.8051	33.90	-	13.557	r i	
Ln.	878		603.79	1004.4	io	734.542	72	34.539	21.369	.8362	÷	-2.03	•	2 000 •	
2	DATA								<b>;</b>						
!							!	!							
3LADE-A	LES	REL FLOW		DEVIATION	L353	3LADE	RELA		RELATIVE	77		PRESSURE	OELTA T IS	SENTROPIC PC	_
SECTION L	LEAN	THELE	E TNCI		305 F	SPEEJ		1	ш.	<del>}</del>	ZATURE	RATIO	 		
0.00				0.00			ľ	76.2111	- 32:376		330	~		9038	\$216
	65 E C	25.6		852	.0513	0.0		1092,33	32,352	5 654.28	289	2.201	.281	. 8967	.9074
317247 -	-21,380	32.124	į	-377	.050	0.0	•	- 1067.70			.231	ņ	.233	5893	2106.
- 649	-19.085	31.7			•0+0•	0	•	045			771	ᅻ '	+62.		1669.
1.507 -	16.698	31.4	- 22	13	0495	0.0	•	-1015.43			129	년 '	582.	1919	.000
- 675.0	14.423	31.216			.0512	0.0	•	39+ • 97			394	٠,	000	0000	0000
30:153 *	192.21	311.112		666	6250	0.0			32.25		607	: •	266		8623
	-10.146	31.0	j	980	.05+1	0.0	•	•	30.045		r «	: "	23.6		\$169.
23.959	71.97	5000	•	, , ,	C .	•	0000	919.00	74.882		3 30	: :	.302		.8345
2/0.5	10.705	20.00		51	1000		•	03.4506			155	7	. 313	1181.	.8036
	F C C C C C C C C C C C C C C C C C C C	20.00						292.49			1.05	7	.325	.7495	.7746
2000	767	32.038		1		F. D		385.35	!		228	7	.337	.7230	1501
142	3,171	31,190		1.048	04.0	0.0	•	383.61	31.677		, 214	∹	6 76 9	6669	.7300
319	5.981	31.364	1		-10445	0:0	ľ	'n	31.756		986	٠,	.361	5779	2011
0.581	9.210	31.621			.0 + 93	0.0		0	32.23		762,	7,	5555	0460	. 0099
-666:0		į		136	.0565	0.0	7.	in i	32.92		335	'n	- C	9350	
1.506	16.718		-	1.030	.0509	0.0		902.49			J. 1.	ř	624	6710	0539
022.2	521.02	1		E	10	פים	16.1.2	06.886			000	•	r ()	מ כ	ME ME
32.851	24.587	33.	<del>-</del>	1.053	~	2.0		1022.58	24.13		700	?"	14.4	4 P P P	) X
	28.225	53.557	r	-	.0885	P	33.65	1064 . 45	24.23	_	7*0	•	•		

į

T 77210 9105.9 17.5 1 10.0 10.0 11.0 11.0 11.0 11.0 11.0	œ	S
7.7220   705.25   251.45   2	SCOPE CORVATORE	
7.7927 755.2 251.4 51.4 51.5 54.2 59 607.13 31.556 23.031 1.0009 17.55 7.7 79 75 75 75 75 75 75 75 75 75 75 75 75 75	N	11011
7, 1922 770, 25 24, 25 24, 26 24, 26 24, 27 24, 27 24, 27 24, 27 24, 27 27 27 27 27 27 27 27 27 27 27 27 27		i I
7.7572 77.75 27.57 75.75		1026
7.9023 747.02 255.99 735.15 07709 677199 31.435 25.8182 6.423 17.91 27.0109 675.99 31.595 25.9187 6.22 27.017 27.0	İ	-
7. 17. 17. 17. 17. 17. 17. 17. 17. 17. 1		
### 1724.01 226.27 763.71 570.764 625.372 31.259 24.077 6.522 17.39 -2.15	30	
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	51	
\$1055 711.0.23 22.0.4.3 705.0.7 37.384 650.3133 31.00. 2.0.224 .0032. II.40 711.0. 6.0.002. II.40 711.0. 6.0.002. II.40 711.0. 6.0.002. II.40 711.0. 6.0.002. II.40 711.0. 6.0.002. II.40 711.0. 6.0.002. II.40 71.0. 6.0.002. II.40 6.0.002. II	g (	1000
8.1549 7111 22 22.56 7.72.39 57.1129 57.22.22 55.57 17.47 1.121 5.22.56 7.72.39 57.22.20 17.43 1.595 1.44 1.44 1.595 1.44 1.44 1.44 1.44 1.44 1.44 1.44 1.4		
6.214.0 771.33 225.00 793.00 391.22 30 391.21 17.50595 6.21 17		1015
\$\begin{array}{c} \$1.200.		
6.256 723.84 226.85 759.75 754.297 565.75 31.759 24.356 6.525 17.64 15.54 15.54 754.71 227 755.75 15.551 31.259 24.356 6.525 17.64 15.55 17.64 15.55 17.65 1		
8.3440 747.55 237.67 784.3 717.27 565.303 31.514 24.356 6.615 17.64 6.65 6.434 71.45 2.435 71.27 717.27 565.303 31.514 24.356 6.615 17.64 6.65 6.434 71.47 71.45 2.435 71.02 835.42 71.45 31.45 25.35 24.349 6.515 18.06 77 6.435 71.47 71.45 71		660.
9.1991- 777:11		•
8,436, 734,30 259,02 835,40 739,199 582,103 32,359 24,349 6513 18,06 588 6,552 18,40 6,552 8,685 19,23	11	
5.4855 50.677 259,00 697137 754,555 685,357 35,652 24.287 16524 18.40 .77 54,553 695 37.471 35.912 24.289 24.196 .6524 18.40 .77 54,535 695,377 35,199 24.196 .6524 19.23 .659 6.5795 844,27 2594,50 697137 754,542 599,377 35,199 24.196 .6550 19.23 .659 846,27 2594,50 697137 754,542 697,377 37,199 24.196 .6559 19.23 .659 846,27 2594,50 697,37 754,59 24.196 .6594 19.23 .659 846,27 15.51 1.40 846,27 15.52 11.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.54 14.40 846,27 15.40 846,	64-	
8.5323 3.55.02 288.73 871.47 754.539 592.471 32.932 24.280 .6576 19.23 .65 8.6576 19.23 .65 8.6576 19.23 .65 9.6576 19.25 .65 9.6576 19.25 .6576		
9LADE DATA  9LADE DATA  9LADE DATA  9LADE DATA  9LADE ANGLES  9LADE DATA  9LADE ANGLES  9LADE ANGLES  9LADE ANGLES  9LADE ANGLES  9LADE ANGLES  15.234 -9414   17.005   17.547   1.365   10.00   1.406	. 200.	
\$\$\text{\$100.00}\$\$\$100.0		0.00
15.234 -9.414 17.205 1.351 .1043 -0.0 .5083 34.05 31.516 604.289 2. 15.181 -8.920 17.547 1.365 .1015 0.0 .5083 34.05 31.516 604.289 2. 15.181 -8.357 17.540 1.406 .0937 0.0 .5645 809.05 31.554 655.144 2. 15.184 -7.717 17.541 1.475 .0938 0.0 .56534 131.554 655.144 2. 15.184 -5.394 17.541 1.475 .1033 0.0 .5534 784.16 31.473 667.329 2. 15.044 -5.394 17.541 1.475 .1033 0.0 .5623 763.7 31.541 667.329 2. 15.044 -5.25 17.391 1.545 .1064 0.0 .5623 763.7 31.394 659.354 2. 15.046 -4.225 17.391 1.545 .1064 0.0 .5623 763.7 31.104 675.384 2. 15.046 -4.225 17.391 1.565 .1073 0.0 .5623 742.57 31.104 675.384 2. 15.046 -1.440 17.449 1.656 .1004 0.0 .5925 742.39 30.897 693.155 2. 15.047 -1.540 17.449 1.656 .1004 0.0 .5925 742.39 30.897 693.155 2. 15.048 -1.440 17.449 1.656 .1004 0.0 .5925 742.39 30.897 693.165 2. 15.049 -1.440 17.449 1.662 .1004 0.0 .5925 752.12 31.004 693.514 2. 15.049 -1.440 17.449 1.656 .1004 0.0 .5925 752.12 31.004 693.514 2. 15.049 -1.440 17.649 1.662 .1031 0.0 .5926 753.10 .31.904 772.39 31.504 77.297 2. 15.049 -1.440 17.640 17.640 17.640 17.653 17.5297 2. 15.049 -1.440 17.640 17.640 17.640 17.653 17.5297 2. 15.040 17.640 17.640 17.640 17.653 17.500 17.5297 2.2 31.504 77.297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5297 2.2 31.504 77.5299 2.2 31.504 77.5299 2.2 31.504 77.5299 3.3 5.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3	RESSURE DELIA I	EFFICIENCY EFFICIENCY
15.151 -8.957 17.547 1.365 .1015 0.0 .6883 834.05 31.616 664.289 2.215.154 -8.357 17.547 1.365 .1015 0.0 .6845 809.05 31.516 664.289 2.215.154 -7.717 1.7.540 1.406 .0937 0.0 .6645 809.05 31.554 656.144 2.215.164 17.512 1.470 .1013 0.0 .65534 784.16 31.548 656.144 2.215.164 17.512 1.470 .1013 0.0 .65534 784.16 31.438 657.832 2.215.944 -9.212 17.512 1.470 .1013 0.0 .6523 784.16 31.438 657.894 2.215 17.391 1.542 11.543 0.0 .6223 784.16 31.438 657.894 2.215 17.391 1.542 0.0 .6223 783.71 31.259 670.764 2.215 17.392 17.392 17.392 17.392 17.393 1.693 1.	.153	
15.153 -8.357   7.540   1.405   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00   0.0545   0.00	. 151	. 5576 . 6609
15.134 -7.717   17.5+0   1.+06   .0937   0.0   .0645   809.05   31.554   656.144   2.     15.166	. 249	
15.166 -6.904- 17.512 1.470 .1013 0.0 -0423 784.11 31.511 667.329 2. 15.041 -6.144 17.512 1.470 .1013 0.0 -0423 784.16 31.473 607.394 2. 15.044 -5.225 17.391 1.542 .1054 0.0 .6228 763.71 31.259 607.394 2. 15.046 -4.225 17.391 1.542 .1064 0.0 .6228 763.71 31.259 670.764 2. 15.046 -4.225 17.391 1.542 .1073 0.0 .6228 763.71 31.259 670.764 2. 15.046 -1.440 17.391 1.656 .1107 0.0 .6091 755.19 31.10 0.72.456 2. 15.013 -1.740 17.391 1.656 .1107 0.0 .5967 745.70 30.897 093.228 2. 15.014 -1.24 17.463 1.665 .1107 0.0 .5967 745.40 30.992 093.228 2. 15.015 -1.301 17.502 1.667 0.0931 0.0 .5992 755.12 31.009 099.514 2. 15.016 3.322 17.504 1.662 .1031 0.0 .6185 764.43 31.504 717.297 2. 15.016 3.322 17.504 1.662 .1031 0.0 .6185 784.43 31.904 729.336 2. 15.016 3.322 17.504 1.662 .1031 0.0 .6185 784.43 31.904 729.336 2. 15.016 3.322 17.504 1.662 .1031 0.0 .003.70.40 31.904 729.336 2. 15.016 3.322 17.504 1.662 .1031 0.0 .003.70.40 31.904 729.336 2. 15.016 3.322 17.504 1.662 .1031 0.0 .003.70.40 31.504 729.336	.147	
15.041 -6.144 17.512 1.470 .1013 0.0 .0423 784.16 31.439 607.594 2.9212 17.395 17.395 10.0 .1013 0.0 .05221 77.395 17.396 10.0 .00 .00 .00 .00 .00 .00 .00 .00 .0	. 144.	3905
15.846	.139	0000
15.846 -5.225 17.391 1.592 1105	101	158
15.749 -2.230 17.37	400	0.00
15.016 -1.440 17.441 1.656 .1104 0.0 .5967 742.39 30.897 631.155 2. 15.013 -734 17.469 1.656 .1104 0.0 .5967 742.39 30.897 637.105 2. 15.013 -734 17.469 1.656 .1104 0.0 .5967 742.39 30.897 637.105 2. 15.014 -1.24 17.469 1.656 .1104 0.0 .5967 742.89 30.897 637.105 2. 15.014 17.469 1.650 1.674 .0931 0.0 .5992 752.12 31.006 175.997 2. 15.016 2.201 17.546 1.662 .1031 0.0 .6165 764.43 31.504 717.297 2. 15.016 3.322 17.604 -1.653 .1130 0.0 .6165 784.43 31.904 729.336 2. 15.10 4.38 18.061 1.650 .1120 0.0 .6157 .6379 32.356 739.199 2.	116	•
15.013 -734 17.469 1.656 .1104 0.0 .5965 742.39 30.897 697.105 2. 15.014 -1.74 17.469 1.656 .1104 0.0 .5966 745.80 30.897 693.228 2. 15.014 -1.74 17.469 1.656 .1104 0.0 .5966 745.80 30.928 693.228 2. 15.018 -1.74 17.469 1.662 .1031 0.0 .5185 764.43 31.504 717.297 2. 15.018 3.322 17.604 1.662 .1031 0.0 .6185 764.43 31.504 717.297 2. 15.10 4.38 18.06 1.650 .1230 0.0 .6315 835.46 32.358 739.199 2.	. 169	
15.014 -124 17.403 1.669 -0955 - 0.0 -3952 752.12 31.000 693.220 2. 15.028	.102	.7246 .7515
15.628 .523 17.502 1.674 .0931 0.0 .5992 752.12 31.008 699.514 2.  -15.875 1.330 17.546 1.670 0.995 0.0 .5022 753.16 51.094 705.990 2.  15.976 2.281 17.637 1.662 .1031 0.0 .6185 784.43 31.504 717.297 2.  15.150 3.322 17.804 -1.653 .1130 0.0 .518 0.35.46 32.354 739.199 2.  15.110 4.438 18.061 1.650 .1230 0.0 .515 33.6 32.356 739.199 2.	.105 .3	
15.075 1.330 17.546 1.670 0.031 0.0 6183 75.16 51.094 705.390 2.15.976 2.281 17.637 1.662 1031 0.0 6183 76.43 31.504 717.297 2.15.916 3.322 17.8041.653 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	.110 .3	6783 .7097
15.976 2.281 17.637 1.662 .1031 0.0 .6185 784.43 31.504 717.297 2. 15.150 3.322 17.604 -1.653 .1130 0.06370013.00 31.940 729.336 2. 15.110 4.438 18.061 1.650 .1230 0.0 .0.515 835.46 32.356 739.199 2.	116	
15.150 3.322 17.3041.65311900.0 15370113.0015.940 729.135 Z-15.410 4.436 18.061 1.650 112.00 0 0 0.515 835.46 32.356 739.199 Z-15.420 4.74844.74.8 4.436 14.64844.74.8 4.74846.348	144	
15.410 4.436 18.061 1.6501250 0 0 0.522 0.5540 1.6540 1.6540 0.5240 0.5440 0.6450 0.5440 0.6450 0.6450 0.6440	202	• •
TO THE PROPERTY OF THE PROPERT		
2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		.5654 .6105
2000-100 - 1	•259	ľ

DESCRIPTION	
FITTO	1
7. Y	
14	1
STATION	
ST	-

.

E- 3: II Le	<u></u> S	!	イイン・コートリ	14171	イクリント・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	ļ	100	2	かいしつとば		211111111111111111111111111111111111111	
<b>-</b>	OTAL	-		<u>~</u>	ر ہ	STATIC	ON	WHIR.		CURVATURE	WEIGHT	!
,	3.9		•	526-133	33.903	25.217	÷2474		-4.29	15.241	.1080	
	1. 4.			527.217	31.857	25.213	10014	> 0	14.00	17.55	10/01	1
60	603.33			529.357	39.700	25.202	.5431	5.48	-3,64	19.943	.1074	
	7.63		ļ	220:055	33.740	25, 196	.5413	5.80	-3. 40	21.510	2/01:	
36 055	00° 50° 50° 50° 50° 50° 50° 50° 50° 50°		557.694 7.69.069	531.705	30.652	25.189	.5338	7.6	-2.87	25.501	.1066	
				535.+63	31.454	25.173	ູເຕ	5.02	-2.57	29.234	.1062	
ו	iņ	1	į	5 37 . 5 05	37.37	25, 165	.5251	ກຸກ	-2,25	31.756	.1058	
1	5.	:		540.500	30.312	25.156	ກະ	, v. v.	1.4	50.597	1003	
	? -			70000	30.179	25.141	5182	5,50	-1.30	54.639	.1033	
į	1 10			657.771	37.251	25, 134	ະຫ	5,49	-1.01	75.073	.1024	
	٥			563.095	31,349	25,128	.5271	5.48	75	125.237	.1016	
67 E75.9J	D.	:	•	558.553	33. 453	25.123	. 5323	5.49	- 53	330,727	. 1008	
ļ	^			577.455	30.7+2	25.120	5453	, 57.7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-, 30	-1357,621	+6FD •	
				537.753	31.055	021.62	2007	,	* ;	-510.000	• 0000	
734.0		<u> </u>	9.199		51,550	221.62	. 2013	7.00 u	• • •	1047 - 100 100 - 100	0 1 C 0 0	
754.72		<b>1</b>	0 0 11	705.759		25,128	.596.0	10.0	90	-311.276	• 0953	
778.64		10	10	13.1	35	25, 132	.5932	1	1, 05	-510.507	2560.	
DEVIATI 'N INCIDENCE		.03S	9LADE SPELJ	RELATIVE VACT VO	SELATIVE VELOCITY	E PELATIVE Y PRESSURE	0,47	AT IVE ERATURE	PRESSURE RATIO	DELTA T IS	SENTADPIC PEFFICIENCY	POLYTROPIC SFFICIENCY
	- 1	1321	0.6	-3474	10.576	٠.	~	.330	2,103 -	- 612	8448	1668.
2.241			0.0	. 5461	571.90	30.3	~	-289	2.100	. 291	<b>60</b> (	.8534
•		1503	b.		570:70			123	2.098	.253		1/15
2.507	- 1	1493	2 6	18+6	45 453			. 561	2.192	546	1620	1886
2.407		.1534	9 0	.5377	663.90			394	2,085	. 258	. 8085	. 8272
504.2	1	1570	þ.	. 53.33	653.53	-		-1690.	2.079	-162	. 7985	. 8180
2.525	- 1	.1602	0.0	• 5294	655.0d	į		.764	2.072	. 293	.7656	5005
2.641		1523	20	. 5235	057.50	30.312		675.384	2.063	.302	.750	.7801
199.2	1	1577	0.0	50.25	19:649			.155	2.057	. 1213 113	1270	8261
2, 721		.1505	0.0	• 5182	550.17			.105	2.054	. 325	.6993	1121.
2,735	(	1431		12.26	697.65	27 • 0£		927.	2.05.5	255.	. 5567	MG 64.
20/30	- 1	1333		1/36	10.000 TRANSPORT	i		- 056	2.072	.351	.6372	11/0
2.683		1549	9 0	97.46	64.769			-297	2.092	. 393	1609	6949
799.2	1	:1773	P. P	5003	721.18		:	.3.36	5:114	404	1295.	9229
2.603		.1933	0.0	. 5713	739.48			661•	2,132	.425	.5644	.5070
2.661		56.02	<b>b</b> (	06./c•	80.567	31.50	\ 	40.386	441.2	654.	5066.	9490
2.723		.2303	0	• 59 60	764.72	31.6	.   .	.239	2.156	. 455	25.5	. 2010
819.2		. 2510	2.0	2566.	10.677	21.02	+0/ 66	• • • •	001.7	*	61764	•

	}				1									ļ :	!		}		1	1	1	POLYTROPIC EFFICIENST	. 6310	.8252	. 8106	. 8122		8787.	20619	7659	.7516	7254-	. 7035	-16655	2899.	1169	5066	1579	. 9660	. 5515	£344
SPECIFIC	•	.1078	-	.1072	н.	-	<b>⊢</b> •		1148	.1036	.1029	.1021	.1012	40	, c	э с	4400	6460	.0934			ENTROPIC Ficiens#	241	690	397	327	357	69.	202	555	.7264	. 996	737	537	340	ב ב ב ב ב ב ב ב ב ב ב ב ב ב ב ב ב ב ב		260	211	150	
RADIUS OF SURVATURE	,	11.117	69	33	23	2	ָרָ בָּי בּי	֡֝֜֜֞֜֜֜֝֓֜֜֜֜֜֝֓֜֜֜֜֜֜֓֓֡֡֜֜֜֜֡֡֡֜֜֜֜֜֡֡֡֜֜֜֜֡֡֡֜֜֜֜֡֡֡֡֜֜֜֡֡֡֡֜֜֜֡֡֡֡	12	5.	7.	34	9	66°×6	157.47 574.69	いつ かんしゅつ		25	37,90			DELTA T IS	•	Œ	40	თ-	•	23		20	. 302	31	VI.	2	ž i	φ γ	, ,	٠,	5	T.	٠
SLOPE		-1.62	-1.58	-1.53	-1.46	-1.33	-1.29	11.11	91	77	ţ0.I	52	1.12	•	200	60.		1 (0)				PZESSURE RATIO	.05	.04	.0.	÷.	• 03	. 13	20.	5 5	2.03	.03	.03	40.	.02	20.	2 6	7	0.00	0.	
WHERE	•	0.00	9	6	ē.	•	•	2 0	9		0	•	•	۵,	•	? =	•					ATIVE PERATURE	3.53	4 . 2 8	5.23	j.14	7.32	7.39	9.00	9 / 6	01 10 10 10 10 10 10 10 10 10 10 10 10 1	1.15	7.10	3.22	٠ ا	9.0		יי יי	1 60	M ( )	
14C4 340	- 4	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	35	4	93	2	\$ 3	,	: 2	4762	470	92	33	93	÷.	1 6	1,6	1 4	5234			NTIVE REL	ça 7	19	71 65	21 25	69 /9	55	55 55	70 91	21 57	75 03	55 63	7.57	3+	00 70	1, 60	77	7.0	37 75	
STATIC	•	25.471	5, 43	5.40	5:47	5.35	5.32		, y ,	2 2	5.23	5.25	5.21	5.21	,	2.50	, . 	, ,	7.23			ACLA	0 . 1	0.1	9.0	0.0	9.9	9.8	9.7		N LO		J. 4	9.5	9.6	ກຸດ	,	֓֞֜֜֜֜֜֝֓֜֜֝֓֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֓֓֡֓֡֓֜֜֜֜֜֓֡֡֡֓֡֡֡֓֜֜֡֡֓֜֜֜֡֡֡֜֜֜֡֡֡֡֡֡	• •		
P SSJ	1	57.197			÷	÷	٠,	٠,	• 6		5	÷	÷	÷.	÷.	٠,	∹,	• -	, -			RELATIVE FELDEITY	=	0	•	3	~	۲-	<b>1</b> 0	N I	190.00	^1	-	'n	~	M.		. 1		. ~	, ,
J (E 3		532.481	554:595	535.349	536.312	537.573	559.161	041.290	170000	- FE 3-1-54	557.573	502.574	557.935	278.844	533.031		7.01.404 40.404	746.550	724:731	ļ		RELATIVE		656+	- 4953	. +345	+9.35	006++	.45.60	. 4317	.4777	4752	• +7 55	6364.	. 4391	• 4974	, ve 5.	2113			
15451-441	į	:	į		1		:			:						•				;		3LAU2 \$P2£3	-	0.3	n.0	0.0	0.0	0.0		0	p = =	- <del>0</del>	0.0	B • B ·	0.0	<b>.</b>	2 f	ָ פּרָ			
	į	L -	٠ ٨،		:					٠,		•	~	31 735	~ ·	! ► •	┙,	0 1				2053 302Fe-	-6486	.2033	2013	.2011	.2015	.2023	-2103	.214+	.21.47	20.71	. 2002	-166T.	.1803	1913	1502.	. 63 93 .		3 5	1 .
Ics	,	1.00 515.1 1.30 513.1	1 - 612	6	7 - 51	3) ėi	. ca	0.0 533.27	200	060 00 000 000	00 00	00 o10.	00 p50.	00 631.	00 000	30 55I.	.475	000	111 69Us			DEVIATION INCIDENCE	į	76	.564	735	995		242	.495		121	923	; 4:	_	ŀ	~ .	: • •	!	9.171	1 1
TIJCTEN	•		, <b>(</b>			ځ.	ċ	<b>.</b>	. ·	• ¢		'n	ċ	ė	o i	<b>.</b>				,		7 . O. H	0000	9			٠,	•	•	•	0.000			•	•	e.	? (		? •	•	•
ERID		, c	612.82	612.4	- 611.71	607.7	503.6.	599.27	70.000	74.050	60041	610.53	620.7:	631.31	346.4	651.87	, t	? ·	0 M	OATA		ν. <del>Σ</del>	*	0.00	010	.017	.015	.013	##:	.010	900	000	.003	000	-•005	00%	- 0 03	.013	010	200	300
340105	,	7.58400	? P~	. ~	•	•	€0	OT (	. ·	<b>,</b> ,	•		N	N	m	ю.	, t	* ·	3.6400	ADE		SECTION LEAR	~	7 . 3	3.0	7 . 73	.90	6	3.24	3,4	44.00	3.0	9.92	3.00-6	6.0.	3.063	3.058	200	4003	3.163	7 / 7
STREAY -LINE	} . }		J #7	*	-6	9		<b>6</b> 0 (		= <del> </del>		1 F	7 [	15	9	<b>.</b>	EO (		2 4			LOCAT									•			1		i				6 6	

				, 11		1	ı	į				•	•
STREAM -LINE	RADIUS	MERID	ELOCITIES- TANGENT	. 10T4L	TOTAL TOTAL	ATJRES	TOTAL	SJRES STATIC	MACH NO	HHIPL	SLOPE	RADIUS DE CJRVATURE	SPECIFIC
-	7.6400	24 *0 29.	00 °0		53.	1.	30,167	25.254	,5110		•	0.334	.1074
~	• 67	62 6 15	00.0	4	504.289	531,390	30,119	25, 253	.5087	00.00	03	1140.289	•1072
m	7, 7195	625.83	0.00	625.33		533.074	33.071	25.253	• 5063	0	•	512.523	10701
<b>3</b>	7.7508	623.41	0.00	623.41	556.144	034.237	30.02.	25.252	S (	•	- 08	441.479	•1066
<b>.</b>	• 8U3	£9.0.29	00.0	Р.		20++656	_1c6.E2	152.52	0	ָם י		114.000	9901+
۱ م	9 4 6	614.95	0.0	514.95		0.55.343	259.62	22,620	1.		•	300 634	*1003
		÷ 1	00.00	01.600		0.00.000	23.62	C2 C43	<b>,</b>	•	•	120.062	2001
•	σ.	m,	0.00	603.13		+06+0+9	53.6+4	25.248	900	•	•	277.545	•1056
σ	•	599.17	0.00	539.17		5+2:393	29,555	25. 246	J		- 13	273.754	1053
10	•	٠	0.00	557.73		646.058	23.521	25.245	4	•	•	279.213	.1048
	5.0817		6	297.44		651:373	- 29,475-	- 25. 243	.475%	6	•	291-739	1038
12	8.1321	539.55	0.00	599,52		657.533	29.455	25.242	.4763	0	•	312.546	•1029
13	8.1832	60 9. 27	6	509.27		262.310	23.574	25.241	• 4 819	-	•	345.435	1201
7.	3.2345	019.05	0	519.05		558.111	23.034	25.240	.4877	0	•	392.940	.1013
	8.2860	52.6.2g	ű. 0G	629.24		573,553	29,800	25,239	• 4937	•	•	462.133	1005
16	8.3377	044.15	0.00	044.15		583.331	23.959	25.238	•5013	٠.	- 03	566.550	9660
	8.3896		6	554.55	53	+62.7E0	-311:0£	25:237	.5033		•	734 - 351 -	
18	8.4417	-		673,33		702.142	31.270	25.237	.5176	•	•	103291	<b>*</b> 960 <b>*</b>
	8.4948	4	0.00	581.33	10	708.452	31), 355 "	25,236	.5215	00.0	02	1567.524	- 560°
20	8.5468	689.91	00.00	689. 31	•	715.971	30.437	22.236	.5255	٠.	٦.	1597.584	• 0945
. 12	8.6000	6	00 00.	699.35	13	154.731	30,519	25,236	+625*	•	<u>.</u>	0.000	-0934
	STATION	MC74 .4I	FIELD DESCRIPTION	CRIPTION			;					•	
		!			;							•	! !
1		; i	- 1,			ٔ ا		0.10	2	1014	Ę	c	717
SIKEAN	KAUTOS	•	-COC11153-			174 - JR 15	0	0110110	5 6		1000	10100	
<b>1 2 1</b>		שנאות	A 46.0	ב ה	1018	-	1 W 1 C .	- -	2	MAT KL	31016	ź	
<b>!</b>	7.6400	63.1.84	Þ	++	555,330	\$30.989	. 30.167 ·	25.236	.5120	•	00.0	0.000	•
~	7.6792	629.39	0	029.33	554.249	531.704	30,119	25.236	6	•	•• 00	0.00	7
m	7,7195	627.02	00.00	\$27.02	1565.23I	- 832,951	30.071	25.236	9	•	- 00	0.000	
	7.7607	624,55	٦	624.15	500.144	534.119	30.021	25 • 235	Š	٠.	. 00	0.100	•
ĸ	7.8029	- 621.78	0	62I.73	520:155	6~2°5°50	23,967	25	22	Ξ.	00	9.000	
9	7.8462	615.98	00.00	615.93	567.894	536.745	23.852	25.236	95	•	01	0,000	•1063
	7:8908	40.019		-610:03	526.659	538:521	29:755	- 25: 236	ሯ	٠.	01	000.0	1
•	7.9367	604.04	00.0	504.04	570.704	640.318	29.644	25,236	85	-	01	000.3	
<u>.</u>	7.9838	599.93	-00.0	599.93	372.458	2+5:351	. 53.556	25,236	8	0	01	00000	•
10	5.0321	598.40	00.00	596.40	375.384	246.002	29,521	25,236	79	•	-• 01	000.0	
: <b>!</b>	8:0815	-59.8: 02	-00.0	- 598.02	581.155	551.52	. 54.62	25.236	475	9	01	0.000	!
12	8.1319	599.93	0.00	599,93	537.105	657.587	29.455	25.236	470	0	01	0.000	7
13	8.1630	609.65	00.0	60.609	593.228	362.762	29.574	25.236	82	0	01	0.000	:
7.4	8.2343	619.34	00.00	619.34	99	568.085	29.684	25.236	37	•	01	00000	
. 41	8.2858	629.45	0.00	629.45	. 705.990	573.535	29.800	25.246	93	Ę	0	0.000	
16	8.3375	644.30	00.00	644.33		583.315	23,959	25,236	02	•	0	0.000	0660•
11	8, 3895	-65 9. 65	_ 00 0	-623.63		**************************************	- 311.02.	. 25, 236	13	0	0	000	
18	8.4416	673.34	00.0	673.3+	739.199	702.137	39.276	25.236	17	0	•• 00	0.000	•
19	- \$£64°B.	- 04.1.89	00.0	581.43		108:450	30:356	-25:52	7	0		000.c	
	8.5467	689.92	00.0	689.92	754.539	715.570	30.437	25.236	.5255	0.00	no	000 • 0	<b>+60</b> •
									1	٠	•		

100			1 1 7 h		ATV:C	030	2.0	3-1	0.71 TA	7 128	DEL TA	TICES	SEJSWA-NC	LEAN	I-ANGLES
101-	CADTUS	RADIOS	H. NO	ENCE	HOLL	Sopre	FACTOR	٦,	Ē	RAFIO	2.00/4	INCET	-007657	INCET	_
**	5.7500	7.3139	1.0187	421-01	066.52	1811.	. 3575	.3756	9426	1884	.6021	-62.567	-11: 816	1	666.3
~	•	7.5867	1.0356	10.330	22.211	. 1243	. 3865	.3338	.5124	.7371	.6002	464.50		10.450	- 1
n.	2.98.07	7.6245	\$250.1	154.01	215.15	1369	#50# •	660+0	1669	5223	2864	-62.034 -62.658	-14,672		
<b>.</b>	0.0340	1.0034	1.0692	10.499	21.332			<b>,</b>	2004 - I		. 6808.			-1	- 1
ک م	7.3207	7.7438	1.1024	10.623	20.458	1271	. 4423	3 (3) (3) (4) (4) (4)		6915	5904	-62.753	-16.451	11.455	
۰,	7.4325	7.7854	1.1127	10.021	966-61	1363	2464	578t	£044.	.6515	.5838	-62.507	,	ı	
. •0	7.5437	1 . 8280	1.1349	10.697	13.557	.1305	. 4585	.+712	.4250	. 6693	.5830	-62.911	-18.100		
6	7.6545	7.8718	1.1510	10.698	19:156	-1339-	-4812	EPH TO	5607*	.6593	.5890	-63.039	ė	ļ	4.340
01	7.7643	7. 4169	1.1069	10.715	18.734	. 2180	. 5008	.5422	.39+1	.6433	.5934	-63.161	-19.509		
Ħ	7.8750	7. 95 43	1.1828	ŧ.	18.422	.2360	:5381	1686	. 3739		.6030	63.1	951.02-		0600
15	7.3851	8.0150	1.1983	7	18.254	. 3111	. 5757	.5700	3044	1672.	.6224	9.00	-20.756		- 1
£ :	3.0956	8.0594	1.2158	10.520	17.357	3479	5600.	2606	. 5506	CD 65 +	66565	100.040	-21.057		
) 1 1	•	6.1275	1.2293	10.631	17:232	. 37.83	<b>:</b>	CR5C.	0.000	. 50.45	10000	000	106 173-	-	ı
15	5.5164	8.1895	1.2445	10.905	024-11	1504.	. 5/1/	10 10 1	2442	6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6.000	-63.867	100.00	4,562	4,926
12	• ,	2 C C C C C C C C C C C C C C C C C C C	1000	111005				17580	3055	40	7227		63	4:119	-
. «	•	8. 404.	1.2907	11.456	13.175		7327	0062	.2977	+0.04	.7423	0	-24.051	3.587	4.592
9 0	•	A. 18 57		11.037	1	515	0110	8113	2912	3317	7519	2	*	166.2	1
202	3.8822	6.5730	32	11.670	13.545	. 5205	. 8+27	.8393	.2861	. 3573	. 7633	•	-24.752	2,386	3.958
12	•	8. 66 99	1.3360	-11.919	15:137	īv	. 3835	.8798	.2835	-, 3223	.7735	-64.478	+54.954	1.835	3.617
	STATOR	THE KE ORINGE	ANCE	!			:		!			,	•		
												•			
LOCAT	INLET	outlet	IALET	LINGE	191	L03S	•			ر .	JELTA	SECTIO	ON-ANGLES	LEAN-	EAN-ANGLES
-104	440105	KADIUS	H-40	- FNGC	NCT 1	-30Ehk-	FACTOR	-FASTON	Š	RATIO	4/04	INLTT	のひてんきで	INET	##### ######
†	. 4.400	- 2-54-00	4000	4			-6444		•	. 5593	000	48.917	en en	-39.941	120
• ~	7.5667	7.6800	.9527	-7.536	7.397	. 2034	539	.5 3 8 9	~	10	000	7.97		-37,355	.020
m	7.7129	7.7200 -	\$			- 2019-	200	3r	65	4	.000	7.1		Į.	610
4	7.7579	7.7626	.9703	-5.754	7.735	. 2011	2 09	0	Φ	.* 1	• 000	÷ 1	-7.735	-31.532	.017
ķ	•	7. 9052		924.9	7.305		S.	₩,	ტ (	9	000		٠,	200	100
9 •	•	7.8488	1976.	-6.12!	8.074	. 2059	. 6242	S I	3 3	0.00	000	40.003	1 2 2 2 4 1	-25.271	210.
. •	1,000	70307	37.24	- 25 LCD	243.6 243.6	24.12		0000	'nq	5271				1 1 8	010
o		6996-4-	9707	696	666.0	215	-0474	.6473	. 3	. 5250	.000	4.7	÷	İ	980.
201	5.0142	8.0352	.9666	-3.632	8.599	. 2147	•	.5522	σ	.5253	.000	10	-9.699	-12	.006
#	5.0575	-8.08 th	-9603	-4.955-	-8-821-	- 1602	59	16655 -	σ	• 527•	• 000	10.4	-8.821	f	548*
12	3.1022	8.1347	.9536	230	8.923	. 2005	•	.06.35	.5037	.5303		<b>.</b>	-8.923	•	200
ï	•	· 6. 1855	-19561	10	200.6	1061	4	- 55517-	9 (	* 0.00 t	9	, d	10:00		200
<b>4</b>	5.1957	8.2365	9446	2.504	6+0-6	. 1853	. 6503	25.98	7 9	47452	000	אית	7. C+0.	2.991	200-
<u>.</u>	3.2443	2.02.2	1016	5.500	9.033	6101.		1000.	0000	3 4		ָ ער	0000	12,358	- 008
۲ <u>۲</u>	1662.6	10 00 00 O	9300	620.0	00000	1007		4517	'n	. o		. 0	-3.852	100	24
		8.4424	5476	10.113	9.089	25		6656		.5635	000	ď	-9.089	27.404	018
É	•	6. 49 45	8	026.11	\$21.6	262	•	5445	39	7 2	.000	÷	19:129	35:003	1965
20	1.5342	A. 54.70		110 011				* * * *	1	;		•			
	٠	2 - 1 - 0	ø	13.21	3.171	. 3101	. 5357	698 6.	S.	9	0000.0	646.64	-9.171	41.043	- 035

### 7. PHASE II WITHIN-BLADE ANALYSIS (100% SPEED) TEST POINT 208300915800

Colored   Colo			RADIUS	A	Val 30 IT I & S		TEMPER	ITURES	P?	SSURES	MACH	ANGLE	E S	RADIUS OF	
Color   Colo	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	- 1		- MEALD -	TAME	101AL	TOTAL	STATE	OT A.	STATE	014	HHERL		CJRVATURE	
6.227 287.97 0.00 267.97 516.688 511.343 14.956 14.027 2593 0.00 15.22 0.00 15.24 0.00 1		-	6.064	287.42	90.0	-287.97	-518+688	-544-843 -	- 3	14,027	2585	00.0	20.93	0.00	8735
Control   Cont	Color	۰ ۲	25	287.97	0.00	267.97	518.688	511.943	14.696	14.027	.2583	0.00	19, 77	0.000	.0735
1,517   207.37   0.100   277.37   210.000   211.013   14.030   14.037   255.99   0.100   17.041   0.000	Color   Colo		.0.0						464	10.027	128		200	900	0735
1,000	6. 697.97	e 14	6-5937	242-37	00.0	287.37	716.086 518.688	##	14.696	14.027	.2589	000	17.41	000.0	.0735
1,557   27.79	7.4514 287.97 0.00 287.97 516.686 5114.02 14.025 2559 0.00 15.47 0.00 12.47 0	, o	6.8472	267.97	0.00	287.97	518.688	=	14.696	14.027	2589	00.0	15,03	000	07.45
7.1517 287.97 0.000 287.97 518.688 511.843 14.695 14.027 2589 0.000 10.30 0.000 10.000 0.0	7.4557 287.97 0.00 287.97 518.688 5113.43 14.695 14.027 2559 0.00 10.00 0.000	7	-9686-9	-29-2-92	90.0	-287.97	-518.6d8	511.843	14.696	14.027	2589	00.0	13.84	0	0735
7.4334 287.37 0.00 237.47 10.000 511.34 14.655 14.027 2569 0.00 10.00 9.416 0.000 0.001 0.	7.535 237.37 3.00 237.37 10.00 511.31 14.655 14.027 2569 0.00 10.1	€ (	7, 1517	287.97	0.00	287.97	514.648	511.843	14.096	14.027	.2589	0.00	12.65	000.0	.0735
1,000   23,797   0,000   23,797   10,000   5,11,000   1,000   1,000   0,000	1,000   27,77   0,00   23,77   18,606   511,001   14,606   14,107   2509   0,00   0,000   0,	5	7 5 34.			100			9694	1000	2589	000	27-67	000	0735
7.7530 287.97 0.00 287.97 514.688 511344 14.656 14.627 2589 0.00 6.00 0.00 0.00 0.00 0.00 0.00 0.0	7.77330 281.97 0.00 287.97 518.68 511.343 14.696 14.027 2599 0.00 6.00 0.00 0.00 0.00 0.00 0.00 0.	3 7	7-6034	242	00.0	247.37	518.588	511.343	14.090	14.027	6862	•	10.30		6570.
1,0912   287,747   0,000   287,97   510,000   511,945   1,0027   2550   0,000   5,0000   5,0001   5,	9, 0912 287,97 0.00 287,97 518,608 5111943 14,659 14,027 2599 0.00 6.00 6.00 0.00 0.00 0.00 0.00 0.	12	7, 7530		0.00	287.97	518.546	511.843	14.696	14.027	2589	000	8.00	0.00	17.45
\$1,091 287.97 0.00 297.97 518.688 511.843 14.696 14.027 2589 0.00 5.00 0.000 0	8.3643 287.97 0.00 237.97 518.68 5118.43 14.695 14.027 2589 0.00 5.00 0.000 8.3643 287.77 0.00 237.97 518.68 5118.43 14.695 14.027 2589 0.00 3.77 0.000 8.4645 287.77 0.00 237.97 518.68 5118.43 14.695 14.027 2589 0.00 3.77 0.000 8.917 287.97 0.00 237.97 518.688 5118.43 14.695 14.027 2589 0.00 3.77 0.000 8.917 287.97 0.00 237.97 518.688 5118.43 14.695 14.027 2589 0.00 1.98 0.000 8.917 287.97 0.00 237.97 518.688 5118.43 14.695 14.027 2589 0.00 1.90 0.000 8.917 287.97 0.00 237.97 518.688 5118.43 14.695 14.027 2589 0.00 1.90 0.000 8.917 287.97 0.00 237.97 518.688 5118.43 14.695 14.027 2589 0.00 1.90 0.000 8.918 287.97 0.00 237.97 518.688 510.695 14.027 2589 0.00 1.90 0.000 8.918 287.97 0.00 237.97 518.688 510.695 14.695 14.027 2589 0.00 1.90 0.000 8.918 287.97 0.00 237.97 518.688 510.695 14.695 14.007 2819 0.00 1.90 0.000 8.918 287.97 0.00 237.97 518.688 510.695 14.695 13.907 2819 0.00 17.11 0.001 8.918 287.97 0.00 237.99 518.688 510.695 13.804 2813 0.00 17.11 0.001 8.918 287.97 0.00 237.99 518.688 510.695 13.804 2813 0.00 17.11 0.001 8.918 287.97 0.00 237.99 518.688 510.695 13.804 2813 0.00 17.11 0.001 8.918 287.97 0.00 237.99 518.688 510.695 13.804 2813 0.00 17.11 0.001 8.918 287.97 0.00 337.99 518.688 510.495 13.804 2813 0.00 17.11 0.001 8.918 887.97 0.00 337.99 518.688 510.495 13.804 2813 0.00 17.17 0.001 8.918 887.97 0.00 337.99 518.688 510.495 13.804 2813 0.00 17.17 0.001 8.918 887.97 0.00 337.99 518.688 510.495 13.804 2813 0.00 17.17 0.001 8.918 887.97 0.00 337.99 518.688 510.495 13.804 2813 0.00 17.17 0.001 8.918 887.97 0.00 339.99 518.688 510.495 13.804 2813 0.00 17.17 0.00 13.90 13.90 13.904 13.804 13.804 13.804 13.805 13.804 13	4	7.9022	287+37	00.00	267.37	914688	5114343	14.690	14. 027-	2589	0 0		0	23.5
\$\frac{3.464}{2.564}\$\frac{3.47.7}{2.646}\$3.4	1.949	14	8.0511	287.97	0.00	287.97	518.688	511.843	14.690	14.027	.2589	0.00	5.80	0000	0735
8.343 267.77 0.00 287.97 518.688 511.843 14.696 14.027 2.569 0.00 3.77 0.000 8.655 0.000 287.97 518.688 511.843 14.696 14.027 2.569 0.00 2.7 0.000 8.659 0.00 8.690 0.000 8.69	8.5450 287.97 0.00 287.97 518.688 511.843 14.695 14.027 2589 0.00 3.77 0.000 8.75 0.000 287.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.000 8.75 0.000 287.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.000 8.75 0.000 287.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.000 8.75 0.000 287.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.000 8.75 0.000		1001	282-32	9	287.97		-548454	- 964A	-14-027	-2583		4.76	9000	0736
8.6450 267.97 0.00 287.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.00 0.99 0.00 0.287.97 0.00 287.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.00 0.99 0.00 0.287.97 0.00 287.97 518.688 511.843 14.695 14.027 2589 0.00 0.99 0.00 0.99 0.00 0.287.97 518.688 511.843 14.695 14.027 2589 0.00 0.99 0.99 0.99 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90	## 5450	91	8.3483	297.07	00.00	287.97	518.588	511.943		14.027	.2589	00.00	3, 77	0.000	.0735
8-79-70 (201-97) (1-10-10-207-97) 518-688 511.843 14-696 144.027 (2589 0.000 1.528 0.000 1.000 1.528 0	### 19417 227.97 0.00 237.97 518.688 511.843 14.695 14.027 2589 0.00 1.99 0.000	1	1064.0	76-782-	0.00	287.92	514-688	-511-843	144696-	14.027	-5583	- 30.0	2-84	0.00	8735
STATION 2 *LOW FIELD DISCRIPTION  STATION 2 *LOW FIELD DISCRIPTION  STATION 2 *LOW FIELD DISCRIPTION  STATION 2 *LOW FIELD DISCRIPTION  RADIUS STATE S	STATION 2 FIGURE STATES THE STATE		8.0430	287.97	00.0	287.97	7 T G 6 C C C C C C C C C C C C C C C C C C	511.843	14.696	14.027	.2589	0.00	1.98	0000	.0735
STATION 2 *134 FIELD DISCRIPINA 511.843 14.895 14.895 14.807 .2589 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	STATION. 2 1-134 FIELD DISCRIPINAL SILEMA SILEMA 14.000 14.027 .2589 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	, 4 c	77744	-	-	**************************************	41-4-04B	511.545	14.000	14. 027	2584	0000	1.24	0.000	07.15
\$\text{RADIUS}\$\	RADIUS	2 5	1146.0	20103	•	76.767	0 1 G • G G G	511.843	14.696	14.027	.2583	0.00	. 55	0.000	.0735
## ## ## ## ## ## ## ## ## ## ## ## ##	## ## ## ## ## ## ## ## ## ## ## ## ##		<i>n</i> 1	٧!	1000	No. 11 c raps									
6.3746 311.77	6.3746 313.77 0.90 311.77 518.688 510.569 13.914 2806 0.00 20.83 -205.758 0.5542 313.24 0.00 31.77 518.688 510.569 13.914 2802 0.00 19.61 -137.572 0.505 314.59 518.688 510.569 13.914 2842 0.00 19.61 -137.572 0.00 315.80 0.00 315.80 510.455 14.696 13.907 2843 0.00 17.19 -92.872 0	REAM		3 A 4 E	LOCITIES		TEMPERA	TURES	PRES	SURES	HACH	ANGL		RADIUS OF	SPECIFIC
6.37%6-313.77 0.90 313.24 510.508 510.509 14.696 13.914 2206 0.00 19.61 -137.572 6.5542 313.24 0.00 313.24 510.508 510.509 14.696 13.907 20.20 0.00 19.61 -137.572 6.5543 13.24 0.00 315.80 510.608 510.496 13.907 20.303 0.00 19.61 -137.572 6.5544 13.500 0.00 315.80 510.498 510.496 13.907 20.303 0.00 15.10 -92.801 6.5924 13.500 0.00 315.80 510.498 510.496 13.804 2.852 0.00 15.97 -92.801 7.6545 13.500 0.00 315.80 510.496 13.804 2.852 0.00 15.31 -60.17 7.4654 13.907 0.00 319.44 510.608 510.205 14.696 13.804 2.852 0.00 13.83 -66.572 7.5545 13.907 0.00 319.44 510.608 510.205 14.696 13.804 2.862 0.00 13.83 -66.572 7.5545 13.907 0.00 319.44 510.608 510.213 14.696 13.876 2.884 0.00 13.83 -66.572 7.5545 13.907 0.00 319.44 510.608 510.213 14.696 13.877 2.884 0.00 13.83 -14.596 13.877 2.884 0.00 13.83 -14.596 13.877 2.884 0.00 13.83 -14.596 13.877 2.884 0.00 13.83 -14.596 13.877 2.884 0.00 13.83 -14.596 13.877 2.884 0.00 2.98 -14.596 13.877 2.884 0.00 2.98 -14.596 13.877 2.884 0.00 2.98 -14.596 13.877 2.884 0.00 2.98 -14.596 13.877 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.844 0.00 3.98 -13.82 -13.83 -14.596 13.877 2.884 0.00 2.98 -13.57 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.98 -13.577 2.884 0.00 2.88 -13.577 2.884 0.00 2.88 -13.577 2.884 0.00 2.88 -13.578 0.00 2.88 -13.578 0.00 2.88 -13.578 0.00 2.885 2.884 0.00 2.885 2.884 0.00 2.885 2.884 0.00 2.885 2.884 0.00 2.885 2.884 0.00 2.885 2.884 0.00 2.884 0.00 2.885 2.884 0.00 2.885 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 0.00 2.884 2.884 2.884	6.5142 313.24 0.00 313.24 518.688 510.589 14.696 13.997 .2819 0.00 19.61 -137.572 6.5142 313.24 0.00 313.24 518.688 510.589 14.696 13.997 .2819 0.00 19.61 -137.572 6.7910 315.24 0.00 315.80 510.688 510.4896 13.997 .2843 0.00 17.18 -92.870 6.7910 315.80 0.00 315.80 510.688 510.4896 13.897 .2853 0.00 17.18 -92.870 6.7920 315.80 0.00 317.89 518.688 510.346 13.894 .2862 0.00 17.18 -92.870 7.6520 313.74 0.00 317.89 518.688 510.346 14.696 13.894 .2862 0.00 14.75 -73.672 7.4964 313.74 0.00 319.44 510.281 14.696 13.877 .2881 0.00 13.83 7.4963 319.97 0.00 319.44 510.213 14.696 13.877 .2881 0.00 9.88 -48.586 7.7937 320.32 0.00 320.32 518.688 510.213 14.696 13.877 .2884 0.00 9.88 -48.586 7.7454 320.32 0.00 320.32 518.688 510.213 14.696 13.877 .2885 0.00 5.92 -73.8285 7.7454 319.93 0.00 319.24 510.213 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 319.73 0.00 319.24 510.213 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 319.73 0.00 319.24 510.23 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 319.73 0.00 319.24 510.23 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 319.73 0.00 319.24 510.23 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 319.73 0.00 310.88 510.875 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 310.73 0.00 310.88 510.815 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 310.73 0.00 310.88 510.815 14.696 13.877 .2885 0.00 5.92 -22.196 8.7564 310.73 0.00 310.88 510.815 14.696 13.910 .2815 0.00 5.92 -22.196 8.767 0.00 310.77 510.88 510.815 14.696 13.910 .2815 0.00 5.92 -22.196 8.767 0.00 310.77 510.88 510.815 14.696 13.910 .2815 0.00 5.77 -16.515 0.00 5.00 5.92 5.90 0.00 5.00 5.00 5.00 5.00 5.00 5.00	*		- XI R II	TANGEN	1614	TOTAL	-SIVIE	101AL	-51415-	9	- MHERE	30013	CURVATURE	NEZCHI
6.5142 313.24 0.00 313.24 518.688 510.589 14.696 13.907 .2819 0.00 19.61 -137.572 6.6526 315.24 0.00 315.24 518.688 510.456 13.907 .2843 0.00 17.18 -92.870 6.7900 315.30 0.00 316.90 518.688 510.456 13.894 .2843 0.00 17.18 -92.870 6.7900 315.30 0.00 317.89 518.688 510.346 14.696 13.894 .2863 0.00 17.18 -92.870 7.0620 317.89 0.00 317.89 518.688 510.265 13.894 .2862 0.00 14.75 -73.672 7.4924 318.74 0.00 317.89 518.688 510.265 13.894 .2862 0.00 12.31 -60.171 7.4954 319.97 0.00 319.49 518.688 510.265 13.872 .2884 0.00 12.31 -60.171 7.5937 320.32 0.00 320.32 518.688 510.213 14.696 13.872 .2884 0.00 5.12 -29.448 7.5937 320.32 0.00 320.32 518.688 510.213 14.696 13.872 .2884 0.00 5.12 -29.448 7.5937 320.32 0.00 320.32 518.688 510.275 14.696 13.872 .2884 0.00 5.12 -29.448 8.4010 316.30 0.00 318.24 518.688 510.275 14.696 13.892 .2852 0.00 5.12 -29.448 8.4010 316.30 0.00 318.24 518.688 510.275 14.696 13.892 .2852 0.00 5.12 -29.448 8.4010 316.30 0.00 318.24 518.688 510.275 14.696 13.892 .2852 0.00 5.12 -29.448 8.4010 316.30 0.00 318.24 518.688 510.318 14.696 13.892 .2852 0.00 5.12 -29.448 8.4010 316.30 0.00 318.24 518.888 510.318 14.696 13.892 .2855 0.00 5.12 -25.196 8.4010 316.30 0.00 318.24 518.888 510.215 14.696 13.892 .2855 0.00 5.12 -25.196 8.4010 316.30 0.00 318.24 518.888 510.215 14.696 13.892 .2855 0.00 3.7 -16.516 8.86 510.758 14.696 13.993 2759 0.00 -2.7 -26.216 8.8610 0.00 318.27 510.808 510.215 14.696 13.993 2759 0.00 -2.7 -26.216 8.8610 0.00 318.282 510.258 14.696 13.993 2759 0.00 -2.7 -26.216 8.8610 0.00 318.27 510.808 510.215 14.696 13.993 2759 0.00 -2.7 -26.216 8.8610 0.00 318.282 510.258 14.696 13.993 2759 0.00 -2.2 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5	6.5142         313.24         0.00         313.24         518.688         510.589         14.696         13.907         2819         0.00         18.688         510.458         510.469         13.907         2832         0.00         18.68         510.465         14.696         13.900         -2832         0.00         17.18         92.870         0.00         17.18         92.870         0.00         17.18         92.870         0.00         17.18         92.870         0.00         14.696         13.884         2852         0.00         17.18         92.870         0.00         14.696         13.884         0.00         14.696         13.884         0.00         14.696         13.884         0.00         14.696         13.884         0.00         14.696         13.884         0.00         14.696         13.884         0.00         14.696         13.884         0.00         14.696         13.872         2884         0.00         14.696         13.872         2884         0.00         14.696         13.872         2884         0.00         14.696         13.872         2884         0.00         14.696         13.872         2884         0.00         14.696         13.872         2884         0.00         14.696         1	-4	6. 3746-	- 311-77	8 3	311-77	518.648	- 510.564-	14.696	13.914	2.806	00-0	20.63	~205.758	. 8731
6+626         314+56         -0+00         314+56         -514+688         -510,519         14,696         13,900         -2832         0+00         -18,109         -18,109         -2843         0+00         -18,109         -18,109         -2843         0+00         -18,109         -18,109         -18,109         -2843         0+00         -18,109         -18,109         -2843         0+00         -18,109         -18,	6*6526         314*56         -0*00         -314*56         -514*68         -514*56         14*696         13*894         -2843         0.00         17*18         -92*870           6*924         315*80         0.00         315*80         518*688         510*1456         14*696         13*894         -2843         0.00         15*87         0.00         15*87         0.00         15*87         0.00         15*87         0.00         15*87         0.00         14*75         -73*672         0.00         14*75         -73*672         0.00         14*75         -73*672         0.00         14*75         -73*672         0.00         14*75         -73*672         0.00         13*876         -2856         0.00         13*876         -73*672         0.00         13*876         -2865         0.00         13*876         -73*672         0.00         13*8*28         -48*586         510*21         14*696         13*876         -2884         0.00         13*8*28         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -48*586         -78*688         -48*586         -78*688<	~	6.5142	313.24	00.00	313.24	518.688	510.589	14.696	13.907	.2819	00.00	19,61	-137,572	.0730
6.7900 315.80 0.00 315.80 518.686 510.456 14.696 13.894 .2843 0.00 17.18 -92.870  12.620 317.03 0.00 316.88 510.348 14.696 13.884 2853 0.00 15.97 -82.82  7.6520 317.03 0.00 316.88 510.346 14.696 13.884 2870 0.00 13.53 -66.872  7.5313 319.44 0.00 319.44 518.688 510.265 14.696 13.876 2876 0.00 12.31 -60.171  7.5464 319.44 0.00 319.44 518.688 510.213 14.696 13.876 2884 0.00 9.86 -48.565  7.5465 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2884 0.00 9.86 -48.565  7.7521 320.45 0.00 320.32 518.688 510.213 14.696 13.872 2884 0.00 8.22 32.674  8.4567 312.24 0.00 310.24 518.688 510.213 14.696 13.872 2884 0.00 5.22 32.674  8.4567 312.24 0.00 316.30 518.688 510.403 14.696 13.882 2855 0.00 2.86 -22.866  8.4010 316.30 0.00 316.30 518.688 510.403 14.696 13.882 2855 0.00 2.86 -22.866  8.4010 316.30 0.00 316.30 518.688 510.403 14.696 13.882 2855 0.00 2.86 -22.866  8.4010 316.30 0.00 316.30 518.688 510.515 14.696 13.882 2855 0.00 2.86 -22.866  8.4010 316.30 0.00 316.30 518.688 510.515 14.696 13.823 0.00 2.85 20.00 2.86 -22.866  8.4010 316.30 0.00 316.30 518.688 510.515 14.696 13.823 27.83 0.00 -2.825 0.00	6.7900 315.80 0.00 315.80 510.456 14.696 13.894 .2843 0.00 17.10 -92.870 16.02. 5.924 115.30 0.00 316.93 518.688 510.456 13.884 .2852 0.00 14.75 -82.82. 7.0620 317.89 0.00 313.74 518.688 510.265 14.696 13.884 .2870 0.00 12.31 -65.572 173.672 174.696 173.672 173.	m	6.6526	. 314.58	-00-00-	314.53	-514v688	-510,519	14.696	13.900	- +2832	00.0	- 1	-108.961	9230
7.0620 317.89 0.00 317.89 518.688 510.346 14.696 13.884 2852 0.00 14.75 -73.672 7.3313 319.44 0.00 319.44 518.688 510.265 14.696 13.876 0.2876 0.00 13.53 -66.571 7.4651 319.44 0.00 319.44 518.688 510.265 14.696 13.876 0.2876 0.00 12.31 -60.171 7.4651 319.44 0.00 319.44 518.688 510.213 14.696 13.876 0.2876 0.00 12.31 -60.171 7.4651 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2885 0.00 8.67 13.855 7.8654 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2885 0.00 8.67 13.855 7.8654 320.32 0.00 320.32 518.688 510.233 14.696 13.874 2881 0.00 3.97 28.688 8.4010 316.80 0.00 316.24 518.688 510.403 14.696 13.882 0.00 3.97 28.628 8.4010 316.80 518.688 510.403 14.696 13.882 0.00 3.97 28.628 8.4010 316.80 518.688 510.403 14.696 13.882 0.00 3.97 18.516 8.4010 316.80 518.688 510.403 14.696 13.882 0.00 3.97 18.516 8.4010 316.80 518.688 510.403 14.696 13.892 2855 0.00 3.77 18.516 8.4010 316.80 518.688 510.403 14.696 13.892 2855 0.00 3.77 18.516 8.4010 316.80 518.688 510.515 14.696 13.893 2759 0.00 -7.7 18.516 8.4010 30.903 518.688 510.515 14.696 13.923 2759 0.00 -7.7 18.516	7.0620 317.89 0.00 317.89 518.688 510.345 14.696 13.884 2862 0.00 14.75 -73.672 7.1962 318.74 0.00 318.44 518.688 510.265 14.696 13.876 2876 0.00 13.53 -66.572 7.4963 318.74 0.00 319.44 518.688 510.265 14.696 13.876 2884 0.00 12.31 -60.171 7.4651 319.44 0.00 319.44 518.688 510.265 14.696 13.877 2884 0.00 12.31 -60.171 7.4651 319.45 0.00 320.32 518.688 510.213 14.696 13.872 2884 0.00 320.47 -38.565 7.5397 320.47 0.00 320.32 518.688 510.23 14.696 13.877 2884 0.00 7.47 -38.283 7.8967 319.24 0.00 319.24 518.688 510.23 14.696 13.877 2884 0.00 5.12 -29.448 8.5597 319.24 0.00 318.24 518.688 510.23 14.696 13.877 2884 0.00 5.12 -29.448 8.5697 319.24 0.00 318.24 518.688 510.23 14.696 13.882 2885 0.00 5.25.620 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2885 0.00 2.75 -16.516 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2885 0.00 2.75 -16.516 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2885 0.00 2.75 -16.516 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2885 0.00 2.75 -16.516 8.69493 300.64 518.688 510.525 14.696 13.910 2815 0.00 -1.10 -1.10 -1.22	<b>.</b>	6.7900	315.80	0.00	315.80	518.688	510.456	14.696	13.894	.2843	0.00		-92.870	.8730
7.3313 319.44 0.00 314.74 0.00 13.94.74 518.648 510.265 14.696 13.878 0.00 14.75 -73.878 -73.878 14.696 31.944 0.00 12.31 -60.878 17.888 0.00 12.31 319.44 518.648 510.265 14.696 13.878 0.00 12.31 -60.878 0.00 12.31 319.44 518.648 510.265 14.696 13.878 0.2884 0.00 12.31 -60.878 0.00 12.31 319.44 518.688 510.213 14.696 13.872 2884 0.00 9.88 -48.555 7.7531 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2884 0.00 8.67 41.256 7.47 7.2884 0.00 8.67 41.256 7.4896 13.872 2884 0.00 8.67 41.256 13.872 2884 0.00 5.20.32 518.688 510.213 14.696 13.874 2881 0.00 5.12 -29.448 8.2664 318.21 0.00 319.24 510.285 14.696 13.882 2885 0.00 2.95 28.628 18.686 510.403 14.696 13.882 0.00 2.85 -25.628 0.00 13.8.21 518.688 510.403 14.696 13.882 0.00 2.85 -22.196 8.401 316.80 518.888 510.403 14.696 13.892 2855 0.00 2.86 -22.196 8.401 316.80 510.288 510.403 14.696 13.892 2855 0.00 2.86 -22.196 8.401 316.80 510.203 14.696 13.892 2855 0.00 2.86 -22.196 8.401 316.80 510.203 14.696 13.892 2855 0.00 312.72 312.72 518.688 510.403 14.696 13.892 2855 0.00 2.86 -22.196 8.401 316.80 510.203 510.215 14.696 13.993 2759 0.00 -1.79 -11.225 8.901 316.80 510.325 14.696 13.993 2775 0.00 -1.22 510.226 14.696 13.993 2775 0.00 -1.22 510.	7.3313 319.44 0.00 314.74 518.688 510.265 14.696 13.876 0.00 12.31 -66.878 7.7313 319.44 0.00 319.44 518.688 510.265 14.696 13.876 0.00 12.31 -66.878 7.8313 319.44 0.00 319.44 518.688 510.265 14.696 13.876 0.00 12.31 -66.878 7.8513 319.44 0.00 319.44 518.688 510.213 14.696 13.872 2.884 0.00 12.31 -66.878 7.8513 319.44 0.00 320.32 518.688 510.213 14.696 13.872 2.884 0.00 9.86 -48.565 7.47 -2.884 0.00 9.86 -48.565 7.852 319.24 0.00 320.32 518.688 510.213 14.696 13.872 2.884 0.00 9.86 -48.565 7.47 -38.285 7.8947 319.24 0.00 319.24 518.688 510.213 14.696 13.877 2.884 0.00 5.12 -29.448 0.13.872 319.24 0.00 319.24 518.688 510.233 14.696 13.877 2.884 0.00 5.12 -29.448 0.13.872 319.24 0.00 310.30 510.30 14.696 13.877 2.885 0.00 2.86 -22.496 0.00 310.30 310.30 518.889 2.855 0.00 2.86 -22.496 0.00 310.30 518.888 510.403 14.696 13.899 2.855 0.00 2.86 -22.496 0.00 310.30 518.888 510.403 14.696 13.810 0.00 3.895 0.00 310.30 518.888 510.515 14.696 13.810 0.00 3.895 0.00 310.30 518.888 510.515 14.696 13.810 0.00 3.895 0.00 310.30 518.888 510.515 14.696 13.810 0.00 3.895 0.00 310.30 518.888 510.30 13.895 0.00 3.895 0.00		7 0630					100 mm		688 - 27	2853		ı	-82-836	0730
7.3313 319.44	7.3313 319.44 0.00 319.44 518.688 510.265 14,696 13.876 .2876 0.00 12.31 -60.171 7.4651 319.97 0.00 319.44 518.688 510.265 14,696 13.876 .2887 0.00 11.09 51.191 7.5597 320.32 0.00 320.32 518.688 510.213 14.696 13.872 .2884 0.00 9.88 -48.565 7.5724 320.40 320.32 518.688 510.213 14.696 13.872 .2884 0.00 9.88 -48.565 7.8654 320.32 0.00 320.32 518.688 510.23 14.696 13.872 .2884 0.00 5.12 -29.448 8.1324 319.24 0.00 319.24 518.688 510.23 14.696 13.877 .2874 0.00 5.12 -29.448 8.6727 318.21 0.00 316.30 518.688 510.403 14.696 13.889 .2865 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.403 14.696 13.899 .2852 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 .2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.525 14.696 13.910 .2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.525 14.696 13.910 .2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.525 14.696 13.910 .2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.525 14.696 13.910 .2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.525 14.696 13.910 .2815 0.00 2.86 2.86 2.86 2.86 2.86 2.86 2.86 2.86	o ~	7.1963	21 8. 74	•	34.4.75	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	910.545	14.090	100 000	7007	20.0		-73.672	02/01
7 + 4651 319 -97	7.5597 320.32 0.00 319.97 518.688 510.213 14.696 13.872 2881 0.00 11.09 517.194 7.5597 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2885 0.00 8.67 14.286 7.5597 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2885 0.00 8.67 14.286 7.8654 319.32 0.00 319.34 518.688 510.275 14.696 13.874 2885 0.00 5.12 -29.448 8.1324 319.24 0.00 319.24 518.688 510.275 14.696 13.877 2865 0.00 5.12 -29.448 8.4010 316.30 0.00 316.30 518.688 510.275 14.696 13.910 2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2815 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.66.48 510.515 14.696 13.910 2815 0.00 2.82 30.60 2.82 3	. 40	7, 3313	319.44	0.00		11 8 5 0 K	11-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	14.696	17.876	2876		22 22	72, 65	27.50
7.5397 320.32 0.00 320.32 518.688 510.213 14.690 13.872 2885 0.00 9.88 -48.565 7.7321 320.44 0.00 320.32 518.688 510.213 14.696 13.872 2885 0.00 8.67 -41.256 7.8654 320.32 0.00 320.32 518.688 510.213 14.696 13.872 2884 0.00 7.47 -38.283 7.8654 319.24 0.00 319.24 518.688 510.273 14.696 13.872 2885 0.00 5.22 -29.448 8.654 319.24 0.00 316.30 518.24 510.403 14.696 13.889 2.852 0.00 2.86 -22.196 8.6010 316.80 0.00 316.80 510.403 14.696 13.889 2.852 0.00 2.86 -22.196 8.6010 316.80 518.24 510.403 14.696 13.899 2.852 0.00 2.86 -22.196 8.6010 316.80 518.88 510.515 14.696 13.899 2.852 0.00 2.86 -22.196 8.6010 316.80 518.88 510.515 14.696 13.893 2.275 0.00 -77 -16.516 8.6010 309.95 518.688 510.515 14.696 13.923 2.759 0.00 -12.228	7.5397 320.32 0.00 320.32 518.688 510.213 14.690 13.872 .2884 0.00 9.88 -46.565 7.7321 320.41 0.00 320.42 518.688 510.213 14.696 13.872 .2884 0.00 7.47 -38.283 7.8654 320.42 0.00 320.42 518.688 510.213 14.696 13.874 .2884 0.00 7.47 -38.283 7.8947 319.93 0.00 319.24 518.688 510.275 14.696 13.882 0.00 5.12 -29.448 8.4010 316.80 0.00 316.80 510.403 14.696 13.882 0.00 2.86 -22.196 8.4010 316.80 0.00 316.80 510.403 14.696 13.889 0.00 2.86 -22.196 8.4010 316.80 0.00 316.80 510.403 14.696 13.889 0.00 2.85 0.00 2.86 -22.196 8.4010 316.80 0.00 316.80 510.515 14.696 13.910 .2815 0.00 .77 -16.516 8.4040 316.72 0.00 312.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516 8.4040 316.72 0.00 316.80 510.525 14.696 13.910 .2815 0.00 .77 -16.516 8.4040 316.72 0.00 316.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516 8.4040 316.72 0.00 316.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516 8.4040 316.72 0.00 316.72 518.688 510.525 14.696 13.910 .2815 0.00 .77 -16.516 8.4040 316.72 0.00 316.72 518.688 510.525 14.696 13.910 .2815 0.00 .10 .10 .10 .10 .10 .10 .10 .10 .1	ø	7.4651	319.97	00.0	-319-97	-518-688	-510-236	14-696	13.87	2884	90.0	11.00	-56.198	07.50
7.7321 320.44 0.00 320.44 510.618 510.212 14,696 13.872 2884 0.00 5.67 417.876 7.8654 320.32 0.00 320.32 510.688 510.213 14.696 13.872 2884 0.00 7.47 -38.283 7.9947 319.93 0.00 319.24 0.00 319.24 0.00 5.12 29.448 8.4564 319.24 0.00 316.80 510.403 14,696 13.889 2.855 0.00 2.86 -22.196 8.4010 316.80 0.00 316.80 510.403 14,696 13.889 2.855 0.00 2.86 -22.196 8.4010 316.80 518.88 510.403 14,696 13.889 2.855 0.00 2.86 -22.196 8.4010 316.80 518.88 510.403 14,696 13.899 2.855 0.00 2.86 -22.196 8.4010 316.80 518.88 510.515 14,696 13.899 2.815 0.00 177 -16.516 8.604 309.95 518.688 510.515 14,696 13.923 2.785 0.00 -77 -16.516 8.9493 306.64 0.00 306.64 518.688 510.325 14,696 13.933 2.759 0.00 -12.228	7.7221 320.44 0.00 320.44 510.518 14.696 13.872 2884 0.00 5.67 47.256 7.88.283 7.88.		7.5997	320.32	0.0	320.32	518.688	510.219	14.690	13.872	.2884	00.00	9.88	-48,565	0729
7.8654 320.32 0.00 320.32 510.688 510.213 14.696 13.872 .2884 0.00 7.47 -38.283 7.9947 319.933 0.00 310.34 14.696 13.874 .2884 0.00 6.28 13.674 0.00 13.9.93 0.00 3.9.948 14.696 13.877 0.00 3.97 -35.283 14.696 13.882 0.00 3.97 -25.496 0.00 316.80 5.12 -29.448 14.696 13.882 0.00 2.86 -22.196 0.00 316.80 510.403 14.696 13.882 0.00 2.86 -22.196 0.00 316.80 510.403 14.696 13.889 0.00 2.86 -22.196 0.00 316.80 510.403 14.696 13.899 0.00 1.79 1.79 14.696 13.899 0.00 1.79 1.79 14.696 13.899 0.00 1.79 1.79 14.696 13.899 0.00 1.79 1.79 14.215 0.00 0.00 316.80 510.515 14.696 13.923 2.785 0.00 1.70 14.215 0.00 1.70 14.215 0.00 17.815 0.00 17.815 0.00 17.215 0.00 17.215 0.00 17.815 0.00 17.215 0.00 17.815 0	7.8654 320.32 0.00 320.32 510.688 510.213 14.696 13.872 .2884 0.00 7.47 -38.283 7.9947 319.93 0.00 319.34 514.688 510.23 14.696 13.874 .2884 0.00 6.28 13.674 0.00 6.28 13.674 0.00 6.28 13.674 0.00 6.28 13.674 0.00 6.28 13.674 0.00 6.28 13.674 0.00 6.28 13.674 0.00 6.28 12.25.488 0.00 6.28 12.25.488 0.00 6.00 6.00 6.28 12.25 14.696 13.882 0.00 6.00 6.28 12.25 14.696 13.882 0.00 6.00 6.00 6.00 6.00 6.00 6.00 6.0	1	7,7321	320-44	90.0	320.44	-5184688-	-540-242	14.696	13.871	2445		7	43.256	67.29
**************************************	6.3324 319.24 0.00 319.24 510.686 510.233 14.696 13.674 2881 0.00 6.28 32.674 6.318.24 319.24 0.00 319.24 510.275 14.696 13.877 2884 0.00 2.92 25.620 8.2864 318.21 29.448 8.2864 318.21 0.00 319.24 510.330 14.696 13.892 22855 0.00 2.95 25.196 8.4010 316.80 510.60 510.403 14.696 13.893 22855 0.00 2.86 -22.196 8.4010 316.72 0.00 312.72 510.688 510.403 14.696 13.893 2285 0.00 1.79 19.26 19.26 8.6727 312.72 0.00 312.72 510.688 510.515 14.696 13.910 2815 0.00 2.77 -16.516 8.4101 310.855 0.00 312.72 510.78 510.78 14.696 13.910 2815 0.00 1.79 11.215 14.696 13.910 2.2783 0.00 1.79 11.215 14.696 13.910 2.2783 0.00 1.212.228 8.9493 310.664 13.893 27.25 0.00 -1.10 -12.228	12	7.8654	320.32	0.00	320.32	518.688	510.218	14.696	13.872	.2884	00.0	7.47	-38.283	.0729
0.1354 319.24 0.00 319.24 510.505 510.275 14.695 13.877 .2874 0.00 5.12 -29.448  4.2664 318.21 0.00 318.21 514.686 510.330 14.696 13.882 .2865 0.00 2.97 -25.620  8.4010 316.30 0.00 314.99 518.688 510.403 14.696 13.990 .2875 0.00 1.79 -10.516  8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516  8.6727 312.72 0.00 309.95 518.688 510.515 14.696 13.923 .2783 0.00 -1.228  8.9493 306.64 0.00 306.64 518.688 510.325 14.696 13.939 .2759 0.00 -1.20	8.6727 318.21 0.00 319.24 518.688 510.330 14.696 13.882 2865 0.00 3.97 -255.620 8.610 316.80 0.00 316.80 510.803 14.696 13.889 2.285 0.00 2.97 -255.620 8.610 316.80 0.00 316.80 510.803 14.696 13.889 2.285 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2.815 0.00 1.79 -19.167 8.6727 312.72 0.00 312.72 518.688 510.525 14.696 13.910 2.815 0.00 1.79 -16.516 8.6727 312.72 0.00 300.69 510.525 14.696 13.910 2.815 0.00 1.77 -16.516 8.6727 312.72 0.00 300.69 510.525 14.696 13.910 2.815 0.00 1.210 -12.12	i	•	25.00	000	349.96		-510-239 ·	ŧ.	13-874	-2881	00.0	6.24	-33.674	0729
8.4010 316.30 0.00 316.30 518.688 510.403 14.696 13.889 2852 0.00 2.86 -22.196 8.4010 316.30 0.00 316.30 518.688 510.403 14.696 13.891 0.00 1.79 -16.516 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 2.815 0.00 11.216 8.8404 33.00.95 0.00 309.95 518.688 510.525 14.696 13.939 27759 0.00 -1.20 18.228	8.6727 312.72 0.00 315.80 518.688 510.403 14.696 13.889 22852 0.00 2.86 -22.196 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 22815 0.00 1.79 -19.167 8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 22815 0.00 1.79 -16.516 8.6727 312.72 0.00 300.32 518.688 510.35 14.696 13.910 2.815 0.00 1.215 8.9493 305.64 0.00 300.64 518.688 510.325 14.696 13.939 27.55 0.00 1.1.10 -12.228	<b>.</b>	0.1324	313.54	) · · ·	319.24	716.555	510.275	14.636	13. 277	•2874	0.00	5.12	-29.448	. 6729
0.4914 310.00 0.00 310.00 510.000 510.000 14.696 15.889 .2852 0.00 2.86 -22.196 6.96 15.884 .2854 0.00 2.86 -22.196 6.96 15.884 .314.696 15.984 .2855 0.00 1.79 1.79 1.8516 15.886 15.986 15.986 15.986 0.00 1.79 1.8516 15.886 15.986 15.923 12.72 0.00 10.989 518.688 510.515 14.696 15.923 12.789 0.00 1.84.215 18.886 510.925 14.696 15.923 0.2759 0.00 1.20 1.20 1.20 1.20 1.20 1.20 1.20	0.901 310.00 0.00 310.00 510.000 510.000 14.696 13.889 .2852 0.00 2.86 -22.196 0.685 314.52 0.00 2.86 -22.196 0.685 314.52 0.00 312.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516 0.885 0.00 312.72 518.688 510.515 14.696 13.923 .2783 0.00 -20 -14.215 0.885 0.00 310.654 518.688 510.325 14.696 13.923 .2783 0.00 -12.0 -12.228 0.000 310.64 0.00 310.72 518.688 510.325 14.696 13.939 .2759 0.00 -1.10 -12.228	: 4 :		- 61.0.c.		12.615	-9-1-4-0-6-	510.330	14.696	13.482	2865	000	3.97	-25.620	0729
8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516 8.6104 309.95 0.00 309.95 516.648 510.758 14.696 13.939 .2789 0.00 -1.10 -12.228 8.9493 306.64 0.00 306.64 518.688 510.325 14.696 13.939 .2759 0.00 -1.10 -12.228	8.6727 312.72 0.00 312.72 518.688 510.515 14.696 13.910 .2815 0.00 .77 -16.516  8.8104 309.95 0.00 309.95 518.688 510.325 14.696 13.923 .2759 0.00 -1.10 -12.228  8.9493 306.64 0.00 306.64 518.688 510.325 14.696 13.939 .2759 0.00 -1.10 -12.228	12	8.525t	31 6. 00	000	315.80	718-553	510.403	•	13.889	.2852	0.00	2.86	-22.196	02/0.
	8.9493 306.64 0.00 306.64 518.688 510.925 14.696 13.939 .2759 0.00 -1.10 -12.228 9.9900 302.72 0.00 306.64 518.688 510.925 14.696 13.939 .2759 0.00 -1.10 -12.228	9	8.6727	31 2. 72	0.00	312.72	518.588	510.515			.2815	00.0		-16.516	0730
8.9493 306.64 0.00 306.64 518.688 510.325 14.696 13.939 .2759 0.00 -1.10 -12.228 .	8.9493 306.64 0.00 306.64 518.688 510.925 14.696 13.939 .2759 0.00 -1.10 -12.228	19-		309-95	00-0	-369-35	-516.646-	-510.758	-14.696		2783	00.0	-20		0731
	9-0900 302-72 0.00 302-72 510-600 511-121 14-696 17-958 27-27 0.00 -1-01	20	8.9493	306.64	00.00	306.64	518.688	510.325	14.696		.2759	00.0		-12.228	.0732

SPECIFIC MEIGHT SPECIFIC NEIGHT RADIUS OF CURVATURE KAUIUS OF CURVATURE -100.940 -100.940 -121.22-22--138.964 -138.964 -138.964 -63.369 -62.369 -26.056 -26.056 -14.124 -16.194 153.096 153.096 153.096 65.106 65.979 74.719 105.996 207.792 335.290 135.290 135.290 136.655 136.655 136.655 136.655 136.655 136.655 20.54 19.53 114.08 114. 19,23 119,23 116,93 14,47 111,83 111, HIRL SLOPE --- ANGLES---¥ d MACH ACH 13.765 13.765 13.765 13.763 13.763 13.690 13.690 13.690 13.690 13.690 13.690 13.690 13.751 13.751 13.750 13.750 13,583 13,583 13,584 13,564 13,564 13,647 13,647 13,643 13,643 13,643 13,643 13,643 13,643 13,643 13,643 13,643 13,643 13,643 ---PRESSURES------PRESSIJRES---TOTAL STATIG 14.696-14 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 14.696 509.094 508.094 508.553 508.441 508.441 508.240 508.240 508.244 508.240 508.240 508.244 508.244 508.244 508.244 508.244 508.244 508.244 508.244 507.161 506.965 506.359 506.359 506.359 506.170 505.995 505.14 505.614 --TEMPERATURES----TEMPERATJRES--FUTAL STAFFC 5116 5 6 8 8 9 11 8 5 6 8 9 11 8 5 DESCRIPTION FILLO DESCRIPTION 379.73 373.63 386.43 386.43 386.43 386.43 397.45 397.95 399.07 399.07 399.07 399.07 399.07 399.07 399.07 399.07 ALO TANGEN TOTAL --- OTAL AIG - TANGEN --FIELD FLORE 37.9.73 37.3.63 37.3.63 37.3.63 38.0.08 38.0.08 38.0.45 38.0.45 38.0.45 38.0.000 38.0.000 38.0000 38.0 4114 XEAIG M STATION 6. 7252 6. 7252 7. 2163 7. 2163 7. 553 7. 553 7. 553 7. 553 7. 553 7. 553 7. 553 8. 215 8. 215 8. 5216 9. 553 9. 5 REDIUS 6, 2599 6, 8651 7, 2062 7, 2062 7, 5411 7, 5511 7, 551 7, 561 7, 8721 7, 8721 7, 8721 8, 2022 8, 2023 8, 2522 8, 5375 9, 6816 9, 6816 RADIUS STREAY -LINE 4042404 20040454046040 NO 24 MUN S 244

	PRESSURE DELTA I ISENTROPIG PULTIKUPIG RAILO — ON I — EFFICIENCY EFFICIENCY	1.000 1.000	0.000 1.0000	0.000 1.0000	0.000 1.0000	0000		0.000 1.0000	0.000 1.0000	1.000 0.000 1.0009 1.0000 1.000 1.000 1.0000	0.000 1.0860	0000-1000-0		0.000 1.0688	0.000 1.0000	0.000 1.0000		0-0001-0000	- RADIUS OF SP	SLOPE CURVATURE MEIGHT			8.251	17-13 10-122 0792	20.567	25 44.958	1	-17,377	5.24 -12.363 .0789	-8.655	-7.919		-6-29
	RELATIVE PRE TEMPERATURE RA	617.181			<b>-</b> •	200 200	0	1 41	-	675.109 1.		7	693,306 1.	-	07.774		7	728.596	ANGLE	MAIR	3735 19,05	3767 18.92	18.62	18.45		18.24	3954 18.48	1	3981 19.43	2	20.96	21.74	ı
. !	RELATIVE	30.258		-	32,369		33.070		36	37.120	38.890	39,817	60.775	42.795	298*24		072.27	48.626	JRES HACH	STATIC	15.757 .37	15.753 .37		734	15 722 3	•	Ι.		•		15.992 .40		844-8448
1	VE RELATIVE	,	٠ 🕶		1315.88		1325-03			44.464		-	1510.61		1	1586.47	;	1643.52	PRESSJRES	TOTAL		17.372		İ	17.0434		17.541						18,067
i i	E RELATIVE		3 1.1517				1 24.38	-	i	6 1.2973	1	÷		1.4003	T	٦,	104519 104519	•	-TEMPERATURES	STAFIC	-531.834	532.079	532.462	532-617	526.023	533.484	534.695			ŀ	541.872	543.230	2724
,	CO.FF SPEED	0.03		-000	000 1259.8	3 3	000	0000 1339.3	0.0000 - 1559.0		0300 1417.7		0000 1456.		3	8	0000 1556.	000 1598.5		LOTAL	\$-6.630		547.931	-548×289	240000	549.812	551.356	3520750	100.00	55%,736	559.439	502.100	\$62.005
	DEVIATION DE	4	ċ	•	548 0.0	,		-10.756 0.0		•	3	å	<b>.</b>	-11.207 U.D.	- 1	÷.	<b>.</b>		1:	TGTAL	423454	427.13	433	8.52	419.00	3	02.4744	1			461.55		۱
	NO. 1	- 1	2.961	- 1	-73.211 -10.	ì		1		-73.957 -11	Į.					5.571	7.484	5.5.0		1	1,478,23		138	137.9	128 47		1.2.44				165.0		2 123.28
	ES RE	12.205		į.		1		7- 104-6	- 1	7-705 -7	1	5.635 -7		4.571 -7	- 1	3.595 -7	1	; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;		AERIO	15.00. 6	3 +0+0			0 410.00	425°	1 420.27	127	.27	624		4.00	440
- 1	T SLADE-AUSL	-012-567	865	665.59-	-52.653					-63.165	-03-413	03-943	-03.663	-03.361	4	-64.059			AM RADIUS		6269.9	~ •	7.2165		7. 5250		1	*				8.6251	]
	LOCAT	- 1		4	<b>#</b> t	<u>.</u>	٥ ٨	•	σ	<b>;</b>	127	77	*	9	\$	<b>9</b> '	4 6	517	STREAM	7	†	~ 1	1	•	9 2	. =0 (	1	**	12	=	16	1 51	7

POLYTROFIC EFFICIENCY	.9018	. 1935	.6856	. 4786	. 1722	. 3665	. 8593	. 6483	. 4 3 6 5	.8259		.7838	.7698	.7601	.7514	.7406	1297	, 7225	.7180	.7115	.7011	025
ISENTROPIC - EFFICIENCY	<b>3689.</b>	. 8910	.6630	.8757	-1690-	.8632	. 8559	9448.	.8345	.8215	7982	.7781	.7637	.7536	05t/·	.7333	2219-	.7144	.7097	.7029	.6921	T NO T AT 150
DELTA T	<b>†50 •</b>	.055	• 056	. 056		. 058	. 059	.060	.061	.063	-066	.068	.071	. 073	.076	• 079	180	.084	. 085	.087	.039	AT 120
PRESSURE RATIO	1.181	1.182	1.183	1.184	44485	1.186	1.188	1.189	1.101	1.194	1.196	1.200	1.203	1.208	1.212	1.217	1-222	1.226	1.229	1.232	1.232	700
ZELATIVE TEMPEZATURE	6+2+312	0+5.181	650.163	653,360	657.373	651.1cg	665.737	559.595	673.579	677.595	631.754	635.364	630.127	634.241	638.509	712,336	707.231	711.593	716.249	720.992	725.345	332 > 00 054
RELATIVE PRESSURE	30.535	31,181	31.790	32.413	37.051	33.703 .	34 . 353	34.979	35.623	36.247	36.776	37.328	37,933	38.000	39.293	39.944	40.615	41.303	42.1 do	43.015	+3.82+	1 2 0
VELATIVE VELOCITY	1158.27	1177.17	1195.03	1214.83	1233.53	1252.01	1269.42	1245.23	1302,95	1318,35	1331.35	13++.32	1357.89	1371.95	1385.95	1399.26	1412.49	1420.87	1445.41	1458.14	1473.84	i
RELATIVE MACH NO	1.3215	1.0391	1. 15 45	1,0709	1.1372	1.1033	1.1183	1.1330	1.1469	1, 1597	1.1599	1.1798	1.190+	1.2315	1.2126	1.2223	1.2329	1.2441	1,2565	1.2592	1.2817	
3LADE SPEED	1225.1	1244.2	1263.3	1201.7	1300.1	1318.4	1330.2	1354.4	1372.2	1396.3	1+07.7	1425.4	1443.1	1+60.3	1478.5	1+95.3	1>14.1	1532.1	1550.1	1260.3	1580.7	
235. 236.FF	.0335	0362	.0385	29 4 6 €	. 34.25	. 0 + 4.1	+0+0	.0501	. 0535	. 05.82	.0072	. 9755	.0313	. 0805	. 2912	6466.	.1023	.1013	1001.	.1123	.110+	
DEVIATION FRUIDLAGE	- 3.523	- 3.500	-3.502	195.6-	- 3-640	-9.011	-3.613	-9.61+	-3.015	- 3. 513	-4.65+	- 3. 53.	-3.053	-3.677	-3.713	-3.752	19.00-	- 3. G. A	-3.347	-13.033	-10.150	
KLL FLOM AMBLE	-53.731	-55.420	-7.00.065	-73.257			-70.032	-70.320	-73.379	-71.135	-71.290	-71	-71.037	-71.1.4	-71.332	-72.323	-72.241	-72. 23	-72.022	-72, 312	-73.230	
443665	1 30 4 32	3.9.7	9.0.0	7.019	46.54	5.539	4.726	4.155	3.73u	3,317	2.453	2.413	2.0.3	1.531	1.033	1.732	1.773	1.832	1.033	1.743	1.534	
SLADE-ANGLES SECTION LLAN	-00.252	-cû.333	-505.503	. dc • 0a-	00-311	-53.341	-01.009	-61.212	-01.305	-11.513	-01.006	-01.309	-121.344	-02.372	-52.192	-52.308	- 02 0 + 2 7	656.50	-1.2.733	-42.374	-03.020	1
LOCAT -ION	-	• ~	, m		'n			٩n	6	1.0	: :	15	. 21					10	•	·	. 77	
1					ł															24	6	

STATION S FLOW FIFLD DESCRIPTION

i					:								!				i		1		į	
													i		1				-			
SPECIFIC	HEIGHT	.0894	+0891	. 0588		.0884	.0843	.0862	.0861	. 8880	9998	.0877	1176	.0875	· 0874	.0874	223	9872	+0274	.0871	-0874	.0870
PADIUS OF	CJRVATURE	4,302	6+106	9.714	20-082	267 • 222	-28.256	-14.862	-10-921	-9.223	-8-420	-6.085		-8.381	-9-017	-10.082	014174	-14.740	-20-138	-31,667	-68-125	1665.883
Sana	SLOPE	27,37	25, 19	25.95	20.62	18.35	15.03	13.72	11.44	9.20	7-04	4.89	2-89	1.00	77	-2.42	4	-5.29	-6.49	-7.57	-8-54	-9.38
TONG	WHIRL	37,98	37.22	36.58	36+06-	35.63	35.26	35.05	35.10	35.17	35.47	36.34	37.18	37.84	38, 35	38.85	45 65	4,0.32	40.88	41.27	41.80	42.58
AACA.	0	4134	. 4236	.4273	4313	.4345	.4377	. 4 414	+42+	.4491	527	.4567	. 4600	. 4638	*4664	• 4.696	4205	.4717	.4713	. 4692	.4661	.4623
125.5	STATIC	19.712	18.643	18.590	18.552	13,527	18.515	18.515	18,528	18.551	18-583	18.524	18.671	19,722	18.777	18,833	18.890	18,948	19.005	13,060	19-114	19.164
SEGRET .	TOTAL	21.117	21.089	21.679	21-079	21,090	21,116	21.102	21,227	21,301	21-384	21.484	21.589	21.693	21,791	21.835	21.978	22.062	22.122	22,158	22.177	22.182
Table Same	STATIC	561.353	561.356	561.465	501.064	561.942	562,302	552.313	563.955	505.057	56.553	569.138	571.725	574.003	576.005	578.017	-340*+55	582.949	584.995	586.600	588.376	590.571
AG. AD. DA	TJIAL	3 3 1 . 0 12	581.412	531.921	332.466	533.061	533.752	534.746	330.222	5:7.738	- 549.657 -	592.702	3 45.85b	5 18.571	600.933	503.258	- 37F-440 -	508.737	510.827	612.272	01.3.769	515.553
	1.)TAL	77.007	+33.33	438.21	502.00	215.25	510.21	5175	519.32	524.55	- ed. 653	35.52	5+1.25	5+0.17	550.18	253.05	- 60 7 ad-	553.53	500.27	558.40		22.34
	TAVSER	300.53	293.41	290,92	232.74	25 . 33	244.55	295.3+	293.33	302,25	207.31	317,35	327.12	335.00	3+1.35	347.32	-35 72	362, 12	360.61	363. +0	37.0.30	373.52
7	15-21-0	355.12	392.3.	+0 0 0 07	-0 p- 13	+11.51	41 b. nil	+2′.39	+2 > + 3 +	+2 3. 43	131.22	+31.35	+3 1. 22	+31.32	+31.43	431.15	10.42	42 6. 74	₩2 3° 5¢	41.9.71	14423-	+16.43
SAUTH		7.0734	7-1757	7.2733	7.3523	7.4527	7.5413	7.6230	71+7	7.8001	2.8450	7.9730	3.0250	8.1417	8.2.34	3.3153	8 4041	8.4937	4.5847	3.6771	3-771-	4.8575
MAGOTA	-LINE	-	~	m	4	۷.	4	~	€0	σ	1.0	11	7	13	4	15	16	17	18	61	20	21
					j												į			<b>-</b>		

3LADE DATA

EFFICIENCY EFFICIENCY	9103	.9816	8036	. 6863	6706	. 6740	1944	. 1560	2442	4000	4105	1967.	77.65	.7624	2511	.7371	7226	.7128	245	. 6961	6843
EFFICIEN	9986	. 8965	444	4088.	27.73	. 1674	4684	1040°	441	.8243	4084	.7784	7618	7489	7368	.7218	7066	5869	6626	E782	5599
- BK 1	128	. 121	122	.123	124	. 125	127	.130	133	.137	44.7	.147	154	.159	163	. 168	47.4	178		.183	-1887
RATEO	14.437	1.435	1.434	1.434	424.4	1.437	1.460	1044	1.468	1.455	294-4	1.469	1.476	1.483		1.496	100	1.505	1.508	1.509	1.509
TEMPERATURE	648-349	652.443	-655-980-	659.473	45.2.34	656.373	669-797	673.217	-676+643	680 - 188	525.549	687-117	-690-722	694.390	638,125	701.938	205 846	709.258	-7154372-	718.220	722.511
-BRESSUAE	31-142	31.636	32.431	32.630	45.1.5	33.648	- 34+132 -	34.5+9	34.978	35.343	35 493	35.665	35.927	36.265	36.618	36.901	- 27 - 22	37.577	38.038	38.602	39.034
VELOCITY	1031.16	1052.14	1071.79	1090.36	1108.32	1124.83	1139.88	1152.65	- 1104.92	1175.11	1179 85	1184.80	1191.75	1200.30	1209-09	1216.26	-1223,26-	1233,10	1245.56	1257,66	1268.37
07 TOUR	. 4854	. 90 35	• 92 02	. 9360	75.09	. 95 51	- 97.75	. 9875	* 99.70	1.004+	1.0052	1.0082	1.1121	1.0175	1+0233	1.0272	1.0303	1.0374	1. 4465	1. 3551	1.0021
	1257.2	1274.5	1291.3	1307.5	43237	1339.4	1364+9	1370.2	1385.3	1400.4	4	1430.7	1440,0	1461.4	1476.9	1492.6	150805	1524.7	1541.1	1557.3	1575.0
	.0679	.0733	. 07 80	.0821	9.54	.0385	. 0930	.1303	- 1020	.1163	7	.1503	-1635	.1732	1823	.1940	2000	.2140	* 2.1.80	.2244	. 2323
ENC! JENCE	-13.+86	-13.350	-13-195	-13,025	1,14,17	-12.071	-12.496	-12,330	-12-178	-12.043	13000	-11.842	11-781	-11.753	-14-199	-11.803	1	-12.022	-12.200	-12.423	-12.700
	-68.376	-53.376	-54.143	-50.129	****	-58.252	-58-30	-58.340	-58.398	-50.469	999	-50.657	-04-782	-54.932	401.50-	-59.321	45.4	-59.911	-70-304	-70.770	-71.308
- <del>                                     </del>	3.732	3.242	2.45+	136	55+6-	171	7£ G	802	8.1	815	77.7	767	1.0.1	8 32	-+501	:29	17	1.023	1.530	2.052	2.300
SECTION—LEAN	-5590	-54.726	->+·00 G	-55.194	-55.390	-55.591	-23.310	-55.015	-55.240	->>++64-	426464	->5.3.6	-57.300	-57.130	-57.351	-57.518	7.694	-57.390	-56+106-	-25.347	->8.598
₹ †	-	~	m	*	٨	s	~	70	σ	=	+	15	7	<b>‡</b>	\$	16	7	18	#	20	51

STATION 7 FLOW FIELD DESCRIPTION

111	7	THE STATE	•		A TEMBER	TURESON .	B4£SSJRES-	JAES	134	TOWN		RADIUS OF	SPECIFIC
MERIC TANGEN TOTAL	TANGEN	•	TOTAL	- 1	FOTAL	STAILC	TOTAL	STATIC	O <b>Z</b>	HHIRL.	SLOPE	CURVATURE	MEIGHT
243.95	243.95 400.14		675.23		534.356	566.300	23.843	19.031	.5771	36.34	26.61	-3.372	0060.
400.23	5644 62- 400423		67.5 · 45		605.189	567.568	23.829	19.918	.5772	36.31	23.47	3,227-	66.69
545.87 462.01	545.87 462.01		677.93		590.330	568.531	23,869	19,032	.5735	36,37	20.43	-3.139	.0898
54.7.00 4077	1,0 2,2		74.494	- 1	607.700	640.694	23.9+6	19,069-	1985	36.50	17.49	307.2	-
247.74 403.13	403.13		683.01		509.307	570.392	24.043	19, 125	.5816	36.68	14.67	-3,121	40
244-14 - +11-75	244-14 - +11-75		- 96-599		-010.941	572.241	24.162	19.198	.5331	35,91	11-97	-3-177	0000
247.03 417.20	247.03 417.20		0d3.63		512.942	573.938	24,302	19,284	.5843	37.29	9.41	-3.265	.0901
246.48 - +25.82	246.48 - +25.82		692.73		015.766	576.259	54.45	19.382	.5872	37,93	6.98	-3.383	2888
545.35 434.83	545.35 434.83		637.49		514.530	578.534	24.659	19,490	•5900	38.57	4.70	-3.537	£060.
		703.03	202.03	Ŧ	D-2-2-83	一次からなか	24.804.	-194607	5935	39,44	2.54	7,47	4866
2 710.43	535.94 466.42 710.43	2 710.43	•	.,	527.613	586.275	25.100	19,730	.5971	41.03	• 62	-4.012	2068
528.44 485.45 717.64	528.44 485.45 717.64	5 717+d+		.4.	33.354	5 30 . 371	25.337	19,857	6009*	42.60	-1+15	4.376	1061
521.ch 502.22 724.11	221.th 202.22 724.11	2 724-11		۵.	34,293	595.165	25 • 55 4	13,986	0 70 0 •	43.91	-2.73	-4.862	0060.
515.35 515.04 729.02	515.35 515.04 729.02	729.02	-	up.	-2.6±0	598.903	25.772	20.115	.6052	45.02	-4.13	-6.6.00	1960
508.37 228.40 733.25	508.37 228.40 733.25	733.25	٠.	43	46.352	502,545	25.308	20.241	6109	46.11	-5.35	-6.378	.0901
40464	7 ··· 3 ··· 3	1	- 4.38 mily	Ť	551.827	697,654	20,163	29, 366	-6609	47.46	-6445	7.624	996
\$.4512 488.09 359.50 742.48	559.5U		7.42.48		555.980	£11.553	25,343	20.488	.6110	48.90	-7.27	-9.643	. 1898
+7 8 . 37 97 0 . 67	570.076	•	744.13		000.986	615.480	26.491	20.666	.6105	50.00	-7.93	-13.396	-1601
469.53 575.72 742.43	575.72 7-2.43	7.02.35		"	63.8.0	618.493	26.586	20,721	. 0081	50,80	-8.48	-21.521	.0698
+53-05 295-44	+57.02 582.44	Ī	143,634		969.696	621.816	20,006	20 832	.6051	51.74	-8.96	-46.578	- 9691*
,	+45.35 591.04 740.54	7+0.54	,	'1)	70.95%	¿25,315	25.750	23.941	.6025	53.03	-9.37+9	96875.344	.0897

3LADE JATA

POLYTROPIC EFFICIENCY	100.7	. 8926	4984	2//0	. 6651	2297	. 6463	1927	9228	1366	7595	.7464	******	.7185	2828	.6916	6742	5620																				ļ
ISENTROPIC P	8468	.8851	376	. 6665	.6553	84.73	.8349		1609.	75.0	7402	.7257	-7119	•6950	6779	1000		3		SPECIFIC	1	6760.	. 0927	3	.0931	6932	0000	. 8931	8888	1060.	4 4 0 0	18813	.0911	Ф	. 8906		0030	9068.
DELT. T IS	165	. 167	-169	•172	178	182	.197	193	•200		231	.239	-+247	.257	257	72.	286	762		DA STITE OF	CJRVATURE	-1.683	-2.671	e3.277	-4.107	*5.273	10.344	-12,557	181-31-	-18.550	-18-227	-13.923	-12.132	949484	-9.399	375	, ,	315564.756
PRESSURE	1-622	1.621	1-624	1.629	1.566	1-654	1.665	1.678	1.692	100	1.720	1.754	-1.767-	1.780	10203	1.803	3 :	1-670			SLOPE	16.56		=				. 53 . 53	1	-2.86	]	-2.		4	-6	10.12	•	37.
S. AF IVE	9	0.361	2.838	665.+73	7.66	3 + 42	676.151	8.301	1.709	7	7 . 5 4 4	693.785	- 65t-z	0.452	3.362	700.7	11.04.30	0000		New	WHIR.	36.92	,	40.57				42.37	ļ	46.4	ı		53.39	-		69-	000	63.4
~ 4		32,370 650.			ı	'				1		33,771 69			1	710 7	005	. ~	6*7	1	ON		7		•			.7321			•		``			144	•	.773
<b>"</b> "					١								ית	~	•	33	55°	7 4		0.00	STATIC	19.710	19.691	20 12	20.290	20.386	*/*·02	20.629	20-70%	20.792	20-890	24.004	21.279	21 - 44	21.624	21.826	22 25 25 25 25 25 25 25 25 25 25 25 25 2	22.465
RELATIVE VELOCITY	1050	1061.19	1070.	1079.4	9.400	1100-1	1102.3	1104.4	1103.62	1001	1084.19	1074.8	72.	1065.6		1059.9	1064.57	1058.4	720 ISE	: :	TOTAL	3.25	30°00°00°00°00°00°00°00°00°00°00°00°00°0	22	9.71	9.62		7.4.400	3	9.47	9.58	•	30.276	9.65	1.12	31,612	֓֞֞֜֜֞֜֞֜֞֓֓֓֞֜֜֓֓֓֓֞֜֜֜֓֓֓֓֞֜֜֜֜֓֓֓֓֜֜֜֜֜֓֡֡֡֜֜֜֜֓֡֡֡֜֜֝֡֡֡֡֓֜֜֡֡֡֜֜֡֡֡֡֡֓֜֡֡֡֡֡֡֡֡	33,329
RELATIVE	40.75	93 63	. 1137	. 34 02		54.6	. 3343	. 93 42	. 9312	- <del>26 16 •</del> -	670E.	60938	. 6889	. 3811	. 8727	39 es •	. 6713	1275.	AILO = 1.	;	STATIC	575.003		Š	8	ŝ	9	541.245	7	93	ģ			325	39	ů,	<u>.</u>	063.471
SPER	1.806+	1311.0	1323.2	1335.3		1.3.71.2	1303.2	1395.2	1407.4	₩ 1	1432.5	1414	1472.5	1456.5	1501. ··	15.	5.5	1564.3	ALSSURE R	1	O TAL	<u></u>	or ∹	a	• ~	~	m,	77.77	. Ф	•	~	79.457	11.449	10-057	09.331	-	•	- *5***** *1.793
1338 23465	3	. 1117	1	7	¥ .	٠,	11.	0	~	2	N.	7F52*	27	· O	3	~	32	24.22	4		¥	٠٥٠	<b>.</b>	<u>ب</u> ا	3.0	9	· n ·	881.45	,	0	ο.	۰.	n vo	`	~	~ (	<b>†</b> 6	7
Javiation Incluence	4	-15.937	.5.	٠'n :	1	: :	-14.120	-13.602	*	43.4.0	-13,301			13.	•	13.72	1 00	707-11-	PERED.		TOT N	<b>U</b> -1	<b>J</b> . 0							4	33 67	00	50 CE		72 92	6 16		06 97
F.C.34		-54.122	59.354	59.2.6	1 7	13.13.2	50.285			ı		01.00	51.039	62.113		53.171	4	750.40-	MEGANESO LOW FIELD	5	14.10=	297.		503	595	531.		33 587.	, 1	533	657.	6 3	7.4		777	302.	226	975
*		3. d 43			1					1					- 1				4; u;		YERIO	740.	722.	200	0 po	670.	960	540	1 3 7	003.	50€	•	9 6 4.	110	*****	47.		.37.1
3LADE-AN		1.145	617-1	. 223	,	3.23.5	105	6+6+	345	-215	523	, m	. 05	422	977	3.451	3.766	0.075 276	STATION	;	40104	47.3	523		662	. 711	761	812	92,	973	680	103	2/10		391	. 47.3	25	6. 735y
LOCAT -104 3	(	* ~				, ; ,	. 0		0	1	~ ~	77 1	· w		4	• •	•	V - 05			SI AEA	=	~ ~	2	'n	9	~	<b>«</b> > 0	10	=	12	m .	<b>3</b> 4		} `.	81	61	202
i					l					1					i		2	48	!										į									

3L ADE- 0AI A

:

					77	2	1000		C	-	2020101010	
										•		
-25-429 -6-276.	-++-626	-13-197	1334	1328.4	+ 8825	1040-04	32.697	663.357	2.058	252	9047	9138
-25.513 -5.931	860.04-	-13.166	.1479	1335.2	. 37.55	1034.22	32.753	605.563	2.048	.253	2468.	.9047
0/4461	40.040	-4134171 .	.1561	1344.2	• 47 02	1030-17	32.823	-667 - 425	2.038	254		8960
0.6.4-	-+7.525	-19.15.	.1033	1352.4	. 3665	1027.01	32,912	569.246	2.029	. 255	.8760	. 8877
4 2 4	4			45694	1 1 1	1026.95	27.018	621.127	2 022	256	4294	4704
-3.531	-+9.250	-19,115	1751	1369.5	8534	1027.36	33.140	673,369	2.016	. 257	.8591	.8722
-30-8812-7-32-	- 149.47S	+60+61-	· 1845	1378.+	. 8613	1026.72	33,207	475-974	2-011	-259	8406	1627
-31.572 -2.0ou	-50.540	-13.074	.1993	1387.0	. 8557	1022.43	33.138	677.152	2.007	.263	. 6333	.8487
-32 +222	-51-275	44044	-2127	- 1397 -	. 8507	- 1018 - 84	-33.083	-579-311	2.004	267		4355
6 37	-51.333	-19.933	.2315	1406.5	. 1417	1011.12	32,907	681.559	2.003	.273	. 8001	.8185
3		7 1 1 1	2 2 2	14.52.1	1011	- 088	22 280	643 328	2 00 5	215	75.45	2888
104.	-52.933	+66 . P	.3011	1427.9	. 7962	966.03	31.704	656.+47	2.013	. 298	.7397	.7637
-526*	P-53++19	- £26-84-	.3263	1439.2	. 7771	947.16	31-284	-689-12-1	2-025	310	7174	745.6
1,317	-53.36%	-13,957	.3467	1451.2	. 7515	932 • 06	31.009	691.342	2.041	. 321	9669.	.7278
1,603	194.349	-14.945	43424	1403-6	. 7455	916.34	39-752	- 694 +312	2 . 060	334	-6634	2134
2.030	-54.322	-13.933	. 3592	1476.6	. 72 23	893.14	30.343	698,152	2.086	.350	2499.	.6970
2.4	4774	18,928	133	1004	6343	865463	29,909	701.398	2116	364	1949	6813
2.647	-22.327	-13.931	. 42 43	1504.9	1670.	848.48	29.718	704.351	2,151	.383	.6348	. 6712
	-30.283	- #18 4 943 -	-4383-	1519.9	46994	839*82	-29.746	-798v574-	-2+184	395	1273	1999
	-56.96-	-13.966	+644.	1535.4	• 0565	820.58	29.708	712.551	2 • 22 3	.411	•6196	• 5589
3.3.7	-57.131	-16. 399	.4655	1551 J	. 6367	805.42	29*493	716,517	2.268	430	- 1005	
	-28.470 -4.930 -30.341 -3.531 -31.981 -3.732 -31.981 -2.732 -32.830 -6.93 -32.830 -6.93 -33.939 -4.31 -33.939 -4.31 -35.992 1.317 -35.996 2.630 -35.906 2.630 -35.906 2.63		1.9507.02519.15.  1.55319.25019.15.  2.7329.25019.15.  2.0005.25019.13.  1.52051.50319.03.  1.69751.50319.03.  1.69751.50319.03.  1.69751.50319.93.  1.69752.60319.99.  1.69752.60319.99.  2.00054.60319.93.  2.00019.10319.93.  2.00019.10319.93.  2.00019.10319.03319.93.  2.00019.10319.033					-4.9307.725 -19.15. 1751 1352.4 3665 1027.81 32.  -3.531 -9.250 -19.15. 1751 1352.4 3665 1027.81 33.  -2.73299.75 -19.13. 1751 1359.5 8534 1027.35 33.  -2.000 -50.540 -19.10.4 1193 1387.0 8513 10226.72 33.  -2.000 -50.540 -19.13. 23.15 1406.8 957 1022.43 33.  -6.97 -51.503 -19.133 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.133 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.133 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.133 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.133 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.13 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.13 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.13 .23.15 1406.8 9417 1011.12 32.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -51.503 -19.99 .3011 1427.3 .79.1 947.16 31.  -6.97 -6.97 -6.99 .4.99 .4.99 .4.99 .6.79 .8.99.02 .29.  -6.97 -6.97 -6.99 .4.99 .4.99 .6.79 .8.99.02 .29.  -6.97 -6.97 -6.99 .4.99 .4.99 .6.79 .8.99.02 .29.  -6.98 -6.99 -6.99 .4.99 .4.99 .6.79 .8.99.02 .29.  -6.99 -6.900 -6.900 -6.900 .4.99 .5.70 .8.900 .20.2 .29.  -6.900 -6.900 -6.900 -6.900 .4.99 .6.79 .8.900 .20.2 .29.  -6.900 -6.900 -6.900 -6.900 .4.900 .6.700 .9.		-4.930 -17.255 -19.15	-4920 -77.25 -19.15 1751 1352.4 1655 1026.95 27.912 669.246 -3.531 -99.25 -19.15 1751 1352.4 1626.75 27.912 673.359 -2.732 -49.475 -11.69 1369.5 13.5 1026.75 27.912 673.359 -2.732 -49.475 -11.69 136.5 137.0 135.3 1026.72 27.152 -2.001 -50.540 -19.07 13.67 13.67 1026.72 27.152 -2.001 -50.540 -19.07 13.67 10.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0	-4.930 -7.725 -19.15. 1751 1352.4 1027.81 32.912 669.246 2.029

STATION 9 FLOW FIELD ULSCRIPTION

			!												-								
CBECTETC	HEIGHT	.0977	6260	6160.	8070	8260.	2260	+160.	9260	• 1965	0057	.0945	89.12	. 1921	1168	2060.	1688	2000	. 6673	0670	1998	. 1866	
DA DITHE OF	CJRVATURE	-5.825	-9.00.	-17.753	286 288	24.297	11.567	7.642	5.707	4.547	1 222	3.234	2.863	2.616	2.458	2.372	2.2	2.398	2.510	2.996	4.152	20.749	
5.5.00	SLOPE	8.54	7.86	7.15	9	5.60	4.77	3,90	-54-88	2.04	1 05	. 02	44 . 64 .	-2.11	=3-17	-4.21	45.34	-6.26	-7.22	-6.07	- By 74	-6.95	
TONG COL	WHIRL	45.65	12.64 21.	46.70	42.42	47.47	47.76	48.14	-48.82-	49.44	50 38	52.46	54.63	56.52	58.11	59.80	20 29	69.49	66.24	66.14	70.02	73.25	
MACH	ON	.92+3	•9195	.9158	9131	.9112	-9464	7606.	+0 10+	.9118	1210	9131	91.70	.9131	9132	.9127	9295	9646	9629	1696	9758	.9818	,
33611	STATIC	21,598	21,722	21.821	21 897	21,952	- 21. 388	22, 905	22 - 005	21,989	21 957	21.915	21.872	21, 831	21.795	21.769	21 754	21.793	21,466	21.985	-22,159	22.428	
24.450	TOTAL	37.432	37,508	37.525	37.544	37,556	37.571	37,589	37.615	37.642	22.64.7	37,568	77-696-	37.421	37.360	37.297	32.922	38.890	39.61	40.134	40.732	41.506	
1.135 Cas	STATIC	5 32 . 7 13	595.273	597.528	-599.762-	601.710	603-477	605.543	608.490	611.306	615.058	522.083	629-310	635.734	641.419	647.355	455 4 25	663.324	-674 v 3 74	677.304	-684×472	694.110	
IC 3CKS TOW	TOTAL	593.165	695.106	630.169	896.46.6	700.740	7.02.538	704.876	708-454	711.976	216.622	724.735	7.33.085	7 + 0 + 525	247.103	753.867	10000	781.937	793.920	602.653	812vo44	325.539	
	TOTAL	1105.45	1102,48	1100.13	100000	1098.2+	1098-47	1100.01	1103.40	1167.01	4112 ef	1118.85	1125-21	1130.95	- 86-5217	11+0-64	1000	1201.58	1225.03	1239.14	1253.42	1209.81	
* 0. 7 Line	TANSEN	790.80	795-48	800.72	105.21	809.35	813.24	319.30	<b>\$30.53</b>	341.54	707	867.12	917.53	9+3-6	964.54	985.85	31-27-01	1086.20	1125-53	1150.08	1178-33	1215.95	
Managa	MERIO	77 3.03	76-2-92	75 4. 48	1 2 2	74.2.35	738.47	734.02	726.93	720.15	2005	68 1. 79	661.33	023.95	60.000	573.74	1	51 3. 76	12.20	461.28	127.31	355.87	
20.1046		7.5499	7.5855	7.6222	7.6593	7.6935	7.7381	7.7730	7.8203	7.8633	2.9027	7,9543	8-00t3	4.0579	1.112	8.1768	4.2424	8.3144	8-3934	6.4763	- 8-5-70	6.6639	
STREAM	-LINE	#1	~	m	*	'n	•	~	•	6		1	<b>.</b>	13	*	15		17		19		21	

RELATIVE PRESSURE DELTA I ISENTROPIC POLYTROPIC TEMPERATURE— RATEO......OM.I....EFFICIENCY. EFFICICACY SPECIFIC WEIGHT AT NO T AT JEG SURVATURE 9.349 9.349 9.349 9.349 9.104 1.004 SLOPE EFF .= 666.707 668.102 667.134 677.344 672.520 677.460 677.460 677.460 677.460 677.202 691.313 694.388 694.388 695.503 695.503 705.085 PO.X. -724 RELATIVE PRESSURE 322.6680 322.6680 322.6680 322.6680 322.6680 322.6680 322.6680 322.6890 322.6890 322.6890 322.6890 322.6890 322.6890 322.6890 322.6890 32330 32330 32330 TOTAL STATIC 2FF+= RELATIVE VELOCITY I SEN. 9943.78 9941.29 9941.29 9941.29 9976.70 9976.70 9976.70 9976.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 9979.70 37.492 37.508 37.508 37.5525 37.5525 37.554 37.554 37.554 37.663 37.663 37.663 37.663 37.663 37.663 37.663 41.503 41.503 2,593 RELATIVE MACH 10 7330 77851 7733 7733 7733 7733 7733 7733 7735 595.857 596.773 596.773 599.876 6003.657 599.876 6003.657 505.652 513.853 630.563 630.563 630.563 630.563 630.563 630.563 630.563 630.563 630.563 630.563 630.563 630.563 -- TE4PERATURES -- TOTAL STAILC RATIO 1340.9 1347.2 1350.7 1350.7 1350.6 1376.3 1376.3 1396.9 14096.9 1421.5 1431.1 1452.3 1464.0 1476.7 1490.5 1565.4 1521.5 1539.d 1441.5 2 4c SSURE 5593.165 035.180 035.180 035.180 037.020 700.740 700.870 700.870 711.976 71 11862 11862 1286 1286 1286 1386 FIELD DESCRIPTION 1114.7.33 1114.7.33 11159.51 11154.55 11154.55 11219.01 1219.01 1248.43 1038.46 1109.22 1110.23 1112.14 11123.35 1123.35 1123.35 HERIO TANCIN TOTAL PE FORMA FLOW DIVIATION -23.059 -22.059 -22.059 -22.35 -23.35 -23.35 -23.55 -17.100 -10.447 -10.714 -10.701 -15.401 -13.18.0 -13.18.1 -13.295 -17.6w7 -18,939 300.00 303.33 816.01 327.32 333.47 884.15 912.17 941.34 983.20 1087.51 1122.00 1153.53 783.25 793.35 797.58 1220.13 INTEGRATED -39.108 -37.132 -33.463 -+1.015 \$6... 750.63 753.92 765.41 765.41 776.24 776.24 7766.24 7766.34 7766.34 7766.34 7766.34 7766.34 777.77 2.539 2.530 2.530 2.014 3.004 3.539 3.800 1.173 1.735 1.043 1.920 686.+ 3.617 STATION 10 SECTION LEAD . . . . . . . . . . . SIATION 7.07.0 7.051.0 7.051.0 7.051.0 7.750.0 3LAUE RAUIUA 11.916 11.916 11.917 11 -23.359 -24.286 -24.647 377 STREAM -LINE 20001

					!,									-		
STREAM	A CAUIUS	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	۲. در	OCITICS-		FOTAL	EMPERATUR AL	FURES	PRESSURES	RES	A A CH	HATRI	LES	RADIUS OF CURVATURE	SPECIFIC NET HEIGHT	2
•	٠	,	·	ų.						23.		•	9	606 30		d
٠ ٨	7.6657	31 00 TC	787.	Q. 1	226.33	•		10	k	1	1 0 4 2 2	40.01	8.97	36,376		
' PS	7.7112	953	~	•	238-92	, .ψ		4			1.0650			53,623		-
*	7.7.51	36 2 . 09	9 795.	22	12+8.03	5 38 . 908		570.758	37.541	10.396	1.0635	39.55	8.67	91.129	1990.	<b>.</b>
Δ,	. 26+2-1	*		Ţ	42.64	Ī.	ŀ		ľ	1		Į				
٥ ٨	1.8423 7.8843	30 % 45 46 A 14		802.44	261.22	- ''		5 t 1		18.255	1.0705	39.60	8.33	-469.561		n m
- 10	7,9265	351.			203.03	. ~		, t		i	-	40.43	8.09	-147.191		6
σ.	FR96 . 2	100		9	265.2+	• •		+ . +1	,	Ì	1.0685	- 44.02	9.02	-175-032		
10	3.0114	34 5. 02	32 845	96	250.85	•		357			1.0659	41.89	7.96	-333.238		m
#	8.0547	- 4 d d d	١	4	2000	1	ı		ı		1-0616	13.63	7	2383.688		
15	d. 0993	396	30 30 pe	~	.272 32	-		262	37.490	8.526	1.0568	45.45	7.76	247.578	.0828	€0 -
M .	8.1452	36 7		<u>د</u>	273.92		, Q	453	37.421	109	4 .	47.10	7.56	121-563		-
<b>*</b> u	3.1364	999	מ מ	0 2	27.4.31	• •	Б		37.350	4004	•	40.07	020	13.040	01000	D (
2 -	2.2910	74.7.47	,	۰ ۳	1203.77		D 11	7 7 7	37.977	18.938	1.0495	52.48	5.18	35.940		20.0
7.4	8.44.37	75.0					1		36896	- 74	, ,	25.25		32 - 246		2
19	3.3997	7.08.5	112	53	329.15	_		515	39.611	.62	1.0619	57.78	3.69	32.430	•	m
19	3.4605	o5 9•	5	۲ ۲	:	3 82.65	٩	8.7	0.13		7	60-23	1.71	37.253		
20	9.5301	282.	3	3.42	1318.93	312.64	29	0.544	+0.732	20.619	1.0372	63.80	20 C	86.281	.082	<b>.</b>
-IOCAT	3LADE-6	t 1 0/2	ALL FLOW	Je VIATION ENGL <del>de</del> nge	, ,,	335 BL	ULADE 2 SPEED N	ELATIVE AG4 NO	RELATIVE	RELATIVE PRESSURE	. 25. 18.45	AT I VE ERATURE	PRESSURE RATIO	DELTA T I	ISENTROPIC EFFECTENCY	POLYTROPIC EFFICIENCY
	2	4	624.07	7	<b>→</b>		7	1255	-1206v99-	9448	3	-165	24551	98	- 1	. <b>916</b> ⋅
~	47.947 -37	-37.417	+0.013	-7.9	•			. 0+22	20	5	_		2,552	340	.8975	.9100
*	3-0-1		34.73	7	9		7	.0550	6.9		16		2.553	778		9019
•	+0.309 -31		39.554	8 · c -	ું	000	0	. 0535	9.8	ŝ	169	• 90e	2.554	.347	.6795	. 8941
٨	+3.4+7 =28		954.44	-013	9	202	_	. 00 85	5.1	ŝ	<u>ک</u> کے ج	074.	2+556-	351	-8710-	2983
۰ ب	6.00	-25.470	39.001	-5.849	0.0	000		. 07.05	1259.86	37.571	70,7		2.557	405.	.8628	.6795
	C - 2 : - 1 ::		,		3		,	37.04	,			127	2.560	146	A 2.7.2	9560
o			11.020	4		500	•	10.00	ָ פּי	• (	- • •	376	9	373	4224	944
10,	24.504 -12	-12.644	10001	-2.6	0	0.00		98.50		37.6643		. 223	2,561	382	. 8030	8269
::			43.632	,	4	240		.0615	9.6		, -	•735	2+556 -	262	7697	2972
12	•	622.4.	45.452	6	0			. 3569	2.3	•	, -	.385	2.551	. 413	.7374	.7690
3	1	1	17.497	1	-	600000		-1543	-4273-92 -	•		125	2.54.5	424	7109	7456
<b>1</b>		2.7+3	48.573	3.569		000		• 0467	1274.31	37 • 36		.103	2.542	077.	.6489	.7261
<b>4</b>			7	*	9	649	- ·	. 0405	1273.91	•		-967	2.538	2007		7872
9 .	- •		56.479		90		- ·	. C. 4.7.	1293.77	•		100.	7.704	0 4	. 0 4 0 0	6726
	• ''		7 78.	1 1	<b>)</b>	•	• •	1000	450-1707	30.03	• •	200	2.695	574	.6120	. 6606
	- 1	27.02	225		,			1-0522	13637446		7	553	2.23		1000	7.4
50	43.158 +1		63.796	÷	•		0.0	. 0372	8	40.732	~	312.544	2.772	. 567	.5912	.6436

,	:: 7	. •				9	6	95 160 cc.	٠,	3	- GR 4		O SULCEO	STELLET SO	
-LINE	440108	- 01te 14	TAMEN	4	1	314	STATE	TOTAL STAFE		2	MATRI	3401	T WAR	RE HETCHT	
-	71 ;	16.2.51	20.4			9.30.16	545.+23	Ġ		1596	32.81	5.21	3.688	4 0922	
• ~	753	3+ 4+ 35	00110		0	95.106	592.177	٥		.9361	32.48	4.87	-3.427		_
m	. 743	45 5. 70	544.5	8 1032	.0.	597.029	548.973	36.509		9806	32.09	49.4	-3-215	-	
3	. 532	30 6. 77	1000		0 1	38.908	500000	٠.		÷ 100	31.70	170	13.00		
Λ,	7	****		•	• ^		0 FC = C = C = C = C = C = C = C = C = C	ی ہ	1	A 20 A	31.17	3.66	-2.88		
۸ ۵	717	15.000	512		` ^	04.30	526.035	Ġ		. 808a	31.08	3 48	-2-84		 
- 10	991	13 4 60	301.		٠ ٨	0.8.424	630.508	ö		.7896	31.01	3.37	-2.81		
, თ	. 032	32 1 - 51	492		۸.	11.976	5 36 - 7 49	36.375		.7727	30.94	3,34	-2-88		
. 0	0	510.63	70	9 9-4-33	^	16.623	543.568	35.354	24.872	.7576	30.88	3.37	-2.806	•	
	• ; ; •	ამ ს∙ ≷5	-474		~	24.739	553.929	36.276	l	7420	9				
	. 100	79 1. 20	473		~ '	33.085	563.435	35.236		.7291	30.92	3.47	-2.91	1026	
	• 50 •	703.93			~ '	46.525	572.015	36.192		7100	- 41. U4	14. m	200	 	
		C*	• · ·			2010	26.4.5.20	701.00		101/	21.17	30.05	7.5	7 1016	ا ا
	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֓֡֓֓֓֡֓֡	746.13	• · · · · · · · · · · · · · · · · · · ·		• •	23.007	596.630	36.772		7 164	31.64	3.34	-4.019		
	345	41 42	613	1	٠٦	41-947	205-423	32-541	9	7327	32-07	2.99	•		
9	431	335.21	535.5		17 7	13.920	713.533	33.162	243	.7568	32.67	2.36	-7.826	Ī	۸.
	70	35 3. 36	561.1	-	œ	.02.653	717.525		5.933	- 5922-	33.33	- 4444	-22-73	İ	
	. 523	378.00	591.3	5 1059	'n	12.044	721.210	39.031	25.544	.8039	33.96	90.	18.477	•	
	AC TO A JE	Safa						:							
LOCAT	3LAUE-ANG	, to	FLUM D	EVEATION	2383	9LADE	RELATIVE	RELATIVE	ERELATIVE	RE A	TVE	RESSURE	DELTA T	ISENTROPIC	POLYTROPIC
NOT-		. '	-	ST JCNCE	20 0				ı.		ų Š		,		0
+		1		-						L			;	0.30	32.00
~	615	უ:	2.+77	. 862	0 0		1986.	1119.43			ם ר ס כי	181.0	944		. 8755
<b>7</b> .	7	- :	36 - 145	100	9740	• •	# C C C C	1041.82	36.510			2.484	347	8648.	.8676
* 4	500	- 1	777	660	נ	•	366.	1839.72				2.454	354	84.09	16597
N 1		2 :5	1.173	937	0574		60309	1014.76				2.481	.354	.8316	. 8514
ر ام د	9	2 4	770	4	06.02	: <b>.</b> ;	80.88	- 992.62	1	-		2-479	359	4281	6412
60	30.031 -10.1	~	31.610	626.	.0631		. 7.895	97 + • 01			+5+	2.477	.366	.8039	•8269
	2*5	<b>+</b>	544.0	986	9	Ċ	.7727	957.80		ļ	376	2-475	373	7885	1133
	304	ò	0.370	1.015	.0570		• 7575	844.03				2.474	.332	.7693	. 7963
	336	7	0.355	1.029	.0075		• 7.+25	932.29			-	2.468	- 262 -	7368	7878
	385	20	0.921	1.033	0		. 7291	922•28				7°404	514.	2007	***
	ġ'	1	87		1			4000		ļ		2 4.62	177	.6622	7013
	\ !	15/	1,194	1.00	0000		1017.	00.006	30.107		201	2.462	154	5430	5.842
	20.5	201	1.641	1.039	0633		7164	928.11			301	2.562	. 478	.6216	.6659
	3.6	1 7 2	2.070	1.034	G		.7371	961.56		٠	337	2.555	508	-6087	5482
	31.536 10.	7 35	32.009	1.033	.0713	0.0	. 7568	992.17			950	•	.531	.5857	.6356
	200	7 36-	3.326	- 650	10763		7263	- 1	3.5	3	15.4	2.626	1	-6752	1
	312 2	5 3 9	3.962	1.050	.0845		. 8039	1059.37	39.031	915	***	•	.567	•5629	.6167
			•		•		ı		•						

C 1 2 1 1 1	4 SADIUS	A	7	IES		TEMPERAT	ATJRES	PRESSURES		HACH	ANGLE	LES	RADIUS	OF SPECIFIC	,
*					4			4	3	*				l.	
-	7.7230	839-72	2 266.	13	\$80.43	393-165	629.487	ď.	-	7147	27	~	-5-196		
، ہ	7.7573	928.0:			809.1+	695.106	633.124	35.515	25.548	.7032	17.55	-2.34	-5.691		<b>N.</b> -
·) .	****	9 0 0 0	1	!	4>8.45	620-16	- 656	4440		474			647		
∌ u	7. 8553	50 6. 50			848.11	200.4000	258.507	35.487	25. 396	4229	17.54	-2.51	-7.050	5U .1U09	
وا	7.9028	790.66			829.07	702.538	646.173	35,384	341	0499	17.52	-2.52	-9.1		
٠	7-9410	782.38	-	-	820-79 .	7 04+876-	- 666.649 -	٠	Ì	-6552-	17.46	-2.46		14 1093	
.o.	7.9816	777.31			614.57	708.424	654.034	35.224		•6485	17.40	-2.34	-12.469		<b>~</b>
•	A-0549	770.67		Ì	17.75	716-623	662.213	35.106	26.704	5.381	17.40	40.	-17.916	16. 1080	
: ‡		75.0	1		8000	72.02.25	62456	35.016		1229			21.0		
12	5.1532	768.03	3 241.64		605.15	733.085	580.031	34.937		.6288	17.46	-1.40	-26.745		٠,
4	4-1492	77 0- 92		1	808-22-	740.525	ł	34.95	İ	-6280	17.47	1.09	32.3	-	
7 L	8.2460	.73.65	243.77		811.14	14 747-103	•	<b>.</b>		.6275	17.49	62	-37.920	501.	<b>.</b>
4 4 4 4	8. 76.17	000		1	41444	756.804	704-007	75. 674	26.926	5414	17.61	100	-45.807		
: ‡	283	2000		1		786.487	7	4					50 652		
<b>6</b>	8. 4364	847.03			891.64	793.920		Š		.6730	18.03	. 41	-60.560		<b>~</b>
4	-	-		1	7	8054653	7	36.875		6819	18037	99	925.0		
20	8.5316	375.00			9536	812.644	743.015	37,212	27.063	•6916	18.77	. 63	-633.076	. و	
	BLADE DA	4 :													
1								- 1							
LOCAT	3LADE-ANGLES	·	F.0	JEVIATION INCENEE	i	1055 BLADE -00EFF SPEED	E RELATIVE	E RELATIVE VELOCITY.	E RELATIVE		RELATIVE FEMPERATURE	PRESSURE RATTO	DELTA T	ISENTROPIC POLYTROPIC EFFICIENCY FFFICIENCY	POLYTROPIC FFFICIENCY
	16.23/9		4864	***		4079	24 22	686.89	45	1263	494	1414	336		46655
~			17.548	1.365		-	•	869.14			901	2.417	.340	\$88¢	.8570
<b>.</b>	1		17-534	1+395	į	•	1	858 - 55	35-505		129	2-426	770	.6290	- 98486
<b>.</b>	15.137 -7		17.544	1.407		-		848-11		698.308	80.	2.415	. 347	. 8198	. 6405
			11.000		!	•	•	0000					100	3000	
		ļ	17	1.507		9 4	0.000	920 20		34	226	2 402	35.0	2882	1122
. 60			17.397	1.5		237 0	•	814.57			24	2.397	.366	.7711	. 7970
		1	17.370-	-145		•		66.68	35	711	7.6	2.392	373	7550	.7827
		-	~	1.607		.1313 0.	•	807.42		716.5	523	2.369	.382	.7358	.7656
	•	_	17 - 4440	1.633	1	•	•	- 885*84	Ì	724.735	135	-54842	262	7043	
	15.911 -		17.465	1.654		0	•	805.15		733.	385	2.377	.413	.6747	.7111
	1	- A 4	17.489	1.676	١.	-	0 . 62.75	811.14	34. 983	747.103	103	2.380	044	6342	6749
, IG	1	i	17.528-		•	• • !	,	814-19	2	753.867	791	2.383	257	919	- 2659
وه پ			17.614	1,662			•	838.41	35.474	766	501	2.414	.478	.5941	.6398
۲,	1	-	17-27-	-1.6	1.	1	•	868-11	36+928	781-337		20454	208	-5714	1029
97	15.382		18.030	1.648	•	1521 0.	•	891.64	36.547	793.920	320	2.487	.531	.5556	.6870
١		7.020	18.775	1.670		6	0 .6316	924.86		812.3	544	2,532	.557	.5316	. 5865
: :							} ;		: 1						

DM FIELD DESCAIPTION	
FLON	
STATION 14	

7.6724 744.75 84.2+ 745.03 543.105 647.630 344.75 741.42 72.59 72.59 72.51 741.42 72.59 72.59 72.51 742.60 72.59 72.51 742.60 72.59 72.51 742.60 72.50	24445	.5961 6. .5950 6.			
7.7043 741.42 75.99 745.51 995.10 549.524 7.7493 74.62 7.949 74.42 77.59 74.50 74.50 549.524 7.742.31 77.59 74.50 7.742 74.50	513 27. 472 27. 427 27. 370. 27.	920	•		.1126
7.7843 741.41 77.59 745.45 347 029 651.409 34.77.843 742.40 77.59 745.45 347 029 651.409 34.77.843 742.40 745.45 347 029 651.409 34.77.941.4 756.41 72.45 74.501 724.53 8551.409 34.77.941.4 756.41 72.45 74.501 724.63 8551.28 34.87.79.40 724.63 724.	472 27. 427 27. 370. 27. 252 27.		*		1122
7.67/ 7.62.09 7.52.01 7.03.01 7.02.03 6.55.281 34.01 7.02.03 7.03.01 7.02.03 7.03.01 7.02.03 7.03.01 7.02.03 7.03.01 7.02.03 7.03.01 7.02.03 7.03.01 7.02.03 7.03.03 7	370. 27. 25.2 27.	3250 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	? 1		97774
7.8639 739.29 743.01 736.38 655.281 34.87 7.95.3 743.01 736.38 655.281 34.87 7.95.2 74.01 736.38 730.426 659.387 7.95.3 72.03	252 27.	03.	90 - 3 00		4111
7.911.0 736.01 73.22 740.05 704.276 659.987 7491.0 7.911.0 73.3.9 72.23 73.49 72.23 714.975 659.987 7491.0 7.911.0 72.23 73.49 72.25 714.975 659.987 749.995 7.19.905 9.001.0 71.91.9 71.0 71.0 71.0 71.0 71.0 71.0 71.0 71.0		9n t 5.	.3		-1105
7.99.6 73.3.9 72.29 73.44 708.424 603.859 34.6 7.99.6 73.3.9 72.2.0 72.2.3 72.2 72.2	200	5860 5	'n		+1100
7.9936 732.03 71.94 735.39 710.023 567.555 33.08 20.41 731.94 74.023 710.023 50.041 731.94 74.023 3.0041 731.94 735.39 710.023 50.041 731.94 74.023 7.0041 73.005 6.1023 6.1027 7.0041 73.005 6.1027 7.0041 73.005 6.1027 6.103 7.0041 73.005 6.1027 7.005 6.1027 7.005 6.102	019 27.	5823 5.	-2		.1092
9.04.1 731.4 71.04 735.39 710.023 572.330 33.4	913 27	5 797 5.	Ņ		. 1085
3.1307 733.99 70.01 736.93 724.735 640.405 33.64 4.1307 7.13.9 7.40.01 756.93 733.045 536.547 33.64 4.2372 74.7.51 7.13.9 7.40.01 7.40.95 33.6547 33.64 6.2372 74.7.51 7.13.9 7.40.91	837 27.	5776 5.	2		.1077
3.13d7       733.59       70.01       735.99       733.00       533.64.54       33.00	742 200	5746 Se	1	i	
8.1876 740.75 71.12 744.13 740.525 595.239 33.86 8.2872 74.751 74.103 701.007 33.86 8.2872 754.21 74.103 701.007 33.86 8.2872 77.853 77	662 26.	5720 5.	-		.1051
8.2875 747.51 71.74 750.34 747.103 701.007 33.78 8.2875 754.21 72.40 757.03 703.867 706.961 33.88 8.2875 754.21 72.40 757.03 703.867 706.961 33.88 8.2875 754.21 724.31 703.867 706.961 33.88 8.2875 754.33 724.31 729.031 34.88 724.32 33.425 34.835 3	72.0 26.	749 5.	4		.1040
8.2875 754.21 72.40 779.31 793.867 706.961 33.82 3.32 37.9 776.30 779.31 793.867 720.031 34.82 3.33.92 738.276 34.30 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 34.30 738.276 738.276 34.590 35.190 312.644 753.593 35.13 35.130 35.10 35	736 26.	5778 5.	·		.1032
3.379 776.33 74.91 779.91 700.801 717.146 34.82 34.82 301.42 301.42 302.43 30.94 30.82 30.93 734.937 729.031 34.83 30.94 30.26.53 73.592 73.592 35.83 35.83 35.80 30.94 30.26.53 73.592 73.592 73.593 35.80 36.90 30.60.40 32.653 74.52 35.80 31.30 31.26.64 755.333 35.80 35.80 31.26.64 755.333 35.80 36.80 31.26.64 755.333 35.80 36.80 31.26.64 755.333 35.80 36.80 31.26.64 755.333 35.80 36.80 31.26.64 755.333 35.80 36	37.0 26.	580o 5.	;		.1023
3.4347 322.35 31.30 820.35 733.920 738.279 34.434 34.245 35.444 35.35 35.44 34.2653 74.53 35.44 35.39 35.44 35.39 312.644 73.593 35.44 35.990 312.644 75.35 35.44 35.990 312.644 75.593 35.45 35.990 35.40 35.40 312.644 75.593 35.45 35.493 764.515 35.493 764.515 35.493 764.515 35.493 764.515 35.493 764.515 36.493 764.515 35.493 764.515 36.493 764.515 3	216 26.	593+ 5.	i		• 1009
3.4367 322.35 31.30 820.35 733.920 738.275 74.5 3.4345 3.24.70 24.73 3.30.94 312.644 753.35 35.1 3.54.40 30 3.544 750.39 312.644 753.35 35.1 3.544. DAIL DAIL DAIL SELVINITION LOSS BLADE RELATIVE RELATI	524 27	6080 5.	•	i	
3.4345 334.72 34.72 35.34 312.653 7.45.33 35.4 3.5.34 34.72 34.72 35.44 31.2.644 753.593 35.4 3.5.54 31.2.644 753.593 35.4 3.5.54 312.644 753.593 35.4 3.5.54 312.644 753.593 35.4 3.5.6 31.2 31.2 31.2 31.2 31.2 31.2 31.2 31.2	973 27.	b199 5.	•	•	.0982
3.5940 d61.13 95.48 060.00 325.539 704.515 35.48 35.48 060.00 325.539 704.515 35.48 060.00 325.539 704.515 35.48 060.00 325.539 704.515 35.48 060.00 325.539 704.515 35.48 060.00 325.539 704.515 704.	195 27	265 5.	•		.0973
3.5940 d61.13 95.48 0600 325.539 704.515 35.65 39 704.515 35.65 39 704.515 35.65 39 704.515 35.65 39 704.515 35.65 39 704.515 35.65 39 704.515 35.65 39 704.515 35.65 39 704.515 35.65 30 3.50 3.50 3.50 3.50 3.50 3.50 3.50	407 27	327	•		. 0963
34 AUG_DATA	623 27.	390 6•		-510.607	.0951
3.965 -1.034 b.142 -2.241 .1503 BLADL RELATIVE R					
3.965 -1.024	ELATIVE RELA ELOCITY PRES	ITIVE RELATIVE SURL TEAPERATUR	PRESSUR E RATIO	E DELTA T IS	SENTROPIC POLYTROPIC FICIENCY EFFICIEND
3.634935 6.074 2.241 1602 0.0 5955 745. 3.702639 5.941 2.390 1611 0.0 5943 745. 3.575639 5.941 2.390 1623 0.0 5943 745. 3.394721 5.404 2.310 1653 0.0 5943 745. 3.315655 5.738 2.404 2.51 1651 0.0 5901 743. 3.010450 5.026 7.520 1961 0.0 5965 737. 2.909409 5.540 2.579 1931 0.0 5775 735. 2.909409 5.544 2.635 1977 0.0 5775 735. 2.741240 5.417 2.642 2.002 0.0 5776 735. 2.744125 5.482 2.724 1994 0.0 5779 744. 2.744125 5.482 2.732 1994 0.0 5779 7579 2.759409 5.482 2.732 1994 0.0 5779 7579 2.759125 5.482 2.732 1994 0.0 5779 7579 2.759125 5.482 2.732 1995 0.0 5805 7579 2.759125 5.482 2.732 1995 0.0 5805 7579		j	2.361	336	2180 8383
3.702922971259 -1611 0.0 -5950 745. 3.575639 5.94 2.370 -1551 0.0 -5943 745. 3.335655 5.94 2.403 -1733 0.0 -5943 745. 3.135655 5.025 2.403 -1733 0.0 -5965 745. 3.100+60 5.025 2.403 -1733 0.0 -5965 740. 3.000+60 5.025 2.520 -1961 0.0 -5929 737. 2.969400 5.540 2.579 -1931 0.0 -5775 735. 2.741240 5.404 2.723 -1977 0.0 -5776 735. 2.742105 5.48 2.723 -1993 0.0 -5779 750. 2.744115 5.48 2.730 -1993 0.0 -5779 750. 2.745115 5.48 2.730 -1993 0.0 -5779 750. 2.747115 5.48 2.730 -1993 0.0 -5934 750. 2.749211 2.591 -1975 0.0 -5934 779.	65.51		34	340	
3.575639 5.841 2.390 1523 0.0 5943 746. 3.335655 5.738 2.443 1713 0.0 5934 745. 3.335655 5.738 2.443 1713 0.0 5931 743. 3.135655 5.025 2.403 1731 0.0 5901 743. 3.00460 5.025 2.520 1931 0.0 5797 735. 2.909409 5.544 2.579 1931 0.0 5797 735. 2.935334 5.17 2.682 2.002 0.0 5775 735. 2.744139 5.42 2.723 1999 0.0 5779 749. 2.744139 5.482 2.732 1999 0.0 5779 750. 2.759105 5.482 2.732 1999 0.0 5779 757.	45.85		34	446.	
3.335 -655 5.738 2.443 .1713 0.0 5934 745. 3.335 -655 5.738 2.443 .1713 0.0 5901 743. 3.135 -655 5.728 2.443 .1713 0.0 5901 743. 3.135 -655 5.025 2.443 .1713 0.0 5901 743. 3.135 -535 5.025 2.520 .1931 0.0 5797 735. 2.959 -409 5.54 2.579 .1931 0.0 5797 735. 2.959 -409 5.54 2.573 .1977 0.0 5775 735. 2.74 -139 5.48 2.72 .1994 0.0 5779 749. 2.74 -139 5.48 2.730 .1993 0.0 5778 757. 2.75 -105 5.48 2.730 .1975 0.0 5905 757. 2.75 -105 5.48 2.730 .1975 0.0 5905 757.	46.01		2.343	.347	.7881 .8116
3.335655 5.738 2.443 .1713 0.0 .5901 743. 3.115514 5.025 2.520 .1861 0.0 .5865 740. 3.001504 5.520 .1951 0.0 .5797 735. 2.969409 5.544 2.635 .1977 0.0 .5775 735. 2.969409 5.544 2.635 .1977 0.0 .5775 735. 2.741280 5.494 2.713 .1977 0.0 .5775 735. 2.744139 5.482 2.722 .1964 .0.0 .5749 7547. 2.744139 5.482 2.732 .1964 .0.0 .5779 7547. 2.744185 5.482 2.732 .1964 .0.0 .5779 7547. 2.744187 5.482 2.732 .1964 .0.0 .5779 7547. 2.759105 5.482 2.732 .1964 .0.0 .5779 7547.	45.92		2	.351	1
3.115 -515 5.025 7.520 .1743 0.0 .5865 740. 3.115 -515 5.025 7.520 .1961 0.0 .5828 737. 3.00000 5.540 2.579 .1931 0.0 .5775 735. 2.935324 5.117 2.632 .2002 0.0 .5775 735. 2.935324 5.117 2.632 .2002 0.0 .5776 735. 2.741240 5.417 2.753 .2013 0.0 .5720 744. 2.744139 5.48. 2.732 .1964 0.0 .5789 750. 2.769105 5.48. 2.713 .1952 0.0 .5805 757. 2.82027 5.21 2.691 .1975 0.0 .5934 779.	+3.01		33	.354	
3.135519 5.025 2.520 .1961 0.0 5828 737. 3.000+60 5.540 2.579 .1931 0.0 5797 735. 2.935340 5.54 2.635 .1977 0.0 5775 735. 2.935340 5.17 2.682 .2002 0.0 5776 735. 2.744234 5.492 2.723 .1999 0.0 5779 750. 2.744139 5.482 2.730 .1999 0.0 5779 750. 2.745165 5.482 2.730 .1975 0.0 5805 757. 2.759211 2.691 .1975 0.0 5805 779 779.	40.05	7.04	2	359	
3.000+60 5.540 2.579 .1931 0.0 .5797 735. 2.959324 5.547 2.635 .1977 0.0 .5775 735. 2.935324 5.417 2.632 .2002 0.0 .5775 735. 2.744139 5.446 2.713 0.0 .5779 744. 2.744139 5.446 2.713 .1999 0.0 .5779 750. 2.744139 5.446 2.730 .1999 0.0 .5779 750. 2.744139 5.446 2.730 .1975 0.0 .5805 757. 2.744125 5.446 2.730 .1975 0.0 .5805 757.	37.4	19 708.424	2.315	. 366	.7366 .7653
2.909409540 2.632 .1977 0.0 .3775 735. 2.835334 5.117 2.682 .2002 0.0 .5746 735. 2.744134242 2.732 .1994 0.0 .5779 749. 2.744139 5.482 2.732 .1994 0.0 .5778 750. 2.759105 5.482 2.733 .1995 0.0 .5805 757. 2.82027 5.481 2.733 .1975 0.0 .5805 757. 2.83027 5.481 2.733 .1975 0.0 .5805 757.	35.52	711.	2+308	. 373	
2.835354 5.17 2.682 .2002 0.0 .5746 735. 2.741280 5.494 2.723 .1964 0.0 .5720 736. 2.744139 5.482 2.732 .1964 0.0 .5779 750. 2.759105 5.482 2.730 .1973 0.0 .5778 750. 2.759215 5.482 2.730 .1975 0.0 .5805 757. 2.82027 5.591 2.691 .1975 0.0 .5934 779.	35,38	7.15	2.302	332	
2.741240 5.494 2.723 .2019 0.0 .5720 736. 2.744139 5.48 2.730 .1999 0.0 .5779 7579 2.749105 5.48 2.739 .1999 0.0 .5779 757. 2.759105 5.48 2.719 .1852 0.0 .5805 757. 2.82027 5.48 2.719 .1875 0.0 .5834 779.	35.89	72.	2.296	162.	
2.744 -13442 2.732 -1964 0-4 -7743 - 7444 2.774 139 142 2.774 1.993 0.0 .5779 750. 2.744 125 5.484 2.719 .1852 0.0 .5805 757. 2.820 2.92 0.0 .5903 779. 2.820 2.82	36.98	7 33	2.291	. 413	
2.744139 >-482 2.738 1993 0.0 .5778 750. 2.759155 5.48. 2.719 1852 0.0 .>805 757. 2.82027 5.48. 2.719 1975 0.0 .5934 7799.	10		2.24		l
2.769165 5.48, 2.719 .1852 0.0 .5805 757. 2.52027 5.511 2.691 .1975 0.0 .5934 779. 2.8032.6 5.1 2.60 216, 0.1 .5080 805.	<b>7</b>	7:7	2.300	9 I	
2.820274 3.511 2.691 .1975 0.0 .5934 779.	68	23	Z-302	+454	· 
	91	765	2 • 32 8	8/4.	
*CDO DODG	*	187	2 - 356	***	i
2.989656 5.050 2.001 .2293 0.0 .0199 320.	36	7.93	2.580	124	
- 1970年					300
*160 /260 f*n 6*62* 22/*2 516*6 5/6* 962*5	7. V	r (	F 2 4 4 7	000	TOOM CRASS
3.508 -1.025 : 0.320 2.644 .7524 0.0 .5344 000.	0	6620	474.7	*	-

HATOL STORE CHRANTINE METCHE		00	100 TO 10	00 -1.63 11.542	2	-1.54 12.627	00 -1.46 13.471	00 -1.37 14.654	16.246	00 - 97 22 341	81 27.845	00	<b>5</b> q	0025 131.248		0.00 .04 -140.525 .0960	36 -44-629	00 52 33,905	HE PRESSURE DELTA T ISENTROPIC POLYTROPIC	2 216 116	2.280 340 7956	2-275	2.270 .347 .7556	2.265	2.24.1	2.232 .366 .7009	2.216 782 5680	2,210 302 6360 6	2-204 .413 .6898	2 24 2 42	2 2 2 2 4 4 0	2.240 .478 .5378		,,	
MACH		5602	2007				9849		5.36.7	6339	5318	5373	5425			5748		461	RELATIVE TEMBERATURE		645.106	697-029	698.308	700-740	70 8 26	708.424	715.57	724.735	733.385	740-525	743-367	736.901	781-337	136.66	113 244
S		27. 096			-		1		26.787		26.738	İ	•	•		6.650	6.710	6.728 - +	RELATIVE	33.582	33,512	33.439	33,364	33.266	32.976	32.802	32. 58	32.472	32.394	^ -	32.703	2.923	27 25	460.00	27 631
PRL SSUR!		31.512	30	364	2 2 2 2				32.558	1					1	33-465	3.574	33.645 2	RELATIVE VELOCITY	703.65	703.82	703.87	703.77	699.22	694.74	690.27	685.16	686.66	687.86	707.64	717.12	m	753.32	ייסי	
URES		654.485	:		ļ		65.324	92	678.070		330	74	20	722.725		3.225	62.042	3.5-20	RELATIVE MAG4 NO		. 5602	46 65 4	יין מינו מינו מינו מינו	.557.5	54.85	.5433	. 5367	. 5339	. 53 19	5473	5+75	. 55 70	. 5961	87.5	
OTAL		595.106			-	02.538	1	424.0	!	1	733.085			801		2.53	2.644	5.539	BLADE SPEED	)   	•		-	9 0	-	0.0	• •		•	֓֟֟֝֟֓֓֓֟֟֓֓֓֓֓֟֓֓֓֟֟֓֓֓֟֟֓֓֓֟֓֓֓֟֓֓֓֟֓	•	0 (	<b>.</b>		•
	ų 1	03.32	7		1	25 2	7.	, , , ,	-	Ī	697.05 7	• •		734.85 7	l	9.23	8.75 81		N LOSS									1		1	24.80	.2654	3105		100
	۸ -	0.00 70	7	_					!		~ ~		,	0.00 73			73	62 6	JEVIATION ENGIDENGE	7.239	7,393	7.556	7, 723	4.057		385			•	3.0%	7-06-	3,058	4.087		0 4 40
MENT TANGEN		95	-				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		) 		7. 45.			734.85		33	.75	.35	RLL FLOW	0.00	0.000	0.000	000	000	0000	000.0	0.000	000-0-	0.000	0000	0000	0000	0.000	0000	000
	2.0	730 703							200		10 C	5.5		<b>~</b> -		622	788	ე 799	- ANGLES	1	. u 20	• 013	0.00	310.	-015	010	.037	40.0	. 503 805	002		038	018	920	
242103	7. 24.	7.673	7.715	1.25	7	7700	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	7 - 966	3.0235	8.022	5.127	3.230	3.282	9,334	7 M 3 * 8	9.492	·v	۰	3LAUE-A	7,249	-7.393	-7.556	22.4.7.	-8.057	-8-223-	-8.335	-3.580	-8-805	-3.311 -3.31	3.0.6	29045-	-3.058	-3.067	-	
N V V V	71	~	**	#	<b>.</b>	۶ م	• 7	o or	10	4	7 1	) J	45	4 4	9 1	10	50	17	LOCAT	- 1					1	 									

STREAM	KADIUS	?	LOCITIE	SS	TEMPEA	RATURES							
		-	# 10 P 1 P 1 P 1 P 1 P 1 P 1 P 1 P 1 P 1	1	1014	TAL STATE	TOTAL	51411C	E O	ANGLES-	ES	RADIUS OF	SPECIFIC
⊶ ヘ	7.640	726.23	0 0	726.23	•	806-649	5.058	26 763					ı.
, M	7 7 7 7 7	30.08			9	552.122	33.	26. 76.2			0000	0.00	1204
و. د	7.7531	20.0	¢		œ.	628*459	33.43	26. 75.2	5777	•	03	1166.185	.1100
5	7.239		0.0			656.507	33.36	26.751	5715	0		619-046	1096
9	7.8419	71 0. 03	0.00		7	159195			5899	9		755 638 755 635	.1093
~ <	7.4858	703.34	2000		- ^	561.218			.5622	00.0	- 11	307.827	
<b>10</b> (	7.9310	٠	0.00		7.0		1	ļ	5567	0000	215	279.358	
יי כ	7.9775	091.49	0.00		. ~	622-808			.5488	0.00	13	263.087	
<b>.</b>	3.024	•	0.00		7.1	677.743		!		99.9	P 13	255.460	
• ^	A 125.4	70 6 7	000	1	724.735	- 16 6 • <del>5 8 9</del>	32-472	26.770	.5391	0.00	13	256.414	
1 M	1031.0	00 / 00	_	687.93		694.372						254.544	2407
, ,	d. 2233	705.41	3 6	c97.12		700.790		26.735	-5310 -5366	•	12	281.050	. 1033
ĸ	8.2830	714-85	, ,	745.91		706.377			.5411	00.0		207-208	1023
۰	3.331	732.29	, ,	732,24		712.122			1646		9	147.073 185.073	.1815
	- 8-3859	-Z50-86		250.6		7.25.0.35			•5550	0.00	- 07	494.028	
<b>.</b>	9.4348	757.44	_	767.44		745.34	ļ	ļ	5640	90 0	98	200 929	1000
<b>.</b>	8.4921	۲.	0.00	777.23	. ~	752 . 22	440.054	26.729	.5728	00.0	+0 •-	686.293	8964
	7	787.01	0	787.61	2,6	762-188	33.402		5773	00-0	03		1980
	2	7	9	799.36	5.5	773.620		20 120	1196.	0.00	01	3058.098	0460.
;	STATEON 13	4C14	£1213.028	METTATASEO			}		-	→ → · · · ·	90	0.00	9260
7. 4	20110			; !		•							
-LINE	3	1 V F.	100		TEMPERA	EMPERATURES	PRESSURES	SJRES	MAGM	2 . 0 . 0			
		<u>.</u>	2	יסואר	TOTAL	STATIC	-T0TAL	STATEC	2	HATRI SLO	u	KAUIUS OF	SPECIFIC
	004	72 7-11	00.0	727 74	,	1			•				METERIAL
		725.45	0.00	725.46	305.406	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	33-583	26-727	1.444	98.8	90.0	0.000	
	7176	723.02	00.0	-723-07	522.120	C+F: 754	33.512	26.727	.5785	0.00	- 00	0.00	000,
	7530	720.54	00.0	720.54	806-9FC	656 200		25.727	5756	÷		900	1005
	7393	71.7-86		7.1.7 . uè	7.00.740	.658.4.05	300°C	26. 727	.5727	0.00	00	00000	1092
	9418	711.27	00.0	711.27	702.53A	661.070	27 430	1274	2696	٠	9	000-0	1888
	950	70.52	000	26,402	204.828	3	32.970	727.02	.5633	0.00	00	00000	.1064
	9303	•	0.00	697,93	738.424	508.512	12.802	25. 25	744	9	100	0000	1878
		74.240	0.00	-692047	711:0976	672-697	32.661	26.720	7646.	0.00	01	0.00.0	.1072
	1110		00.0	689,90	716.623	677.646	32.568	26. 724	200		3	0.000	1065
	1010	0 1	1000	084.76	124.735	685-308	32-472	26. 728	0000	000	01	0.00	.1058
	1763	, n	•	5000	733.085	694.303	32.394	26.728	5222			800-0	1046
	. 2231	706.23	-	207,02	740-525	200-734	32.498	26. 728	5369	9 6	100		. 1032
	-2804	715.13	000	715.13	7.7.103	706.333	32,603	26,728	.5414	0.00	5	٠	1823
	.3330	732.47	0.00	/32.47	755 951	712-083	32,209	26, 728		000	10.		.1815
	.3054	750-73	00.0	750.79	784 027	723.012	32,923	26.728	.5551	00.00	01	0.00	9000
		767.51	0.00	767.51	797.920	7/5 036	33.138	26.728	-5641	0.00	00	• (	1007
	6920	22.30	9		802.663	753.552	33.354	26.728	.5729	0.00	- 00	0.000	.1961
	1010.	\ 0	c c				Þ				•		
			) ·	19.70	t t	762.187		26. 724					25 65

	LEAN-ANGLES INLET OUTLET	17.205	16.462 2.590	15.461	14.188 3.054	22.000	11.481	1		7.706	734	6.168	5.635	Ŗ.	486	4.571 4.939 4.541 4.944	7.595	2.997	2.389	1.836			INC TALET OUT	-70 044 42A	-37.417	149.45	-31.685 .018	-35 1.20	22.128	-19.205	-16.041			-4.779 .083	2.743	\$ \$23 m.00	11.862888		26.776018	
	SECTION-ANGLES INLET OUTLET	-11-816	-12,710	-13-622	-14.539	4444	-16.328	1000	-17.956	7 2 0	10.082	-20.587	-21-176	-21.755	-22.318	-22.861	-24. ASO	24.286	-24.647	-54.964		ECTION-ANGLES	OUTLET	_7 22B	-7.393	-24.556	-7.723	4 4 6 5	-0.037	-6.385	-6-539	-8.680	500.0	-6.911	940.6-	4	-9.058	٠	-9.087	
	SECTION	*62.567	-62.598	-65-599-	-62-663	62.726	-62.760	-62-813	-62.916		-63.167	-63.413		-63.663	m i	-63.861	10.00	,	-64.346	‡		SECTIO		V 0 0 4 7	47.947	47-056	46.369		45.450	44.847	۰	s.	077.477	624.44	45.003	45.402	45.741	46.085	46.711	
	DEL TA	5887	.5908	5916	.5919	6866	.5917	5936	0865.	444	60105	.6494	-16591	.6692	6288	.7050	7554	7667	4422	-1887		DELTA	H/Uss2		0.0000	•	0.0000		0.000	0.	0000-0	0	00000	000000	00000	•	000000	•	0.0000	
	REL V	7567	.7381	7223	.7077	1685	.6843	6723	. 6565	67.67	- 0243	. 5592	- 5303-	. 5073	193	. 4503	20.00	2627	. 337+	297		AEL V	RATIC	20.73	.5745	1895	. 5635	Ų,	+666.	.6463	5453	. 5415	2046	. 5405	.5553	6296	. 5683	5713	57.92	
	DELTA BON Q	1084	.4688	出	.4437	14302	.4165	+024	.3882	25.55	2,57	.3316	- 3185	.3060	2964	2.03.0	2550	οd	. 0	253		OEL TA	300		.4417		6644.	2064	0644	.4431	2624	.4300	オオのオト	0664.	4594	.4270	.4072	43814	.3587	
-	3-0 D	.3695	*390*	2507.	.4261	4	.4541	.4083	.4867	9205	07740	.6017	•6345	.6616	6889.	.7293	4 9	. 84.40	96	9		3-0 0	FACTOR -	i i	.5647	- 65260	.5856	.5937	6136	.6237	+6327	.6+00	£679°	.6575	6544	.6510	.6510	.6518	.6461	
!	2-3 D FACT OR	3615		402	+024•	*	. 4500	. 4549	0 7 9 7 0	5015	5000	6015	. 6348	. 6525	• 6903	. 7312		8170	856	6		(* (	FACTOR		. 5548	-57.61	. 5857	1266	. 53 35	. 6238	. 6328	. 64 01	• 6+95	. 6579	6369	. 6515	. 6516	. 6523	. 6466	4,004
•	LOSS	. 17 03	. 1824	. 1933	. 2029		. 2133	• 5298	. 2483	• 2053 2000	. 2690	3704	0 + 0 + 0	. 4341	. 4578	. 4875	*:	. 5500	5556	585		5501	C 08FF		. 2143	. 21.57	. 2182	. 2210	52593	2490	. 22-80	. 2637	. 2006	. 2587	2543	. 2480	. 2554	. 2913	. 3105	- 16991
	OEVIA TION	23.521	23.1.5	22.018	22.356	23.444	20.300	20.280	19.288	18.448	10.174	17.149	10.846	15.714	15.790	15.401		13.170		16.551		. v.	*CI +-	•	7.393	4.500	7.723	-7 - 3 9 L	8.057	8.385	656.8	ម.១៦០	d. 805	8.911	9.1.6		9.0.6		~ 1	Ni I
•	INCIO	10.150	10.303	10.492	10.548	10000	10.082	10.7.6	10.756	10-772	10.75	19.865	10-913	10.332	11.041	11.207	469411	11:511	11.841	12,076		INCTO	30#2*	4	-7.933	-2-350	-0.815	-0.317	10.040	-4.421	-3.621	-2.509	609	476.	3.569	4.760	b.73d	9-16+	11.073	150116
	19761	1.1331	1.1517	1.1703	1.1939	7.07.	1.2256	1.2+33	1.2019	1.2790	1.697.5	1.3322	1.3.95	1.3667	1.3633	1.409	10+11+0-	1.404	1.4043	1.4491	, 0,	16	074		1.3422	4.0904	1.0630	1.0069	1.0705	1.9701	1-0635	1.4653	1.9615	1.0203	1.145.7	1+0+0	1.3495	1.000.1	1,3019	7967
	SU ILE I	7. 24 99	7.5055	7.0222	7.0598	7007	1.7301	7.1786	7. 32 33	7. 35.53	7. 3C .	8 40 43	0. 3579	8.115+	4.1768	8-2428	44 65 44	4265.0	8. 35.70	8. 66 99	A Company of the first of	1 1 1 1 1 1	KAJIUS	,	7.02 90	7-7190	7.7598	7. 60 16	7.3445	7, 9340	7. 44 00	8. 32 05	4- 97 76	6.1279	A- 23.06	4.2826	8.3343	0.3871	0. 4397	-3.26
	INLE T RADIUS	7.	9	6	9	20	31	3	ž.	۵,	υ,	. T	3	20	31	9.4252	7	5 4	2 3	9.0000	21113	12	343105		7.9627	7.7112	7.7557	7.7992	7.5420	7.3265	1.9089	3.0114	3.0547	8.0993	4.1924	3.2408	9.2910	9.3437	8.3997	
	LOCAT	-	۰ م	m	3	1	9	~	20	σ,	2:		13	<b>*</b>	51	91	· · ·	2 0		512		1400	701	•	2	<b>m</b>	*	. ی	۰ م	20	œ	10	11	12	1 2	12	16	17	18	1 4

2.247 ISENTROPIC EFFY = .500+ POLYTROPIC EFFY = .6421 DEL T/T = .4306 i STATION

1 2 3 4 5 5 7 8 9 10 11 12 13 14 15 16 17

MID BLOCKAGE 0.0 0.0 0.0 1.0 1.0 1.5 2.0 2.0 1.9 0.0 7.0 9.4 11.8 15.0 16.6 17.9

INT BLOCKAGE 0.0 0.0 0.0 1.0 1.5 2.0 2.0 1.9 0.0 7.0 9.4 11.8 15.0 16.6 17.8 17.9 ł ŧ ; 1 SUMMARY POINT NO. 1 THE CALCULATION IS CONVERGED PASS 20 1 FLOK = 20.76 SPEED = 20352.2 PRESSURE RATID = MAKE AND BOUNDARY LAYCH BLOCKAGES (PERCENT) : EST POINT TIT.: = 239330915830 ı ; į ì

### APPENDIX B

### COMPUTER INPUT DATA FOR DATA REDUCTION

Presented in this appendix is the computer input data used in conjunction with the programs of References 4 and 5 (as modified) to perform Phase I and II reduction of the experimental test data. Sections 1 through 4 of this appendix are listings of decks and subdecks which were relatively standard. The cards which were subject to change from test point to test point are indicated by an "\*" in each section, and the changes to these cards are presented in Section 5 of this appendix as "exceptions" to the "common" or "standard" decks of Sections 1-4. Section 5 also presents a key for interpreting the information presented for each test point.

### I. COMMON PHASE I DATA

\$10. \$10. \$10. \$10. \$10. \$10. \$10. \$10.		~	-													
100   100	ı Cr															
500, 502, 510, 510, 510, 510, 510, 510, 510, 510	•	60	$\sim$	0	an a		+	0	.,•	92	*	46		ď		499
516. 513. 524. 522. 524. 525. 556. 556. 556. 556. 556. 556. 556	ın	<u>s</u> .	co	S	0		'n	9	ın	9	เก	70		12		-
552. 554. 556. 554. 566. 554. 566. 567. 568. 568. 568. 568. 568. 568. 568. 568	'n	15.	-	າ	N		'n	N	in	t N	w	25		23		530
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	ıV	32.	m	•	M		'n	Ø	ıv	<del>,</del>	ın	ţ,		\$		ż
. 10185 . 10199 . 10205 . 1030	'n	. 04	'n	0	S		in	#	ß	36	יני	5,0		9		
1217 .1115 .1216 .1420 .1532 .1652 .13180 .13181 .2383 .1380 .13918 .2383 .2453 .2453 .2453 .2453 .2453 .2453 .2453 .2453 .2463 .2567 .2567 .2569 .13182 .228 .228 .228 .228 .228 .228 .228 .	•	185	2	0	0		$\overline{}$	Ö		ສ	•	96	•	104		. 1126
. 22432244226127492749316233623363416332645249376254695256526579254635560	-:	217	7	4	#		-	m		65	•	28	•	191	_	9
** 5363	٠,	£12	2	æ	\$		^1	#		9	٣.	16	•	333		362
12.687	~	589	7	'n	<b>*</b>		+	.#		5	6	3	•	517		15
12.66 7 23-5155 2.25 5.131 10.12.66 7 23-5155 3.3701 .013917 1. 1. 1. 10.12.66 7 23-5155 3.509 3.3701 .013917 1. 1. 1. 10.470	•	555	69	80	2		~	0		7	•	93	•	948		
12.667   23.5155   10.011917   1.   1.   1.   10.011917   1.   1.   1.   1.   1.   1.   1.	•	2.0		N	2		•	ന								
10	~	687	3.51	S												
10 1		217	66.2	ı G	37	-	0.10	-								
10   10   10   10   10   10   10   10				,	;	,		•								
950. 950. 950. 950. 950. 950. 950. 950.	,	70.		C	T				10	10	រេ	5		M		540
9550. 9550. 9550. 3609, 24+5.1 170+.9 1206.1 958. 368. 468. 468. 4550. 1.01  9.994. 5546. 5510. 4.01  1. 1.01  1. 1.01  1. 1.01  1. 1.01  1. 1.01  1. 1.01  1. 1.02  2. 1.04  2. 0.01  2. 0.01  2. 0.02  2. 0.02  2. 0.02  2. 0.02  2. 0.02  2. 0.03  2. 0.02  2. 0.03	. "	. 05		-	١.			,	•	•	`	,		•		
3 494, 556, 6 994, 546, 556, 6 10, 12, 14, 14, 101 11, 14, 15, 15, 15, 15, 15, 15, 15, 15, 15, 15	4	50.	ø	ď	9		3		7	;	N	٠,٥	ď	58		533.7
3 494. 5+6. 561.  • 993  • 10. 1.01  10. 1.02  10. 1.03	7	4.6	S	•												
99. 5-6. 5-61.  9 13.																
9993 1. 1.001  1. 1.2  1. 2. 4. 4.50  1. 4.20  1. 4.30  1	*	Ť	+	ø	9											
0       1	•	66			. 30											
10	Ð	-														
14.696  1		•						•		;		÷		;		1.8
14.696  14.696  16. 1.2	٠	93	9	~	8		•	4		9		90	•	990		d)
16 1 1.2 1.2 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.4 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	t.	69.														
16 1 3.5	<b>1</b> 0	•	•				,									
16 1 1			-		-					• ^		• 0		· ·		
2.5 565.8 579.3 579.5 492.5 507.5 522.5 539.3 50.5 565.8 539.3 50.5 565.8 565.8 579.3 593.8 503.5 523.3 5539.3 50.5 565.8 579.3 579.3 520.0 510.0 510.0 510.0 520.0 520.0 540.0 550.0 50.0 50.0 50.0 50.0 50.0	4	>	•	4	•			3	•	?		_		*		^
2.5 565.8 579.3 533.8 503.5 523.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 539.3 529.0 510. 510. 510. 520. 510. 520. 510. 520. 510. 520. 510. 520. 510. 520. 510. 520. 520. 520. 520. 520. 520. 520. 52	, ,	3	•			7.7		.1		_	•		ζ,		37.	
0.	3	• •	•	0		. ~				· ~			6		656.0	
0. 500. 510. 520. 520. 500. 500. 550. 500. 500. 50	6	, v		2		3		) (S		۱ (	•		6		6	
6 0.25637954c-00 -0.80812823=-04 0.23122066E-06 -0.3 6 0.43483235c-00 -0.855483c=-15 -0.5522926236-06 -0.3 6 0.43483235c-00 0.109404402-03 -0.5522926236-06 0.1 6 0.43483235c-00 0.227244832-15 -0.5522926236-06 0.1 7 1 1 2 4 1 2 4 1 1 1 1 1 1 1 1 1 1 1 1 1				3		? ?		10		1			0		9	
0.25c37954c-00 -0.80812825-10 0.27497128c-12 -0.3554393c-10 0.43483235c-00 0.10940442-03 -0.522926236-06 -0.3 -0.73236516e-12 0.22724483e-15 -0.522926236-06 0.1 1 24 1 24 1 143 145 147 1 143 145 147 1 243 245 247 2 24 1 243 245 247 1 3 3 3 3 5 3 7 3 3 3 3 1 3 1 3 1 3 1 3 1 3 1 3 1 3	•	•	•	•		;		,		•						
5.27497128c-12 -0.3554393c2-10 6.43483235c-03 6.4348323c-03 6.434832c-03 6.4348325c-03 6.4348		.250	9546-	9	•	0812	2.3	0	0	.2312	066	0	•	0 3	16091	95-09
5 0.434832362-00 0.109404402-03 -0.522926235-06 0.10 4 -0.73236162-12 0.227244832-15 1 24 1 143 145 147 1 243 245 247 2 243 245 247 2 243 245 247 3 24 1 343 345 347 4 1 343 445 447 1 443 445 447 1 443 445 447		.274	1282-	**		5549	305	+	ı							:
0.43483255=-00 0.109804462=-03 -0.522926236=-06 0.10 -0.732365162=-12 0.227244832=-15 1 24 1 103 105 107 109 111 113 115 117 119 121 123 125 127 129 131 133 1.41 143 145 147 2 2 4 2 2 4 2 2 4 2 2 5 5 6 5 6 7 3 2 6 7 3 2 7 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		i	;					•								
-0.742303105-12		4 348	235=-	ο .	•	0980	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9		• 5254	623	P		4	1821	21=-08
1 24 01 103 105 107 109 111 113 115 117 119 121 123 125 127 129 131 133 1. 41 143 145 147 02 24 03 205 207 209 211 213 215 217 219 221 223 225 227 229 231 233 2 41 243 245 247 01 303 305 307 309 311 313 315 317 319 321 323 325 327 329 331 333 3 41 343 345 347 01 403 405 407 409 411 413 415 417 419 421 423 425 427 429 431 433 4 11 40	•	5 26 1 •	2101-	-	•	*>>>	1000	н								
01 103 105 107 109 111 113 115 117 119 121 123 125 127 129 131 133 1.   41 143 145 147   2 4		J														
41 143 145 147  42 24  62 24  61 243 265 207 209 211 213 215 217 219 221 223 225 227 229 231 233 2  41 243 245 247  61 303 305 307 309 311 313 315 317 319 321 323 325 327 329 331 333 3  41 343 345 347  61 403 405 407 +09 +11 413 415 417 419 421 423 425 427 429 431 433 4  61 443 445 447	01 1	3 10	1 70	9 11	11	15	17	19	21 1	3 12	~	59	31	33	35 13	7 139
01 203 205 207 209 211 213 215 217 219 221 223 225 227 229 231 233 241 243 245 247 247 249 211 213 215 217 219 221 223 225 227 229 231 233 2 24 243 245 247 249 311 313 315 317 319 321 323 325 327 329 331 333 3 3 10 3 3 3 3 3 3 3 45 3 47 20 411 413 415 417 419 421 423 425 427 429 431 433 441 443 445 447 20 411 413 415 417 419 421 423 425 427 429 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 433 41 443 445 447 20 431 431 431 431 431 431 431 431 431 431	41,	# 12 12 12 12 12 12 12 12 12 12 12 12 12 1	47													
41 243 245 247 3  24 101 333 345 347 41 343 445 447 101 403 445 447 101 403 445 447 101 403 445 447 101 403 445 447	^ خ د	~	0	2	2	ď	÷	0		200	•	00		~	34 23	2 2 3 2
3 3 3 3 5 5 3 5 3 3 9 3 1 1 3 1 3 1 5 3 1 7 3 1 9 3 2 1 3 2 3 3 2 5 3 2 7 3 2 9 3 3 1 3 3 3 3 3 4 1 3 4 3 3 4 5 3 4 7 4 1 4 1 3 4 1 5 4 1 7 4 1 9 4 2 1 4 2 3 4 2 5 4 2 7 4 2 9 4 3 1 4 1 3 4 1 5 4 1 7 4 1 9 4 2 1 4 2 3 4 2 5 4 2 7 4 2 9 4 3 1 4 3 3 4 1 4 4 3 4 4 5 4 5 4 5 7 4 2 9 4 3 1 4 3 3 4 1 4 4 3 4 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5	117°	3 A 3 A 3 A 3	, r	7 J	1	3		64	2 1 2	2	v	, ,	10	?	J	S -
41 343 345 347 41 343 345 347 42 44 61 403 405 407 409 411 413 415 417 419 421 423 425 427 429 431 433 4 41 443 445 447	? ?	: :		200	ř	'n		9	*	7.	C	0	*	2		7 7 2 2
4 24 01 +03 +05 +07 +09 +11 413 415 417 419 421 423 425 427 429 431 433 4 41 443 +45 447 1 1 4J	413	3 2 2	° ~	10 50	31	2	``.	£.	۲ ا ۲ ا	25	v	2	7	?	2	2
01 +03 +05 +07 +09 +11 +13 +15 +17 +19 +21 +23 +25 +27 +29 +31 +33 + 41 +43 +45 +47 1 +u	<b>.</b>	ا و		,		1	(					-	i	,	•	•
ž	01 41 41 42	7 T	t 2t	1 <del>+</del> 10	3	15	17	13	2 <b>1</b> 4	ر در در	N	5	31	33	S S S	65 <del>+</del> 75
Ť																
		>														

			m 0	ın
7.8 9.8 2.0 4.0	8 2 2 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		\$ N	# ************************************
77 97 19 39	0084 0267 6452 0631 0809		453	
76 96 14 38	00000		30	0
75 57 17 17	525 592 78 78 500 500 750 840		35	<b>₩</b>
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0000 00042 00042 0000 0000		333	
73 93 35	10. 700. 300.		437	\$ 2 °
72 92 14 34	00 10 10 10 10 10 10 10 10 10 10 10 10 1		427	<del>el</del>
333		N 4 0 N	+1.7 2.7	•
70 90 12 32	25 25 25 25 25 25 25 25 25 25 25 25 25 2	6 8 8 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	32	1.0
69 11 31	00 01 00 13 00 36 00 55 00 74		337	
8 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7 00 00 H	313 313	+ 1 3 1 1 9	• 73
52 87 9 29	0000 31752 31752 37752 37752 47753 47753	ω ω α α α α α α α α α α α α α α α α α α	421	129
60 80 80 80 80	0000	मूर्य हुट स्ट स्ट्रास	411 29 231	127
65 85 72	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	M M M M M M M M M M M M M M M M M M M	3.4	0.5 125 211
0 0 to 0 0 0 0 0	• 000 0015 0013 0052 0063	2 10 E S E S E S E S E S E S E S E S E S E	331 39 227	123 209
8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2 20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 M	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	121 121 139
£ \$ 55	00 1238 3132 3132 5132 676 676 677 77	2 1 2 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2 2 3 3 3 5 1 5 3 3 5 3 5 5 5 5 5 5 5 5 5 5	0 1119 137
9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	415 415 28 28 28 34 26 517 28	1117 1135 1135 1147 247 347
9 0 0 0	5 7 2 7 2 7 2 7 2 7 2 7 2 7 2 7 2 7 2 7	5 371. .466. 7.867. 2 207. 2 207. 4 10. 3 323. 110. 120.	2	0.0 2.0 1115 1133 307 307 145 245 345
58 79 11 21	000000000000000000000000000000000000000	9 <del>1</del>	22 22 23 24 24 25 24 25 25 25 25 25 25 25 25 25 25 25 25 25	

143 445 447
223 221
189 111
10 2
101 201
39 58
1
14•1100 15•
• U5

33. • 35

# 2. COMMON PHASE II FIXED (LOG I) DATA, ACROSS-BLADE

13 • 0134613 • 2392 41 • 0132460 • 2236 64 • 0132460 • 2126 15 • 012723 • 2077 16 • 012723 • 2077 17 • 012723 • 1970 18 • 0122145 • 1970 78 • 0121359 • 1935
3 .013+613 392 8 .0132+60 2286 9 .0131327 2195 9 .0127239 2126 10 22 345 2027 10 22 153 1970 11 22 145 1935 9 .0121359 1935
3 .0154613 .2392 1 .0132460 .2392 6 .0131527 .2136 6 .0127233 .2136 7 .012733 .2136 8 .012733 .2136 1 .012733 .1997 1 .012557 .1970 1 .012145 .1935 2 .012145 .1935
3 .0134613 .2392 1 .0132460 .22392 6 .012323 .2366 7 .012733 .2126 8 .012733 .2126 1 .012733 .2125 1 .012733 .1977 1 .0127557 .1970 2 .012145 .1935
3 .013*613 .4392 1 .0132*60 .2286 8 .0131927 .2286 9 .012733 .2195 9 .012733 .2071 2 .012733 .2077 1 .0122557 .1970 9 .012145 .1935
3 .013+613 .<392 1 .0132+60 .2286 6 .01310-27 .2196 6 .0127239 .2071 7 .012734 .2072 7 .012735 .1970 1 .0122557 .1970 2 .012145 .1935
3 .013.613 .2392 1 .0132.60 .2286 8 .0131.27 .2286 1031.27 .2126 9 .012339 .2071 2 .012339 .2071 1 .0122557 .1970 1 .0122557 .1970 2 .0121.59 .1935
3 .013.613 .2392 1 .0132.60 .2286 8 .0131.27 .2195 9 .012339 .2196 1 .012733 .2126 2 .012733 .2126 3 .01245 .1970 1 .0122557 .1970 2 .012145 .1935
3 .013.613 .2392 1 .0132.60 .2286 8 .0131.27 .2195 9 .0127334 .2196 1 .0127334 .2071 2 .012335 .1970 1 .0122557 .1970 2 .012145 .1970 2 .012145 .1970
3 .013.613 .2392 1 .0132.60 .2286 8 .0131.27 .2286 9 .0131.27 .2126 9 .012339 .2071 2 .012339 .2071 1 .0122557 .1970 1 .0122557 .1970 9 .0121.959 .1935
3 .0134613 .2392 1 .0132460 .2236 6 .0131927 .2195 6 .0127339 .2126 7 .012733 .2126 8 .012733 .2126 1 .0122557 .1970 1 .0122557 .1970 1 .012159 .1935
3 .0134613 .2392 1 .0132460 .2236 0 031927 .2236 0 0127239 .2071 2 .012739 .2071 2 .012739 .1970 1 .0122557 .1970 2 .012145 .1970 3 .012145 .1970
3 . 0134613 . 239 1 . 0132460 . 239 8 . 0137877 . 219 8 . 012723 . 203 3 . 0127345 . 203 3 . 0127345 . 203 4 . 0127357 . 197 6 . 0127359 . 197
3 .013+613 .<392 1 .0132+60 .2286 8 .0131927 .2196 9 .0127233 .2071 2 .0127333 .2072 3 .01271557 .1970 1 .0122557 .1970 5 .012145 .1935
3 .013+613 .<392 1 .0132+60 .2286 8 .0131927 .2196 9 .013927 .2126 2 .012345 .2071 1 .0122557 .1970 2 .012145 .1949
3 .013+613 .<392 1 .0132+60 .2286 8 .0131927 .2196 9 .0127233 .2071 2 .0127343 .2072 3 .0124154 .1997 1 .0122557 .1970 5 .012145 .1970
3 .013*613 .7392 1 .0132*60 .2286 8 .0131.27 .2195 9 .012930 .2126 8 .012733 .2071 2 .012733 .2077 1 .0122557 .1970 1 .0122557 .1970 9 .012145 .1935
3 .013*613 .7392 1 .0132*60 .2286 8 .0131527 .2195 9 .013990 .2126 9 .012733 .2027 1 .012733 .2027 1 .0122557 .1970 1 .012159 .1935 9 .012145 .1935
3 .013*613 .4392 1 .0132*60 .2296 8 .0131527 .2195 9 .0127239 .2126 0 .012739 .2027 1 .012739 .1970 1 .0122557 .1970 2 .012145 .1970 3 .012145 .1935
3 .013*613 .<392 1 .0132*60 .2286 8 .0131*27 .2195 9 .0127*39 .2126 2 .0127*39 .2071 2 .0127*39 .1977 1 .0122557 .1970 5 .012145 .1949 6 .012146 .1935
3 .013%613 .<392 1 .0132%60 .2286 8 .0131927 .2195 9 .013930 .2196 2 .012339 .2023 3 .01245 .1970 1 .0122557 .1970 5 .012145 .1935 9 .012146 .1935
3 .013%613 .2392 1 .0132%60 .2296 8 .0131927 .2196 9 .0127339 .2126 2 .0127339 .2126 3 .012745 .1977 1 .0122557 .1970 5 .012145 .1979 9 .012146 .1935
3 .013.613 .2392 1 .0132.60 .2286 8 .0131.27 .2195 9 .0127339 .2126 2 .012739 .2071 2 .012739 .1970 1 .0122557 .1970 2 .012145 .1970 3 .012145 .1970
3 .013.613 .2392 1 .0132.60 .2286 8 .0131.27 .2195 9 .0130.37 .2196 10 .012.39 .2071 2 .012.39 .2071 1 .0122.55 .1970 2 .0121.45 .1970 9 .0121.46 .1935
3 .013.613 .2392 1 .0132.60 .2286 6 .0131.27 .2196 6 .0127.39 .2126 7 .0127.39 .2021 1 .0122557 .1970 1 .0122557 .1970 5 .0121.59 .1935
3 .013+613 .2392 1 .0132+60 .2286 6 .013157 .2196 6 .0127253 .2071 7 .0127253 .2072 3 .0127155 .1997 1 .0122557 .1970 5 .012145 .1949
3 .013+613 .2392 1 .0131+600 .2286 0 .013157 .2195 9 .0127239 .2126 8 .0127239 .2071 2 .012734 .297 1 .012557 .1970 1 .0122557 .1949 9 .012145 .1949
3 .0134613 .2392 1 .0132460 .2296 9 .0131027 .2195 9 .0127239 .2126 2 .012739 .2071 2 .012739 .2071 1 .0122557 .1970 1 .0122557 .1949 5 .012145 .1949
3 .0134613 .2392 1 .0132460 .2296 8 .012930 .2195 9 .012930 .2126 2 .012733 .2027 1 .012235 .1970 1 .012255 .1970 2 .012145 .1970 3 .012146 .1935
3 .013*613 .4392 1 .0132*60 .2286 8 .0131527 .2195 9 .012990 .2126 2 .012733 .2071 2 .012733 .2077 1 .0122557 .1970 1 .012159 .1935 9 .012146 .1935
3 .013.613 .2392 1 .0132.00 .2286 8 .0131.27 .2195 9 .0123.93 .2126 2 .0127.39 .2071 2 .0127.39 .2071 1 .0122.55 .1970 1 .0122.55 .1970 2 .0121.45 .1970 3 .0121.46 .1935
3 .013*613 .<392 1 .0132*60 .2286 8 .0131*27 .2195 9 .0127239 .2126 2 .012739 .2126 2 .012739 .2071 1 .0122557 .1970 1 .0122557 .1970 5 .012145 .1970 6 .012146 .1935
3 .013.613 .2392 1 .0132.60 .2296 6 .0131.27 .2196 9 .0127239 .2071 2 .012739 .2071 2 .012739 .2071 1 .0122557 .1970 1 .0122557 .1970 2 .012145 .1970 3 .012146 .1925
6 0132401 6 0132401 7 013240 9 012323 2 012733 2 012733 3 012733 1 0122557 1 0122557 1 012145 1 012145 1 012146 1 012146 1 012146 1 012146
6 013127 .2195 9 0139030 .2126 8 0127233 .2071 2 0127233 .2072 3 0127233 .1997 1 0122557 .1970 1 01212145 .1949 9 0117146 .1935
2 012525 6 0127233 2071 2 0127233 2071 3 0127133 1997 1 0122557 1970 1 012145 1949 5 0117146 1935
2 .01.7233 .2071 2 .01.7233 .2071 3 .01.7335 .2025 3 .01.72557 .1970 1 .01.72557 .1970 5 .01.7146 .1935
2 0120395 .2071 3 0120395 .2325 31 0122557 .1997 1 0122557 .1349 1 012145 .1949 5 0117146 .1935
3 0124153 .2325 3 0124153 .1997 1 0122557 .1970 1 01.2145 .1949 5 0121359 .1935
1 .0124154 .1997 1 .0122557 .1970 1 .0122145 .1949 5 .012146 .1935
2 .01.2145 .1949 5 .0121359 .1935 9 .0117146 .1927
5 • 5121359 • 1935 9 • 5117146 • 1927

. 5 35	321	. 343	120cm	.135		
.7 39	. 200		523+0	.107		CJ
.0-1	. 212	+ 1 + •	345723	.139		M
.23+	5.372	. 105	3 3339	.110		.t
2+5.	11.523	. 385	33847	.111		10
.839	17.395	186.	28339	.113		ı,
400.	21.233	0 + 2 +	25599	.115		7
3.3355	-23, 3443	とのけの・ナ	. 112 3 3 9 5	1188	w w	α,
50€.	25.333	166.	21373	.121		ጥ
cta.	25.353	.290	20+17	.122	<b>H</b>	_
.673	20.07	. +12	1 90 + 0	• 124	+	
	-4					
<b></b>	-					
<b>c.</b> 7	5.150	43.753	10135	.113		
. 059	3.530	1.73	17223	• 035		ر.
717.	J. 533	33.144	15350	• 034		m
860.	7.1+0	21.200	14+51	.077		, t
.021	5.375	11.329	13323	.072		'n
.1+5	4.433	313	13575	.071		(O
.271	4.15+3	9.033	013353	. 572		7
J.	+2.5152	25.7732	. 3133257	0770		ar:
. 5 33	9.532	1.553	013734	• 033		መ
.572	4.432	3.754	011299	. 1.14	+4	0
-1						
.500	J. 750	115	09943	33		
22	-7.1350	.0202	.0097913	.0301	S	(J
.750	7.036	115	4408 0	0		M
· 875	8.172	112	ù 95 0 <b>1</b>	J Ü U		. <b>+</b>
0000	3.699	10.7	69333	O O		ın
.125	3.900	303	0 9227	ن 0		ıΩ
.250	9.050	. 102	7606n	330		_
.375	4.055	311	005952	00		αn
.536	3.133	. 325	08358	30		ന
. 525	. 233	.341	008727	Ú.		<b>_</b>
	<b>+</b> +					
	-4					

# 3. COMMON PHASE II LOG4 - PART I DATA, ACROSS - BLADE

100 0.0 100 0.0 100 0.0 100 0.0 100 1.0 100 0.0 100 0.0 100 0.0 100 0.0 100 0.0 100 0.0

### 4. COMMON PHASE II FIXED (LOG I) DATA, WITHIN - BLADE

STAGE A	21 23	1440-145-4240. FIXED 0 11	(-031)	) AT A
	ı !			
9.05do	90 T			
·	:			
•	-1.3			
	-			
4				
	•			
•				
. 75	٠			
9• 00	0.3			
5.4474	:			
9				
40 VD * V	n ,			
000	•			
312	•			
3.0013	٠ د د			
	•			
9.7359	1.j			
7.5434	2.3			
. 223	•			
,				
• 57.4	v:			
•	3.			
•				
٠. م	2.4.0			
	? (			
. 53.	٠			
;				
	•			
	*244			
\$ 79.	7			
+ 00 •	976.			
751				
9. 2873	2.7290			
•	`			
610.	•			
.715	4005			
7.8335	3.2001			
196.	.311			
. 055	3/5			
.174	.393			
299	350			
423	455			
. 573	.057			
7,7230	3.5189			
	.71:			

```
1000010111011
                                                                                                                                                                                                                                                                                                                                                                                          .2392
.2286
.2195
.2126
.2071
.2029
.1997
.1970
                                                                                                                                                                                                                                                                                                                                                                                      .1296
.1161
.1110
.1178
.1055
.1039
.1028
.1018
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         0252
0233
0207
0185
0177
0180
0184
0190
                                                                                                                                                                                                                                                   .0134513
.0132450
.0131827
.0127288
.0127288
.01275985
.0122557
.0122557
                                                                                                                                                                                                                                                                                                                                                                                    .13 o 7 0 7 4

.12 5 5 1 9 o

.11 5 2 8 0 6

.10 6 4 7 7 8

.0 9 2 1 8 5 8

.0 8 7 1 0 3 4

.0 7 9 0 6 5 2 1

.0 7 3 4 0 0 3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       .185212
.185212
.1582353
.152521
.1391285
.1194649
.1127583
.1070491
                                                                                                                                                                                                                                                 17.3413
15.3441
13.2208
10.44999
8.4418
5.5942
4.0131
4.0131
13.5278
1.1399
                                                                                                                                                                                                                                                                                                                                                                                   10.9501
10.7028
9.533
6.8749
4.5033
3.4595
2.34695
1.7092
1.7869
1.7863
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     4.59983
2.5.550
2.5.550
2.5.550
2.5.550
2.5.550
2.5.550
2.5.503
                                                                                                                                                                                                                                     1. -62.9005 -62.9400. -62.9254 -03.1427 -63.6300 -64.1454 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.09012 -61.0901
3.7826
3.8256
3.8370
3.9123
3.7453
                                                                           4.172
4.2010
4.1725
                                                                                                                       4.725
                                                                                                                                                                                                                                    6.65904

6.65904

7.41721

7.41701

7.66322

7.91170

8.16170

8.16170

7.01124

6.55530

7.01444

8.75448

8.7512

7.75313

8.7513

8.7513

8.7513

8.7513

8.7513

8.7513

8.7513
7.9538
6.0536
6.1835
6.3126
8.4397
8.5795
7.6720
8.19
                                                                                                                                                                             ~
                                                                                                                    7.64
8.6
                                                                                                                                                 6
4
                                                                                                                                                                                .c. 0
```

																																					•																	
	-	~	M	4	ın	<b>ທ</b>	~	en (		3		٠	<b>→</b> (	v	A 3	<b>+</b> 1	<b>n</b> ,	0 1	٠.	n n		-		-	١ ٨	<b>M</b>	*	ın	Φ	~	æ	m	7			•		N I	m.	<b>.</b> + 1	•	1 0	<b>.</b> α	0 17	7	7	-	~	M	<b>.</b>	w.	10 P	- 0	¥O
	ŧ	\$	ŧ	\$	ŧ	\$	4	<b>.</b>	<b>.</b>	<b>.</b>	ŧ	t	v n	n ı	v n	U i	חי	v n	n u	n u	n 4	) 'C	•	•	ω (	ص	.0	9	9	•	9	g	ø	Q			, a	<b>-</b> 4 -	┥.	↔ .	<b>-</b> 4 •	4 •	<b>-</b> +	4 +	٠,	H	~	~	~	~	N	~	u c	N
								29							60															61								25.														<b>4</b> 1		
	9	9	02	02	02	<b>*</b>	7	30.	0	<b>†</b>	<b>†</b>	•	2 3	7		2 6	2 6	200	ב כ	ב כ	ב ב ב	ğ	,	1	2 0	2	H	11	픾	.116	11	12	12	12				6	80	7	6	2 6	٠ĸ	- d	9 4	Š	0.5	70	9	63	03	.028	2 6	<u> </u>
	ĭ	ř	ĭ	ĭ	ĭ	ĭ	ř	ř	ĭ	ř	ĭ			Ĭ	ĭ	ĭ	ĭ	Ŭ	ĭ	ĭ	•			i	ì	•	ĭ	ĭ	ĭ	ĭ	ĭ	ĭ	ĭ	ĭ				ĭ	ĭ	ř	ĭ	ĭ	Ĭ		ĭ							ĭ		
	20	11	37	ᅻ	1,	35	0	31	æ .		97				<b>3</b> C															93								80														1 C		
	30	56	56	31	80	20	16	251	9	0 1	8		2 1	7	220	? (	7	<b>9</b> 9		2 0	2 7		•	1	. 3	75	38	48	89	559	50	87	4	70		1	M 1	722	9 .	2	2	0 0	9 6	2 6	2 0	Š	58	11	20	9	ę,	991	9	S
	4	-	-	7	7	4	-	9	•	0	0	•	⊣•	Η.	= =	-	9 (	<b>-</b>	9 0	<b>-</b> 0	9	<b>-</b>	•	=	, =	0	0	0		• 02	0	0	0	0			0	• 01	0	0	0	<b>-</b>	<b>&gt;</b> <	<b>5</b> 6	9	∍	-	+1	Ö	0	0	• 09	5 (	0
	ũ	\$	~	0	۵	*	0	in t	S.	•	ø	Ċ	۰ رو	o ·	. t.	ות	9	ווית	0 6	าน	V V			M	t c		ۍ .	S	~	6.8	Ø	۴-	0	~				ر ا ری									ın	*	m	ŝ	ß	37	<b>T</b>	q
	6	۲.		•	ij	•	Ċ.	200	Ÿ		7	•	V	٠	9 1	•	າ	+	•	Ö	י ת	? =	•	-			•	~	•	3.0	60	Ţ.	~	*			75	.77	7	52	8	2 2	9 6	- 15	5	C	٧.	3	2	٧.	<b>.</b>	.97	3	۲
						1		•	(	<b>~</b>	M	t	ויי		•	•	v.	2	•	- r	٧ ٢	<b>,</b> ~	,	~	۷ د	۱ ۸	-	~	M	*	4	m	m	~			# 1	-37	m	N	₩.			Q -			N	N	-23	4	<del>1</del> 9	2.		12
	H	7	'n	m	8	0	ပ	17	s o	۰	თ		9	Э,	ر ان دو	<b>-</b>	n,	<b>-</b> 1	0	<b>&gt;</b> :	Ť d	) (	•	-	4 0	~	S	თ	Ø	91	σ	ĝ	ጥ	0			9	9	0	0	<b>•</b> (	א עב	วัน	'n	u r	V	σ	ø	00	~	m	12	י פי	M
	ď	٠,	•	<b>.</b>	+	ŝ	٥.	5.	9		9	ŧ	ů.	•	,	• ·	J.	• •	•	•	•	) a	•	۷			l M	ıv	M	29	30	m	6	r.			ᅻ'	53	٠ ھ	٠,	<b>م</b>	<b>.</b>	Ü,		٠.	<b>.</b>	. 7	6	6	M	*	. 83	<b>•</b> 1	~
		*	•	+	3	ŧ	ŧ	80 1	* 1		S.	┙,	⊣,	-1	-20	v	V	<b>?</b>	2	2	つ 🏲	) P	•		, "	•		-	+	-21	N	~	Ò	2	-1		iV IV	0.	တ ၊ †	<b>*</b>	<b>.</b>	<b>.</b>	# U	n 7	<b>.</b>	V T						53		
	#	~	N	0	σ	æ	20		<b>T</b>	<b>O</b>	0	- 0	n t	•	35.3	# (	N	NO	U d	<b>*</b> (	0 0	•	4 +	1 4	0			~	0	*	ю	N	9	0			\$	ന	~	•	<b>+</b> 1	Ω,	40	n ~	0 (	7 7	• +4	m	٠Đ	m	M	<b>60</b> 1	m (	60
	ď		•	?	5	۲.	•	3.2	r,	`	0		۱٠	•	0.7	V 1	ů	٠	• r	Ų u	ů		•	ي	1		N	Ŋ	80	9.0	m	'n	8	•			ŝ	7.65	٠.	φ,	•	٠,	v	3 11	٠,	٥	S	٩٠	~	20	•	8.10	Ņ	~
~		_				-		'	~ .	~		v `	- `		•	- '			- 4	•		,	1	_			•			~	٠,	/	~		0		. 🤜	'			~ `	4		<i>-</i> 4	- "	~		,-	,-		~	~ '	_	~

C1 (	1									00 00		₩									(D		-1						ڻ. ما					+1	
- 10353	· 0 43		.915	.012	.039	. 137	.005	.005	.035	-,0359	.007	• 0 9 9		3,2	0.32	3.0.5	003	0.33	<u>n</u> 03	0.03	.3036	0 0 3	0.04		J 0 0	000	3 3 0	0.00	.3000	0.00	000	0 0 3	000	000	
. 0807335	192+53		120113	111005	097035	085993	078303	074359	073579	. 97 64 38 8	083225	094559		83573	74459	56721	60225	55705	53253	520 48	. 1541.345	57305	<b>ù</b> 64613		1650	16260	395+4	0 95 01	.0093536	009227	16060	008962	0 88 33	003727	
23.1254	2.343		9.337	0.259	9.120	6.750	773	1.175	.543	2. 3555	J 3.+	. 159		1.397	.101	. 313	.552	4110	.303	.135	. 338	+ 200 •	9		18	23	13	112	• 197 i	003	ข ก 2	.011	325	. 141	
52.4772	5.532		9 co • ¢	5.337	ာ• ပါပ်+	5. 323	5.735	5.303	5.351	10.0537	ò. 735	7 + 80 9		. +73	. 113	. 533	. 336	off.	831	.750	, 37,7	. 137	3,0112		6 - 750	7.135	7.585	8.175	3.539	3.300	9.055	9.053	3.133	. 23	
5 )	.033	T	7.500	. 625	.75U	5.30	.000	.125	.250	75	.500	3.025	44	7.500	625	750	875	00 p	.122	.250	.375	.500	625	-	.500	.525	.750	.875	. 0 00	125	.256	.375	.500		

### APPENDIX B

### 5. INDIVIDUAL TEST INPUT DATA

### a. Key

### TEST IDENTIFICATION

- (1) Exceptions to Common Phase I Data (Appendix B.1 cards indicated by " $\sharp$ ").
- (2) Exceptions to Common Phase II Fixed (LOG1) Data, Across-Blade (Appendix B.2, cards indicated by "\*").
- (3) Exceptions to Common Phase II LOG4 Part 1 Data, Across-Blade (Appendix B.3, cards indicated by "\*").
  - (4) Other LOG4 Data Required, Phase II Across-Blade FOR TESTS CONSIDERED WITH WITHIN-BLADE ANALYSIS
- (5) Exceptions to Common Phase II, Fixed (LOG1) Data, Within-Blade (Appendix B.4, cards indicated by "\*").
  - (6) LOG4 Data Required, Phase II Within-Blade
- (7) Stator Surface Static Pressures, obtained from Phase I Reduction.

### b. Test Points

### Test 208180514040

- 1. None
- 2. None
- 3. None
- 4. STATICH ELCCKAGE DISTRIBUTION FACTOR

```
1
         C.01C00
                            1.0000
 2
         0.00000
                            1.0000
 3
         0.00000
                            1.0000
         0.00000
                            1. CO 00
         0.00000
                            C. CO GO
 ε
         .05200
                            C.0000
         G • G U C O D
                           1.0000
 8
          .16300
                            1.000
 9
          .05400
                           1.0000
10
          .05400
                           1.0000
```

### SCLUTION TYPE INDICATORS

### WITHIN-BLADE ONLY

- 5. None
- 6. ROTOR SENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 4 POINTS

4-CUORD LUBS COEFF/TOTAL LOSS COEFF

0.0000 0.0000 1.0000 1.0000

OUTLET RADIUS = 7.5+93

M-COORD DEVIATION ANGLE (DEGREES)

.2000 -1.4700 .4900 -2.1300 .6000 -2.9430 .6000 -5.0700

DUTLET RADIUS = 7.7254

M-COORD DEVIATION ANGLE (DEGREES)

.2000 -1.2700 .4000 -1.7300 .6000 -2.5400 .8000 -4.3800

```
OUTLET RADIUS = 7.9130
         1-COURD DEVIATION ANGLE (DEGREES)
           .2000
                         -1.1400
                         -1.5600
           •4000
           ·5J00
                         -2.2800
           .3003
                         -3.3400
OUTLET RAJIUS = 5.1291
         4-COORD DEVIATION ANGLE (JEGREES)
           .2000
                         -1.1400
           . 4000
                         -1.5600
           60000
                         -2.2800
           .5000
                         -3.9400
QUILLIT RADIUS = 3.3352
         M-COORD DEVIATION ANGLE (DEGREES)
           .2000
                         -1.3300
           .4000
                         -1.3200
                         -2.3790
           .0000
           .8000
                         -4. 6100
OUTLET RADIUS = 3.0539
         1-CUORD DIVIATION ANGLE (DEGREES)
           .2000
                         ~1.9800
           · + 999
                         -2.7000
           .0303
                         -3.9500
           .8300
                         -6.3400
STATOR SENERALISED PIKFORMANCE LOSS 2 POINTS DEVIATION 6 POINTS
         1-CUORD LOSS COEFF/TOTAL LOSS COEFF
          0.0000
                          0.3033
          1.0000
                         1.0000
OUTLET FAULUS = 0.0000
         M-COORD DEVIATION ANGLE (DIGREES)
                           .1000
          J.3000
           .2003
                           .1100
           • → 00 o
                           .1500
           .6000
                           .2200
           . 6000
                           .3800
```

1.0000

1.030J

NUMBER OF TEST POINTS TO BE ANALYSED = 1

PSCALE= .50 PLOWLR= 14.00 DAMPF= 5.000 NSAVE= 1 NEX= 2

NGITATE	BLOCKAGE	NOITURIPTEIL	FACTOR
317112011	)	D131 (1//0110/4	1 -015.0

1	ា • ប្រព្ធា	1.0000
2	0.0000	1.0000
3	0 • 0 0 0 0 0	1.0000
4	0.00000	1.0000
5	.03000	• 3000
5	• 0 5 0 0 0	•5000
7	• U 549 û	.2000
ક	• 9 54 3 0	0.0000
9	• 05+06	1.0000
10	• 0 2 4 4 0 0	1.0000
11	• 0 90 0 0	1.0000
12	•09100	1.0000
13	•09200	1.9009
1+	• 0 93 0 u	1.0000
15	• 0 o 0 0 0	1.0000
16	0 0 0 0 0	1.0000
17	.03497	1.0600

### SOLUTION TYPL INCIDATORS

		SS
7.	PUSITION NO.	PRISSURI(PSIA)
	1	13.184
	2	12.347
	ê	13.35.
	₩	13.379
	,	1+.325
	၁	15.274
	7	15.240

### Test 208180106840

- 1. None
- 2. None
- 3. None
- 4. STATICN ELCCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	G • 6 0 C O C	1.0000
3	C.OC808	1.0000
4	0.00000	1.00CO
5	.02500	G. 60 CG
6	.02500	0.0000
7	.05000	1.0000
8	.13600	1.0000
9	.05400	1.6060
10	.05400	1.0000
-	· ·	

### SCLUTION TYPE INCICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

### Test 208180315240

- 1. None
- 2. None
- 3. None
- 4. STATION BLCCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0060
4	0.00000	1.0000
5	.0259G	0.0000
E	.0250G	0.0000
7	.05000	1.0000
8	.14300	1.0000
9	•05400	1.0000
16	.05400	1.0000

### SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

### Test 208180415840

- 1. None
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBLTICA FACTOR

1	C.00000	1.0000
2	0.00000	1.000
3	0.00000	1,0000
4	0.00000	1.0000
5	•02500	0.0000
ε	•02500	0.0000
7	•05000	1.0000
8	·153G0	1.0000
g	.05400	1.0000
10	•65400	1.0000

### SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -C -0 -C -0 -0 -0 -C

### Test 2081806840

- 1. None
- 2. None
- 3. None
- 4. STATICH BLCCKAGE DISTRIBUTION FACTOR

```
0.00000
                          1.0000
 2
        0.00000
                          1.0000
         0.00000
                          1.0000
 4
         0.00000
                          1.0000
 5
          .02500
                          0.0000
 ε
         .0250J
                          0.0000
 7
         .05000
                          1.0000
 8
         •20006
                          1. CO 00
 G
         .05400
                          1.0000
10
         •0540J
                          1.0000
```

### SCLUTICH TYPE INCICATORS

STATICN 1 2 3 4 5 6 7 8 9 1C NMACH 0 0 -0 -C -0 -C -C -C -C -C

- 1. None
- 2. None
- 3. None
- . STATICN BLOCKAGE DISTRIBUTION FACTOR

1	<b>.</b> .06600	1.0000
2	J.DGC0G	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.02500	0.0000
6	.02500	T. COGC
7	.05000	1.8600
8	.18500	1.0000
g	.05400	1.0000
10	.05400	1.0000

#### SOLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 1T NMACH 0 0 -0 -C -0 -C -0 -C -0 -C

## Test 208180711240

- 1. None
- 2. None
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

```
1
         0.00000
                           1.0000
 2
         0.00000
                           1.0000
 3
                           1.0000
         0.00000
                           1.0000
         0.00000
 5
         .02500
                           C.0000
 E
          .02500
                           C. 0000
 7
          .C500C
                           1.60G0
 8
          .1EC00
                           1.0000
 9
          .05400
                           1.0000
          .05400
10
                           1.0000
```

## SOLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 E 7 8 9 1C NMACH 0 0 -0 -C -0 -0 -0 -0 -C -C

- None
   None
   None

4.	STATION	BLCCKAGE	DISTRIBUTION	FACTOR
----	---------	----------	--------------	--------

1	0.00000	1.0060
2	0.00200	1.0000
3	0.0000	1.0000
4	0.00000	1.0000
5	.02500	0.0000
6	.02500	0.0000
7	•05C0C	1.0000
8	.16000	1.0000
9	.05400	1.6000
10	.05400	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5  $\in$  7 8 9 10 NMACH C 0 -0 -C -0 -0 -C -0 -0 -C

- 1. 14.0916 15.0 30.0
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000	
2	0.0000	1.0000	•
3	0.00000	1.0000	
4	0.00000	1.0000	
5	.02500	0.0000	
6	.02500	0.0000	-
7	.05000	1.0000	
8	.15300	1.0000	•
9	•0549 B	1.0000	
10	.05400	1.0000	

#### SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 "9 10" NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

## WITHIN-BLADE ONLY

- 5. None
- 6. ROTOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 14 POINTS

M-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 3.0000 1.0000 1.0000

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

.2000 -1.4700 .4000 -2.0000 .6000 -2.9400 .8000 -5.0700

OUTLET RADIUS = 7.7254

Y-COORD DEVIATION ANGLE (DEGREES)

-2000 -1.2700 -4.000 -1.7300 -6.000 -2.5400 -8.000 -4.3800

```
OUTLET RAJIUS = 7.9130
         M= C0037
                    DEVIATION ANGLE (DEGREES)
           .2000
                          -1.1400
           .4000
                          -1.5600
           .6000
                          -2.2800
           .8000
                          -3.9400
OUTLET RAJIUS = 3.1291
         (150CD =1)
                    DEVIATION ANGLE (DEGREES)
           .2000
                          -1.1400
            . 4000
                          -1.5600
           • 5000
                          -2.2800
           .3000
                          -3,3400
OUTLET RADIUS = 8.3552
         M- COORD
                    DEVIATION ANGLE (DEGREES)
           .2000
                          -1.3300
           • 4000
                          -1.8200
           .5000
                          -2.5700
           .8000
                          -4.5100
OUTLET RADIUS = 6.6699
         M-COORD DEVIATION ANGLE (DEGREES)
           .2000
                          -1.9800
           • 4 00 0
                          -2.7000
           • b 000
                          -3.9500
           .8600
                          -6.8403
STATOR GENERALISED PERFORMANCE
                                  LOSS 2 POINTS
                                                   DEVIATION 5 POINTS
         M-COORD LOSS COEFF/TOTAL LOSS COEFF
          0.0000
                           0.0000
          1.0000
                           1.0000
OUTLET RAJIUS = 0.0000
         1<del>-</del> COO3U
                   DEVIATION ANGLE (DEGREES)
          0.0000
                            .1000
           .2000
                            .1100
           .+000
                            .1500
           .6000
                           .2200
```

.3800

1.0000

.8000

1.0000

## NUMBER OF TEST POINTS TO BE ANALYSED = 1

PSCALE = .50 PLOWER = 14.00 DAMPF = 5.000 NSAVE = 1 NEX = 2

## STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	• 0 5 0 0 0	•5000
6	.05000	.5000
7	• 0 5 4 0 0	.3500
·8	•05400	0.0000
9	.05400	1.0000
10	• 05400	1.0000
11	• 0 9 0 0 0	1.0000
12	•09100	1.0000
13	.09200	1.0000
14	.09300	1.0000
15	.06000	1.0000
16	•08000	1.0000
17	•0540v	1.0000

## SOLUTION TYPE INDICATORS

STATION 1 2 3 4 5  $\circ$  7 8 9 10 11 12 13 14 15 16 17 NMACH 0 0  $\circ$ 

		SS
7.	POSITION NO.	PRESSURE (PSIA)
	1	12.798
	2	12.562
	3	13.725
	4	14.052
	5	16.369
	õ	16.108
	7	16.387

	PS
1	16.716
2	17.384
3	17.605

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	6.05000	1.0000
3	0.0000	1.0000
4	0.00000	1.0000
5	.02500	0.0000
6	.02500	0.0000
7	• 05060	1.0000
6	•13600	1.8090
9	.65469	1.0000
10	.6548û	1.9000

## SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 19 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208220315550

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.00000	1.0006
3	0.00000	1.0003
4	0.00000	1.3000
5	• 0 25 ú P	0.0000
6	.02500	0.0000
7	.050(0	1.0000
8	• 1430 b	1.0000
9	.05400	1.0008
10	.05408	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 3 5 -6 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.00000	0.0000
6	• 0520 G	0.0000
7	0.00006	1.0000
8	.1630G	1.0000
9	.05480	1.0000
10	.C540C	1.0000

## SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208220613650

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICH BLCCKAGE DISTRIBUTION FACTOR

1	0.60008	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.02500	0.0000
6	.02500	0.0000
7	.05000	1.0000
8	.18500	1.0000
9	. 6540 C	1.0000
10	.05460	1.5000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICN BLOCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	J 0 0 0 0 0 0	1.0000
3	0.0000	1.0000
4	0.00000	1.0000
5	• J 25 G O	0.0000
ε	.02500	0.0003
7	.05000	1.0000
8	.160CC	1.0000
9	.05463	1.0000
10	• û <b>5</b> 4 6 G	1.0000

## SCLUTION TYPE INCIDATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208220810950

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.00000	1.0000
3	C • 5 C O O O	1.0000
4	9.55000	1.0000
5	.02500	0.0006
6	• C 25 C C	0.0000
7	.05000	1.0000
8	•2000C	1.0000
9	.05400	1.0000
10	.05400	1.0000

## SCLUTION TYPE INCICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 1. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.02500	0.000
ь	• 0 25 0 0	0.0000
7	.05000	1.0000
8	.16000	1.0000
9	.05400	1.0000
10	.0540 Û	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.0916 15.0 30.0 2. None 3. None

- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.0000	1.0000
5	.025 u Q	0.0000
6	• 0 25 0 G	0.0009
7	•0500C	1.0000
8	.15300	1.0000
9	.05400	1.0000
10	•05400	1.0000

## SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0

## WITHIN-BLADE ONLY

- 5. None
- 6. ROTOR GENERALISEU PERFORMANCE LOSS 2 POINTS DEVIATION 4 POINTS

4-COORD LOSS COEFF/1014E LOSS COEFF

0.3000 0.0000 1.0000 1.0000

OUTLIT MADIUS = 7.5499

M-COORD DIVIATION ANGLE (DIGREES)

·2000 -1.4700 -2.0000 00000 -2.9400 • 6000 -5.0790

OUTLET FADIUS = 7.7294

M-COORD DEVIATION ANGLE (DEGREES)

. 2000 -1.2799 • 4 0000 -1.7300 •6000 -2.5400 00064 ~4,3800

```
OUTLET RADIUS = 7.9180
          M-COORD DEVIATION ANGLE (DEGREES)
            .2000
                           -1.1488
                           -1.5600
            . 4083
            000 a
                           -2.2800
                           -3.9400
            . 8 30 3
OUTLET RADIUS = 3.1291
          4-GOURD DEVIATION ANGLE (DEGREES)
            .2003
                           -1.1430
            .4900
                           -1.5600
                           -2.2800
            .5000
            .8000
                           -3.9400
OUTLET MAJIUS = 8.3552
                  DEVIATION ANGLE (DEGREES)
          4- C0033
            .2000
                           -1.3300
            .4801
                           -1.8293
            .6000
                           -2.5790
            .8000
                           -4.6100
OUTLET RADIUS = 5.5699
          4-COGRO DEVIATION ANGLE (DEGREES)
            .2300
                           -1.9600
            .400ú
                           -2.7030
            .5000
                           -3.9600
            . 6 00 0
                           -6.8490
STATOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 5 POINTS
          M-COURD LOSS COEFF/TOTAL LOSS COEFF
                            0.0000
           0.0000
           1.0000
                            1.0000
OUTLET RADIUS = 0.0000
          4<del>-</del> 00000
                    DEVIATION ANGLE (DEGREES)
                            .1000
           0.0000
            .2000
                             .1100
            .4000
                             ·150J
                             .2200
            .6000
            . o 00 J
                             .3803
           1.0000
                            1.0000
```

NUMBER OF TEST POINTS TO BE ANALYSED = 1

PSCALE= 1.00 PLOWER= 14.00 DAMPF= 5.000 NSAVE= 1 NEX= 2

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00036	1.0000
4	0.00000	1.0000
5	00000	•5099
ь	• 0 = 0 0 U	
7	.0.400	
8	<del>-</del>	.3500
	• 0 5 4 0 0	0.0000
9	• 3 > 4 0 0	1.0000
10	• 0 > 4 3 3	1.0000
11	• 06000	1.3000
12	•07090	1.3000
13	• 0 30 0 5	1.7033
14	• 0 > 0 U 0	1.0000
15	• 11 = 0 11 11	1.0000
16	• U 30 C U	
17	· · · · · · ·	1.0000
11	.35400	1.0003

JOLUTION TYPE INDICATORS

7. POSITION NO.  1 2 3 4 5	SS PRESSURE (PSIA) 11.704 13.826 13.843 15.552 15.689 16.617
,	16.785

PS 17.752 18.319 3 19.132

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00090	1.0000
5	.02500	0.0000
6	.0250C	0.0000
7	.05000	1.0000
8	.13600	1.0000
9	.05406	1.0000
10	.05400	1.0000

## SOLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208221315560

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATION BLCCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.0000	1.0000
3	0.00000	1.0000
4	n.0000J	1.0000
5	.U250G	0.0000
6	.02500	0.0000
7	.05000	1.0006
8	•14300	1.0000
9	•65466	1.0800
10	.05400	1.0000

## SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.00000	0.0000
6	•05200	0.0000
7	0.00000	1.0000
8	•1630C	1.0000
9	• 5545 0	1.0000
1C	• 65400	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208221614460

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

0.63630	1.0000
0.01000	1.0000
ŭ.∂003ĕ	1.0000
0.00000	1.0000
• 0 25 G u	0.0000
.02506	0.0000
.05000	1.0600
.185GC	1.3000
.35400	1.0000
.35400	1.0000
	0.03000 0.00000 0.00000 02500 02500 05000 18560

## SCLUTION TYPE INCICATORS

STATION 1 2 3 4 5 6 7 8 9 13 NMACH 3 0 -6 -3 -0 -6 -6 -0 -0 -0

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATION BLCCKAGE DISTRIBUTION FACTOR

1	0.01000	1.0003
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.02560	0.3000
6	.02500	0.0000
7	.05000	1.0000
8	·16000	1.0000
9	.05400	1.0000
10	•0540a	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 3 6 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208221812760

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.0000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.02500	0.0060
6	.02500	0.0000
7	.05000	1.0000
8	.2000U	1.3000
9	.05400	1.0000
10	.05400	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH J 0 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.0916 15. 30.
- 2. None
- 3. None
- 4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.0000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	•02500	0.0000
6	.02500	0.0000
7	.0500G	1.0000
8	.160C0	1.0000
9	• U540 C	1.0000
16	• 05400	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

1.	14.1586	15.0	30.0
2.	4	11	0
	0	0	Ö
	1	10	Ö
	3	10	Ô
_			



3. None

4. STATICH BLCCKAGE DISTRIBUTION FACTOR

••	••		
1	0.0000	1.9380	
2	0.00000	1.0000	
3	0.00000	1.0000	
4	0.99888	1.0000	
5	• J 25 0 C	0.0000	
6 -	• 0 25 0 6	6.0660	
7	.95000	1.300ú	
8	.13200	1.0000	
9	• 3540 ú	1.0000	
10	• v 54 0 û	1.0000	

---- SCLUTION TYPE INGICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 3 6 -0 -0 -0 -0 -0 -0 -0 -0 -0

## WITHIN-BLADE ONLY

5. 2 11 0 2 11 0 2 11 0 2 11 0 4 11 0

6. ROTOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 4 POINTS

M-GOORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 0.0000 1.0000 1.0000

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

.2000 -6.0000 .4000 -6.0000 .6000 -6.5000 .8000 -9.5000

```
OUTLET RADIUS = 7.9180
                  DEVIATION ANGLE (JEGREES)
          M- C0020
            . 2000
                          -6.0000
            .4000
                          -6.0000
            .6000
                          -6.5000
            .80GO
                          -8.5000
OUTLET RADIUS = 8.6699
         M-COORD
                   DEVIATION ANGLE (DEGREES)
            .2000
                          -6.0000
           .4000
                          -6.0000
           .60DD
                          -6.7000
           .8000
                        -11.8000
STATOR GENERALISED PERFORMANCE
                                 LOSS 2 POINTS DEVIATION 6 POINTS
         M-COORD LOSS COEFF/TOTAL LOSS COEFF
          0.0000
                          0.0000
          1.0000
                          1.0000
OUTLET RADIUS = 0.0000
         M-COORD DEVIATION ANGLE (DEGREES)
          0.0000
                           .1000
           .2000
                           .1100
```

NUMBER OF TEST POINTS TO BE ANALYSED = 1

4000

.6000

.8000

1.0000

PSCALE= 1.50 PLOHER= 14.00 DAMPF= 5.000 NSAVE= 1 WEA - 2

.1500

.2200

.3800

1.0000

## STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.00000	i.0000
3	0.00000	1.0000
4	-01000	1.0000
5	•0 <b>1</b> 000	1.0000
6	•01500	•5000
7	• 0 20 0 0	•5000
8	.02500	.3500
9	.02500	.2000
10	• 0 5 5 0 0	1.0000
11	•03000	1.0000
12	•05000	1.0000
13	•07000	1.0000
14	• 0 90 0 0	1.0000
15	•06000	1.0000
16	.08000	1.0000
17	.05400	1.0000

## SOLUTION TYPE INDICATORS

7.	POSITION NO.	PRESSURE (PSIA)
	1	11.677
	2	9•453
	3	14.253
	4	16.372
	5	17.782
	0	18.243
	7	18.748

PS 19.505 2 21.34 21.470

```
1. 14.1586 15. 30.
2. 4 11 0
0 0 0
1 10 0
3 10 0
```

3. None

4. STATICH BLCCKAGE DISTRIBUTION FACTOR

1	0.06620	1.0000
2	ú.09 <b>0</b> 00	1.0000
3	0.66000	1.0000
4	0.96000	1.0000
5	• 0 25 0 ù	0.0000
<b>'</b> 6	• 9 25.0 ນ	0.0000
7	.3502g	1.0000
8	·14369	1.0900
9	• ü = 4 ú C	1.0000
10	• 0540 û	1.0006

# SCLUTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 9 6 -C -0 -C -0 -C -0 -C -0 -C -0

## Test 208240415370

```
1. 14.1586 15. 30.
2. 4 11 0
0 0 0
1 10 0
```

3. None

4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	v • J 60 ú ú	1.0000
2	9 • ୧୬ଗ୍ରେଖ୍	1.0000
3	0.01000	1.0000
4	0.00000	1.0000
5	• 425 ú C	6.9000
6	• 925 9 6	0,0000
7	•3500L	1.3000
8	.15360	1.0000
9	. 35433	1.0000
1u	• 3546 €	1.9069

# SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

- 1. 14.1586 15. 30. 2. 4 11 0 0 0 0 1 10 0 3 10 0
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.60000	1.0000
2	0.0.000	1.0000
3	9.60000	1.0000
4	0.03000	1.0600
5	• 5 25 6 A	0.0000
6	• 9 25 9 6	0.0000
7	• 6503 0	1.0000
6	•1630 °	1.0000
9	•0546 L	1.0000
1ย	• ú54º b	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMAGH J 3 -0 -3 -3 -5 -6 -7 8 9 10

## Test 208240614270

- 1. 14.1586 15. 30. 2. 4 11 0 0 0 0 1 10 0 3 10 0
- 3. None
- 4. STATION BLOCKAGE DISTRIBUTION FACTOR

1	0 • 6 ១៤ ចំ ប៉	1.3000
2	0.05000	1.0000
3	33003.0	1.3000
4	0.05006	1.0000
5	• 0 25 0 G	0.9003
ö	• 6 25 v E	0.0000
7	.66036	1.0000
8	.18000	1.0000
9	. 35405	1.0000
1	- 11 E to 11	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH J 0 -5 -0 -1 -1 -5 -0 -0 -0

```
Test 208241115882
```

```
1.
    14.1586
                15.0
                        30.0
2.
                11
                         0
     0
                 0
                         0
     1
                10
                         0
     3
                10
                         0
3.
     2
                14
                         5
    STATION
4.
               BLCCKAGE CISTRIBUTION FACTOR
       1
                J • 6 30 8 6
                                   1.3000
       2
                0.0006
                                   1.3500
       3
                4.660000
                                  1.3900
                9.6.035
                                  1.0000
       5
                 •02700
                                  6.0000
       б
                 • 527 6 6
                                   0.0000
       7
                 .05000
                                  1.0000
       ö
                 •11930
                                  1.9083
       9
                 032436
                                  1.0000
      14
                 .65436
                                  1.3000
```

SCLUTION TYPE INCICATORS

STATION 1 2 3 4 5 0 7 8 9 13 NMACH 3 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

## WITHIN-BLADE ONLY

```
5.
       2
                   11
                               0
      2
                   11
                               0
      2
                   11
                               0
      2
                   11
                               0
       4
                   11
                               0
```

6. RUTOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 4 POINTS

M-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 1.0000 1.0000

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

-2000 -8.4000 -4000 -8.3000 -6000 -10.5000 -14.4000

```
OUTLET RADIUS = 7.9180
```

```
M-COORD DEVIATION ANGLE (DEGREES)
```

-8.3000 -4000 -8.4000 -6000 -10.3000 -8000 -13.7000

OUTLET RADIUS = 8.6699

M-COORD DEVIATION ANGLE (DEGREES)

.2000 -8.3000 .4000 -8.4000 .5000 -11.0000 .8000 -14.0000

STATOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 6 POINTS

M-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 0.0000 1.0000 1.0000

OUTLET RADIUS = .0.0000

M-COURD DEVIATION ANGLE (DEGREES)

 0.0000
 .1000

 .2000
 .1100

 .4000
 .1500

 .6000
 .2200

 .8000
 .3800

 1.0000
 1.0000

NUMBER OF TEST POINTS TO BE ANALYSED = 1

PSCALE = 1.50 PLOWER = 14.00 DAMPF = 5.000 NSAVE = 1 NEX = 2

#### STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	•01000	1.0000
5	•01000	1.0000
6	.01500	•5000
7	.02000	•5000
8	•02569	.2000
9	•02000	0.0000
10	• 0 55 0 0	1.0000
11	• 0 30 0 0	1.0000
12	•05000	1.0000
13	•07000	1.0000
14	• 0 90 0 0	1.0000
15	•06000	1.0000
16	• 0 80 0 0	1.0000
17	.05400	1.0000

## SOLUTION TYPE INDICATORS

		SS
7.	POSITION NO.	PRESSURE(PSIA)
	1	11.393
	2	10.824
	Ś	16.394
	4	17.811
	<b>5</b> .	19 a ú 55 ·
	6	19.418
	7	19.804

PS .
1 21.610
2 23.187
3 23.597

1.	14.1586 4 0	15. 30 11 0 0 0 10 0	Reproduced from best available copy.
•	3	10 0	
3.	Z. STATICA		0 1 2
4.	STATICA	SECORAGE	DISTRIBUTION FACTOR
	1	6.00036	1.3038
	· 2	3.00000	1.0000
	3	0.00000	1.0000
	4	0.60000	1.3000
	5	• 02703	0.433 <b>69</b>
	ย	• ( 27 5 0	<b>∂.</b> 9606
	7	. J50 . (.	1.9689
	8	.13256	1.3698
	9	• J 54 J U	1.0605
	10	. ( 64.71	1.4686

## SCLUTION TYPE INCICATORS

STATICN 1' 2 3 4 5 6 7 8 9 19 NMACH 0 6 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208241315682

1.	14.1586 4 0 1	15. 30 11 0 0 0 10 0	
2	3 2.		
3.			.0 1 2
4.	STATION	3L CCKAGE	DISTRIBUTION FACTOR
	1	0.00000	1.0000
	2	0.000Bc	1.)000
	3	0.00000	1.3030 -
	4	6.00000	1.3000
	5	.9270t	4.0000
	6	• £ 27 0 c	0.0600
	7	.59063	1.0609
,	ä	.14303	1.000
	3	. 6482	1.3360
	<b>1</b> ί	.05430	1.3366

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH U L -L -C -U -J -L -L -C -U

```
14.1586
1.
                15.
                       30.
2,
     4
                11
                        0
     0
                0
                        0
     1
                10
                        0
     3
                10
                       0
3.
     2.
               14.
                       5.0
                             1
                                   2
    STATION
              BLCCRAGE DISTRIBUTION FACTOR
```

1 6.33066 1.00005 2 0.00000 1.3000 3 5.51605 1.3000 0.03000 1.0000 5 .32700 0.3003 € . v 270 L C. 4000 7 • 55000 1.3800 8 .1520 U 1.0005 9 .35430 1. 3600 10 .(5466 1.3000

# Feet of reils ple to to by.

# SCLUTION TYPE INCICATORS

STATION 1 2 3 4 5 6 7 8 9 13 NMACH 3 8 -1 -6 -3 -3 -5 -6 -9 -5

## Test 208241515382

1. 14.1586 15. 30. 2. 4 11 0 0 0 0 1 10 0 3 10 0 3. 14. 5.0 7 STATICA BLCCKAGE CISTRIBUTION FACTOR

> 1 J . 1.0 5 1.7700 2 0.0 (... 1.3016 3 3.0.05 1.0365 0.0.000 1.0000 . 75%. 0.0903 .02761 0.0000 . . 500 1.0660 6 ·13000 1.3600 9 . . 54 ' L 1.5662 . . . 4 . . 1.5600

# SCLUTION TYPE INUTGATORS

STATICN 1 2 3 4 5 6 7 8 9 10 NMACH 1 1 -1 -2 -3 -1 -1 -1 -5 -3

```
Test 208300315990
```

```
1.
    14.2770
               15.0
                       30.0
               11
     0
                0
                        0
               10
                        0
               10
                        0
3.
     2
               14
                        5.0
                               1
4.
    STATION
              BLCCKAGE DISTRIBUTION FACTOR
               0.00000
                                  1.0000
       1
       2
               0.00000
                                  1.0000
       3
               0.00000
                                  1.0000
               0.00000
                                  1.0000
```

#### .07700 6 .08000 .8500 7 .10000 1.0000 8 .12700 1.0000 .05400 9 1.0000 10 .05400 1.0000

#### SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

## WITHIN-BLADE ONLY

- 5. 2 11 0 2 11 0 2 11 0 2 11 0 4 11 0

## OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

-9.2700 -4000 -10.3000 -6000 -14.3000

```
OUTLET RADIUS = 7:9180 -----
     "M-COORD "DEVIATION-ANGLE" (DEGREES)
       .4000
               -9.6500
      -17.0000
OUTLET RADIUS = 8.6599
     M-COORD DEVIATION TANGLE TOEGREES)
      .4000
               -10.1500
     · · 6000 ~ · · · · · -13.5000 ~ · · · ·
       .800ō
              -17.0000
STATOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 5 POINTS
     M-COORD LOSS COEFF/TOTAL LOSS COEFF
                0.0000
      0.0000
     1.0000
OUTLET RADIUS = 0.0000 " ' " ' "
   M-COORD DEVIATION ANGLETT (DEGREES)
      0.0000
       .2000
                 .1100
                 71500
       .4000
               •2200
       .6000
       8 30 0
      1.0000
                1.0000
NUMBER OF TEST POINTS TO BE ANALYSED = 1
PSCALE = 1.50 P_OHER = 14.00 JAMPF = 5.000 NSAVE 1 NEX = 2
```

#### STATION 3L OCKAGE DISTRIBUTION FACTOR 0.00000 1.0000 0.00000 2 1.0000 3 0.00000 1.0000 1.0000 4 .01000 5 .01000 1.0000 6 .01500 .5000 7 .02000 •5000 .2000 8 .02300 9 .01900 0.0000 10 .05000 .5000 11 .07000 1.0000 12 1.0000 .08500 13 .10000 1.0000 14 1.0000 .11000 15 .06000 1.0000

## SOLUTION TYPE INDICATORS

.08000

.05400

16

17

1.0000

1.0000

		SS
7.	POSITION NO.	PRESSURE(PSIA)
	<b>.</b>	11.172
	2	11.332
	3	17.515
	.₩	18.119
	5	≥0 <b>1</b> 8
	р	23.494
	7	21.988

PS 23.276 2 23.361 25.541

```
14.277
                    30.
2.
     4
              11
                     0
                     0
     0
               0
              10
                     0
              10
                     0
3.
     2.
                     5.0
                           1 2
              14.
    STATION
              SLCCKAGE DISTRIBUTION FACTOR
               0.00000
                                 1.0000
       1 .
                                 1.0000
       2
               0.60606
                                 1.0000
               0.00000
       3
                                 1.0000
               0.00000
                                 .8500
                .67000
       5
                                 .8500
       6
                .07000
                                 1.9000
       7
                .10000
                                 1.0000
       8
                .12800
                .0540G
                                 1.0000
       9
                                 1.0000
                .05400
      10
```

## SOLUTION TYPE INCICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

## Test 208300415890

1.	14.277 4 0	15. 30 11 0 0 0	•
	i	10 0	
	3	10 0	
3.	2.		.0 1 2
4.	STATICA	BLCCKAGE	
	1	0.00000	1.0000
	2	0.00000	1.0000
	3	0.00000	1.0000
	4	0.00000	1.0000
	5	•0750 U	.8500
	ь	.07500	. 9000
	7	.16060	1.0000
	8	.14400	1.0000
	9	• 05400	1.0000
	10	• 05400	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 6 -0 -0 -0 -0 -0 -0 -0 -0

```
14.277
               15.
                       30.
2.
      4
                11
                        0
      0
                0
                        0
                10
                        0
                10
3.
      2.
               14.
                        5.0
```

4. STATICN BLCCKAGE DISTRIBUTION FACTOR

1	0.00090	1.0000
2	0.66006	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.36000	.7300
6	.96000	.7000
7	.16000	1.9900
8	•16000	1.0000
9	•0540G	1.0000
10	•0540 U	1.0000

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 +0 +0 +0 +0 -0 -0 -0 -0 -0 -0

## Test 208300615090

```
1.
    14.277
               15.
                      30.
2.
     4
               11
                      0
     0
                0
                       0
               10
                       0
     1
     3
               10
                       0
     2.
                      5.0
3.
               14.
                             1
                                  2
    STATICA
              BLCCKAGE DISTRIBUTION FACTOR
```

0.00000 1.0000 1 2 0.06000 1.0000 3 0.00006 1.0000 0.00000 4 1.0000 5 . 372 û û .6000 6 .07200 .6500 7 .10000 1.0000 8 .19400 1.000G 9 .05400 1.0300 .05400 1.0000

## SCLUTION TYPE INGICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

```
14.2770
                15.0
                        30.0
                11
                         0
       0
                 0
                         0
                10
                         0
                10
                         0
 3.
                14
                         5.0
                              1 2
      STATION
               BLCCKAGE DISTRIBUTION FACTOR
                0.00000
                                 1.0000
         1
         2
                0.060CL
                                 1.0000
         3
                0.00000
                                 1.0000
                0.06000
                                 1.0000
         5
                 .26646
                                 1.9606
                 . 60000
                                 1.2500
         7
                 . 67500
                                 1.0000
         8
                  .1750 G
                                 1.0000
         9
                  .0540D
                                 1.0000
        10
                 .05400
                                 1.0000
      SCLUTION TYPE INCICATORS
                 2 3 4 5 6 7 8 9 10
      STATION 1
                 0 -0 -1 -1 -6 -6 -0 -0 -6
      NMACH
 WITHIN-BLADE ONLY
      2
. 5.
                11
       2
                11
                         0
       2
                11
                         0
       2
                11
                         0
                11
 6.
     ROTOR GÉNERALISEU PERFORMANCE
                                       LOSS 2 POINTS DEVIATION 4 POINTS
               M-COORD LUSS COEFF/TOTAL LOSS COEFF
                0.0000
                                 0.0000
                1.0000
                                 1.0000
     OUTLET RADIUS = 7.5499
                         DEVIATION ANGLE (DEGREES)
               14-00031
                 .2000
                                -9.5000
                 ...4ú0.J.
                               -13.5000 -----
```

-16.0700

-19.0000

.6000

.3000

```
OUTLET RAJIUS = 7.9180
 ---- A-COURD DEVIATION ANGLE (DECREES)
    . 4000
                 -12.0000
   . 6000
                 -19.0000
OUTLET RADIUS = - 8.6699.....
      M-COORD DEVIATION ANGLE DEGREES)
        . 4000
                  -12.7000
        •6000 - ~ -15.0000 ....
        .8000
                  -19.0000
STATOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 6 POINTS
      M-COORD LOSS COEFF/TOTAL LOSS COEFF
       0.0000
              0.0000
    --- 1.0000 · · · · 1.0000 -
OUTLET RADIUS = .... 0000 ....
      -M-COORD DEVIATION ANGLE (DEGREES)
       0.0000
                  - .1000
        .2000
                    .1100
        ..4000------1500-----
                   .2200
        . 5000
        .8000
                   .3800
       1.0000
                   1.0000
NUMBER OF TEST POINTS TO BE ANALYSED = 1
PSCALE = 2.00 P.OWER = 14.00 DAMPF = 5.000 NSAVE = 1 NEX = 2
```

```
STATION BLOCKAGE
                   SCICAR NOITUEISTEIG
          0.00000
                            1.0000
. .. 2...
        ---0.0000.0-
                           --1-0000
   3
          0.00000
                            1.0000
  4
          . 41000
                            1.0000
  5
           .01000
                            1.0000
  б
           .01500
                            .5000
  7
           .02000
                            .5000
  8
           .0200C
                          ----2000.
  9
           •019ûu
                            0.0000
```

.5000

.07000 1.6000 12 .09+00 1.0000 13 •11800 1.0000 14 •1500 Q. .. 

•05000

15 000000 1.0000 10 • 6 S O O U 1.0000 17 • 8 >+ Ů Ū 1.0000

# SOLUTION TYPE INDICATORS

10

11

STATIUN 1 2 3 4 3 9 7 8 9 10 11 12 13 14 15 16 17 NMACH 0 -0 -0 1 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0

7.	POSITION NO.	SS
		PRESSURE (PSIA)
	1	11.191
	2	13.396
	<u>ક</u>	17.516
	<del>4</del> ဗ်	18.325
	•	19.531
	່ 7	19.926
,		25.359

PS 1 25.7)3 2 26.749 27.136

```
1.
    14.277
               15.
                       30.
2.
      4
               11
                        0
      0
                0
                        0
      1
               10
                        0
      3
               10
                        0
      2.
3.
               14.
                        5.0
                               1
    STATION
               BLCCKAGE
                           DISTRIBUTION FACTOR
                6.00000
        1
                                    1.0000
        2
                0.06003
                                    1.0000
        3
                0.00000
                                    1.0000
        4
                0.60000
                                    1.9000
        5
                  .01600
                                    1.9000
        6
                  .03500
```

#### SCLUTION TYPE INDICATORS

. 45000

.18400

.05406

.05400

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 3 6 -0 -0 -0 -0 -0 -0 -0

1.0000

1.0000

1.0000

1.0000

## Test 208301115500

7

8

9

10

- 1. 14.277 15. 30. 2. 4 0 11 0 0 0 1 10 0 3 10 0 3. 2. 14. 5.0 1 2 4. STATION DISTRIBUTION FACTOR BLCCKAGE
  - 0.00000 1 1.0000 2 0.00006 1.0000 3 0.00000 1.0000 0.00000 1.0000 5 0.00000 1.0000 6 .02100 2.0000 7 .05000 1.0000 8 .19700 1.0000 . . 05400 9 1.0000 10 .05400 1.0000

#### SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0

```
1.
    14.277
              15.
                     30.
2.
              11
                      0
     0
               0
                      0
              10
                      0
     3
              10
                      0
3.
     2.
              14.
                      5.0
                             1
4.
    STATION BLOCKAGE DISTRIBUTION FACTOR
       1
               0.00000
                                 1.0000
       2
               0.00000
                                 1.0000
       3
               0.00000
                                 1.0000
       4
               0.00000
                                 1.0000
       5
               0.00006
                                 1.0000
       6
                002500
                                 2.0000
                .0500C
                                 1.0000
       8
                .22800
                                 1.0000
       9
                .05400
                                 1.0000
      10
                .05400
                                 1.0000
```

## SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 2 0 -0 -0 -0 -0 -0 -0 -0 -0

### APPENDIX C

### MODIFIED PROGRAM LISTINGS

This appendix presents listings of new and modified computer routines used in conjunction with the programs of References 4 and 5 to reduce the experimental test data.

# 1. PHASE I - SUBROUTINE TPRED

	-GXST-T-COT-NT-COMEN-T-R-ANTMA-ALIGE GOOD - GIVE - GIVET - GIV	40	-
	2	TPR	1
	IVOLT	TPR	~
16	(2,0) (A(1),A(512))	TPR	m
	2)) 10,	TPR	<b>.</b>
10		TPR	w.
	IF (NN.LT.2) WAITE (6,45)	TPR	တ
	60 TC	TPR	٠,
	<b>+</b>	TPR	<b>50</b> (
		TPR	ָר פּ
	10	4	70
	(1,55)	40	1
	READ (1,55) N2	1 PR	15
		1PR	13
	ANS=N2	TPR	14
	AMCD=AN1+1 0. + + 9+ AN2	TPR	12
		1 2 1	9 !
	IF (LSKIP.EQ.0) 60 TO 15	7	11
	HCJ (I)	1PR	8 .
	JMCJ(1).LT.NTEDE) GO TO 5	7 E	5 (
	(NUMCD(1).GT.NTEDE) CALL E	1 P.R	20
	(NUMC)(1).61.NTEDE) LERJR=1	TPR	21
	(1) .GT.NTEDE)	1 P.	22
15	CONTINUE	TPR	53
		-PR	54
	WRITE (1,50) (A(J),J=3,NW)	TPR	52
	REWIND 1	TPR	52
	ENW/2-1	7 P.	27
	Z	- I	9 0
	J=1, NC	4 d l	621
		7 1	ء د
	(1,70) CHAR, I	7 1	1 C
	(CHAR.EQ.PLUS) 6	- t	2 1
	IF (SHAR-EQ.AMINS) IVOLT(I, J) =-IVCLT(I, J)	- H	0.
20	Ľ	- + F 0	† u
,	•	- F	2 6
C,	יירור האמלי (ש) יירור האמלי (ש)	TPP	37
	רבהטלון	100	. W
	00 DE 000	TPR	6
30	10 N C C C C C C C C C C C C C C C C C C	TPR	1
<b>u</b>	U OI DO	TPR	4
2		40	2
	ACIUCA T (1.1.Y. T.1.2)	TPR	i M
ي د ج		TPR	‡ ‡
) C	(410)	TPR	Ę
י נה יוי	(110)	TPR	10 10 10 10 10 10 10 10 10 10 10 10 10
1 10		TPR	44
6.0	(7×,13)	4	<b>9</b>
70	FORMAT (2x, 41, 16, 11)	401	<b>5</b>
		F.	20-

### 2. PHASE I - PROGRAM INPUT

```
INTEGE ZPT9_ZTYPE

UNFECE ZPT9_ZTYPE

UNFECE ZPT9_ZTYPE

UNFECE ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTYPE

UNFEC ZPT9_ZTY
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              LINT TOL.

GOMNO'! R,RA,LAD, RCONV,RECOV, RELH,RHUB,RPH,RTIP,RV,SPEED,SRAD,STOP, INP

LSTD; TCTE; JOAT; TDATA,TEDAT; TEF, THETA,TOLMS,TOPT; TORT; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST; TOST
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       DIMENSION WAGT(1), WGORK(1), WSPCO(11), WINT(1), X(20), ZFEGI(1), 1ZFAGZ(1), ZPRES(20), ZREG(20)
UINENSION BHALS(1,12), UHALA(1,10)
DIMENSION INTGG(5), PCAL(1,0), PATH(1,5)
COM 40N IN, IVOLT, IEXP
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       AGAO (5,455) NR, ISGT, NREAL, NPNCH
WKITE (5,455) NR, ISGT, NREAL, NPNCH
GO TO (20,45,180,130,195,15), ISET
CALL ERROR (1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     (TCTEF(K), K=1,NPTEF)
(TEF(K),K=1,NPTEF)
NUPTS,MTYPE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              LPTS,NVTYP
(TEDAT(K),K=1,LPTS)
(APDAT(K),K=1,LPTS)
X1,X1A,X1B,X2
B,UI
CQ,C1,CZ,C3,G,Z
HPTS,NMTYP
(BETA(K),K=1,MPTS)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                IF (NJ1-1) 10,10,5
WRITE (6,490)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                NPTEF
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  (5,455)
(5,450)
(5,450)
(5,460)
(5,460)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                (5,409)
(5,425)
(5,460)
(5,460)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            (5,455)
(5,455)
(5,450)
(5,450)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       LEROR=1
60 TO 450
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       READ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  READ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   READ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     READ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              6 4
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              12
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            20
```

```
(TCTEF(K), K=1,NPTEF)
(TEF(K),K=1,NPTEF)
NUPTS, MTYPE
(CALBM(J), J=1,NUPTS)
(RECOV(J), J=1,NUPTS)
                                                                                                                                                                                         LPTS,NVTYP
(TEOAT(K),K=1,LPTS)
(APDAT(K),K=1,LPTS)
X1,X1A,X1B,X2
8,01
                                                                                                                                                                                                                                                                                                                                                                                                 ZPREF
ZPTS, ZTYPE
(ZPRES(K), K=1, ZPTS)
(ZREG(K), K=1, ZPTS)
KPTS, NKTYP
(EQTEM(K), K=1, K?TS)
(OPT(K), K=1, KPTS)
                                     ZPIS,ZTYPE
(ZPRES(K), K=1,ZPIS)
(ZREC(K), K=1,ZPIS)
KPIS,NKTYP
(EQIEM(K), K=1,KPIS)
(DPI(K), K=1,KPIS)
                                                                                                                                                                                                                                                          CQ,C1,G2,C3,G,Z
MPTS,NMTYP
(3ETA(K),K=1,MPTS)
(82K(K),K=1,MPTS)
NPTEF
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      NSC=NSCX(NSCV)
READ (5,455) (II(NSCV,K),K=1,NSC)
MRITE (6,455) (II(NSCV,K),K=1,NSC)
(GALBA(I), I=1, NUPTS)
(RECOV(I), I=1, NUPTS)
ZPREF
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     (MCPCO(J), J=1, NMCPC)
                                                                                                                                   READ (5,470) (AGPGO(J), J=1,NACPG)
READ (5,455) NWGPG
READ (5,470) (MGPGO(J), J=1,NWGPG)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             (ACPCO(J),J=1,NA3PC)
NHGPC
                                                                                                                                                              (NCPCO(J), J=1,NMCFC)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           READ (5,455) NTCV,NTCX(NTCV)
WRITE (6,455) NTCV,NTCX(NTCV)
NTC=NTCX(NTCV)
READ (5,455) (I2(NTCV,K),K=1,NTC)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             READ (5,455) NSCV,NSCK(NSCV) WRITE (6,455) NSCV,NSCK(NSCV)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            READ (5,455) JT
WRITE (6,455) JT
DO 46 JR13 JT
IF (J-2) 35,38,35
KRITE (6,498)
          KITE (6,475)
                                                                                                                                                                                            (6,455)
                                                                                                                                                                                                          (6,460)
                                                                                                                                                                                                                      (6,460)
                                                                                                                                                                                                                                     (6,460)
                                                                                                                                                                                                                                                   (6,460)
                                                                                                                                                                                                                                                                (6,460)
                                                                                                                                                                                                                                                                             (6,455)
                                                                                                                                                                                                                                                                                           (6,460)
                                                                                                                                                                                                                                                                                                        6,460)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          MRITE (6,455)
MRITE (6,470)
READ (5,455)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         (6,470)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           (6,495)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 2
```

318

	MRITE (6,455) (IZ(NIGV,K),K=1,4IG) READ (2,455) (IZA(NICV,K),K=1,NIG) WRITE (6,455) (IZA(NICV,K),K=1,NIG) REAG (5,455) NUATA(NICV),KIYTE(NICV)		121 122 123 124 125 125
	NDA(JENDALE(NICV) NDA(JENDALC) ARITE (6,4e0) (VDATA(NICV,K),K=1,NDATC) ARITE (6,4e0) (VDATA(NICV,K),K=1,NDATL)	S I I I	127 128 128
	READ (5,450) (TDATA(NTCV,K),K=1,NDATJ) ARITE (5,460) (TDATA(NTCV,K),K=1,NDATJ)	d NI P D	129 130
t t	CONTINUE	UNI P P	131 132
;	MAITE (6,490)	d N L	133
	+55) JREON, HTAP, KREON, VRAKE, NTAP,	N N	135
	(6,45)	A A	136
	WRITH (69-40) SPEND ANDRA NATIO	O NI	133
	66,46	d N	140
	59450	S N	141
	5,450	ON I	143
	MRITE (6,+63) (SRAD(J),JHI,NTAP) Annihatip-falia	N N	144
	00 50 J=1,NTAP	N N	146
016	) = (SH40 (J)	S S	147
	ATTO (5,460) STOP,STOT,RA,2V,RCONV	N N	149
	5 I=1,16	H	150
	3	N N	151
	30 TO (55, 60, 65, 70, 75, 80, 85, 90, 95, 100, 105, 110, 115, 135, 140, 145), L	~	
52	ī	d i	
90	10=NO-	d N	
65	IF (NOL) 155,155,150 NOTPJENO.	N N	
3	IF (NOL) 155,155,150	N.I.	
70	NORIJ=NOL IF (NOL) 155:155:150	d N	
15	SJ=NOL	A S	
80	IF (NOL) 195,135,136 NOSTJ=NO.	d NI	
¥	IF (NOL.) 155,135,150 Modeleno	O N I	
	IF (NOL) 155,155,150	d N	
06	NOVAJENO. TF (NO!) 155.135.130	A A	
96	SJ-NOL	Z	
9	155,	O X	
•	(5,400)	Z	
4	MRITE (5,460) (X(X),K=1,NUL) IF (NOL) 155,155,150 NOBS:	L Q Q	175
	IF (NOL) 155,155,150	d Z	
110	NOƏPJ=NO. IF (NOL) 155,135,150	LAN	
115	WUCAJ =NOL	U Z D	

	DO 130 J≖1,JJ		191
- (	IF (J-3) 125,120,125		182
) (C	AT IN (09490)		7 .5 1 0 T
,	455)		185
	(6,455)		186
	READ (59459) (ICALF(5,K),KH1,NOCA)	L A	188
130	NUE		189
,	GO TO 153		190
135	70545.80. TR (NO.) 155.155.155		161
140	CY16671667		193
!	IF (NOL) 155,155,150		194
145	NOATENO.		195 196
150	55) (ITPR(L1,K),		197
	WRITE (6,455) (ITPR(L1,K),K=1,NOL)		196
155	CONTINUE DEAD GELEES TWODE	N A	199
	(6,455) (6,455)		201
	(5,455)		202
	WALTE (6,455) JOUR	d a	203 204
160	AFAD (5.435) NLPIS.KTYPE		205
	WRITE (6,455) NLPTS, KTYPE		506
	READ (5,460) (VDAT(K),K*1,LPTS)	2 2	702
	RKIIK (OP400) (VURICK) PRIPARTIO) READ (Setso) (TOAICK) FRIPAS)		502
	WRITE (6,460) (TDAT(K), K=1,NLPTS)		210
	175		211
165	NEPTMENDATA (JOUR)		212
	00 170 KaleNFPTS		214
	VDAT(K) = VDATA(JDUM, K)		215
170	TOAT(K) = TOATA(JOUM,K)		216
17.2	CONTINUE		717
9 6 7	#\$1TE (6.465)		213
	5,455) (IATGG(K),	AN	220
	WRITE (b)455) (IATGG(K),K*1,403AJ)		221 223
	) 1-19RK (5.460) (PSI(I.K).		223
	460) (PSI(I,K		224
165	CONTINUE	A A Z	225
•	TOLMS, PPRTL, PTTO		227
- (	(6,460)		228
135	CONTINCE DO 200 1x1.NR		230
	SKIP. EQ.	dNI	231
•	GALL IPREU (LSKIP)LEROK,PLUS,AJINS,F,1,NUMCU,IN,1VULI,IEKP,NU,MIEU 18)	LUL	233
200	8		234
	DO 215 I=1,N2 DO 215 JE1,NC	N N	235 236
	IF (IN(I,J)-INRPH) 210,205,210		237
205	RPH(I)=FLOAT(IVOLT(I)J))+10. VOL'IS(I,J)=RPH(I)		238 239
	60 1'0 215	N D	240

200	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	200 11.00 10	
NININININININININININININININININININI			
	PSCAN(LL, KH1) = VOLTG(I, J) GO TO 230 CONTINUE CONTINUE NN=NN+JT NNV=NN+JT-1 NNV=NN+JT-1 NNV=NN+JT-1 NNC=NTCK(L) NO 245 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC DO 246 KH1=1, NTC	TEMP(L, KHI) = VOLTG(I, J) GO TO 245 CONTINUE CONTINUE CONTINUE IF (NOAT4) 290,290,250 CONTINUE DO 265 K=1,NOAT8 KK=ITPR(16,K)/100 NADAI=0 OO 260 J=1,NOCAJ JINTEK+(I-1)*JJ IF (IATG(J)) 260,255,26 NADAI=NADAI+1 ICALJ=(ICALP(KK, J)-KK*10 XDATA(NADAI)=PSCAN(JINT, YOATA(NADAI)=PSCAN(JINT, YOATA(NADAI)=PSCAN(JINT, YOATA(NADAI)=PSI(I, J)	
215 215 .	225 230	25 25 25 25 25 25 25 25 25 25 25 25 25 2	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

290	00 295 J=1,NOCAJ PCAL(I,J)=PSI(I,J)		301
305	CONTINUE CONTINUE MAINTENAME	ZZZ	1 to 0
	1117		300
	11, NC		308
310	<pre>IF (IN(I,J)-INOOP) 315,310,315 xoum(1)=volt6(I,J)</pre>		310
315	₹ 2		311
	CALL DR (#104;) DR; MRIS; YOUN, YOUN, 1, NKIYP)		313
	OUPTT(I)*XDUM(1) DO 320 JJP=1.4		314 315
320	VENPR (I , J.) P) #0		316
	てつ ・ ア・ ア・ ア・ ア・ ア・ ア・ ア・ ア・ ア・ ア・ ア・ ア・ ア		318
	00 340 L=N,NV		319
	NEL=L=JJ*(1=1) 00 325 K=1;NOCAJ		321
			322
325	YDATA (K) *PCAL (I, K)		324
	NSCHNSCX(KLL)		325
330	NOUNCK) =PSCAN(L,K)		327
	NITY HETYPE (KILL)		328
	OF 335 K=1,NSC		330
335	PSCAN (L, K) =YDUM(K)		331
3 + 5			333
	BNN+CT-1		334
	DO 365 L=NN,NNV		335
	AFE (- ) ( ( T - 1 ) ATOTH NTCK (KL )		337
	NOATU #NOATA (KL.)		336
372	DO 345 XH19NTOT		333
n	00 350 K=1,NDATJ		341
	XDATA (K)=VDATA (KL,K)		345
350	YORTA (K) HIDATA (KL»K) NTTHNITYTH (KL)	L C	りまり
	CALL DN (XDATA, YDATA, NDATJ, XDU4, YDUM, NTOT, NTT)		345
4	OO 3555 KRIPATOT TERBO. (X)=YDUM(X)		340
}	00 360 KM1=1,NTOT		348
4	JKL=I2A(KL,KM1) Temos (I, K)) +ISMB(I, KM4)		340
365			351
370	CONTINUE CON		352
	60 70 (375,380,385,390,395,400,405,410,415,420,425,430,445,435,4		354
375	1), L NL≃0	Z Z	355
			357
	AFFO		359
360	H=1		300

### DALL ALLOT (NOPTJ, TEMPA, M, NR, TOPT, ITPR, L, JT, ML)  ###################################

# 3. PHASE I - SUBROUTINE OUT

```
SUBSECT TYPE

SUBSECT OF THE STATUS OF THE STANTON, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TATAVICAD, TAT
```

	WRITE (6,340) (PCAL(I,K),K=1,NJCAJ)	100	19
	WRITE (b, 345)	96	2 5
	IF (NOPLI-NOPPJ) 55.55.50	5	9
50	UNDER OF L	90T	65
55	SO J=1, NOUNJ	5	99
;	IF (4-NOPJ) 65,65,60	2 5	۵:
9		3 8	9 0
92	IF (J-NOF) J) 75,75,70	5 8	P 6
2;	:	3 5	2 7
C	CONFICENCE TANDA	5 5	12
	CONTINUE OF TABLE TO FOREST IN CORPUS TOP TO THE TABLE OF TABLE TO TABLE TABLE TO TABLE TO TA	5	, F.
0	711111111111111111111111111111111111111	50	4.
	355)	100	25
	360)	90	92
	IF (NOATA) 90,90,85	OUT	11
92	365)	901	78
	WRITE (6,370) (J,PATH(I,J),J=1,NOATH)	- S	62
;	WALTE (6, 295)	000	
0			1 0
4	۳ م	001	) PO
100	MRITE (6,375)	901	40
	## <b>X</b>	901	85
	LTAP=HTA>	<b>100</b>	96
105	DO 110 JC=KaLTAP	100 1	84
	-LTAP+MTAP	100	10 (
	WRITE (6,380) JL, TORT(I,JK), TOPPR(I,JK), RAD(JL)	הלים הלים הלים	60
110	•	3 8	3 3
	125,115	3 5	1 6
115	7	3 5	) P
-		50	3
	E112 (6, 365)	3	93
	GO TO 105	OUT	96
125	CONTINUE	00 T	97
1	WRITE (6,280)	100	96
	(6,3	3	66
	LQ*0	56	D 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	M 1	3 5	101
	PRINTE.		707
	7 JEKSTIA 16.295)	500	104
		100	105
	(6,320)	100	106
	_	DOL	101
	ĭ	100	103
	LN=J	5	109
130		5	
	DO 185 LEL PRAKE	3 5	111
135		(TOOT)	113
,	ARHO (I, LL), AMACH(I, LL), AV(I, LL)	. ;	114
	MRITH (6,410) TOBAV(I,LM),PONAV(I,LM),GV(I,LM),GAMAV(I,LM),CMACH(I	TOOL	115 116
	41.	90	117
140	IF (NNOUL) 145,145,160	100	116
18	CNS C+ SRACE + STAP		119
		3	150

121	122	123	124	125	921	721	129	130	131	132	133	134	100	120	133	139	140	141	145	143	144	145	91		0 C	,	17	152	153	154	155	156	157	120	15.4	161	162	163	164	165	1001	168	169	170	171	172	173	175	176	177	179	180
00T	100	g	20	5	5	3 8	000	Pno	9	P	3	5		3 5	25	OUT	9	등	5	100	100			3 8	5 6	3 8	3 5	9	9	티	<b>00</b>	OCT OCT	S	3 8		i a	9	OUT	5	58		OUT	50	OUT	OUT	OGI		100	OUT	5 5	95	100
												:	3					HA							;	C E					2																					
										₹			Y MUDBLY NOORS		X			(K,UWALA(I,K),X1A,K=NOUWK,NOUWA)	:	, AMALS(1,K), X(<), K=1, NJAMJ)			3		2	• X TO • K = NOO MY • NOOM • )		2	•		-NOONK, NOON-																					
										3 9 2			CAR.		DON.	•		S X		1, NO		ì	202		3			NOON			DKK,			:	Ŝ	6	•		;	ŝ												
										(K, UWALS(I,K), X1, K=1, NOUWK)		1	N M Y		.X1A.K=1.NOUMK)			X IIX		, X		•	,X13,K=1,NODWK)		3	¥ .		K=1.NODWK)	ì :		¥			2	K, BLASP(I,K), K=1,NOBSJ)	(K. PBLAP(I.K), K=1, NOBPJ)				=1,NOVNU)												
										, X 1,		;	9 X 19		. X 1A			, X 1A		××		•	, X 13		,	, X 13		. X 2.			, x 2,			3	, K = I	KEİ			•	¥=1												
										I,K		•	197		Ğ.	•		1,8		1,4		•	1 , K)		5	198		I.K			Š			Ś	3,5	Z, K			:	ENPR(I,K),K			•			Ι,Κ		190				
										ALS(			201		ALAC			LAC		ALS (		(	נרציכ			12		OWALSCIAN			, DWALS ( I				SPC	AP				2 2 2						SP (	•	90,185				
		5,160					•			YOU'S			(K,UAALS(I,K)		(K.UMALA(I.K)			Y OH		C, AN		;	(K, BYFLS(I,K)			(K) BMALS (T) K)		/HO * 3			C, DH			i	36.	Pai	i :		•	~						IK, OMXSP(I	8	1909				
:		5,155,		:	2		_	: .:						2 5			. ++			<b>3</b>	<u> </u>			÷.			2 2	¥ 2		÷	3	=	<b>:</b> :	٠	_			æ		ક ::	2 2	•		TAP	AP.	<b>≘</b>	•	1,00				
.385)	30	1551		1	(6,260)		5.280)			6,420)	6,425)	#+XMCON#	69 4 203		6.420	(52)	NOUNT - NOUNT + 1	(6,450)	1,435)	6,420	69 440)	=N03MJ/2	(6,420)	(69 4 25)	NOCATANOUANT OF	(02+69)	/C++69) 3113M	(6.4.20)	425)	T+XHCON=XHCON	6,420)	6,450)	6,455)	69460)	6, 465)	5.465	6.280)	6,475)	6,460)	6,465)	6,480	A - CA		1,0=	IK=K+NTA9-LTAP	9465	ŝ		WRITE (6,385)	TAP	, <del>p</del>	
_	-	(LQ)	1+0			CUSCLET.	₹~		ž	_	9	) = N	ָ ֖֖֖֭֭֭֭֭֓֞֞֝֞֞֞	ב ב ב		_	X=X		_	_	اد	\     		֓֞֞֜֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓	ZI V		1	֓֞֝֝֝֞֜֜֝֝֓֜֝֝֓֓֓֓֓֓֡֓֜֜֜֜֓֓֓֓֓֡֓֜֜֜֓֓֓֡֓֡֓֡֓֡		X=X	9)	_	<b>.</b>	<b>.</b>		-		_	•	•	-	<b>,</b>		7 5 K	+NTA	Э Э	CONTINUE	A KRIC	9	TAP= 2*N	50 13 170	CONTI NUE
HRIT	50 53	11	11	00	1 K		WRITE	HRITE	NOU.	WRI TE	KRIT	YNON	14 L	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	KRIT	HRI TE	S	WRIT	ARI TE	WRIT	HRIT	200	WRI T	HKI T		#41 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	127	22.7	WRITE	KOON	REIT	WRIT	112	171	MAI LE	WET.	#RIT	HRIT	WRIT	HRIT TIT	174	LTAPENT	1	00 1	IK=X	#RIT	CONT	- L	WRIT	LTAP	500	CONT
		0	מו	,	-	u	•																																					0			ın					
		Ē	'n	•	160	•	7																																					17			17	*	135			130

	WRITE (6,485) TOLMS,PPRIL,PITO. CALL BADPI (NRAKE,NIAP,THETA,TJTPS,TOST,KREDM,I) WRITE (6,490)	100 100	181 182 183
4	IF (NPNC4) 265,265,195	500	184
•	WRITE (7,493) NUMCO(I)	5	106
	WRITE (7,500) GASK(I), AMASS(I), WCORR(I), CORN(I), STOP, STOT	3	187
	WRITE (7,505) MTAP	3	189
	DO 205 K=1,MTAP	5	190
	1041A(K)=1041(1,K)	5	191
			192
200	CLEX+ETA	5	194
	T(I,JL))/2	100	195
	TOP 24 (K) = (TOPRA(K) + TOTPR(I, JL)) /2.	00T	196
202	CONTINUE STATES	בוס דופ	197
	DO CLO RELEGIENT HETT: (7,540) DANCED TOPOACED		961
0 12	NITOTOL AND NATIONAL PROPERTY.	5	200
	WRITE (7,505) HIAP	901	201
	DO 215 K=1,MTAP WOTTE / FESS DAD/S TODIA/S	00.	202
215	CONTINUE	3	204
}	MRITE (7,505) NTAP	100	205
	DO 225 K*1,NTAP	100	206
	PSTAV (K) = POSAV (I, K)	50	207
	ISTAMINATIONAMILAND TE CERENA 000,000,000		0 0 0 0
220	THE CANADA CONTROL OF THE CANADA CANA	000	210
!	PSTAV (K)=(PSTAV(K)+POSAV(I,JL))/2.	001	211
	T3TAV (K)=(T3TAV(K)+T03AV(I,JL))/2.	00T	212
<b>522</b>			213
	IF (KRED4) 2+0,2+0,230	ğ	215
230		<b>001</b>	216
216	IF (DMXSP(1,K)-DMXSP(1,JL)) 235,240,240 DMX=DMXS2(1,H)	35	217
637	GD TO 245	3 5	570
240	DMX=DHXSP(I,K)	3	220
542	WRITE (7,510) SRAD(K),P3TAV(K),DMX	OUT.	221
250	CONTINUE	100	222
	MRITE (75005) NIAP		223
	WRITE (7,510) STAD(K), T3TAV(K)	5	225
255	CONTINUE	3	226
	NEW-CONTRACTOR OF THE CAMPACTURE AND THE CAMPACTURE		777
	(7,510)	5	229
	(7,510)	5	230
	NON 6 T	5	231
26.0	MRIII ('9316) X(R) AMALS(L)R) CONTINUE	3 2	233
•	510)	OUT	234
	(7,510)	25	235
	(7,505)	3 5	237
	(7,510)	20	238
	EXII: (7,510) XIA,PINER(1,4)		24.0
	(a) ( ( ) ( )	3	<b>*</b>



			001 285 001 285 001 285 001 285 001 286 001 289 001 291 001 295 001 295
NI), VOLTS(I,NI), IN(I,N2), VOL , VJLTG(I,NC)	COMPRESSOR DATA REDUCTION  + + + + + + + + + + + + + + + + + + +	L9/SEC,/,21H GORRECTED-F MTESRATED FLOW RATE(STAGE LOW RATIO(CORRECTED FLOW) SPEED=, 9f10.3,5H 3PHS,/23 23H PER CENT DESIGN SPEED 4 DEGRES,/19H RELATIVE H 5HSPECIFIC HEAT RATIO(HIX 57.4.1HF7.4.1HF7.4.1HF7.4.1H.	0SITION,5%,14HPRESSURE(PSI (E(GE3 2),5%,14HCORRECTEO T (E13%,F7.3) (ITHHETIC) = ,F7.3,16H DEGRE (ITHHETIC) = ,F7.3,5H PSIA,///) (SUREWENTS ,/,20%,8HPOSITI (SUREMENTS ,/,20%,8HPOSITI (SUREMENTS ,/,20%,8HPOSITI (SUREMENTS ,/,20%,8HPOSITI (SUREMENTS ,/,20%,8HPOSITI (SUREMENTS ,/,20%,8HPOSITI (SUREMENTS ,/,20%,8HFOTAL TEH (SUREMENTS ,/,20%,17HTOTAL TEH (SUREMENTS ,/,20%,17H
10) X2,PINER(I,2) 15) ,IC 20) IN(I,N),VOLT3(I,N),IN(I, IC) IC+1) WRITE (6,520) IN(I,NS) IC+2) IC1=NC-1 IC+2) WRITE (6,520) IN(I,IC)	AF ~ ARL(LF) SUPERS  * * * * * * * * * * * * * * * * * * *	16=959. 18014 350-14 354 3PH 1954 3PH 106=953 11015-19	CALLBRAILON FRESSOR (7.4) 14) 17.4,14) 17.4 1. 14. 17.4,14) 17.4 1. 17.3,113,57.3 12.9X, F7.3,11X, F7.3 15X,3344VERAGE TEMPE 13. 4THOSPHERID PRE- 13. 4THOSPHERID PRE- ESSURE (PSIA),7) 12.9X,512.4,7 12.9X,512.4,7 12.9X,512.4,7 12.9X,712.4,7 12.9X,712.4,7 12.9X,713.4,7 13. STAGE OISCHARGE AND RECOVERY RAIIO 17. 17. 17. 17. 17. 17. 17. 17. 17. 17.
WRITE (7,5 CONTINUE CONTINUE CONTINUE ICENC/3 N==2 N==2 N==2 N==2 N==3 N==4 N==4 N==4 N==4 N==4 N==4 N==4	16(1,NC) CONTINUE RETURN FORMAT (1H1) FORMAT (35%) 1) FORMAT (75%) 1/4%, 1941551 FORMAT (134) FORMAT (134)	FORMAT (174 (EDI) FORMAT (174 (EDI) FORMAT (1722H) 110M RATE=, F30 + 75 2 DISCHARGE PLANE) 3 INTE; RATED FLOM) 44 GORRECTED WHEE, FORMAT (234 DEW F FORMAT (114,204 GA) 10HIDITY=; F6.3) FORMAT (114,204 GA)	19, 77. 49, 14.91 19, 77. 49, 14.91 18, 57. 14.400 2EMP, 7) 2EMP, 7) 2EMP, 7) 160. RAN (10.91 160. RA
25.0	IA CIA C IAC IAC	202 202 203	2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

0 0 7	PSIA,//) NRMAT (1x.8HRAKE NO5X.54THETA.5X.10HTJTAL TEMP.5X.	301
)	2X,8HTOT PRES,5X,11HSTAFIC TEMP,5X,1040ENSITY(LBM/CF) ,2X,8HMACOU	<b>C</b>
	ANO., 3X,13HVELOCITY(F/S),/)	0
405	FORMAT (3x,11,3x,F5.2,5x,F3.3,7x,F8.3,6X,F7.3,8x,F7.3,9x,F7.5,8x,F	0
	.496X9F7.2)	<b>5</b> (
410	FORMAT (/,31H CIRCUMFERENTIAL MASS AVERAGES ,4X, F7.3,6H DEGR,,4X,F	
	.3,6H PSIA,,4X,F7.2,8H FT/SEC,,4X,6HGAMMA=,=8.5,4X,9HMACH ND.=,F7	0 0
•	.4)	<b>&gt;</b> •
412	FUKBA (1/ )/2H 4. MAEE SIAILO	4 +
		312
2	FORMAT (35X, 12, 18X, F7.3, 18X, F7.3)	4
2	ORMAT (19X,5HOUTER)	-
M	ORMAT (10X,20HROTOR ENTRA	4
M	ORMAT (10 X,14HOPPOSITE ROTOR)	4
ŧ	ORMAT (7X,17HINTRA-STAGE,INNER)	7
.+	ORMAT (8X,15HDOWNSTREAM,INNER)	7
in	ORMAT (//,33H 5. STATOR BLAD	4
S	ORMAT (15H SUCTION SURFACE,//)	2
.o	ORMAT (30X,12HPOSITION NO.,10X,14HPRESSURE(PSIA))	2
'n	ORMAT (35X,12,18X,F7.3)	322
~	ORMAT (//,17H PRESSURE SURFACE,//)	2
475	ORMAT (//, 49H 6. VENTURI PRESSURES (USED TO SOMPUTE FLOW RATE) ,	324
Ø	ORMAT (77,69H 7. MAXIMUM MEASJRED STASE DISCHARGE PRESSURE AT EAC	2
	RADIAL PUSITION, /)	2
485	FORMAT (///+0X,37HTOLERANCES USED IN THESE CALCULATIONS,//,45X,12H	0
	WALL STATICS, 13X, F5.3, 8X, 1, 45X, 16HPLENUM PRESSURES, 9X, F5.3, 8X, 1, 45	2
	,19HPLENUM TEMPERATURES,6X,F5.3)	2
თ	ORMAT (//,2%)	M
ന	ORMAT (I1	M
0	ORMAT (3F12.5,F12.3,2F12.4)	3
505	ORMAT (16)	M
+	ORMAT (5F12.4)	M
#	DRMAT (35X,15HTAPE DUMP, VOLTS, ///, 84 CHANNEL, 5X,7HVOLTAGE, 5X,7HCHOU	m (
	NNEL, 5X, 7HVOLTAGE, 5X, 7HCHANNEL, 5X, 7HVOLTAGE, 7, 2X)	
520	ORMAT (3X,13,4X,	337

# 4. PHASE II - PROGRAM B2X

COMMON WETRAL STREET, PLONER, DARYE, NEXTALL, NSTRILL, NS																																																										ĺ		
PROCEAM BZX COMMONEAT RAP FSCALE, PLONER, DAMPF, NSAVE, NEX COMMONEAT RAP FSCALE, PLONER, DAMPF, NSAVE, NEX COMMONEAT RAP FSCALE, PLONER, DAMPF, NSAVE, NEX, NSTAT, 1787, LASE, LOSE, LOGS, LOGS, LOGS, LOGG, ATTOR, PROPERTY, NPP, NSTAT, NSAVE, 1787, LASE, LOSE, LOGS, LOGS, LOGS, LOGG, ATTOR, PROPERTY, NPP, NSTAT, NSAVE, 1787, LASE, LOSE, LOGS, LOGS, LOGS, LOGG, ATTOR, PROPERTY, NPP, NSTAT, NSAVE, 1787, LASE, COMMON NAIL (CAL), NSACC (CA.), NGALC	- 1	•		1341	4 6	101	1040	1344	1345	1345	1347	 1:40	1349	1350	7	1221	1352	1353	1354	14.5	4 4 6 6	100	135/	1358	1359	1300	1361	1362	1363	1354	1365	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1757	120	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7707	1370	13/1	1372	1373	1374	1375	1376	1377	1373	1379	1380	1381	1382	1383	1384	1385	1336	1387	1338	1389	1070	1331	1393	1394
	1	7	75	2	1 0	9 :	2	2																		22	S S S	<b>G</b> 2	<b>0</b> 2	112	2	5	: :	2 5	2 5	2 5	2 5	2 5	75	2	20	20	<b>N</b> 2	20	2	22	7	25	20	2	20	75	20	35	3	25	2 5	2 5	72	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		PROGRAM B2X						(24), N4ACH(24), IST4T1(24),																		56,34160319,.274	97128085548936/.(H20(J).J=1.6)/.43433286109804452292523.1.	01801017903651620704483/	MRITE (1032,100) IGASE	FORMATION TOTAL SOUTHER DATA DATA DATA FOR BOTH NO. 13. (.23. 14.)	DEADLINES AND TITLE			HANTING ALCOHOLING THE TANK TH	70478 (KASVINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESSINESPIESPIESPIESPIESPIESPIESPIESPIESPIESPI	NEW CALCOS GAS GAS TACALLOS TANDOS TA	FORM& 1 (6+12-0)	WRITE (LOSZ) 14016ASR, FRCAIR, FLO4, RPH, PIN, TIN	FCRMAI(2x,/,10x,12HGAS CONSTANT,37x,1H=,=8.4,/,10x,17HAIR MASS FRA	CTION,32x,1H=,F8.5,/,IGX,8HFLOMRATE,41X,1H=,=8.4,/,10X,11HROTOR SP	EED.38x.11=.78.1./.10x.20HINLET TOTAL FRESSURE, 29x,1H=,F8.4./.10x,	234INET TOTAL TEMPERATURE, 26X, 1H=, F8,3					FORMAT(10X,14HT IN/T IN(STD) + 35X,1H=,F8.5,/,10X,14HP IN/P IN(STD),	135X,1H=,=65,5)			10 160	E (L052,150)	FORMAT(111)		LNCT=LNCf+5+NRP	READ(LOG3, 170) (RRP(J), PR(J), J=1, NRP)	FORM 1 (2=12-0)	ANTIHE (LOSS) JEDONARY (KRYL) PARTHONARY ANTIHONARY ANT	TOTAL   LEAD   A   A   A   A   A   A   A   A   A	
																														-	•		1	į	77	Ì	13		77									•					ī		5,4	į	17	•	9	

190	FORMAT(15) IF(LNGT+5+NRT.LE.NL)GO TO 200 WRITE(LO32,150)	222	1395 1395 1397
200			1398 1399
	REAU(LOG3, 210) (RRT(J), TR(J), J=1, NRT)		1400
612			1405
220	FORMATICES, / 10%, 32HROTOR OJI ET TOTAL TEMPERATURE (, IZ, 8H POINTS),		1403
-	49 F 14.311		+ C+
			1406
			1437
230			1409
}	READ(LOG3, 240) (4SP(J), PS(J), 3S4(J), J=1,NSP)		1410
240	(607)		1411 1412
25.0	LLUSS, 250 JANSP, KASPLUJ, PSKLUJ, 151-15157 F(2%, 7, 10%, 30HSTAGE OJTLET TOTAL PRESSURES (, IZ, 84 POINTS), //		1413
	PRES,//, (F18.4,F12.4,F13.4)		1414
	.063, 190) NST		1415
	IF(LNCT+5+NST.LE.NL)G0 T0 260		1417
			1473
25.0			1420
0	, 1=L .		1421
27.0			1422
			1423
280	FORMAT(2X,//10X,33HSTAGE OUTLET TOTAL TEMPERATJRES (,12,8H POINTS)	2 5	1454
		7	6241
	READ(LOG3, 190) NSA	22	1426
N	REAU( LOGS, 170) (RSA(O), SA(O), J=1, NSA)	V	1647
	75 5 1 1 0 0 0		
	IF(LNCT+5+NSA.LT.NL)GO TO 282	25	1427
		2 5	1479
282		2 2	1430
J	1, NSA)	20	1432
285	LES (,12,8H POINTS),//,12X,6HRA	20	1433
		2 2	1434
		۷ <u>۲</u>	1432
	•	20	1437
•	WRITE (L032,150)	20:	1439
. 6		2 5	アウナマ
162	LNGI=LNGI+5+NMSU READ(LOG3,340)(XWSO(J),WSFJ(J),J=1,NWSO)	22	1441
		* *	* *
	NOST NEW DOCUMENT OF THE PROPERTY OF THE PROPE	. A	• • • • • •
	MSO(NMS)-1)-#-725	*	*
300	FORMA T(2-12.0)		1445
	Write (Losz, 310) neso, (xeso (l), espo (l), l=1, meso)	7	1443

	•		
31.0	STATIC PRESSURES (.12.8H POINTS).//.12X.	12 1444	_
	,//,(4X,2F14.4))	U2 1445	
315		12 1446	
		7441 21	
	10 320	2441 20	
		6551 21	_
		12 1450	
320	ISBN+5	15 1451	
	300) (XMSI (J), MSPI (J), J=1, NMSI)	12 1452	
		***	
		***	
		***	
		*	
	MRITE (LOSS, 330) NMSI, (XMSI(J), MSPI(J), J=1, NMSI)		
330	.84 POINTS),//,12X,7HX		_
) )			
331	READ(LOG4, 332) (BLCKGE(I), BDIST(I), I=1,NSTNS)		
332			_
	S.LE.NL)60 10 333		_
			_
			_
333			- •
			••
334	CATION,//,16X,38HST		
	3.5,F15.4))		_
	•		
335			
	IF(LNGT+5.LE.NL) GO TO 336		
336			_
337	5413)		•••
į	MRITE (LOSE, 338) (NMACH(I), 1=1, NSTNS)	12 1473	
338			
	101 47054 101	104 1200	_
200	LIGHTROWING Asid: Turball, 40, 0, Asid: Triball, 40, 0, And, 1		
	**************************************		
		12 1475	
			_
			_
	x3= (RSTN(L1) - RSTN(1) / FLOAT (ITJB)		
,			_
			_
			•
340	-X1)/X2		
			<b>.</b> .
	06022 (17) + (21) + (21) (17) - (2) 06022 (17) + (21) (17) - (2) 06022 (17) + (21) (17) +	U2 1490	_
	X2=X5TN(_2) **2-X1	U2 1492	

# 5. PHASE II - PROGRAM C2

U2 1513	161 20	17	20	32	2	22	U2 1520	3F UZ 1521	T (200), DATEP 32 1522	31M(11), SLOSS U2 1523	TREST - PSP( 112 1524	CT (26) HODI ( 42 452)	101 (C4) 9171 to 4 to 4/1/	(1) puvaja (c1) je 1569	1) b1(20) crr UC 1521	12(21), HIR(2 JZ 1928	CKGE (24), VV UZ 1529	3), x4S(23) J2 1530	.40EV(11,21), UZ 1531	02 1532	201 20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8,2,0/,KEC/1,0,0,9 UZ 1534	20 /606 •																2 2	2 C			U2 1559				102 102 103	2 2		
_	PROGRAM UZ COMMONINATON/OCCALTONO CAROLIDAMOFILACIA	COMMON ENTRY CONTENT OF THE STATE OF THE STA	131.N3 2.N31.N32.N0601 %.N05TC1.N3P.N3T.N3P.N3P.N3T.N3P.N3T.N3P.N3P.N3P.N3P.N3P.N3P.N3P.N3P.N3P.N3P	ZLOSZ.LOG3.LOS4.ITUB.IPASS.IVFAIL.IFFAIL.ILAST.4SA.IST.	30.NR3.NS3.NPLOT. ISTOP, IRLE, ISLE, LOSS	COMMON N3L (24) .NSPEC (24) ,NCAL C(24) ,NDATA (24) , N4ACH(24)	11STRT2(24)	COMMON G.EJ.GASS.FRCAIS.FLOM, RPH, PIN, TIN, PI, PRATIO, C1,	COMMON TITLE (18) . RSTN(200) . XSTV (200) , DATZAD (200) , DATBE	1S(200), DATAB(200), RIN(11), RLDSS(11), TFW(21), DMPP(21), S	141 DEALON CODE (241 DEALONDE			424) DELF(21) ABCOIM(21) SIADEV(21) KUIDEV(21) JACSIATIC	5,EPS(21),JVHDH(Z1),IDSDH(Z1),GAMA(Z1),IANA(Z1),IANK(Z1	5G(21), OR)Z2(24), SA(21), 82(20), TITLE1(13), DAT4ET (200), T	71), WR (21), WS (21), RTEMP (21), CR (21), PHI (21), ORV WJM (21), B	8(21), RRD(21), RSD(21), DS(23), DR(23), RI(21), SI(21), XMR(2	COMMON R(21,24), P(21,24), T(21,24), VM(21,24), VM(21,24),	1SOEV(11,21),R2M(11,21),S2M(11,21)	OIMENSION XX1(21), RECM(11), REG(11)	DATA REC4/0.0,0,0.2,0.4,0.5,0.8,1.0,1.2,1.4,1.5,1.8,2.0/	3976 y 0 e 996 0 y 0 e 9944 y 0 e 9929 y 1 e 991 99 u e 9917 y 0 e	00 I=2,N	IF(NCALC(I).EQ.4)60 TO 110		UD IZU I=LIPNSINS	14 CD 1170 18 C	4	TOTAL STATE OF THE TOTAL STATE O	17 (NT 75 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	 00 14.0 U=1.NSTRBS	IF(ABROTY(J) -LE-1-9)60 TO 140	X1=FFI(T(J,NSTN1))-(VM(J,NSTN1)+*2+VM(J,NSTN1)**2)/(2.	X1=FF2(X1)	X1=F=3(X1)	X2=X1+1.0	1	X4HDBROT4(U)++2		144(1.0/AS)		·		CALL G2 (2RT, TR, NRT, R(1, NSTM1), T(1, L1), X1, NST2HS, 1,0)	CALL G2(RECM, REC, 11, ABROTM, XX1, X1,NSTRMS, 0, 0)	4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		10/1 * 0. 10 1 40 CO 10 10 CO	25
																										001	110		404	) C	2											) *	150	155				150		170

```
1563
                                                                                                                 1575
                                                                                                                               1575
                                                                                                                                                        1578
                                                                                                                                                                         1573
                                                                                                                                            1577
                                                                                                                                                                                                      1581
                                                                                                                                                                                                                     1582
                                                                                                                                                                                                                                   1563
                                                                                                                                                                                                                                                                  1585
                                                                                                                                                                                                                                                   1584
                                                                                                                                                                                                                                                                                                                                       1590
                                                                                                                                                                                                                                                                                                                                                       1591
                                       CALL G2(RECH, REC, 11, ABSTAM, XX1, X1, NSTRMS, 0, 0)
D0 180 J=1, NSTRMS
T(J, L1) = T(J, L1) / (XX1(J) - (1.0-XX1(J)) * ((14.69444/PC), NSTN2) *PRATI
10)) ** 0.8-1.0))
                                                                                                                DO 200 J=1,NSTRMS
IF(A3STA4(J).LE.1.0)GO TO 200
X1=FF1(T(J,NSTN2))-(VM(J,NSTN2)**2+VM(J,NSTN2)**2)/(2.0*6*EJ)
                                                                                                                                                                                                                                     X1=(X2+X4/(X3+X4+2.0))++(X1/X3)+(X2/(2.0+X1+X4-X3))++(1.0/X3)
P(J,L2)=P(J,L2)/X1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                          T(J,L1)=X1+(T(J,L1)-X1)/2.0
VM(J,L1)=3+EJ*(FF1(T(J,L1))-FF1(TIN))/(PI*R(J,L1)+RPH)*360.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            IF(R(J, NSTN1).GE.X2)GO TO 300
T(J,L1) = X1+(T(J,L1)-X1)/2.0
VM(J,L1)=GFEJ+(F1(T(J,L1))-FF1(TIN))/(PI+R(J,L1)+RPH)+360.0
T(J,L2)=F(J,L1)
                                                                                                                                                                                                                                                                                                           DO 220 J=1,NSTRMS
T(J,L2) =T(J,L1)
VM(J,L1)=3+2J+(FF1(T(J,L1))-X1)/(PI+2(J,L1)+2P4)+360.0
                                                                                     CALL G2(RSP, PS, NSP, R(1, NSTN2), P(1, L2), X1, NSTRMS, 1,0)
                                                                                                                                                                                                                                                                                                                                                                                                                 GALL G2(2(1,NSTN1),T(1,L1),NST2HS,X2,X1,X1,1,1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      CALL G2(2(1,NSTN1),P(1,L1),NST2MS,X2,X1,X1,1,1)
D0 250 JJ=1,NSTRMS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CALL G2(2(1,NSTN2),P(1,L2),NST2HS,X2,X1,X1,1,1)
D0 270 JJ=1,NSTRHS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CALL G2(2(1,NSTN1),T(1,L1),NST2HS,X2,X1,X1,1,1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     GALL G2(2(1,NSTN1),P(1,L1),NSTRHS,X2,X1,X1,1,1)
                                                                                                                                                                                                                                                                   F(NPRSS.EQ.1) P(J,L1) =P(J,L1) /X1
                                                                                                                                                                                                                                                                                                                                                                                                                                                           IF(R(J,NSTN1) - LE. X2) GO TO 240
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 IF(R(J, NSTN1).LE.X2)G0 T0 260
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        IF(R(J,NSTN2).LE.X2)60 T0 280
P(J,L2)=K1+(P(J,L2)-X1)/2.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              P(J,L1)=X1+(P(J,L1)-X1)/2.0
IF(I>ASS.EQ.1) GO TO 190
                                                                                                    IF(IPASS.EQ.1) 60 TO 210
                                                                                                                                                                                                                                                                                                                                                                                    IF(NEX.E2.0)60 TO 340
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     IF (NEX. E3.1) 50 TO 340
                                                                                                                                                                                                                                                                                                                                                                                                                               DO 230 JJ=1,NSTRMS
J=NSTRMS+1-JJ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 DO 290 J=1,NSTRMS
                                                                                                                                                                                                                       X4=ABSTAY(J)++2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          (1),12)=[(1,11)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   J=NST RMS+1-JJ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           J=NST RMS+1 − LU
                                                                                                                                                                                                                                                                                                                                                                                                   X2=RRT (NRT)
                                                                                                                                                                                                                                                                                                 X1=FF1(TIN)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              K2=RSP(NSP)
                                                                                                                                                             X1=FF2(X1)
                                                                                                                                                                             X1=FF 3( X1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         (2=:RP(N2P)
              GO TO 190
                                                                                                                                                                                         X2=X1+1.0
                                                                                                                                                                                                          X3=X1-1.0
                                                                                                                                                                                                                                                                                 CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    K2=R2T(1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        X2=RRP(1)
                                                                                                                                                                                                                                                                                                                                                        IRT=L1
IST=L2
                                                         180
                                                                                      190
                                                                                                                                                                                                                                                                               200
210
                                                                                                                                                                                                                                                                                                                                          220
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       230
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              250
260
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     27 0
28 0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        290
300
```

DO 310 J=1,NSTRMS

IF(R(J,NSTN1).GE.X2)GO TO 320

IF(R(J,L1)=X1+(P(J,L1)-X1)/2.0

320 X2=RSP(1)
CALL G2(R(1,NSTN2),P(1,L2),NSTRMS,X2,X1,X1,1,1,0)

DO 330 J=1,NSTRMS
IF(R(J,NSTN2).GE.X2)GO TO 340

IF(R(J,NSTN2).GE.X2)GO TO 340

340 CONTINUE
END

# 6. PHASE II - PROGRAM D2

	OVERLAY(JOTHO, 4, 0) PROGRAM JZ COMMON/FYTRA/PSZAL Z, PLONER, DA MPF. NSAVE. NEX	U 2	1595 1596	
	COMMON ISTINS, NSTRMS, NMAX, MFORGE, NPRSS, NTEMP, AL, NSTNI, NSTN2, NDASE, N LRI, NRZ, NSI, NSZ, NOROTR, NOSTAT, NRP, NRT, NRP, NST, NASO, NMSI, ICASE, LOGI, 2, 002 - 002 - 1710 - 120 - 120 - 120 - 121 -	22.5	1597	
	COGES FOOTS FOOTS ISSUED IN THE STATE OF THE STATE OF STATE OF THE STA	225	1600	
	LISTRY Z(24)	20	• ++ •	
	COMMON G,EJ,GASR,FRCAIZ,FLDM,ROM,PIN,IIN,PI,ORATIO,G1,ZF COMMON TITLE(18),RSTN(200),XSTN(200),UAT3AD(200),DATEP	2 2		
	1S(200), DATAB(200), Q1H(11), 2, 3SS(11), TFH(21), 3NPP(21), S1H(11), SLOSS	25	-	
	2(11), RSA(21), SPG(21), BDIST(24), RRP(21), PR(21), RRT(21), TR(21), RSP( 321), PS(21), PSH(21), RST(21), TS(21), XMSO(24), MSPJ(24), XMSI(24), MSPI(	2 2	-	
	424) , DELF(21) , A BROTH(21) , STAJEV(21) , ROTJEV (21) , A BSTAM(21) , JVHJH (21)	20		
	5,EPS(21,)OVWOM (21),TDSOM(21),GAMA(21),TAWA(21),TAWK(21),51(20),CPP U2 66(21),ORJ22(2+),SA(21),B2(20),TITLE1(18),DATHET(200),TIR(21),H1R(2 U2	22.0	н н	
	71), W. (21), WS (21), RTEMP(21), CR (21), PHI (21), DRVW)H (21), BLCKGE (24), VV	20		
	8(21), KCD(21), CSD (21), DS (23), DK(23), KI (21), ST (21), SARK(23), SAS(23) COMMON R(21,24), P(21,24), T(21,24), VM(21,24), VM(21,24), RDEV(11,21),	2 2		
	150EV(11,21), R2M(11,21), S2M(11,21)	25	44.4	
	DIMENSION XX1(21),XX2(21),VMULJ(21),UL(20),UHU_(20),USDL(20),UKSMU 1L(20),A(20),B(20)	2 2	-	
	ITHAX #20	22	₩.	
	TTX(1) #0.0	2 2	1618	
	13. AST 12. OC 70 1113. NSTNS	0 0 0 0	1620	
i	IF(R(1,1), EQ.0.0) ISTAG=I	25	1621	
2	CONTINCE		1623	
	00 50 1-1, ITU8	2 2	1624	
90	81(3) *0.0	<b>0</b> 5	1625	
	26 = 1 = 0 0 = 1 - 0	<b>0</b> 5	1625	
	CALL H2 (I)	02 0	1527	
	CALL I2(0, I, DWDV, ACTFLO)	25	1628	
	IC1=KCAFC(1)+1 DO 100 Le1.8SFRHS	2 0	1630 1630	
	IF(IPASS.EQ. 1. AND. I.GT. 1) V4(J, I) = (VM(1, I-1) +VM(NSTRMS, I-1)) /2.0	25 125	1631	
100	7	2 2	1633	
,		U2	1634	
-	60 TO (110,110,130,140,130),ICI DO 120 J=1-NSTRMS	2 2	1635 1636	
		20	1637	
	IF(I.GT.ISTAG.OR.J.NE.1) VM(J,I)=VM(J,I-1)+4TEM3(J)/R(J,I) I/IJ)-I/II-1	2 2	1638	
120		22	1640	
66	GO TO 180 CALL E2(0.1)	2 2	1641 1642	
•	1.80	72	1643	
140	CALL G2(RSA,NSA,R(1,NSTN2),XX1,X1,NSTRMS,1,0) If(IPASS,GT,1)G0 T0 160	222	1544 1645	
	J=1,NSTRMS	25	1645	
150	z ~	220	1648	
	60 TO 180	<b>N</b> 2	1649	

U2 165U U2 1651 U2 1652 U2 1653 U2 1653	U2 1655 U2 1655 U2 1657 U2 1658	U2 1659 U2 1660 U2 1551 U2 1552	U2 1664 U2 1664 U2 1655 U2 1667	2222	מממה מממ	222222	UZ 1585 UZ 1585 UZ 1683 UZ 1689 UZ 1690	u2 1692 u2 1693 u2 1694 u2 1695	U2 1695
0 00	_		AAZ (3) = K(3) 00 22 0 J=1 0HDC (J) = (X 0RVWDC (J) = (X	OSDL(J)===4(I(J+1,I),I(J,I),P(J+1,I),P(J L3=1 IF(I.EQ.ISTAS)L3=2 DO 240 J=L3,IIU3 A(I)=-D3.L3,IIU3	V(J) +D{VWDY(J+1) / VV (J+1) - GPPS(J) +GR(J) - GPPS(J) + VV(J) - DVWDY(J+1) / VV (J+1) M(J, J) - DVWDY(J+1) / VV (J+1, I) - GPPG(J) + GR(J) - GPPG(J (J) / VM(J, I) - DVYDM(J+1) / VY (J+1, I) (J+1, I) ) / Z, O) - ( (VV (J) + VV (J+1, I) / Z, O) ** Z + ((VM(J, I) / I) TO Z3B TO Z3B TO Z3C	1 460	1F(II ER.=3.ITMAX.AND.ILAST.=I X1=10.0 X1=FF2(X1) 3(J)=2.0*(OHOL(J)-X1*OSOL(J)-DRVHOL(J))+X1*(TOSOH(J)+TOSOH(J+1))*G 1*EJ VV(IMIO)=VV(IMIO)*+2	DO 250 J=_1,VSTRMS IF(A3S(A(J-1)).LT.0.000001)50 TO 250 X1=-DL(J-1)*A(J-1) IF(X1.GT88.0)50 TO 2+3 L2=J-1	WRITE(LO32,241)IPASS,ITER,I,L2,X1 FORMAT(1DX,4HPASS,I3,54 ITER,I3,2H I,I3,3H L2,I3,3H X1,E11.4) LNGT=LNGT+1 X1=-88.0 GONTINUE IF(X1.LE.88.0)GO TO 248
15. 17. 18.	196			0 0 0 0 0 0 0 0	<b>0</b> 0	232	236 238 240		241

U2 1695

. 3	IF(IPASSE.NFORCE)GO TO 246 IF(LNCTT.NL)GO TO 244 MRITE(LU32,440) LNCT=1 LNCT=1 LNCT+1 L2=J+1	22222	1697 1598 1699 1700 1701	
24.5	L2*J-1 WRITE(L032,245)IPASS,I,L2,ITER FORMAT(10X,44PASS,I3,64 STATION,I3,11H STREAMTJEE,I3,10H ITERATION 1,I3,37H EXPONENTIAL ARGUMENT LLMITED TO 88.3) TECTIFE,T3,TIMAX,AND,TLAST,ED,10,ILAST.ET		1703 1704 1705 1705	
246 245	X1=88.0 X1=EXP(X1) VV(J)=VV(J-1)*X1+B(J-1)/A(J-1)*(1.0-X1)	2222	1707 1709 1709	
250 260	60 10 25u CONTINUE 2 = 1 + 10 + 2 - (J-1) +8 (J-1)	2222	1711 1712 1713 1713	
	IF(I.Eq.ISTAG) L3=IMID-1 DO 280 JJ=2,L3 J=IMID+1-JJ I=(A3S(A(J)).LT.0.00001)G0 T0 270	12222	1714 1715 1715 1715 1717	
	X1=DL(J)*A(J) IF(X1.6T88.D)GO TO 263 MRITE(LO52,241)IPASS,ITER,I,J,X1 L.CT=LNCT+1 X1=-88.D	22	1718	
263	CONTINUE IF(X1.LE.06.0)GO TO 268 IF(IPASS.LE.NFO?CE)GO TO 266 IF(LNCT.LI.NL)GO TO 264 WRITE(L032,440)	2222	1713 1720 1721 1721	
5 64	LNCT=1 LNCT=LNCT+1 WRITE(L032,245)IPASS,I,J ,ITER WRITE(L032,245)IPAX,AND.ILAST.E3.0)ILAST=I	22222		
70 P	P(X1) =VV(J+1) 280	22222		
280	VV(J) =VV(J+1)-DL(J)+B(J) CONTINUE DO 32 D J-1,NSTRMS IF(I.EQ.ISTAG.AND.J.EQ.1)GO TO 320 IF(ILEQ.ISTAG.AND.J.EQ.1)RT)RF=1.0/(1.0-RPM*PI*2(J,1)*TAN2(J)/(360.0*1VMOLD(J)))	222222		
290	<pre>IF(RF.LT.0.1) RF=0.1 IF(VV(J).LT.1.0) GO TO 290 VV(J) = SQRT(VV(J)) GO TO 320 IF(IPASS.LE.NFORCE) GO TO 315 VV(J) = SORT(VV(J))</pre>	22222		
300	IF(LNCTI.NL) GO TO 300 MRITE(LO32,440) LNCT=LNCT+1 LNCT=LNCT+1 HRITE(LO32,310)IPASS,I,J,ITER,VV(J)	122222		

1748 1749 1750 1751 1752	1753 1754 1755 1755		1767 1768 1770 1771 1773 1774 1775 1775 1776 1780 1781	
2222	2222		, , , , , , , , , , , , , , , , , , ,	ם מממממממממ
ਜ ਜ	3)CALL E2(1,1) 0 340 0.1)G3 T0 330 0.17 0 00E AN) TOASS OF 200 TO	IF (ABS(VV(J)/VMOLU(J)-1.0).51.0.005.50 TO 190  IF (ABS(VV(J)/VMOLU(J)-1.0).67.0.005)50 TO 190  CONTINUE  DWOV=0  0 40 0 J=1,ITUB  X1=F1((T(J,I)+T(J+1,I))/2.0)-(((VV(J)+VV(J+I))/2.0)**2+((V)  1)+VM(J,I)/2.0)**2)/(2.0*5*5J)  IF (X1,GT,GT,GJ) GO TO 390  IF (IPASS,LE.NFORCE)GO TO 380  IF (LNCT.I.NL) GO TO 360  WRITE (L052,440)	LNCT=1  LNCT=LNCT+1  WRITE(L052,370)IPASS,15,J,ITER  DEAGHAT(1012,44PASS,13,34) STATION,13,11H STREAMTJBE,13,10H ITERATION  113,23H STATIC ENTHALPY UNREAL)  IF(ITER.=20.ITMAX.AND.ILAST.EQ.0)ILAST=I  X1=F10.0  X1=F2(X1)  X2=(T (J,I) + T (J+1,I)) / 2.0  X3=FF5(X1,X2)  X4=(V (J) + V (J+1,I)) / 2.0  X5=K+X4/(FF3(X1)*G*GASR*X1)  IF(IC1.E2,3)X5=X5*(1.0+1))*DL(J)*(R(J+1,I)) / 2.0)**2)  X6=X4*(G*PG(J)+PG*PG(J+1))*DL(J)*(R(J+1,I))*PI*(1.0-31(J)-B2  I(J))*(P(J+1,I))*C*PG(J)+X6  TEM(J+1)=TFM(J)+X6	
# ## Z Z	ý	0 0 M M O M M	0 K 8 K K	0 7 7 0 0

420	INMACHII).EQ.O)GO TO 430 (ACTFL2.LT.FLOW)VHIN=VV(IMID)	220	1794
430	RCE) GO TO 470 O TO 450	222	1736 1797 1798
0 1 1		222	1793
450		225	1902
460	LOH ITERATION, IS, 27H CONTINUITY	200	1804
	1LAST. E3.0) 1LAST=1	200	1805
470		75	1807
	HAX-VV(IHID)+(VHIN-VHAX)/50.0	2 C C C	1809 1809
		25	1810
0 9 4	IF(IPASS.LE.NFORCE)60 TO 500 IF(LNCTT.NL)60 TO 490	25	1811 1812
		20	1813
061		2 2	1514
•	460)IPASS,I,ITER	20	1816
11	ST.EQ.O) ILAST=I	25	1817
2		220	1619
ì	IN) DELTAV=VMIN-VV(IMID) - (VMIN-VMAX) /50.0	20	1820
210	DO 520 J=1,N51KH5 IF(I.EQ.[5]TAG.AND.J.EQ.1)GJ TO 520	2 2	1951
		12	1823
200	IF(VV(J).LT.1.0) VV(J)=1.0	22	1824
,	IF(ABS(A3TFL0/FL0M-1.0).GT.0.00025.0R.(OHDVE.0.0.AND.NMACH(I).EQ	32	1825
	AND.NM434(I).EQ.1)) GO TO 5+0	2 5	1827
	5. AND. J. EQ. 1) 63 TO 530	200	1829
i	)-1.0).ST.0.00025)SO TO 540	20	1830
530	CONTINUE GO TO SÃO	2 Z	1631
240	ER.SE.ITMAX) GO TO 550	25	1833
	EQ.1.0R.IC1.NE.3)GO TO 190	2 2	1834
	GALC EZ(1,1) GO TO 190	220	1836
950	10 580	20	1837
	IF(LNCT.=:.NL) GO TO 560	2 2	1635
		22	1840
560		25	1841
		750	1843
		22	1844
570	FORMAT(10%,44PASS,13,44 STATIO4,13,35H UNCONVERGEO FLOW/SPECIFIED	225	1846
586		1 2 E	1848
		22.0	1850

50 00 00 00 00 00 00 00 00 00 00 00 00 0	DO 581 II=I,NSTNS IF(NCALC(II).eQ.3)GO TO 583 IF(NCALC(II).eQ.3)GO TO 582 CONTINUE X2=RPM*PI/360.0 DO 590 J=1,NSTRMS X1=FFI(T(J)1) - (V(J)**2+VM(J,I)**2)/(2.0*G*EJ) IF(X1.GT.0.1*TIN)GO TO 5838 MRITE(LO32,5832) IPASS,ITER,I,J,X1 FORMAT(LOX,44PASS,I3,54 ITER,I3,24 I,I3,24 J,I3,34 X1,E11.4) X1=0.1*TIN LNCT=LNCT+1	222222	1852 1852 1853 1854 1855 1855
80 80 80 80 80 80 80 80 80 80 80 80 80 8	CONTINUE HIR(J)=XI+(VV(J)**2+(X2*R(J,I)~VH(J,I))**2)/(2,D*G*EJ) TIR(J)=F=2(HIR(J)) X1=FF2(XI) OMPP(J)=1.6-FF5(X1,TIR(J))	2222	1858 1859 1850 1861
	IF(X2.EQ.0.0)GO TO 584  X1=HIR(J)-(X2*R(J,I))**2/(2.0*3*EJ)*(1.0-(R(J,IRT)/R(J,I))**2)  X1=FF2(X1)  X1=FF2(X1)  X3=FF5(TL2(J),X1)  X3=FF5(TLJ,IRT),T(J,I)  X3=P(J,IRT)/(P(J,I)*X3)  NR(J)=(1.0-X3)/(X1*OHPP(J))	, , , , , , , , , , , , , , , , , , ,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
<b>6 0 0 0</b>	WS(J) = (1.0-P(J,IST)/P(J,I))/OMPP(J) CONTINUE IF(IG1.NE.4.DR.NOSTAT.EQ.0)GO TO 602 DO 601 J=1,NSTRMS	2222	1870 1871 1872 1873
66 901 60 001 60 001	STADE V(J) = (ATAN(VM(J) I) /VV(J) ) - ATAN(TAN (J) ) * J I IF(ICL.NE, 5.0%-NO2OTR-EQ.0) 50 TO 604 X1=RPH*PL/350.0 DO 603 J=1,NSTANS ROTUEV(J) = (ATAN((J) I) -X1*R(J, I)) /VV(J)) - AFAN(TANA(J)) * J I IF(I.NE, VSTAI, AND, I.NE, NSTA2) 63 TO 606	222222	1875 1875 1877 1878 1878
·	DO 6D5 J=1,NSTRHS X2=VW(J,I) **2+VV(J) **2 X1=F=1(I(J,I) -X2/(2.0*6*EJ) IF(X1.LT.10.0) X1=10.0 ASTF E(X1) = SQAT(X2/(G*GASR*K1*F=3(X1))) IF(I.EQ.ASTA) = BROTH(J) = ABSTAH(J)	00000000000000000000000000000000000000	1880 1881 1882 1882 1884 1885
6005	CONTINUE DO 610 J=1,NSTRMS IF(I.eQ.ISTAG.AND.J.EQ.1)GO TO 508 IF(ABS(VV(J)/VM(J,I)-1.0).3T.0.001)IVFAIL=IVFAIL+1 IF(ABS(VV(J)/ACTE)	22222	1887 1888 1989 1890 1891
9 4 C	IF (A3S(T=M(J))-DELF(J)).GT.G.G.G.G.G.TEFAL-1 VM (J, I)=VV (J) RTEMP (J)=R (J, I) X1=DW DV/AGTFLO IF (X1.LT.G.S) X1=G.5 X1=1.G ((1.0+DROZ2(I)*X1/9.0) X2=6.G IF (DAMPF.NE.G.G) X2=DAMPF X1=1.G ((1.0+DROZ2(I)*X1/X2)	מממממממ	1893 1893 1894 1896 1894
	CALL G2(IFW, 21EMP, NSTRMS, DEL <sup>=</sup> , XX1, X2, ITUB, 1, 0)	7 7	18 38

520	00 620 J=2,ITUB R(J,I)=RTEMP(J)+(XX1(J)-RTEMP(J))*X1
)	IF(ILAST.NE.0.AND.IPASS.GT.NFU2CE)30 IJ 540
	IF(NBL(I).Eq.1.AND.IPASS.GI.2)SALL I2(1,I,DWDV,ACTFLO)
c	IF(NBL(I).E.4.1)CALL I2(1,I,JWDV,ACTFLO)
630	CONTINUE
049	CONTINUE
	END

### APPENDIX D

### RAW EXPERIMENTAL DATA

This appendix presents a listing of the experimental data after being dumped from magnetic tape onto computer cards. The first two ten-character "words" of each test contain the test identification number.

00000	18010634000000000057	0+00194450 00 0000058 0+00123550 00 0000062	0+:00280460000000000559 0+001243600000000063	0+0000126 3+0012486
ı٥	+0019306000000000000	+001906500000000006	+001886600000000000	+001866
00000000	+0013046000000000006	+001362600000000007	+00188360000000000	+001863
70000000	+001893500000000000	+001875600000000007	+0019166000000000007	+001975
700000000	+001937600000000007	+00192460000000000	+0019506000000000007	+001877
00000000	+001930600000000000	+00197360000000008	+001927600000000000	+0011939
00000000	+00190460000000000	+00193060000000008	+00101000000000000000000000000000000000	+001913
0000000	+001900600000000000	+00186660000000000	+00133460000000000000	+001916
600000000	+001396600000000000	+001912600000000000	+0018726000000000000	+072570
60000000	+001383600000000000	+001915600000000000	+001901600000000000	F000838
00000000	+01715360000000020	+01798550000000033	-0074186000000000000	+001798
00000010	+01664160000000020	+01746160000000030	-007418600000000000	+001457
00000010	+0171336000000000000	+01796450000000030	-00832160000000000	+001448
00000010	+0163276000000020	+0.1712960000000030	-00778060000000000	+001577
00000010	+01594660000000000000	+0160506000000030	-007612600000000000	+001459
00000011	+0160186000000021	+0159196000000031	-006454600000000041	+001889
00000011	+01503550000000021	+01690260000000031	-006444630000000041	+001463
00000011	+01621060000000021	+0169046000000031	-006440600000000041	+001246
00000011	+01652160000000321	+0168615000000031	-006453600000000041	+001515
00000011	+01709260000000021	+0159635000000031	-0064336000000000041	+001533
00000012	+01672860000000022	+01793660000:00032	-00645060000000042	+001921
00000012	+01687350000000022	+01777260000000032	-0064356000000000042	+001700+
00000012	+017047600000000022	+0174076000000032	-006458600000000042	+001514
00000015	+017166600000000022	+01738860000000032	-006451600000000042	+001601
00000012	+017234600000000022	+01747560000000032	-006461600000000042	+001588
00000013	+013146600000000023	+01720460000000033	-006585600000000043	+001841
0000013	+01179860000000023	+01715760000000033	-00690960000000043	+001664
00000013	+0118366000000023	+01731460000000033	-006882600000000043	+001441
00000013	+01289460000000023	+01744760000000033	-0.06688600000000000	+001731
0000000	+01491260000000023	+01731760000000033	-006976600000000043	+001577
00000014	+01715+60000000002+	+01798260000000034	-0074186000000000044	+00001
0000001+	+017155600000000024	+01798150000000034	-007418600000000044	000018
0000000	+035395500000000024	03661960000000034	-000012600000000004	+001847
0000000	+0538736000000000	5544150000000034	+006275600000000004	14795

+000015	+001244	+002023	+001972	+005101	+302168	+002105	+002003	+00200+	+053119	F 90 0837	-005265	-005484	-005466	-005380	-005436	-005417	-005373	-005354	-005352	-005423	-005381	-005339	-005368	-005336	-005414	-005375	2896DD-	-005375	-005368	-02470	0-0053786	-005280	-005350
+0027776000000000000	+001239600000000006	+002072600000000000	+0019956000000000000	+0021156000000000000	+002124600000000000	+0020416000000000000	+002107600000000008	+00/50076000000000000	+061997600000000000	+005038600000000000	-007418600000000000	-0074196000000000000	-006881500000000040	-006754600000000040	-0.067076000000000041	-0061986000000000041	-0061926000000000041	-0061946000000000	-006199600000000041	-006153600000000000	-00615960000000000	-006152600000000000	-006153600000000042	-006158600000000042	-006156600000000043	-00624860000000043	-0061796000000000	-00631.260000000043	-00/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/	-072361600000000-	0-03/419600000000000444	-0006136000000044	+00627460000000004
+00199260000000000	+001231500000000006	+005135600000000006	+002012500000000007	+001961600000000007	+00206350000000000	+002152600000000008	+0020396000000000	+.0020000000000000+	+005063600000000000	+00198760000000000	+01798550000000030	+01754860000000030	+0179686000000030	+01747060000000030	+0190235000000035	+0190895000000031	+01732360000000031	+017326600000000031	+0173045000500031	+01730460000000031	+0188306000000032	+0187376000000032	+01981550000000032	+01977759000000032	+0198515000000032	+0197276000000033	+0195296000060033	+01973050000000033	+0193366000000033	+019748500000000003	0+01798250 00 0000341 0+01793150 000000343	+0366136000000034	+0224436000000034
8021584000000000000	+001239600000000000	+00215350000000000	+0020456000000000000	+001378600000000000	+002014600000000007	+0020626003000000	+00204460030000008	+002085600000000000	+00198060000000000	+00202960000000000	+0171556000000000000	+01682660000000020	+017141600000000020	+016652600000000020	+0153755000000000000	+01652960000000021	+01648060000000021	+0168856000000021	+01745360000000021	+0172126000000000	+01789160000000022	+0180316030000032	+01313760030000022	+01317560000000022	+0181956000000000022	+01601760000000023	+01620560000000023	+016782600000000023	+017234600000000	+0180186909090023	0+01/154600000000241	+035400600000000054	+053893600000000
ē	90000000	00000000	00000000	000000000000000000000000000000000000000	00000000	00000000	00000000	00 1)n 0 0 0 3	60000000	60000000	000000000	00 00 0 010	01000000	01000000	00000010	00000011	00000011	00000011	00000011	00000011	00000012	00000012	00000012	00 00 0 012	00000012	00000000	00000013	00000013	00000013	00 00 0 013	0000000141	00000014	00000014

÷000012	0+0012516	+002012	+001971	+0000	+005T30+	+00200+	+00200+	+043505	F000839	+002126	+002176	+001950	+002185	+1302043	+002131	+002140	+001933	+002173	+002019	+00200+	+002136	+001950	+002135	+00200+	+002058	+002089	+001637	+002081	+002021	+000978	+00004	+067845	+014798
+0027826000000000000	0+001245500000000063	+00202760000000000	+001989600000000000	+0050000000000000000000000000000000000	+005000000000000+	+00207560000000000	+00198860000000000	+001386600000000000	+002001600000000000	-007420600000000040	-0074206000000000046	-097036600000000040	-00688560000000000	-006828600000000040	-006260600000000041	-006260500000000041	-00621060000000041	-006225600000000041	-00617060000000041	-006177600000000042	-006182600000000042	-006182600000000042	-006184600000000042	-00618260000000000	-006261600000000043	-0062146000000000043	-006370600000000043	-00622860000000043	-0064246000000000043	-0074205000000000044	-007420600000000044	-000615600000000044	+00627460000000044
+00197750000000000	0+00123760000000000000	+002082606006000006	+00199760000000000	+ 00 1 3 6 2 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+ 00 < 00 00 00 00 00 00 00 00 00 00 00 0	+00202950000000000	+00198250000000000	+002029500000000000	+00197760000000000	+0179886000000030	+01751060000000030	+017972500000000030	+01739260000000030	+01864460000000030	+018570600000031	+01722960000000031	+0172286000006031	+017199600000000031	+01720360000000031	+0185516000000032	+0135896000000032	+01948560000000032	+0194586000000032	+01954160000000032	+01939560000000033	+01928350000000033	+0193995000000033	+0195206000000033	+01945250000000033	+01798760000000034	+01179866000000034	+03663360000000034	+022473600000000034
803152400000000000	0+0012456000000000000	+0021076000000000006	+0020316000000000000	\n\n\n\n\n\n\n\n\n\n\n\n\n\n\n\n\n\n\n	+00202220010 +0020225200103008	+0019986000000000	+00206460000000008	+00196760000000000	+0020036000000000+	+01715560000000029	+01678960000000120	+01713860000000020	+016572600000000020	+01527460000000020	+01641050300000021	+01642260000000021	+01673660000000021	+017277600000000021	+01719060000000021	+017688600000000022	+0178206000000000022	+01794260000000022	+017 3976000000000022	+018024600000000022	+01553160000000023	+01555600000000023	+0160836000000023	+0165806000000023	+01751660000000023	+01715560000000024	+01715560000000024	+03540460000000024	+053883600000000
	C 000	0000000	9	7000000		0000000	0000000	6000000	6000000	0000010	0 000 0 10	0000000	00000000	0000010	0000011	0000011	0000011	0000011	0000011	0000012	0000012	0000012	0600012	0000012	0000013	0 000 013	0000013	0000013	0000013	0000014	0000014	000001	0000014

0+0010136 0+0012526 0+00120636 0+0019796 0+0021036 0+0021116 0+0021056 0+0021036 0+0020986 0+0020986 0+0020986 0+0021036 0+0021036 0+0021036 0+0021036	+002166 +502128 +002168 +002153 +002169 +002139 +000978 +010847
0+00277350000000053 0+002087600000000071 0+00200160000000071 0+00213160000000075 0+002131600000000075 0+0021136000000000075 0+0021136000000000075 0+0021166000000000000 0+00211660000000000000000000000000000000	-006151600000000042 -0061596000000043 -0062576000000043 -0061896000000043 -0061966000000043 -0074216000000044 -0074216000000044
0+0020015000000058 0+002152500000000056 0+002152500000000074 0+002019500000000074 0+0021525000000000074 0+00215250000000000000000000000000000000	+0199086000000032 +0198846000000032 +019756000000033 +019758600000033 +019863600000033 +019815600000033 +017989600000034 +01798960000034 +01798960000034
1804158400000000000000000000000000000000	+01819060000000022 +0182096000000022 +0160716000000023 +0168576000000023 +0173016000000023 +0171556000000024 +0171576000000024 +0354106000000024
208 00000000054 00000000058 0000000000000	000000012 00000013 00000013 00000013 00000013 00000014

C	T C C C C C C C C C C C C C C C C C C C	30000000000000000000000000000000000000	30000000000000000	4700013
0 00 0	1803140400000000000000000000000000000000	0+001244600000000000000	0+0012526000000000000	0+0012576
0000000	+002023500000000000	+002003600000000006	+001984600000000000	+001966
0000000	+00200760000000000	+0013666000000000007	+00197760000000000	+001954
7000000	+001968660000000007	+00134960000000000	+002033600000000007	+005021
2000000	+0019756000000000000	+0020316000000000	+002055600000000000	+002086
0000000	+0020226000000000000	+002065600000000008	+001997600000000000	+00200+
000000	+001973600000000000	+00139660000000000	+00200560000000000	+0011998
0000000	+00198760000000000	+001960600000000000	+00196260000000000	+002011
6000000	+0019+36000000000000	+00138050000000000	+001956600000000000	+036723
6000000	+002000600000000000	+001955600000000000	+001981600000000000	F000838
0000010	+01715660000000020	+01799260000000030	-007422600000000000	+0000+
0000010	+0167376000000020	+01756960000000030	-007423600000000040	+001978
0000010	+0171416000000000000	+01797460000000030	-007326600000000040	+001793
0100000	+01645760000000020	+01727860000000030	-00713060000000000000	+00200+
0000010	+01613260000000020	+01793860000000030	-00705360000000000	+001895
9000011	+016244600000000021	+0178996000000031	-006340600000000341	+00200+
0000011	+01627760000000021	+0170886000000031	-00635060000000041	+001948
0000011	+0155076000000021	+0170886000000031	-00629060000000041	+001797
0000011	+0169816000000021	+01705360000000031	-00630060000000000	+002080
0000011	+01715860000000021	+01705660000000031	-006262600000000041	+001841
0 000 0 12	+017324600000000022	+01833250000000032	-00626760000000000	+00200+
0000012	+017459600000000022	+0182936000600032	-00626860000000000	+00500+
0 000 012	+01759160000000022	+018881600000032	-0062756000000000042	+001825
0000012	+01769160000000022	+01886250000000032	-006271600000000042	+00201
0 000 012	+017740600000000022	+0189496000000032	-006280600000000000	+001894
0 000 013	+01476460000000023	+01877060000000033	-00635560000000000	+001958
0000013	+014498500000000023	+01856350000000033	-0063366000000000043	+001958
0000013	+01496160030000023	+0187956000000033	-006556600000000043	+001800
0000013	+015543600000000023	+0189216000000033	-006340609000000043	+00100+
0 000 013	+01671560000000023	+01884360000000033	-00655460000000000	+001891
0000014	+01715760000000024	+0179906000000034	-0074226000000000044	+000078
0000014	+01715860000000024	+01799060000000034	-0074236000000000044	+0000+
0000014	+0.35405600000000024	+03654160000000034	-000614600000000044	+007848
0 0 0 0 0 1 4	+05389760000000624	+02248060000000034	+0062746000000000044	+014801

+000015	+001252	+001830	+001911	+002016	+002037	+0011994	+001316	+001375	+039635	F000838	+001365	+001798	+001667	+001833	+001733	+001332	+001865	+001727	+001827	+001801	+00200+	+0011963	+001733	+0011963	+001814	+001915	1161101+	+001689	+001911	+001100+	086000+	6/6000+	0+0148056
+0027736000000000000	+00124760000000000	+001949600000000000	+001933600000000000	+001087630000000007	+0020116000000000007	+00196060000000000	+001983500000000008	+0010406000000000000	+001056600000000000000000000000000000000	+001378600000000000	-0074226000000000040	-007422600000000000	-007595600000000000	-00733360000000000	-007230600000000000	-0063756000000000041	-006369600000000041	-006343600000000041	-006347600000000041	-0063456000000000041	-00635360003000000	-006338600000000042	-0063416000000000042	-006359600000000000	-006358600000000042	-006414600000000043	-006514600000000043	-006692600000000043	-006457600000000043	-00558150000000043	-00/4226000000000	-00/422600000000044	0+00000000922900+0
$+001965 \circ 0000000005$	+00123960000000000	+00100000000000000000000000000000000000	+001923500000000000	+00191760000000000	+001382600000000007	+002024500000000008	+001339600000000008	+00193260000000000	+001949600000000000	+0013306000000000000	+01799360000000030	+01752850000000030	+01797560000000030	+01722450000000030	+01735760000000030	+01728860000000031	+0170216000000031	+01701760000000031	+01699060000000031	+0169826000000031	+01815460000000032	+01809660000000032	+01841360000000032	+01838750000000032	+01847960000000032	+0182595000000033	+0.18186500000000033	+01831760000000033	+0184466000000033	+01835560000000033	+01739150000000034	+017992600000000034	0+055465690000000347
805127409000000000	+001245600000000000	+001390600300000006	+0019676000000000006	+001935600000000000	+00195160000000000	+001955600000000000	+00195560000000000	+001955600000000008	+00191760000000000	+001979600000000000	+017159600000000020	+016694600000000020	+01713960000000000000	+01640560000000000000	+0150636000000000000	+01615660000000021	+015185600000000021	+016526600000000021	+0167796000000000021	+017140500000000021	+017091500000000022	+017241600000000022	+01737360000000022	+0174906000010052	+01756760000000022	+014158600000000023	+0136016000000000023	+01398150000000023	+014671600000000	+0160776000000023	+0171586000000024	+0171586060000000024	0+0538946800000000247
0	00000000	00000000	00000000	00000000	0000000	000000000	0000000	00000000	00000000	60000000	0000000	00000010	000000000	00000010	000000000	00000011	00000011	00000011	00000011	00000011	00000012	00000012	0000012	00000012	00000015	00000013	00000013	00000013	00000013	00000013	00000017	00000014	0 00 00 00 0142

+000012	+001248	+001894	+001890	+001985	+00200+	+001962	+001847	+001956	+035505	F000838	+001888	+001636	+001279	+001737	+001634	+001971	+001654	+001679	+001677	+001689	+002000	+001782	+001650	+001783	+001725	+001884	1201 nn+	+001576	+001847	4001C0+		105000+	0+0148056
+002768600000000000	+001243600000000006	+001915600000000000	+00130360000000000000000	+0010496000000000000	+001080600000000000	+001940600000000000	+00194760000000000	+00194160000000000	+001902600000000000	+001847600000000000	-0074226000000000040	-0074226000000000040	-00788460000000000	-007521600000000000	-00739360000000000	-0064126000000000041	-0064126000000000041	-0063916000000000041	-006403600000000041	-006388600000000041	-006399600000000042	-006386600000000042	-0064046000000000045	-00639560000000000	-006406500000000042	-006490600000004300-		-0067656000000000043	-00654060000000043	-0067966000000000-	**************************************	***************************************	0+000000000272000+0
+00196060000000000	+001236600000000006	+001931600000000006	+001889600000000007	+00189860000000007	+00195060000000000	+00139060000000000	+0019386000000008	+00190260000000000	+001932600000000009	+001915600000000000	+01799560000000030	+01749350000000030	+01797560000000030	+01719260000000030	+0168216000000030	+01672460000000031	+0169746000000031	+01697460000000031	+0169306000000031	+0159316000000031	+01799550000000032	+01794750000000032	+01799650000000032	+0179686000000032	+01806260000000032	+0178236000000033	+017753600000000033	+017901600000000033	+0.18039603000033	+01792450000000033	+01799260000000034	+01/993600000000000000000000000000000000000	0+055484600000000347
8071124000000000000	+0012426000000000000	+001956600000000000	+001930600000000000	+00191460000000000	+001942600000000007	+00194060000000000000	+00193160000000000	+00192860000000000	+001905600000000000	+00193860000000000	+01715960000000020	+01667960000000020	+01714260000000020	+01636760000000020	+01601360000000020	+01609460000000021	+01612060000000021	+016390600000000021	+016675500000000021	+017119600000000021	+01691460000000022	+017031600000000022	+017221500000000022	+017349600000000022	+017427500000000022	+01368550000000023	+01283160000000023	+013091600000000023	+013905600000000023	+01555160000000023	+01715860000000024	+017159500000000024	0+05389660030000247
(2)	00000000	00000000	00000000	00000000	20000000	00000000	00000000	0000000	60000000	600000000	00000000	00000000	00000010	00000010	00000010	00000011	00000011	00000011	00000011	00000011	00000012	0000000	00000012	00000012	00000012	00000013	00 00 0 0 13	00000013	00000013	00000013	0000014	00000014	0000000142

8. Test 208180806840

+000015	+001255	+001875	+001870	+0011984	+001887	+001350	+001925	+001927	+035057	F000839	+001791	+001455	+001459	+001585	+001461	+001890	+001459	+001552	+001523	+001533	+001917	+001605	+001517	+001606	+001595	+001840	COOTION	+001459	+001729	116100+	+00004	+000000+	0+0148006
+0027705000000000000	+001251605000000006	+0018946000000000000	+0018346000000000007	+001927600000000000	+0019616000000000000	+001937600000000000	+00192660000000000	+0010446000000000000	+001886600000000000	+0019146000000000000	-007423600000000000	-0074236000000000000	-008325600000000000	-0077356000000000000	-007617600000000000	-006457600000000041	-0064486000000000041	-0064456000000000041	-0064576000000000041	-0064416000000000041	-006454600000000000	-0064426000000000042	-006463600000000042	-006456600000000042	-0064676000000000042	-006602600000000043	540 00 00 00 00 T 69 00 -	-0068856000000043	-00659960000000-	-006976600000-	**************************************	***************************************	0+000270600000000447
+001956600000000000	+0012446000000000000	+001914600000000000	+00187460000000007	→ 00 18 86 60 00 0 00 00 0 0 0 0 0 0 0 0 0 0 0	+001932500000000007	+00198160000000008	+00193960000000000	+001876600000000000	+00132460000000000	+0019266000000000099	+01799560000000030	+01746560000000030	+017374600000000030	+01714360000000030	+016063500000000030	+0159316000000031	+01691850000000031	+01691560000000031	+0168686000000031	+01687260000000031	+01784360000000032	+01778360000000032	+01741760000000032	+01.739660000000032	+01748760000000032	+01721550 00 000033	+01/1040000000	+017321600000000033	+01746060000000033	+0173316000000033	+01799460000000034	+01/334200000000000	0+05548660000000347
3030684000000000000	+001250600000000006	+0019386000000000000	+001914600000000000	+00190560000000000	+001945600000000000	+001938600000000000	+001913600000000000	+00191160000000000000	+00190760000000000	+001899600000000000	+0171586000000000000	+016641600000000020	+01713860000000020	+01632760000000020	+01595060000000000000	+01602460000000021	+01604260000000021	+01521760000000021	+01652460000000021	+01709560000000021	+016735600000000022	+01688160000000022	+01705160000000022	+017172600000000022	+017236600000000022	+01315160000000023	+011800000000000000	+0118426000000000023	+012901600000000023	+014919600000000000	+017159600000000	+0171595000000000	0+053899600000000247
0	00000000	00000000	00000000	00000000	70000000	0000000	0000000	0000000	660000000	60000000	00000010	00000010	000000000	00000000	01000000	00000011	00000011	00000011	00000011	00000011	00000012	00000112	00000012	00000012	00000015	0000013	00000013	00000013	00000013	00000013	00000014	00000014	0000000147

2	180901340000000000	0+0019675000000000	0+002764500000000	0 + 0 0 0 0 1
0000000	0+0012586000000000	0+0012546000000000	0+00126060000000	140040
000000	0+0019416000000000	0+0019195000000000	0+0318976n6n6n6n6n6n6n6n6n6n6n6n6n6n6n6n6n6n6n	0 + 0 0 + 0
000000	0+0019196030000000	0+001876600000000		VOT DO LO
0000000	0+001911600300000	0+00139060000000	0+004040404040	70100.0
0000000	0+001952600000000	0+0013326000000000		
000000	0+0019466000000000	0+0019826000000000000000000000000000000000000		0+00198
0000000	0+0319116003000000	0+001945510010000		\$6100+0
00000000	0+0019096000000000	0+0018745000000000000000000000000000000000000		26100+0
0000000	0+0019136000000000	0+0013736100+0		16100+0
0000000	0+001891600000000	0+0019336000000000000000000000000000000000		72780+0
0000000101	0+0171596000000000000	0+01799660000000000000	0.0010000000000000000000000000000000000	266640040
1000000	0+01663960a0aann2	0+01747060000000		0.100.0
3000001	0+0171396000000000	0+017975600000000000000000000000000000000000		0+00130
0000000	0+0163156000000000	3+01212120000000000000000000000000000000		0+100+0
0000000	0+0159316000000000	0+01550250000000000000000000000000000000		0+00148
0000011	0+016004500000000	0+04 55 58 50 00 0 00 00 00 00 00 00 00 00 00 00 0		0+00138
000000	3+01501550100001000101	14 046 9096 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	n-nnere2e200220004	0+001843
	0+0+04505000000000000000000000000000000	U+ 01689960 00 0 000 31	0-006464600000000041	3+001376
100000	12 90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0+01090150000000031	0-006462600000000041	0+001496
100000	0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 +	0+0108508000000031	0-00647660000000041	0+001436
	0 + 0.1 / USSB UUUU UUE 21	0+01685400000000031	0-006458600000000041	3+001462
	22000000000000000000000000000000000000	0+017784500000000032	0-0064756000000000042	0+00187
	0.51550555555	0+01772350090000032	0-006458600000000042	0+001511
	0 +01 4 8 6 5 0 0 0 0 0 0 5 5 5 5 5 5 5 5 5 5 5 5	0+01715060000000032	0-006477600900000042	0+001460
	0 + 0 + 2 + 6 + 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0+0171305000000000	0-006470600000000042	0+001527
	22 N	0+01/21660000000032	0-00648260000000000	0+001522
	0 + 0 4 6 4 5 5 5 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0+01593150000000033	0-00667260000000043	0+001812
	9 + 0 + 1 3 C C O I O O O O O O O O O O O O O O O O	0+01253760 00 0 00 0 33	0-007010600000000043	3+001594
	C2896000000000000000000000000000000000000	0+01/06/56/03/0/00/33	0-006950600000000043	0+001379
	0+0+0+0+0+0	0+01719550000000033	<b>9-0067636000000000</b>	0+001683
	0+01+0100000000000000000000000000000000	0+01/0240000000033	0-007073600000000043	0+001502
400000	0 + 0 T	0+01/3256000000034	0-007423600000000044	146000+6
4100000	0 + 0 1 / 100 00 00 00 00 00 00 00 00 00 00 00 00	0+01799550 00 0 0 0 0 34	0-007424600000000044	1+0000+0
	0 + 0 2 2 4 7 2 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0+03555000000000	0-00051560000000044	0+007851
+ + 0 0 0 0 0	\$2000000000000000000	0+0>>0>0000000000000000000000000000000	0+03627760000000000	0+014807

1+000116 0+0011386 0+0021386 0+0021286 0+0021286 0+0023276 0+0023276 0+0023276 0+0023276 0+00113806 0+00113806 0+00113806 0+00113806 0+00113806 0+00113806 0+00113806 0+00113806	+001988 +000867 +000867 +007720 +014673
0+0027376000000063 0+0010660000000000000000000000000000000	-00652860000000000+3 -007394600000000044 -00739560000000044 -00603600000000+4
0+0022465000000068 0+00105760000000066 0+002202600000000074 0+00212960000000074 0+00212960000000074 0+00212960000000074 0+002133500000000086 0+01220260000000000000000000000000000000	+0169466000000034 +0173966000000034 +017396600000034 +036480600000034 +055277600000034
22010755000000000051 0+0010726000000000051 0+0022236000000000055 0+0021526000000000073 0+002152600000000073 0+002152600000000073 0+002152600000000073 0+0021526000000000000000000000000000000000	+0121336000000023 +0170956000000024 +0170956000000024 +0353086000000024 +0537895000000024
00000000000000000000000000000000000000	00000013 00000014 00000014 00000014

+014685	+000288600000004	+0553126000000034	+05382560000000024	00000014
3+0008676 0+0077236	0-007403600000000443 4-000602600000000000	0+01/30060;00000000343 0+035439500000000345	0+03633160000000000000	0000000143
+000867	-007403600000000044	+0179016000000034	+017101600000000024	00000014
+002722	-005717600000000043	+02095060000000033	+018610 500000000	00000013
+302772	-005442600000000043	+02092360000000033	+017520600000000023	00000013
+002530	-00568560000000043	+0207606000000033	+016711600000000023	00000013
+002768	-00542960000000043	+0206146000000033	+0156256000000023	00000013
+002627	-00 2246600000000000000000000000000000000	+02076560000000033	+015249600000000023	0000013
+002696	-005375600000000042	+0209636000000032	+018792600000000022	00000012
+002777	-005375600000000042	+02084760000000032	+018787600000000022	00000012
+002532	-00536860000000042	+02091660000000032	+018697600000000022	00000015
+002781	-005377600000000042	+0191716000000032	+01854560000000022	00000012
+002547	-00539060000000042	+01930260000000032	+01830960000000022	00000012
+002643	-00537060000000041	+01683960000000031	+01719950000000021	00000011
+002801	T+000000000+t500-	+01683769000000031	+017569600000000021	00000011
+002784	-005441600000000041	+01587060000000031	+01506460040000021	
+002561	-002449600000000041	+0196306000000031	+016120600000000021	00000011
+002654	-0062616009090960	+01950250000000033	+015879600000000020	00000000
+002828	-0053296000000000	+0170906000000030	+01630950000000020	00000000
+002492	-006537600000000000	+01788250000000030	+01708360000000020	00000010
+002834	-00740360000000000	+0173866000000030	+0165916000000000000	00000010
+002602	-0074036000000000	+0179016000000030	+0171006000000000000000	00000010
F001042	+002353600.0000000	+0622696000000000	+00234260000000000099	60000000
+041718	+00229260000000000	+00238850000000000	+00225360000000000	00000000
+002417	+002290600000000000	+00230350000000000	+00241760000000000	00000000
+002439	+00245360000000000	+0023436000000000	+002357600000000008	0000000
+002447	+00234860000000008	+00251450000000008	+0023756000000000000	000000000
+002537	+00248060000000000	+002393600000000007	+0023026000000000000	200000000
+002432	+002465600000000007	+00222960000000000	+002251600000000007	70000000
+002250	+00227360000000007	+002311600000000007	+002346600000000000	000000000
+002375	+00240160030000006	+0025126000000000006	+002530600000000000	00000000
+00100+	+001093600000000000	+00109050000000000+	+00109360000000000	00000000
+000001	+0027476000000000005	+00226360000000000	2021585000000000000	00000020

12. Test 208220315550

0+000100 0+000100 0+00023236 0+00023236 0+00022386 0+00023326 0+00023326 0+00023326 0+00023326 0+00023326 0+0002336
0+0127456000000053 0+012337600000000071 0+01232760000000071 0+01242760000000075 0+01232960000000075 0+012329600000000073 0+0122576000000003 0+0122576000000003 0+0122576000000003 0+0122576000000003 0+0122576000000003 0+0122576000000003 0+01225760000000003 0+01225760000000003 0+01225760000000003 0+01225760000000003 0+01225760000000003 0+01225760000000003 0+01225760000000003 0+0123986000000043 0+01547460000000043 0+0154746000000043 0+0154746000000043 0+0154746000000043
0+00223150 00 00 00 058 0+00244950 00 00 00 00 00 00 00 00 00 00 00 00 0
220315550000000057 0+001091600000000165 0+0023076000000000000000000000000000000000
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

0000071 0+002213 0000075 0+002400	0000079 0+002466 0000093 0+002392 000091 0+002326 0000095 0+031672 0000099 0F001041	0000403 0+002646 0000403 0+002268 0000407 0+002754 0000411 0+002441 0000413 0+002624	0000415 0+002776 $0000417 0+002776$ $0000421 0+002620$ $0000423 0+002620$ $0000425 0+0026291$ $0000427 0+002724$	
+001096600 +002287600 +002230600 +002381600	+002418600 +002318600 +002366600 +002248600 +002251600 +002272600	-007402600 -006928600 -006654600 -005594600	-005547600 -005472600 -005455600 -005465600 -005501600 -005512600	0-0056336000 0-0055376000 0-0059286000 0-0055386000 0-0059066000 0-0074036000 0-00066000
+ 00109560000000006 + 00237660000000006 + 00224360000000007 + 00220460000000007	+00236050000000007 $+002453600000000008$ $+00230150000000000$ $+00224450000000000$ $+00224450000000000$	+ 0173016000000030 +0178826000000030 +0169286000000030 +018520600000031 +016668600000031	1555530000000031 $166156000000031$ $16820600000031$ $189486000000032$ $138576000000032$ $20043600000032$	+019914600 $+019752600$ $+019933600$ $+020114500$ $+020105500$ $+017903600$ $+01790360$ $+01790360$
+0010996003000000006 +0023936000000000006 +00222760000000000	+002272600000000000000000000000000000000	+0165136000000020 +0170806000000020 +01556000000020 +015860600000021 +0159136000000021	+01536060000000021 +0171836000000021 +0178676000000022 +0180636000000022 +0184045000000022 +0184045000000022	0+01406160300000231 0+01391260000000233 0+01508160000000235 0+01610260000000237 0+31766163000000239 0+31710160000000243 0+01710050000000243 0+05383860000000247
20000000000000000000000000000000000000	00000000000000000000000000000000000000	00000010 00000010 00000010 00000011	00000011 00000011 00000011 00000012 00000012 00000012	0 0 0 0 0 0 0 1 3 1 0 0 0 0 0 0 0 1 3 3 3 0 0 0 0 0 0 0 1 3 3 5 0 0 0 0 0 1 3 7 0 0 0 0 0 1 4 1 3 9 0 0 0 0 0 0 1 4 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

4. Test 208220514450

00 00 073 0+00220150 00 00 077 0+00233250 00 00 085 0+00228560 00 00 093 0+00227560 00 00 203 0+00223750 00 00 203 0+01223750 00 00 203 0+0179660 00 00 203 0+01794460 00 00 213 0+01794460 00 00 213 0+01794460 00 00 213 0+01794460 00 00 213 0+01794460 00 00 213 0+0165850 00 00 213 0+0165850 00 00 223 0+01957760 00 00 223 0+01957760 00 00 223 0+01957760 00 00 223 0+01957760 00 00 233 0+01957760 00 00 233 0+01957760 00 00 233 0+01957760 00 00 233 0+01957760 00 00 233 0+01957760 00 00 233 0+01957760 00 00 233 0+01957760	0+002279600000000073 0+00221500 0+00222760000000073 0+002201500 0+00231560000000073 0+00223260 0+002254600000000003 0+002285600 0+0022796000000003 0+002227600 0+0022796000000003 0+002227600 0+01710160010000003 0+00223760 0+017702600000000201 0+01796600 0+01571600000000213 0+0158460 0+01571600000000213 0+0158260 0+01712660000000213 0+01658260 0+01726600000000213 0+01658260 0+01746600000000221 0+016580 0+01726600000000221 0+01656260 0+01726600000000221 0+01957600 0+01784060000000221 0+01957600 0+01784060000000221 0+01957600 0+01784060000000221 0+01956260 0+01340660000000231 0+01957600 0+01340660000000231 0+01957600 0+013406600000000231 0+01956260 0+01340660000000231 0+01956600 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+019550600 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000 0+01340660000000231 0+01956000
0000073 0+0 0000073 0+0 00000381 0+0 00000382 0+0 0000203 0+0 0000213 0+0 0000213 0+0 0000213 0+0 0000223 0+0 0000223 0+0 0000233 0+0 0000233 0+0 0000233 0+0 0000233 0+0 0000233 0+0 0000233 0+0 0000233 0+0 0000243 0+0	+ 002227600000073 0+ 0022276000000077 0+ 0023156000000000181 0+ 0 022546000000000181 0+ 0 022546000000000185 0+ 0 + 00225460000000000003 0+ 0 + 0022106000000000000003 0+ 0 + 012266000000000000000000000000000000000
	+ 10226460 + 10231560 + 10227960 + 10227960 + 10221060 + 10231160 + 11710160 + 11710160 + 1159860 + 11577160 + 11577160 + 11578660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 1176660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 117660 + 11770 + 11710 + 11

0000000000	22061365000000000057	0022525000000000	00275160000000000	+00000
90000000	+001103600000000000	+001099500000000000	+00110160000000000	+00110
000000000	+002291600000000000	+002275600000000006	+002222600000000000	+00220
90000000	+0022546000000000000	+00220460000000000	+002201600000000000	+00218
00000000	+002208600000000000	+002185600000000007	+002276600000000000	+00534
20000000	+002239600000000000	+00228750000000007	+002357600000000000	+00541
00000000	+002265600000000000	+00237450000000000	+00225860000000000	+00229
00000000	+002216600000000000	+002250600000000000	+002289600000000000	+00226
0000000	+002242600000000000	+00220160000000009	+002231600000000000	+00227
60000000	+002188600000000000	+002223600000000099	+00221960000000000	+02760
600000000	+002562600000000000	+00221850000000000	+002262600000000000	F00104
00000010	+017102600000000020	+01790860000000030	-0074036000000000	+80213
00000000	+016439600000000020	+61721960000000030	-007404600000000040	+00218
00000010	+01708160000000020	+01788460000000030	-00756960000000000	+00191
00000010	+0160446000000000000	+01682550000000030	-00712250000000949	+00233
00000016	+01553660000000020	+017112500000000030	-006979600000000040	+00212
00000011	+015688600000000021	+0170146000090031	-005658600000000041	+00215
0000011	+015756600000000021	+01652850000000031	-005654600000000041	+00232
00000011	+016304600000000321	+01653050000000031	-00559260000000041	+00194
00000011	+01683860000000000	+01647560000000031	-01560860060000041	+00238
00000011	+017165500000000021	+016469500000000031	-00555860000000041	+002198
00000015	+0174516000000000	+0185860000000032	-00557160000000000	+002421
21000000	+0176346000000000022	+01851460000000032	-005585600000000042	+002461
00000015	+017905600000000022	+0189666000600032	-00559760000000042	+0000+
000000015	+018055600000000022	+01893360000000032	-002289600000000042	+002581
00000015	+0181036000000000	+01904060000000035	-00559860000000000	+002323
00000012	+012736600000000023	+01875650000000033	-00596860000000000	+002567
00000013	+011468600000000023	+0186116000000033	-00592860000000000	+002472
00000013	+0127706000000000023	+0188095000000033	-00628760000000043	+0000+
00000013	+01436860000000023	+019002500000000033	-0057876000000000	+002487
00000013	+016324600000000023	+01894760000000033	-006207500000000043	+002374
0000007	+017103600000000024	+01790660000000034	-007404500000000044	+00087
00000017	+01710360000000000000	+01790560000000034	-0074046000000000	+0000+
00000014	+035339600000000000+	+0364996000000034	-0000202000000000	0+0022406
00000014	+053844500300000054	+ 02235660000000034	+00528660900000	+01469

16. Test 208220712550

9 0+0000116 7 5 5644466	0 + 0 0 1 1 1 0	3 + 03 C C 0 3 C	06720048	155200+0	00+200+0	0+002308	0+002232	0+002226	0+023621	0F001040	0+002155	3+002002	3+001828	0+002191	3+001925	0+005555	0+002137	0+001856	0+032186	0+002029	0+005355	3+002354	0+001857	0+002392	3+002201	0+002345	0+005284	3+031862	0+005433	0+005562	6 2 8 9 0 0 + 0	678000+0	04//00+0	1+01+02
C+0027576000030000000000000000000000000000000	+00111560000000000000000	+00226260000072700+	10000000000000000000000000000000000000	+0022/2800000000	+005328600000000000	+00227160000000000	+0025496000000000000	+002241600000000000	+002210600000000000	+0025426000000000000	-007404500000000000	-0074045000000000000	-0079646000000000000	-007347600000000000	-007162600000000000	-005677600000000041	-005675600000000041	-00562060000000041	-0055396000000000001	-00558760000000000	-00560560060000042	-005614600000000042	-00562960000000042	-00561760000000042	-005634600000000042	-002888000000000000000	-006156600000000043	-00632869000000043	-00284060000000000	-006324600000000043	-007405600000000044	-00 240 28 000 000 044	-000204200000000-	+000228260000000000+
0022876	+001114500000000000000	+ 00 225550 00 0 000 0	+ 005501600000000	+00218950000000000	+0022786000000000	+00235950000000000	+002237600000000	+002130500000000000	+00222950000000000	+002228~0000000000000	+0179086000000030	+01721360000000030	+01788550000000030	+01679860000000030	+01631960000000030	+0162926000000031	+01650250000000031	+01650350000000031	+01644160000000031	+01643760000000031	+01347860000000032	+0183866000000032	+01837550000000032	+0183526000000032	+01849150000000032	+01819360000000033	+01798960000000033	+01822760000000033	+0184546000000033	+0183276000000033	+01730750000000034	+01790660000000034	+0365076000000034	+055301500000000034
00000000	+001117600300000	+0.02285600000000000000	+0022566003000100	+102212600000000000	+09525360099000000	+0022586003000000	+0422036000000000000	+002245600000000000	+002189600000000000	+902245600000000000	+01710260000000120	+01642860000000020	+0170816000000020	+01601650000000020	+0155036000000020	+01564760000000021	+01571460000000021	+01630060000000021	+01673760000000021	+01709960000000021	+0173386000000000	+017510600000000022	+017778600000000	+01796160000000022	+01798160000000022	+0124006000000000023	+010663600000000023	+011531600000000023	+0137236000000000023	+01560760000000023	+0171626000000000024	+017102600000000024	+0353386000000024	+053838600000000054
0 3 3 3 3 0 0 1 2 0 8	000000000000000000000000000000000000000	00000000	00000000	0000000	0000000	000000000	00000000	00000000	90000000	00000000	00000010	0000010	00000010	00000010	00000010	00 00 0 11	00000011	00000011	00000011	00000011	00000012	00000012	00000012	00000012	30 000 012	0000000	00000013	000000013	00000013	00000013	00000014	00000014	00000014	00000014

17. Test 208220810950

	*			
+01420	+00628660000000004	+05532550000000034	0578196000000000024	0.00.000.0147
0+0008826	0-007404659000000443	0+017906500000000343	0+	000000
+00008	-0024055000000000	+01790660000000034	+0171036030000002+	910000000
+00514	-00640950000000043	+0176556000000033	+01,328460000000023	00000013
+002341	-00613160000000043	+ 07 7 7 9 3 5 0 0 0 0 0 0 0 0 3 3 4 0 0 0 0 0 3 3 4 0 0 0 3 3 3 4 0 0 0 0	+11889261111010111123 +1116246111101011123	00000013 00000013
+00238 +00181	-006154600000000043	+01732950000000033	+0103566000000000023	00000013
+002010	-000164600000000043	+0175646000000033	+012230600000000023	00000013
+002011	-005635600000000042	+017948500000000032	+01796560000000022	06 00 3 0 1 2
+002152	-005615600000000042	+01757250000000032	+01794860000000322	21000000
+001722	-005625600000000042	+01775260000000032	1775160000000022	500000000000000000000000000000000000000
+002327	-0056146000006042	+01836260000000032	2260000009474.	0000012
+00103	-002567600000000-1	+ 616 + 57 + 60 30 0 0 0 0 31 + 01 8 4 5 9 5 0 30 0 0 0 0 32	0.17.035500000000000000 0.17.3176000000000000	
+001091	-00563760000000000	+01643560000000031	+01671760000000000021	00000017
+001663	-00562760000000041	+0164926000600031	+01623460000000021	00000011
+00200+	-005575600000000041	+01649660000000031	+0157046999999931	00000011
+001788	-00567660000000041	+015893600000031	+011555600000000001	0000011
+001756	-00747960000000040	+01492850000000030	+015492500000000000000000000000000000000000	000000000000000000000000000000000000000
+002941	-00776560000000049	+01679350000000030	+0150095000000050+0+	
+001659	0 70 00000000 TT 71 00 -	+ 01/29450 09 0 0 0 0 3 0 4 0 0 3 0 0 3 0 0 3 0 3 0 3	+0.16412600.109.0020	
759100+	0.0000000000000000000000000000000000000	+01790960000000030	+01769160000000000	03000010
F901041	+002259600000000000	+00228250600000009	+00226+600000000000	60000000
+025254	+00222760000000000	+00220360000000009	+00220360000000000	60000000
+002200+	+00223160000000000	+002222606000000000	+00222660000000000000000000000000000000	000000000000000000000000000000000000000
+002228	+00222060000000000	+ 00552000000000000000000000000000000000	+002200600000000000	000000000000000000000000000000000000000
+002298	+00228160000000000	+ 032335000 00 00000000000000000000000000	+0052125002123005 +00525466640000000	0000000
+002379	+00235260000000000	+00513530000000000	+ 00222880000000000 + 0022186000000000000	
+0021204	+002192600000000000	+002190600000000007	+00225160000000000	0000000
+002195	+00220860000000000	+0022545000000000000	+0022786000000000000	0000000
+001112	+0011-0660000000000	+001109500000000006	+00111369999999999	000000000
+000C011	+03275760000000000	+002293600000000005	2031095000000000005	0200000

+00//45 +014706	-10050460000000044 +005291600000000044	+ 036 5 07 50 00 0 0 0 0 0 34 + 05 53 35 60 00 0 0 0 0 0 34	+035338600000000024 +0538486000000000024	90 00 00 014 00 00 00 014
0+0008336	0-0074056000000000043	0+01/90550000000341 0+017906500000000343	0+91/1026000000000241 0+0171026000000000243	000000143
+002011	-0065406000000043	+0169645000000033	+01212760000000023	0000013
+002150	-006265600000000043	+0.17095600000000033	+010233500000000023	000000000000000000000000000000000000000
+002326 +001593	-006188600000000043 -006729600000000043	+016587500000000033 +0158205060000033	+01031460000000000 +0187206000000000	09 000 013 66 66 67 68
+001676	-0064896000000000	+0163815000000033	+01220960000000023	0000003
+001877	-005641600000000042	+0171756000000032	+01795060000000022	00000012
+002039	-00562,460000000042	+01697950000000032	+01792360000000022	00000012
+001466	-00563160000000042	+01708450000000032	+017739600000000	0000000
+002273	-005622600000000042 -00562260000000000042	+0183496000000032 +01834960000000032	+017465600000000022	00000012
+001694	-005593600000000041	+01643550000000031	+01709960630000021	00000011
+001745	-0056426000000000041	+0154286000000031	+0166986000000021	00000011
+001394 +001394	-005631600000000041	+01649160000000031 +015485000000031	+015/05600000000071	000000011
+001551	-00568160000000041	+01456760000000031	+015638600000000021	00000011
+001603	-007728600000000040	+0135346000000030	+0154976000000020	0000010
+001773	-0079736000000000	+01679560000000030	+01601660000000320	01000000
+001405	-009820600000000040	+ 01788360 00 0 00 0 30	+01708160000000020	00000010
+001822	-0000000000000000000-	+0172006000000000000000000000000000000000	+015405500000000000000000000000000000000	200000000000000000000000000000000000000
+00100+	-002405600000000000	+ 00225350 90 0 000 39 + 01790850 00 0 0 0 0 30	+0023195000000000000	
+026695	+00225360000000000	+0022346000000000	+005183600000000000+	60000000
+002232	+00 225 46 00 00 00 00 00 0	+002213500000000009	+002261600000000000	00000000
+002228	+002247500000000008	+0022825000000000	+0021996000000000	000000000000000000000000000000000000000
+002335	+002259600000000000	+00235650000000000	+002320600000000000	១១០១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១
+002398	+00238960000000007	+002263500000000007	+002212600000000007	20000000
+002380	+00256960000000000	+ 00 5 5 T ± 00 00 0 00 0 0 0 0 0 0 0 0 0 0 0 0	+0822//8889888988 +0822356888	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
+005505	+00/2234600000000000000000000000000000000000	+ 00 22 7 7 50 00 0 00 00 00 05 + 00 22 1 1 50 00 0 00 00 00 0	+0023016J690000000 +3322750030000006	000000000000000000000000000000000000000
+001141	+00113860000000000	+ 00 1 1 3950 00 0 000 0	+10111396000000000006	00000000
210000+	+0000000000011200+	+002329500000000000	20 30 1220 100 100 10 10 12	00000020

+014/02	+10062836000000000+	* 05 5 5 5 5 5 6 0 0 0 0 0 0 0 5 4	+0538580000000004	10000n
+007744	-00000000000000-	+036500600000034	+03533460000000024	00000
0+0008836	00740660090000000 007405600000000	0+0179055000000000341 $0+017905500000000343$	0+0171026000000000241	000000141
+001928	-00663060000000043	+0165375000000033	+011445600000000023	0 000 013
+002022	-0063576000000000043	+0166596000000033	+009934600000000023	0000013
+001433	-00686060000000000	+01637250000000033	+0084716000000023	0000013
+002264	-0062086000000043	+0161326000000033	+010292600000000023	0000013
+001767	-00000000445600-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	+ 01646560 00 0 000 33	+0121956000000000023	0000013
+3017945	-00255550000000000-0555500-	+01655350000000032 +01675650000000032	+0179136003000005+0+	0000012
+001318	-00263460000000000	+01665860000000032	+017734600000000022	0000012
+002251	-00562760000000042	+0183386000000032	+01745460000000022	0000012
+001473	-0055166000000000000-	+0184396000000032	+01728160030000022	0000012
+001629	-005643600000000041	+016430500000000031.	+015693600000000021	0000011
+001244	-005634600000000041	+01643860000000031	+01628960000000021	0000011
+001879	-0056806000000041	+01649350000000031	+01569960000000021	0000011
+001391	-00568350000000041	+0137496000000031	+01,563260000000021	0000011
+001514	-007886600000000000	+012831600000030	+0154896000000000000000000000000000000000000	0000010
+901680	-0981016000000000	+0167916000000003	+016012600000000000000000000000000000000	0000010
+6011776	0 70 0 0 0 0 0 0 0 0 0 7 0 0 <b>-</b>	+ 01/21350 00 0 0 0 0 0 3 0 + 0 1/2 8 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+0164256000000000000	
+001473	-0024026000000000	+0179096000000000000	+01710260000000000000	0 00 0 0 1 0
F001041	+00230160000000000	+00226460000000000	+002304600000000000	6000000
+027946	+002234600000000000	+00223060000000000	+00216560000000000	60000000
+002230	+00225160000000000	+002182500000000000	+0022526000000000	0000000
+002198	+002231600000000000 +00231600000000000	+ 00227550 00 0 000 08	. 025233000000000000000000000000000000000	00000000
+000230 +000230	**************************************	**************************************	**************************************	
+602371	+002241600000000007	+0021996000000000	+392224603000000000	2000000
+002195	+002207600000000000	+00220160000000000	+00220760000000000	900000
+002208	+00222260000000000	+002267600000000006	+002292600000000000	0000000
+001132	+001130600000000000	+001127500000000006	+00113160000000006	0000000
+000015	+0027566000000000005	+002325600000000000	2100245000000000000	0000000

. Test 208221107960

0000000057 0+50283 $000000071 0+00274$ $00000075 0+00306$	000000079 0+00319 000000033 0+00313 000000087 0+00262	000000091 0+00292 0000000095 0+03472 000000099 0F01125 0000000000000000000000000000000000	000000403 3400201 000000405 0+00111 000000407 0+00247 000000411 0+00185	000000413 0+00290 000000415 0+00105 000000417 0+00245 000000419 0+00182	000000423 0+00313 000000423 0+00313 000000427 0+00270 000000429 3+00204 000000431 0+00164	1000000633 0+003204 $1000000635 0+001305$ $1000000437 0+002821$ $1000000443 0+000888$ $1000000445 0+000888$
0+0031546	0+00256596	0+0029016 0+0026956 0+0029606 0-0074066	0-00/4055 0-0092486 0-0078126 0-0077466	0-0045195 0-0045066 0-0045146 0-0044266	0-0044908 0-0044908 0-0044938 0-0044938	0-00503960 0-00578460 0-00530760 0-0054066 0-0074066 0-0074060
	0+0027855000000000 0+00278550000000000 0+0031095000000000000000000000000000000000	0+0025875000000000000000000000000000000000	0+017947500000000000000000000000000000000000	0+0161786000000031 0+0161736000000031 0+0161055000000031 0+016103600000031	0+019576000000032 0+0194576000000032 0+0162326000000033 0+0165546000000033	0+015593600000000333 0+016027600000000335 0+01646160000000337 0+01628160000000334 0+01791160000000341 0+0179116000000343
+11500000000000000000000000000000000000	+10257060000000000 +00257060000000000 +002978600000000000 +002539600000000000	+00302260000000000 +00259760000000000 +00297060000000000 +01710560000000020	+01625960000000020 +01707560000000020 +0157326000000000 +0150596000000020	+01551560000000021 +01633860000000021 +01738260000000021 +01717360000000021	+0183616000000000000000000000000000000000	0+010122600000000233 0+00737460000000235 0+0097986000000237 0+01009760000000237 0+01710560000000241 0+03534560000000245
	, , , , , , , , , , , , , , , , , , ,	00000000 00000000 000000000 000000000	00000010 00000010 00000010 00000010	00000011	00000012 00000012 00000012 00000012 00000013	0 0 0 0 0 0 0 0 1 3 3 0 0 0 0 0 0 0 1 3 5 0 0 0 0 0 0 1 3 5 0 0 0 0 0 0 1 4 1 0 0 0 0 0 0 0 1 4 5 0 0 0 0 0 0 0 0 1 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

0+0000136 0+0011186	+00200+	+002810	+003078	+003250	+003089	+003095	+003057	+031788	F001252	+003325	+003841	+003188	+003781	+003496	+003194	+003800+	+003185	+003703	+003517	+003503	+003799	+003327	+003675	+003646	+003385	+003765	+003372	+003690	+003717	+0000888	+000988	+007751	+014/10+
0+00277060000000000000000000000000000000	+003030800000000000	+002851660000000007	+0031396000000000007	+00312960000000000	+00294360000000000	+00310360000000000	+00289360000000000	+002868600000000000	+00297560000000000	-00740860000000000	-00740850000000000	-00616460000000040	-005836600000000000	-005735600000000000	-004457600000000041	-0044716000000041	-004439600000000041	-004425600000000041	-00431260000000041	-00432860000000042	-0.04380600000000042	-004344600000000045	-)04353600000000042	-004348600000000045	-004729600000000043	-0044356000000000043	-034958600000000043	-00445760000000043	-00482960000000043	<b>-007408600000000044</b>	-007409500000000044	-000607600000000044	+100629060000000004
0+00294950000000058 0+00111650000000062	+00313550000000000	+00291960000000000	+002799600000000000	+00302160000000000	+00319160000000000	+00295860000000000	+00288150000000000	+00301150000000000	+00285160000000000	+01791060000000030	+01714360000000030	+01788660000000030	+01672360000000030	+0200226000000030	+02024360000000031	+01635060000000031	+01538850000000031	+01633550000000031	+01634160000000031	+02007150000000032	+01991860000000032	+02238250000000032	+02229050000000032	+0224396000000032	+02219360000000033	+02194760000000033	+02215460000000033	+02238660000000033	+02231850090000033	+01790960000000034	+017909600000000034	+03020650000000034	+02233220000000034
221215860000000000057 0+0011196000000000000	+003213500000000000	+0029576000000000000	+00280860030000007	+002867600000000000	+0.0300160000000000	+0029596000000000000	+00304+600000000	+00279560000000009	+002979600000000009	+01710350000000020	+01637560000000020	+01707960000000020	+01594660000000020	+01527560000000020	+01563260000000021	+01557760000000021	+01658060000000021	+01782269090909321	+0172536000000021	+018964600000000022	+01928460000000322	+0195446000000022	+019724600000000022	+019659600000000022	+013827600000000023	+01438450000001053	+0156746003000023	+018066600000000023	+01915560000000023	+0171036000060020	+0171025903000024	+03533760000000024	+6228286000000005+
0 0 0 0 0 0 0 0 0 0 0 0 0	00000000	00000000	200000000	200000000	0000000	60000000	0000000	60000000	60000000	00000010	00000010	000000000	000000000000000000000000000000000000000	00000010	00000011	00000011	00000011	00000011	00 00 0 11	00000012	0000012	0000012	00000012	09009012	00000003	00000013	00000013	00000013	00000013	00000017	00000014	0000000	00000017

+000124 +00134 +002963 +002816	+ 00 30 64 + 00 30 84 + 00 30 84 + 00 30 59 + 00 30 24	F001252 +003299 +003788 +003041 +003041 +003743	0 + 00 37 826 0 + 00 37 826 0 + 00 36 16 0 + 00 34 116 0 + 00 37 806 0 + 00 37 806 0 + 00 37 806 0 + 00 36 46 0 + 00 36 56 0 + 00 36	+014/12
+00277960000000000 +001130600000000000 +00298560000000000 +00284160000000000	+0.0311460000000000000000000000000000000000	+0029446000000000000000000000000000000000	0-0045256000000411 0-00444360000000413 0-00444360000000413 0-00443600000000413 0-00440660000000421 0-00440760000000421 0-00440760000000423 0-00446760000000423 0-00446760000000423 0-00446760000000423 0-00446760000000423 0-00446760000000423	+006288600000000
+ 602851500000000005 + 661131500000000066 + 003132500000000066 + 00289260000000007	+0028105000000000000000000000000000000000	+ 00285450 00 000 09 09 09 + 01791050 00 00 00 03 0 + 01710560 00 00 00 03 0 + 01738450 00 00 00 00 03 0 + 01936560 00 00 00 00 03 0 + 01938650 00 00 00 00 03 0 + 01938650 00 00 00 00 03 0 + 01938650 00 00 00 00 03 0 + 01958650 00 00 00 00 03 0 + 01958650 00 00 00 00 03 0 + 01958650 00 00 00 00 03 0 + 01958650 00 00 00 00 00 03 0 + 01958650 00 00 00 00 00 00 00 00 00 00 00 00 0	0+0199866000000313 0+01629360000000313 0+01623360000000315 0+0162376000000317 0+0199006000000323 0+0219316000000323 0+0218526000000323 0+0217276000000333 0+0217356000000333 0+0217366000000333 0+0219356000000333	+ 02534560 00 0 000 34
213155500000000005 +0011335000000000 +003153500000000 +0029385000000000	+ 0 0 2 8 2 4 6 0 0 0 0 0 0 0 0 7 4 0 0 2 8 6 1 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+002967609000000099 +01710260090000320 +0153116000000020 +0170766000000020 +0151846900000020	0 + 015519600000000213 0 + 01553960000000213 0 + 016489500000000215 0 + 01767360000000219 0 + 018736600000002219 0 + 01904660000000223 0 + 01956860000000223 0 + 01956860000000223 0 + 01959600000000233 0 + 01710160000000233 0 + 01710160000000245	+053848600300000
00000000000000000000000000000000000000	00000007 040000007 00000008 00000008 0000000000	00 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000000113 $0.000000113$ $0.000000113$ $0.000000113$ $0.000000113$ $0.000000123$ $0.000000133$ $0.000000133$ $0.000000133$ $0.000000133$ $0.000000133$	00000014

0 + 00 23 0 1 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	$\begin{array}{c} 0 - 0.04404600000000000021\\ 0 - 0.0447660000000000023\\ 0 - 0.0447660000000000023\\ 0 - 0.044760000000000023\\ 0 - 0.044760000000000023\\ 0 - 0.04532600000000433\\ 0 - 0.05316600000000433\\ 0 - 0.05316600000000433\\ 0 - 0.0517600000000433\\ 0 - 0.051160000000443\\ 0 - 0.0741160000000443\\ c + 0.0528860000000445\\ \end{array}$	0+01975660 00 00 0321 0+01975660 00 00 00 323 0+0213760 00 00 00 323 0+02147160 00 00 00 327 0+02147160 00 00 00 323 0+02121460 00 00 00 333 0+0212160 00 00 00 333 0+02135650 00 00 00 337 0+02135650 00 00 00 337 0+01791160 00 00 00 341 0+01791160 00 00 00 345	0+01856160000000221 0+01856160000000223 0+01920360000000223 0+01934560000000225 0+01934560000000229 0+01934560000000233 0+01489960000000233 0+01489960000000233 0+015742600000000235 0+01710460000000245 0+01710460000000245	0000000121 0000000123 0000000123 0000000131 0000000133 0000000133 0000000133 0000000133
+002981 +003737 +003110	-00447660000000042 -00447660000000042 -0044760000000042	+0197565000000032 +019606600000032 +021377600000033	+01856160000000022 +01885060000000022 +0192036000000022	00000012 00000012 00000012
+002930 +003638 +003307	-004487600000000041 -00449860000000041 -0046460000000041	+0162346000000031 +01616360000000031 +01616660000000031	+01640060000000021 +017520500000000021 +01721060000000021	000000011 000000011 00000011
+003152 +003040 +003727	-00610660000000000 -00458560000000041 -00458060000000041	+01871460000000030 +01889960000000031 +0162336000000031	+01511960500000020 +015438600000000 +01553660000000021	00000010 00000011 000000111
+003699 +002856 +003678	-00741150000000000 -0066616000000000 -00523260000000040	+ 01 7 0 8 2 50 00 0 0 0 0 0 3 0 + 01 7 8 8 5 50 00 0 0 0 0 0 3 0 + 01 5 5 9 8 50 0 0 0 0 0 0 3 0	+016300600000000020 +01707760000000000 +0158216000000000	00 00 0 0 1 1 0 0 0 0 1 0 0 0 0 0 0 0 0
F001251 +003201	+002929600000000000000000000000000000000	+0028806000000000 +01791350000000030	+0029796000000000000000000000000000000000	000000000000000000000000000000000000000
+003008 +003008	+002693600000000009 +002893600000000009 +00287060000000000	+ 0028650000000000 + 00286500000000000 + 00294950000000000	+005999600000000000000000000000000000000	80000000
+003213	+003119600000000000 +002938600000000000	+ 00303960000000007 + 00319260000000008 + 003192600000000	+002862600000000007 +0030146000000000000	000000000000000000000000000000000000000
+002833	+002858600000000007 +003087600000000000	+ 0028 9260 00 0 0 0 0 0 0 7 + 0028 30 50 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+0029516000000000000000000000000000000000000	000000000000000000000000000000000000000
+001165 +001165 +002942	+0011636000000000000 +0011636000000000006 +00297060000000006	+0.0162500000000000000000000000000000000000		900000000 900000000
400004	100 000 000 00 10 10 10 10 10 10 10 10 1	BOOD OF THE STATE OF THE	24 24 52 50 00 00 00 00 05	0000000

+014725	+006289600000000044	+0223326000000034	+053863600000000000	00000014
0+0077596	0-00/41/06/00/00/00/45	0+017912500000000343 0+03651460000000345	0+0171046000000000243	0000000143
+000084	+0000000000044	+01791260000000034	+017104600000000000+	0000000
+003463	-00519560000000043	+02085660000000033	+017349600000000023	00000013
+003516	-00469860000000043	+6208826000000033	+016294600000000023	00000013
+002838	-00541460000000043	+0205916000000033	+01418260000000023	00600013
+003636	-00478960000000043	+0203486000000033	+01073860000000023	00000013
+003065	-004895600000000043	+0206876000000033	+012417600000000023	00000013
+003284	-00449260000000042	+02034360000000032	+0192356000000000022	00000012
+003628	-004489600000000045	+02075860000000032	+0193236000000000	00000012
+002796	-004473500000000042	+6208345000000032	+01905860000000022	00000012
+003661	-00448260000000042	+0195296000000032	+018723600000000022	000000000000000000000000000000000000000
+003028	-00,000,000,000,00- -00,000,000,000,00-	+01011 00 00 000 00 0 + 0 + 0 + 0 + 0 +	+01/13068#0900000<	000000011
+003595	-00451160000000041	+01611960000000031	+017429600000000021	0000011
+002733	-00449360600000041	+01618860000000031	+0163506003000321	00000011
+003499	-00451860 00000041	+01619650000000031	+015522600000000021	00000011
+002989	-004605608,00000041	+0183666000000031	+01538360000000021	00000011
+002942	-005238600000000040	+0180916000000030	+015073600000000000	00000000
+003525	-006385500000000000	+0165695000000030	+0157876000000000	000000000000
+002741	-0069006000000000	+01788650000000030	+3170786000000000000000	000000000000000000000000000000000000000
+003314	-007408600000000040	+0170515000000030	+01625760000000000000	00000010
+00210+	-007408600000000040	+0179146000000030	+01710460000000020	00000010
F001253	+002949600000000000	+002878500000000009	+00296960000000000	65000000
+019895	+00288860000000000	+00293150000000000	+002797600303030303	60000000
+002978	+00290560900000000	+00286150000000000	+00300000000000000000000000000000000000	000000000000000000000000000000000000000
+002966	+003046600000000008	+00236360000000000	+002879600000000000+	000000000000000000000000000000000000000
+003087	+00293060000000000	+0031716000000000	+00301760000000000	000000000000000000000000000000000000000
+003219	+00312560000000007	+0029976000000000000	+0028515000000000000	00000000
+00200+	+00303660300000007	+00282850000000000	+80584850808088485084	00000000
+002821	+002838600000000007	+00287850000000000	90000000009956005+	00000000
+002917	+002340600000000000	+00307250000000006	+00311960000000006	000000000000000000000000000000000000000
+001169	+001167600000000000	+001168500000000006	+001107648888888888	
+00000+3	+00277869090000095	+002907500000000005	215148500000000000000	0.000000

0+0077646 0+0147266	0+0006036000000000445	0+03552450 00 0 000 345 0+05535250 00 0 000347	0+03535060000000000245 0+0538546000000000247	000000145
+0000897 +0000897	-00741050000000004+ -007410500000000004+	+ 017913600000000034 + 017913600000000034	+0171056000000000000000000000000000000000	0000014
+003367	-005335600000000043	+02012250000000033	+01532160000000023	0000013
+003483	-00498760000000000	+02014150000000033	+01305950000000023	0000013
+002691	-00567360000000043	+0198065000000033	+01119960000000023	0 000 013
+003627	-00 48305000000063	+0195835000000033	+010235600000000023	0000013
+002885	-005294600000000043	+0199676000000033	+0123126003000023	0 000 013
+003176	-004490600000000045	+0202226000000032	+019179600000000022	0000012
+003530	-004486600000000045	+01997950000000032	+01927560000000322	0000012
+002610	-00 4467600000000042	+0201395000000032	+01904260000000022	0000012
+003665	-00448360000000042	+0134865000000032	+0186816000000022	0000012
+002714	-00 443260000000000	+01954750000000032	+0183946000000000	3000012
1400000+	-004508600000000041 -00441760000000041	+ UI 61 U / 50 UU U U U U SI + U1 61 U 860 OU U U U U SI	+0174036000000000021 +01749160030000021	0 000 011
+002476	-00420060000000041	+0161816000000031	+01634660000000021	0000011
+003455	-00461260000000041	+01518863000000031	+01551260000000021	0000011
+002601	-00461260000000041	+0175975000000031	+01536160000000021	0000011
+002790	-006595600000000000	+0168686000000030	+0150536000000020	0 000 0010
+003257	-006805600000000040	+0165450000000030	+01575560000000020	0 000 0 10
+002467	-007528600000000000	+01783660000000030	+01707560000000020	0000010
+003263	-00740960000000040	+0170505009000039	+011526260000000020	0.0000000
+002736	-0074096000000000	+01791550000000030	+01710560000000020	0000010
F001252	+002902600000000000	+0028806090000000	+002933600000000000	000000
+023725	+00285760000000000	+00288160000000000	+00230260000000000	6000000
+002926	+00288360000000000	+00282160000000000	+00295360000000000000	000000
+002918	+1029906000000000000	+0029435000000008	+00283460000000000	8000000
+003055	+00293560000000000	+0031325000000000	+0030046000000000	0000000
+003187	+0000000009460000+	+00295850000000000	+00281760000000007	7000000
+003070	+00299360000000000	+002796500000000007	+00281760000000000	0000000
<b>\$002793</b>	+0028076000000000	+002847500000000000	+002910600000000000	000000
+002881	+0029046000000000000	+00303035600000000006	+0033946000000000000+	0000000
+001147	+001143600000000000	+00114160000000000	+001145500000000000	0000000
+00000+	+002779600000000000	+00289760000000035	2151.46000000000005	u 00 0 0 2 0

1+0000126 0+0011486 0+0028796	0+003073	0+003183	3+002874	0+002935	0+023736 0F001253	0+002364	0+003150	0+003028	0+002624	0+002219	0+003333	0+002152	0+003070	0+602714	0+003579	0+002270	0+003275	3+002969	0+002541	0+0035/0	0+003270	0+003152	668000+0 0+000899	0+007766	0+014728
0+002781600000000059 0+001144600000000053 0+002901600000000067	+0053246000000000000000000000000000000000000	+003097600000000000	+0023816000000000008	+002885603000000000	+002840600000000000 +00291150000000000	-00240360000000000	-007409600000000040	-66 /85 ISBBBBBBBBBB -007117606600000000	000000000000000-	-00462060000000041	-00461860000000041	-0045096000000041	-00451260000000044	-004425600000000041	-0044402000000000045	24000000009424400-	-00 4493600000000045	-004495600000000045	-00200000009E49E00-	-0043220000000000043	-005070600000000-	-002532600000000000	-00741 060000000000- -00741 060000000	44000000000000000	+00629360000000044
0+002914500000000058 0+0011445000000000052 0+003037500000000055	+00284400000000000 +002796600000000007	+002916600000000007	+ 00 23 4 20 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+002794500000000000	+ 0029036000000000000 + 00287260000000000	+01791360000000000	+01704750090000030	+ OI / 55560 00 0 0 0 0 3 3 3 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	+0150326000000030	+0158366000000031	+0161706000000031	+01516760000000031	+01609850000000031	+01610550000000031	+ 01 952950 00 0 0 0 0 0 32 + 01 9450 69 00 0 0 0 0 0 32	+01920560000000032	101902850000000032	0192775000000032	+ 01 90 20 50 00 0 00 0 0 33	- 01 85 01 50 00 0 0 00 0 3 3	+ 01917660 00 0 0 0 0 0 33	10191555000000033	+ 01 79 1250 00 0 0 0 0 0 34 + 01 79 1250 00 0 0 0 0 0 34	+0365216000000034	+0553586000000034
221713650000000000057 0+0011486000000000061 0+003090600000000065	+00290%5000000000000 +002813600000000000	+90277360000000000000	+032134660146060 +0027966001000000	+00296760030000	+0027596000000000000 +00295460000000000	+01710163000000320	+0152576030900920	+01/0/56/00/00/00/20 +015/52/60/00/00/00/00	+015057600000000020	+315557600000000021	+01550560000000000	+010328600000000	+01737860030000021	+01718860090000021	+018374o003000000 +0186565000000000	+01902564000000322	+01925260030303022	+019151500000000022	+01228860000 0 00 23	+818185588888888888	+012030600000000023	+013629600000000	+0171016000000000 +0171015000000000	+03534660000000024	+053873600000000024
000000000000000000000000000000000000000	00 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00 00 00 00 00	មម្រុក មួយ មួយ មួយ មួយ មួយ មួយ មួយ មួយ	0000000	60000000000000000000000000000000000000	00000010	000000000000000000000000000000000000000	00000010	0000000000	00000011	00000011	00000011	00000011	06900011	00 000 012	00000012	00000012	00000000	00000013	00000013	00000013	00000013	00000014	0000001+	00000014

7. Test 208221812760

+014731	+00059360000000000+	+03535560000000034	0+053868600000000024	00000014
0+0009006	0-0074105000000000443	0+01/9125000000000000000000000000000000000000	0+0353486000000000245	0000000143
006000+	-007411600000000044	+01791250000000034	0+017103600000000024	00000014
+002951	-0056456000000000043	0184536000000033	0+0125576001000023	00000013
+003154	-005149600000000043	+01845850	0+011399600000000023	00000013
+002078	-006156500000000043	+0131365000000033	0+009912600000000023	00000013
+003483	-00496760000000043	01785060000000033	0+010125600000000023	00000013
+002543	-0058836000000000	101831350 00 0 000 33	0+01227760000000023	000000
+002770	-00 4497600000000042	-0185906000000032	0+0191546000000000022	00000012
+003168	2400000009264400-	0183136000000032	0+01924760000000122	00000012
+001978	-00447760000000000	101850760000000032	0+019015600000000	00000012
167200+	2+00000000+++00-	10194516000000032	0+0186455000000000022	00000012
+002516	-004431600000000041	- 016	0+01/18850JJJJJJJJJZ1 J+0183726JJJJJJJJJJZ1	
+002935	-00451560000000041	-016104600000000031	0+017381600000000021	0000011
+001889	-00450860000000041	101617260000000031	0+016321600000000	00000011
+003280	-00462260000000941	1016169600000000031	0+015500600000000021	00000011
+001069	-004621500000000	101455260 00 0 0 0 0 0 3 1	0+015350600000000021	00000011
400000+	- 0.0 1.0 1.0 0.0 0.0 1.0 1.0 0.0 0.0 0.0	- 013809600000000000000000000000000000000000	0+01505260000000020	00000010
+801918 +1109800	-000000000000000000-0	- 01 655 n 60 n 0 n n n n 3 n	0+01577560060000020	0000000000
+00 3098	-007410500000000000	FU17059600000000030	0+01026060000000000000000000000000000000	000000000000000000000000000000000000000
+00200+	-00741060000000640	-017913600000000030	0+017102600000000020	0000010
F001253	+00292060000000000	<b>- 0028756000000000</b> 00	0+0029886000000000	6000000
+024788	+00282960000000000	+00293160000000000	0+0027396000000000	60000000
+002951	+00289960000000000	+00277460000000000	0+00299560000000000	0000000
100001	+ 0 0 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0+0027596000000000	80000000
+000191 +004004			0+0030175000000000000000000000000000000000	
+003084	+002915600000000000	+002805600000000000	0+0058296000000000000000000000000000000000000	
+002798	+00281560000000000	+ 00284950000000000	3+002914600000000000	0000000
+00298	+00290660000000000	+00304360000000000	0+013098600100011	90000000
+00115	+00115360000000000	+001152600000000006	0+00115560000000000	90000000
+00001	+00278260000000000	+0029316000000000	22181276000000000000	000000020

0+0000136	+002874	+003086+	+903211	+003117	+002752	+005048	+030035	F001253	+001753	+00 3069	+001523	+002714	+002569	+001608	+003172	+001440	+002693	+002200+	+0012100+	+003303	+001240	+005884	+005480	+001823	+003308	+001685	+002929	+005674	+00000+	+000001	+ 4 4 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	ナウンナイコト
0+002780600000000059	+00289360000000000	+002832600000000007	+00313660000000007	+00274060000000000	+002363600000000000	+00290160000000000	+002803600000000000	+00293560000000000	-0074106000000000040	-007410600000000040	-00857960000000000	-00757550000000000000	-0074986000000000040	-0046216000000000041	-004617600000000041	-004507600000000041	-00451260000000041	-004427600000000041	-004439600000000042	-004491600000000042	-004471600000000042	-0044856000000000045	-004432600000000045	-0061086000000000	-00 43 22 20 00 00 00 04 3	-0064546000000000043	-0052516000000000043	-002893600000000000	-00741160000000000044	-007411600000000044	***************************************	+000589600000000
0+002948500000000058 0+0011406000000000062	+00302960000000000	+ 00279350 00 0 00007 + 00279350 00 0 000007	+0028095000000000+	+00313460000000000	+002945600000000008	+002719600000000000	+002339500000000000	+00235350000000000	+01791469900000030	+917057600000000030	+01783560000000030	+01654960000000030	+01225350000000030	+01286450000000031	+01617460000000031	+01617250000000031	+01610650000000031	+01609960000000031	+0195335000000032	+01945560000000032	+0175096000000032	+01731260000000032	+01761150000000032	+017301500000000033	+01674960000000033	+017078600000000033	+01749950000000033	+017397500000000033	+01791260000000034	+01791250000000034	+03551450000000034	+02255420000000000
2213110500000000000057 0+00114450000000000051	+003088600000000000000000000000000000000	+0029035000000000000000000000000000000000	+00265860000000007	+00300460000000000	+002680600000000000	+003015600000000000	+0026796000000000000+	+0030116000000000000	+017103600000000000000	+016252500000000320	+017072600000000020	+015775600000000020	+015053600000000020	+0153496000000000	+0155056909000021	+01633060000000021	+01738560000000021	+01719060000000021	+01836860000000022	+0185515009000022	+01902360000000022	+01925160000000022	+019150666000000022	+01227269030909023	+0101036000000000023	+008763600000000023	+01068060000000023	+01124960000000023	+0171026000000000024	+017102600000000000+	+032344600000000000	+0538866000000000054
0 0 0 0 0 0 0 0 2 0 8	000000000	000000000000000	26000000	00000000	0000000	0000000	6000000	60000000	00000010	00000000	00000000	00000010	000000000	00000011	00000011	00000011	00000011	00000011	00000012	00000012	00000012	00000012	00000012	00000013	00000013	00000013	00000013	00000013	00000014	00 00 0 0 14	00000014	00000014

000000000000000000000000000000000000000	22210106000000000057 0+0011556000000000000	0+002939500000000058 0+0011535000000000062	0+002778600000000059 0+001152600000000053	0+0000136 0+0011556
90000000	+00303052000000000000+	+00304060000000000	+002904600000000000	+002883
30000000	+002915500000000000	+002849600000000007	+002315600000000000	+002797
2000000	+002823600000000007	+00280550000000000	+002737500000000000	+003120
3000000	+30260060000000000000	+002382600000000000	+0032676000000000007	+003241
00000000	+0030396500000000000+	+00313860000000008	+002734600000000000	+003230
១១ ដា ០ ១០១	+0025166003000030	+00300350000000000	+002940600000000000	+002608
0000000	+003036600000000008	+0025935000000000000	+002324600000000000	+002950
60000000	+005535600000000000	+ 30 30 32 50 00 0 000 00	+00,270,2600000000000	+028928
60000000	+002965600000000000	+0023305000000000000	+00302060000000000	F001254
00000000	+01710360000000000000	+01791560000000030	-00741160000000040	+001377
000000000	+015259600000000020	+01706350000000030	-00741160000000000	+002627
30 000 010	+017075600000000020	+0178376000000030	-009437600000000040	+0000+
000000000	+0157756903090329	+01656350000000030	-0080396000000000	+002562
000000000	+015 055600000000	+00985360000000030	-00792560000000000	+301487
0000001	+0153696909090000	+0101406000000031	-004623600000000041	+001164
00 00 0011	+015509600000000021	+01517260:00 0 00031	-004624600000000041	+002671
00000011	+016330500000000021	+01016650000000031	-004514600000000041	+0000+
00000011	+0173726000300021	+0160956000000031	-004519600000000041	+002561
00 30 6 011	+01718860000000021	+0151016000000031	-004431600000000041	+001441
00000012	+01836960000600022	+0195316000000032	-004446000000000045	+001288
00000012	+01854560000000022	+01946350000000032	-0049760000000042	+002972
0000012	+019019600000000022	+01553550000000032	-00476600000000042	+000828
00000015	+01924560000000322	+01539050000000032	-004499600000000045	+002826
00000015	+01914660000000022	+01575650000000032	-004499600000000045	+001632
00000013	+012267630303030333	+01533960 00 0 000 33	-006265600000000043	+001584
00000013	+01009460000000023	+01471560000000033	-00520160000000043	+003158
00000000	+00859060000000000+	+0151775000000033	-007021600000000043	+001010
00000013	+0084936000000023	+01563860000000033	-0053076000000000	+00/2957
00000013	+00330560000000023	+01545260000000033	-00659060000000043	+001840
00000017	+017102600000000024	+01791260000000034	-0074116000000000044	<b>406000+</b>
90900014	+0171046000000000	+01791360000000034	-007411600000000044	<b>+06000+</b>
00000014	+035350500000000024	+03651950000000034	-000060560000000000	+007773
00000014	+053874600000000024	+0553606000000034	+0023660000000000	+014729

0.000.0000	222101060000000000057 0+0011556000000000000	0+0029395000000000058 0+0011535000000000062	0+0027786000000000059 0+0011526000000000053	0+0000136 C+0011556
0 0 0 6	+00308560000000000	+003040600000000006	+002904600000000000	+002883
0000	+002915600000000000	+00284960000000000	+002315600000000007	+002797
2006	+002823600900000007	+002805500000000000	+0027375000000000007	+003150
0.637	+302600500300000007	+002382600000000000	+00326760000000000	+003241
00000	+0030306000000000000+	+00313860000000008	+002734600000000000	+003230
110003	+00251560030000308	+003003600000000008	+0029+060000000000	+002608
0000	+0030305600000000000	+002593~00000000000	+0003000009+56200+	+0056200+
60000	+0026356000000000000	+ 30303250000000000	+002702600000000000	+028928
60000	+01295560010000139	+00230050000000000	+003020600000000000	F001254
00.019	+0171035000000000000	+01791560000000030	-007411600000000000	+001377
01000	+01525960000000020	+01706350000000030	-00741160000000000	+002627
00010	+01707560030000020	+01783760000000030	-000000000000000000	<b>548000+</b>
00000	+01577569000000120	+01656350000000030	-00803960000000000	+002562
00010	+015 055600000000	+00985360000000030	-007925600000000000	+301487
00011	+01536969090000021	+0101406000000031	-00462360000000041	+001164
00011	+01550960000000001	+01517250.000000031	-004624600000000041	+002571
00011	+01533050000000021	+01516550000000031	-004514600000000041	+0000751
00011	+01737260009000021	+01609560000000031	-004519600000000041	+002561
06011	+017188600000000021	+01510160000000031	-004431600000000041	+001641
00012	+01836960000500022	+0195316000000032	-00444400000000045	+001288
00012	+01854560000000022	+01946350000000032	-0049760000000042	+002972
00012	+01901960000000022	+01553550000000032	-00476600000000042	+000858
00012	+01924560000000322	+0153905000000032	-00463660000000065	+002826
00012	+019146600000000022	+01575650000000032	<b>-00 463 36 00 00 00 00 00</b>	+001632
00013	+01226760000000023	+01533950 00 0 00033	-006265600000000043	+001584
99013	+0100946000000000	+01471560000000033	-00520160000000043	+003158
00013	+002230200000000023	+01517760000000033	-007021600000000043	+001010
00013	+00849360000000023	+01553850000000033	-00530760000000000	+00°2957
21000	+00930560000000023	+01545260000000033	-006590600000000043	+001840
0.0.114	+017102600000000024	+01791260000000034	-007411600000000044	+06000+
00014	+017104600000000	+01791360000000034	-007411600000000044	<b>†</b> 06000+
00014	+035350500000000024	+0365190000000034	-000060560000000000	+007773
00034	+05387460000000024	+02236060000000034	+00236600000000000	+014729

l. Test 208240108070

+01080700000000007 0+00320460000000	+00320460000000005		+0025825000000	0000
	300000000000000000000000000000000000000	+00003000000000+	+000937600000000000	+000038
+00	74060000000007	+003674500000000000	+00344440000000000000	+003395
+00	368600000000000	+003265600000000007	+00 32 0 56 0.0 00 00 00 07	+003182
+00	235600000000007	+003211600000000007	+003283600000000007	+003674
0+	2546000000000000000000000000000000000000	+003562600000000007	+0039176000000000007	+00400+
+0	356460030000309	+0038316000000000	+003360600000000000	+003901
+0	3002600000000000	+00350769000000008	+00357960000000000	+903704
0+	372060000000000	+0030000000000000000+	+003332600000000000	+003574
0+	3208500000000000	+00358860000000000	+003216600000000000	+056515
-	3257600000000000	+003407~000000000	+0035096000000000000000	F001449
+0	712160000000020	+0179336000000030	-00739160000000000	+002278
+	1609460000000020	+01532360000000030	-007391606000000040	+003649
+	1708760000000220	+01794760000000030	-003840600000000049	+000032
+	155545000000020	+0163736000000030	-0003466000000000040	+004171
+	14625600000000020	+00756860000000030	-00861160000000000	+001400
+	151776000000021	+00763760000000031	-003269600000000041	+30200+
₹•	152346000000021	+0.1587960000000031	-00332860000000041	+003536
+	1562060000000021	+0158715000000031	-0032326000000000041	+00004
+	180866000300321	+01580360000000031	-003229600000000041	+004050
+	1736260090000021	+01581550000000031	-00311250000000000041	+001458
+	19615600000000022	+0211106000000032	-003131600000000042	+001853
+	199976000000022	+0203196000000032	-003112600000000042	+003438
+	205636000000322	+01554350000000032	-003078600000000042	+000260
+	20809600000002	+0155106000000032	-00306460000000000	+003871
+	2057360000000022	+0155825000000032	-0030486000000000042	+001482
+	1223360000000023	+01496660000000033	-005371600000000043	+002388
+	0982150000000023	+01413360000000033	-004195600000000043	+003880
+	0710360000000023	+0150956000000033	-006748600000000043	+0000662
+	05441600000000023	+0153916000000033	-00404660000000043	+003819
+	0677260000000023	+01504360600000033	-007049600000000043	+001977
+	1711960000000024	+01797960000000034	+0001393600000000000	+0000963
)+0	117119600000000243		0973936000000000044	+00000+
+	35324600000000024	+0366216000000034	-00020360000000000	+007815
+	5379760000000024	+02245350000000034	+00027760000000000+	+014759

2. Test 208240215670

	+00349760000000057 0+003439	+0032496000000011 0~00321/ +0036.7600000000075 0+003682	0+00362660000000079 0+0035555 0+00362660000000079 0+0038056	+00338560010000083 0+003567	+003626600000000087 0+003598	+00334560000000001 0+003540	+003299600000000095 0+041897	+003433600000000099 0F001448	-007395600000000401 3+004114	-007395600000000403 0+005024	-00506560000000000000000000000000000000	-005458600000000407 0+004941	-00528,5600000000409 0+004267	-00324160000000411 0+003891	-00332060000000413 0+004973	-003227600000000415 0+003928	-003211600000000417 0+004800	-00308860000000419 0+004397	-03312860090000421 0+003864	-003102600000000423 1+004982	-003061600000000425 0+004113	-00304860000000427 0+004666	-003038600000000429 3+004626	-00386360000000431 1+004028	-00325560000000433 0+004982	-004340600000000435 0+004214	-00334360000000437 0+004649	-004080500000000439 0+004815	-007396600000000441 0+000963	-00739560000000443 0+000962	-00060460000000445 0+007816	+0025/3200000000044/0+014/22
+0000043900000000004	+0037216000000000066	+ 00331750 00 0 000 070 + 0033350 00 0 000 026	0+0020202020202020202020202020202020202	+0037555000000000082	+003+18600000000036	+0033176000000000090	+0034516000000000094	+00328450000000098	+017979603000301	+01693250000000303	+01794660000000305	+01639060000000307	+02022450000000303	+02080460000000311	+01590950000000313	+01591250000000315	+01584660000000317	+01584350000000319	+02112560000000321	+02089150000000323	+02367550000000325	+02351260000000327	+0237806000000329	+02348560000000331	+023939500000000333	+02331360000000335	+02367450000000337	+02352166000000339	+017977500000000341	+01797750000000343	+035518500000000345	+0>>4/3000000000004/
0+000947600000000000	+003790600000000000	+003403600000000000	+003305600000000000	+003483600000000000	+000000000000000++000+	+003520600000000000	+003232600000000000	+003480600000000000	+017118500000000020	+01610+60000000020	+01708560000000020	+015567600000000020	+014646600000000020	+01519960000000021	~01524560000000021	+0165556000000021	+01813260000000021	+01736760000000021	+01968360000000022	+02012260000000022	+02062260000000022	+02089760000000022	+020682600000000022	+012354600000000023	+0099876000000000023	+015095600000000023	+0173516000000000	+01485260000000023	+017120600900000024	+01711860000000024	+035335000000024	+023802600000000050+
0 0 0 0 0 0 0 0 0 0 0 0	30 00 0000			60000000	80000000	000000000	60000000	60000000	00000010	00000010	000000000000000000000000000000000000000	00000000	01000000	00000011	00000011	00000011	00000011	00000011	00000012	00000012	00000012	00000	00000015	0000013	00000013	00000013	00000013	00000013	00000014	00000014	00000014	00000014

0+0000126	+003430	+003214	+003588	+003812	+003263	+003280	+003538	+035731	F001449	+004008	+004959	+003748	+004872	+004215	+003774	+004951	+003820	+004745	+004331	+003749	+004942	+004025	+004639	+004608	+003942	+0020010	+004126	+004621	+004829	+030963	\$ 0.50 nn+	+014766
0+002569600000000059	+00349060000000000+	+003242600000000007	+0036416000000000007	+003627600000000000	+00336960000000000	+003625600000000000	+00334660000000000000	+003298600000000000	+0034306000000000000	-007395600000000000	-0073966000000000040	-00613660000000049	-00555160000000040	-005395600000000000	-00324860060000041	-00332360300000041	-0032306000000000041	-00322150000000041	-00310360000000000	-0031346000000000042	-003114600000000042	-00307960000000042	-00307060000000000	-00305060000000000	-00 396 860000000043	-00326066000000043	-004403600000000043	-003404600000000043	-00411360000000043	-0073976000000000	-00/28/28/2000/00/00/00/00/00/00/00/00/00/00/00/0	-nnaonzonanna++00020000000000++
0+003318600000000058	+0037146000000006	+003306600000000007	+003234500000000007	+00345460000000000	+003758600000000000	+003416600000000008	+003296600000000000	+00345960000000000	+00329760000000000	+01797660000000030	+01694350000000030	+01794150000000030	+016372500000000030	+01979660000000030	+02037850000000031	+01590160000000031	+0158966000000031	+01583360000000031	+01584650000000031	+0210946000000032	+02083350000000032	+0233756000000032	+02321950000000032	+02351350000000032	+02320460000000033	+ 02272750.00 0 0 0 0 0 33	+02303450000000033	+0233996000000033	+0233506000-000033	+0179756000000034	+01/9/4500000000034	+02027220000000034 +0227420000000034
	+00378260000000000000	+00340260000000000	+00326260000000007	+003295600000000000	+003483600000000000	+00342960090000308	+00351+6000000000000	+003223600000000000	+0034936000000000000	+017117600000000020	+0160876000000020	+41707860000000020	+01556460000000020	+01463160000000020	+01518560000000021	+0152436000000021	+01664160000000021	+01811160000000021	+017362600000000021	+019645600000000	+02005360000000022	+0205916000000022	+02084360010000022	+020623600000000022	+012354500000000023	+0100566000000000023	+014755600000000023	+0167786000000000023	+018360600000000	+0171176000000002+	+0171156000000000000	+0537966000000000000+0+053796600000000000000000000000000000000000
0000000	000000000000000000000000000000000000000	00000000	70000000	00000000	00000000	00000000	00000000	9000000	60000000	00000010	0100000	00000000	00000000	G 0 0 0 0 0 1 0	00000011	00000011	00000011	00000011	00000011	00000012	00000012	0000012	00000012	00000012	00000013	00000013	00000013	00000013	0000013	00000014	0000014	0 0 0 0 0 0 0 1 4 7

34. Test 208240415370

0+0009636 0+0078196 0+0147726	0-0073966000000000443 0-000802600000000445 0+00628060000000447	0+01797450000000343 0+0361760000000345 0+0554766000000347	0+0171166000000000243 0+03532960000000245 0+053803500000000247	0 00 00 0 0 1 43 0 0 0 0 0 0 0 1 43 0 0 0 0 0 0 0 1 47
+003929	-004592600000000043 -003528600000000043	+ 02242250 00 0 00033 + 02279960 00 0 00033	0+01+23260000000023 0+01591260000000023	00000013
+003763 +004967	-0041326000000000043 -003379600000000043	+0226216000000033 +02210760000000033	0+012344600000000023 0+010021600000000023	00000013
+004511	-003034200000000045 -003036000000000045	+ 02252850 00 000032 + 02232250 00 0 000 32	0+020840600000000022	000000012 00000012
+003779	-00306760000000000	+0227376000000032	0+0205856003000022	00000015
+0073264	-0031026000000000-	+ UZ I I U U DU U U U U U U SC + UZ U 8 35 50 00 0 0 0 0 0 32	0+020030600000000022	<b>6</b> 666612 <b>0</b> 066012
+004503	-003099600000000041	+0158386000000031	0+0173576030000021	0000011
+004568	-0032196000000000041	+015576599999994451 +01531950000000031	0+0180516000000000	11000000
+004868	-00 3322600000000041	+0158876000000031	0+01523560030303031	00000011
+003578	-003259600000000000	+01924550000000031	0+01517260000000021	0000011
+004027	-01263660000000000	+ 01 85 7650 00 0 000 30	0+01+623600000000020	000000010
+003551	-0063076000000000	+0173405000000030	U+U1708460000000020	u0000010
+004826	-0073966000000000040	+0169306000000030	0+01610760000000020	00000000
+003810	-00739560000000000	+01797650 00 00 00 00 00 00 00 00 00 00 00 00 0	0+01711560000000000000	03300010
F001448	+0034346000000000000	+ 00 331550 00 0 000 09	0+003218640444040	60000000000000000000000000000000000000
+003545	+0033576000000000000	+00323560000000000	0+003535600000000	00000000
+003245	+003624600000000000	+003424500000000000	0+00338460030000000	00000000
+003577	+00334760000000000	+033774500000000000	0+0034836000000000000	00000000
+003829	+003630603000000000	+003+3760000000007	0+003265600000000007	
+003212	+ 50 32 386 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+00329560000000007	0+00339760000000000	00 00 00 00
+003421	+00347660000000000	+60370550000600006	0+1037c9600000000	00000000
+00004	+00000000946000+	+000000000000000+	0+0000000000000000000000000000000000000	00 00 00 00 00 00 00 00 00 00 00 00 00
+0000012	+005570600000000000	+0033246000000000005	24041537000000000000	00 00 0 020

1+0000126 1+0000506 1+0000506 1+00037096 0+0037096 0+0037096 0+0037096 0+0037096 0+0037096 0+0037096 0+0037096 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706 0+0033706	0+005050 0+004605 0+004619 0+000964 0+007621
0+00257160000000053 0+00095060000000053 0+00322360000000073 0+00322360000000073 0+00331060000000000 0+00331060000000000 0+00331060000000000 0+00332360000000000 0-0032360000000000 0-0032360000000000 0-0031106000000000 0-00311560000000000 0-003115600000000000 0-0031156000000000000000000000000000000000	-00444500000000043 -00365760000000043 -00739760000000044 -0073976000000044 +0066776000000044
0+0033396000000062 0+0009496000000062 0+00328160000000074 0+00322560000000074 0+003762600000000078 0+00376260000000000 0+00376260000000000 0+00376260000000000 0+0037626000000000 0+003766000000000 0+00376600000000 0+0179476000000031 0+017746000000031 0+015826000000031 0+0210825600000032 0+02108256000000032 0+0210826000000032 0+021082600000033	+ UZ135350 UU 0 UU 0 33 + DZ135350 UU 0 UU 0 33 + DZ131050 UU 0 0 0 0 0 33 + D1797860 UU 0 0 0 0 34 + U3562660 UU 0 0 0 0 0 34 + U5547160 UU 0 0 0 0 34
24051507000000000057 0+000952600000000051 0+003385600000000059 0+003252600000000077 0+003252600000000077 0+003485600000000077 0+0034856000000000000000000000000000000000000	+0145446000000023 +01454460000000023 +0171186000000024 +0171176000000024 +0353396000000024
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000014 00000014 00000014 00000014

5. Test 208240614270

00000000	4061427000000000	+00335950000000000	+002567600000000005	+000012
0.0000000000000000000000000000000000000	0+00095250000000000000000000000000000000	0+0002402000000000000000000000000000000	0+0034746000000000357	0+0034196
000000000000000000000000000000000000000	+00333560000000000000+	+003299600000000004	+103235600000000007	+003210
20000000	+0032636000000000007	+003240500000000000	+00 3455600000000000	+003646
200000000	+003172600000000000	+003430500000000000	+003659600000000+	+003884
00000000	+0035066000000000008	+00377850000000000	+00329660000000000	+003516
00000000	+003228600000000008	+00342550000000000	+00323060000000000	+003351
60000000	+033578600000000000	+ 60 31 37 50 00 00 00 00 0	+003220600000000000	4003564 4003564
60000000	+0031086330333033	+003524600000000000	+00 323860000000000	+035300
60000000	+0035146000000000000	+003294600000000000	\$00 <b>0000000000000000</b>	F001445
00000010	+0171166000000000000	+01797850000000030	-0013976000000000000	+002992
00000011	+0150846000000000000	+0169366000000030	-00239660000000000	+004221
00000000	+01708350000000320	+01794750000000030	-00231360000000000000	+002200+
000000000	+015554600000000000000	+01637460.0000000030	-006495600000000000	+004503
00000010	+01462560000000020	+01+912500000000030	-006439500000000046	+003200+
00000011	+01517260000000021	+0152825000000031	-003271600000000041	+002828
0000011	+0152455,0000000021	+0158886000000031	-00332460000000000041	+004572
00000011	+01663160000000021	+0159775000000534	-00322860000000341	+002595
00000011	+01310360000000221	+0153216000000931	-00321960000000000	+004013
00000511	+017355600000000021	+ 3158 30 50 00 0 000 31	-3031036000000000041	+003200+
00000012	+0190336000000000	+0211056000000032	-0,0 31 2 7 50 0 0 0 0 0 0 4 2	+002955
21000000	+02000076000000022	+02082350000000n32	-¢0 310 86 00 30 00 042	+004686
000000	+02055960000000022	+020+475000001032	<u>-0030745000000000045</u>	+002722
00000012	+02081450000000022	+02024150000000032	-003067600000000042	+004105
000000.2	+020565600000000022	+02057050000000032	-00304.8600000000042	+003825
00000013	+01229660000000023	+02024566000000033	-0048465000000000043	+003524
00000013	+0098136000000000	+01967660000000033	-00369260000000000	+004789
00000013	+01117260000000023	+02301450000000033	-005321600000000643	+005000
00000013	+01254760000000023	+020454660000000033	-003391600000000043	+004213
00000013	+01367960000000023	+02044560000000033	-00427660006000043	+004163
000000014	+017115600000000024	+011977600000000034	++0000000926200-	+00.0965
0000000	+017116600300000024	+01737750000000034	++0000000926200-	+00000+
00000014	+0353286000000000	+03652360000000034	-00060460000000044	+007821
00000014	+05381360000000054	+0554776000000000034	+10000000000000000000000000000000000000	+014111

000000000000000000000000000000000000000	2407125700000000000057 0+00096960000000000000	0+003390500000000058 0+000968500000000062	00256	0+0000126 0+0009706
	+003//2000000000000000000000000000000000	+ 00 33 0 50 00 0 00 00 00 00 00 00 00 00 00 00	+0035516000000000000000000000000000000000	003224
000000000000000000000000000000000000000	+00313860070000007	+0034776000.0000007	+0038426000000000007	+003942
0000000	+003571600000000000	+00380960000000008	+00330060000000000	+003797
80000000000000000000000000000000000000	← £030/960000000000000000000000000000000000	+00304860000000000	+00000000998+00+	+003530
60000000	+00303636000000000000	+00361860000000000	+00 3147600000000000	+03,8061
609000000	+00333360000000000000	+0033605000000000	+00324560000000000	F001448
00000010	+01711960000000000020	+0179826000600030	-007397600000000040 -007397600000000040	+005438
00000010	+0170836000000000	+017950600000000030	-008846600000000048	+001775
000000000000000000000000000000000000000	+01552960000000020	+0163596000000030	-00717763000000040	+003892
00000010	+0146156000000000000	+01121050000000030	-00704760000000000	+005644
30000011	+01517160000000021	+01151760000000031	-0032806460000041	+002200+
00000011	+015243600000000021	+01589050000000031	-003334600000000041	+003918
00000011	+0106276000000021	+0158805000000031	-00324450000000001	+001731
00000011	+018084600000000	+01561660000000031	-003230600000000041	+0032666
00000011	+017358600000000021	+01583350000000031	-00312060000000041	+002571
00000015	+019625600000000022	+0211025000000032	-04313760000000042	+002265
0000012	+019995600000000	+02030660000000032	-803125600000000000	+004117
00000012	+0205526003000322	+01913960000000032	~003082~0000000045	+001826
00000012	+4218105000000000+	+01785650000000032	-0030846000000045	+003704
000000012	+0'c 0549600000000022	+0182765000000000	240 00 00 00 00 00 00 00 0 0 0 0 0 0 0 0	# 1 2 2 2 2 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5
000000000000000000000000000000000000000	+015204650090000000 +0084550000000003	+ OT / SCOSO CO O O CO 33 + O1 / O / O / O O O O O O O 33	24000000000077600 <del>-</del>	+00700+
00000013	+0023846000000000000000000000000000000000000	+01751550000000033	-00612060300000043	+001980
000000	+00940760000000023	+01804860000000033	-0039836000000043	+003874
000000013	+0104706933009023	+0179870000000033	-0057296000000000043	+003199
00 00 0 0 1 4	+01711960930000324	+017979600000000034	-007398600000000044	+0000967
00000014	+01/1196000000000000+03+03560000000000000000000	+03653050000000034	**************************************	+007822
00000014	+05381360000000024	+05548450000000034	+000276600000000004	+014775

0 0208 0 0030	240508070000000000057 0+0009806000000000000	0+00,0351,50-10,0000058 0+00,097850,00,0000062	0+0025716000000000000000000000000000000000000	0+0000126 0+0009806
	+003785609000000000	+ 00371050 00 0 000006. + 00370660 00 0 000005	+003490600000000000	+003434
	+003250÷000000000000	+003261600000000	+00332860000000007	+003723
	+003304600000000000	+0035065000000007	+00 395760000000000000	+004003
	+0035056000000000000	+003866500000000000	+00340860000000000	+002620
	+0030336000000000000	+003546500000000008	+00360860000000000	+003144
	+003764690400000008	+003346500000000000	+003371600000000000	+003583
	+0.03235000000000000	+003724600000000009	+00 326660000000000	+037691
_	+0032/3600000000000	+00344860000000000	+00324160000000000	F001448
	+01711760000000000000	+017979600000000030	-007397600000000000	+002255
-	+018093500003030320	+01893450000000030	-0073976000000000	+003972
	+01768465.000000020	+017942600000000030	-00885660000000000	156000+
	+01554650000000000	+01637850000000030	-003323600000000000	+004188
_	+0146316000000000000	+00765650000000030	-008455600000000040	+501417
	+01517460030000021	+007723500000000031	-003283600000000001	+001992
	+0152565000000000	+015388500000031	-03331600000000041	+003484
	+016625600000000021	+01587950000000031	-00324560900000041	+0000772
	+01808466030000021	+0.15814500000000031	-003233600000000041	+00400+
_	+017356500000000021	+0158256000000031	-00312860000000641	+001667
	+01960860000000000	+02108360000000032	-00314360000000000	+001919
	+31998560030000322	+0203055000000032	-0031326000000000042	+003437
	+020533600000000022	+0156516000000032	-0030986000000000	+00002
	+02075950000000022	+01548050000000032	-00309760000000000	+003898
_	+02053560000000022	+01560550000000032	-0030716000000000042	+001487
	+0122836000000023	+01484150000000033	-005397600000000043	+005254
	+00384660000000323	+01421350000000033	-004285600000000043	+003921
	+007093600000000023	+0150856000000033	-00673060000000043	+000175
	+00537660000000023	+01540250000000033	-00405660000000043	+003819
_	+005881600000000023	+01503950000000033	-00698760000000043	+001395
	+017115600000000024	+01797750000000034	-0073986000000000044	+00000+
	+01711860090000124	+01797850000000034	+0002338600000000000	+00000+
	+032360000000024	+03661960000000034	-0000000000000000-	+007822
_	+05381560010000024	+05548350000000034	+00627660000000004	+014775

+000012 +000985 +003445 +003239	+103960 +003941 +003257 +003542 +034730 F001446	+003413 +001094 +0012954 +001222 +001918 +003113 +002993	0.+00.10.20 0.+00.21.736 0.+00.037.36 1.+00.091.86 0.+00.091.86 0.+00.361.16 0.+00.12.336 0.+00.12.336 0.+00.16.296 0.+00.096.86 0.+00.096.86 0.+00.096.86
$\begin{array}{c} 0+00.256.06.0009.0000\\ 0+00.034.975.0000000000\\ 0+00.326.860000000000\\ 0+00.352.960000000000\\ \end{array}$	0+0039646000000000000000000000000000000000	0-0073986000000000000000000000000000000000000	$\begin{array}{c} 0 - 0.315760000000419\\ 0 - 0.03153600000000421\\ 0 - 0.03199600000000423\\ 0 - 0.03073600000000425\\ 0 - 0.0307360000000427\\ 0 - 0.0508860000000429\\ 0 - 0.058016000000433\\ 0 - 0.0580160000000433\\ 0 - 0.0580160000000433\\ 0 - 0.07899600000000443\\ 0 - 0.0789960000000443\\ 0 - 0.07899600000000443\\ 0 - 0.07899600000000444\\ 0 - 0.078996000000000444\\ 0 - 0.0789960000000000444\\ 0 - 0.0789960000000000444\\ 0 - 0.0789960000000000000000445\\ 0 - 0.0789960000000000000000000000000000000000$
+ 00 326460 00 0 00 00 06 + 00 0 9 8 2 50 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+0035816000000000000 $+0036186000000000$ $+00317060000000000$ $+00367960000000000$ $+0036360000000000$	+ 01692660 00 v g t g t g t g t g t g t g t g t g t g	0+02108260000000321 0+02108260000000323 0+01475160000000325 0+01415360000000325 0+01356960000000331 0+01402160000000333 0+01402160000000333 0+014735696000000333 0+014735696000000339 0+01798150000000341 0+01798150000000345
4090097000000000000 +00098460000000000 +00379250000000000 +0034256600000000000	+0033806009000000000000000000000000000000	+016108600000000000000000000000000000000	1+0.1959560000000000000000000000000000000000
00000000000000000000000000000000000000	000000007 0000000000000000000000000000	00 00 0 \ 10 00 00 0 0 10 00 00 0 0 10 00 00 0 0 11 00 00 0 0 11 00 00 0 0 11	0000000123 0000000123 0000000123 0000000133 0000000133 0000000133 0000000133 0000000133

40. Test 208241010082

3+0000126 0+0010126	+004204	+903947	+004752	÷005160	+00200+	+604525	+004338	+037056	F001700	+003410	+003715	+002208	+00400+	+001647	+003207	+003935	+001594	+003741	+001588	+003357	+004360	+001611	+003678	+001762	+004234	+003262	+001391	+004474	+00/192	2/6000+ 2/6000+	**************************************	+014734	
0+002554600000000059 0+001011600000000053	+004627600000000000	+000400260033000004	+00000000000000000000	+0020666000000000007	+0043556000000000000000	+004283600000000000	+004150600000000000	+00+0286000000000000	+00000000000000000000000000000000000000	-007399600000000040	-007400600000000040	-0083976000000000043	-009356600000000000	-008624600000000000	-0015915000000000041	-001940600000000041	-002108600000000041	-0022366000000000041	-001947600000000041	-002415600000000042	-0019236000000000042	-002155600000000042	-00170360000000000	-00 200 020000 00 00 045	-003982600000000043	-00411365000000043	-00452260000000043	-00329660000000000	-0064636000000000	-00/401600000000000	-000 to 1000 000 000 000 000 000 000 000 000 0	**0000003T <i>5</i> 2001-	
0+004647+0000000000058 0+001008600000000062	+00504850000000000	+004221600000000007	+00392460090000007	+0045246000000000007	+00200750000000008	+00437550000000000	+00395750000003309	+00454060000000000+	+0033937500000000000	+01798850000000030	+01679550000000030	+01794660000000030	+01617450.0000000030	+00372250000000030	+0043015000800031	+01557560000000031	+01557850000000031	+0155346000000000	+01556660000000031	+02187560000000032	+02124460000000032	+0149016000000032	+01357660000000032	+01597060000000032	+01490269000000033	+01446060000000033	+014032600000000033	+0156886000000033	+01551250000000033	+01798550000000034	+01/986600000000000	+0282428000000000+0850+	
241010082000000000057	+0051556001000306	+00+32360000000000	+0040106000000000000	+0041456000000000000	+004565000000000000	+00000009666200+	+00480160000000000	+003910600000000000	+004113600000000000	+01712460000000000000	+015943600000000000	+01708450000000000000	+015353500000000020	+01405263030000020	+014950600000000021	+01490260000000021	+01578560000000021	+01723660000000021	+017215600000000021	+019631600000000022	+020685600000000022	+02119750000000022	+0217076000000000	+021574600000000022	+01169860000000023	+010563600000000023	+007076560000000023	+005721~00000000	+003155600000000023	+01712160000000024	+0.17.1236000000000000000000000000000000000000	+03232460000000000004 +05333360000000000000	
9 00 00 0 0 0 2 0 8 0 0 0 0 0 0 0 0 5 0	อ ข จ ฉ ฉ ฉ ฉ ฉ ฉ	00000000	2000000	20000000	0000000	00000000	00000000	60000000	600000000	00000000	000000000	6.0000013	:0000010	60000010	0000011	00000011	00000011	00000011	00000011	000000012	00000012	00000012	00000015	00000015	00000013	00000013	00000013	00000013	00000013	\$1000000 \$100000	00000014	00000014	100000

1. Test 208241115882

2. Test 208241215782

3+0000126 3+0010256	+004274	+003949	+7004474	+004850	+004471	+004248	+004248	+034285	F001698	+004832	+005720	+004578	+005555	0 46/4 00+	+00(4571	+002800	<b>+00,400+</b>	+002434	+002744	+004284	+002953	+004818	+002400+	+005259	+004712	+00900+	+00500+	+005515	+005883	**************************************	100787001	+014792
0+0025876000000000059	+0000000000000+	+00000000000000000	+00 466660000 00007	+004527600000000000	+00421960000000000	+00 463360000000000	+004187600000000000	+00 +1 5 06 00 00 00 00 00	+00442360000000000	-007403600000000040	-00740460000000000	-00546160000000040	-00485960000000040	-004723600000000040	-001633600000000041	-001957600000000041	-0021946000000000041	-002255600000000041	-002011600000000041	-00244360030000045	-001985600000000042	-0022006000000000	-001770600000000042	-002028600000000042	-0030336090000000	-00261860000000043	-003280600000000043	-0027686000000000043	-0035126000000000	**************************************	775 00 00 00 00 95 05 00 00 00	+0062876000000004
0+004207600000000058 0+001021500000000062	+0050526000000000	+004252600000000000	+ 00 39 40 50 00 0 000 0 0	+004344500000000000	+00478560000000008	+004215500000000008	+00418260000000000	+004462500000000000	+034078600000000000	+01798960000000030	+0.1690350000000030	+01795250000000030	+01619250000000030	+02051360000000030	+02094.750000000031	+01551360000000031	+01561460.000000031	+01556950000000031	+01560960000000031	+02183960000000032	+02122350000000032	+02524060000000032	+0250586000000032	+02543760000000032	+0250676000000033	+024339500000000033	+02475850000000033	+02522550000000033	+ 4251895000000033	+01738860000000034 +01738660000000034	+ OT / 30380 00 0 0 0 0 0 34 + UXEEE4 50 00 0 0 0 0 0 54	+0555146000000034
24121578200000000057 0+00102+5000000000000	+0051856000000000	+004336600000000000	+00399550000000000000	< 0.040736000000000000	+00+27160000000000	+004334600000000000	+0044496000000000000	+0000000009+00+00+	+00+461600000000000	+0171246000000000	+0159776000000000	+0170886000000000	+015384600000000020	+0140976000000000020	+014892600000000021	+0149586000000000	+015832600000000021	+017170600000000021	+017205600000000021	+0196655000000000	+02066560000000	+321224600000000322	+02170369090000022	+127543600000000000	+0118356000000000	+01104360000000000	+016597600000000023	+01792360000000000	+0191756000000000	+017125690900090034	~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~	+02384869000000154
000000000000000000000000000000000000000	00000000	00000000	70000000	00000000	00000000	20000000	000000000	600000000	600000000	000000000	000000000000000000000000000000000000000	00000010	00000010	00000010	00000011	00000011	00000011	60000011	05000011	00000012	00000012	00000012	00000112	C000001	00000013	00000013	0000000	00000013	00000013	00000014	**************************************	00000014

+014792	+00628360000000000+	+05552860000000034	+05385860000000024	000014
0+0009756	0-0074046000000000043	0+01799060000600343	0+0171266000000000243	000
+00001	-00 240 46 00 00 00 00 04 4	+0113916000000034	+017125600000000024	00000014
+002879	-003572600000000043	+0248356000000033	+018435600000000023	00000013
+002449	-002781600000000043	+0248546000000033	+01726760000000023	00000013
+004954	-0036846000000043	+0243666000000033	+01603560000000023	00000013
+006159	-002648600000000043	+0239466000000033	+01080360000000023	0000000
+004591	-0031736000000000043	+0247285000000033	+01175960600000023	00000013
+005200+	-00200760000000042	+02509250000000032	+02157260000000022	00000012
+005315	-0017386000000000042	+02457560000000032	+021717600000000022	00000012
+004679	-002177600000000042	+0248746000000032	+02121260000000022	00000012
+005953	-001927600000000042	+021245-0000000032	+02056360000000022	00000012
+004428	-002427600000000042	+0219536000000032	+01568469000000052	0000012
+002200	-00/22/28/90/00/00/04/1	* 01555650 00 0 0 0 0 3 1 * 01557550 00 0 0 0 0 0 3 1	+01/12660003000021 +01/220/600000000000	99 00 0 011
+0044400+	-002113600000000041	+01559150 10 0 0 0 0 31	+01581360000000021	00000011
+002774	-001931600000000041	+0155926000000031	+01492560000000021	00000011
+004479	-001604600000000041	+02020460000000031	+614372600000000021	00000011
+904854	-004873550000000040	+0197586000000030	+014072500000000020	00000010
+005501	-004982600,00000000	+0161896000000030	+01537460000000000000	00000010
+004457	-002269600000000000	+0179546000000030	+0170976000000000000	00000000
+005664	-99740360000000000	+01681960000000030	+0153696000000020	00000000
+004739	-007403600000000040	+01799160000000030	+017124600000000000000	00000010
F001702	+0004470600000000000	+00000000000+0000+	+004472600000000000	60000000
+038858	+0041616000000000000	+00443560000000000	+004011600000000000	60000000
+004569	+004216600000000000	+004185600000000000	+004475600000000000	00000000
+004551	+00065360000000000	+00422950000000008	+00433260000000000	000000000
+004472	+00421360000000000	+00048305000000000	+00429660300000000	0000000000
+004876	+00 453860000000000	+0043466000000007	+00408080000000000	00000000
+004446	+000000000000000000	+00394260000000007	+004027600000000007	70000000
+003966	+004011600000000007	+0042435000000000007	+004358600000000000	9000000
+004529	+00.4562600000000000	+0050795000000000+	+005195600000000000	90000000
+001018	+001017600000000000	+00101450000000000	+001019600000000000	90000000
+000012	+00257660000000000	+00424160000000005	413156820000000005	00000000

44. Test 208241415582

TOT 14 1 22	+0000000000000000	+ 65553350 00 0 000 34	+0238286000000000	00000014
3+0078376	0-0000000000000000000000000000000000000	0+017991600000000345	0+0171256000000000243	0000000143
+000075	-007405500000000044	+0179915000000034	+0171256000000024	00000014
+005789	-003692600000000043	+02450460000000033 +02450460000000033	+016/396000000000 +017865600000000	00000013 00000013
+004/66	-003787600000000043	+02402060000000033	+01553960000000023	00000013
+006143	-00266360000000043	+02353450000000033	+010683600000000023	00000013
+004200	-003227600000000043	+0243996000000033	+01175060000000023	0000000
+005427	-00200360000000042	+02476250000000032	. 0216136000000000022 +02161360000000000	00000012
+005267	-001702600000000042	+ 05 43 41 60 00 0 00 0 00 35	+02120360000000000	
+00777	-01139461111111111142 -012163611111111111142	+ 02126/50 40 0 0 0 0 32	+023695600303030022	00000012
/05400+	-602427600000000042	+02189560000000032	+01970169000000022	00000012
+004983	-0019476000000000	+01557550000000031	+0172196000000021	00000011
+005262	-00222260000000041	+0155366000000031	/ 41720456666688821 + 0172095000000000	00000011
+002122	-00192860000000041 -00208660000000041	+015588500000000031	+014923600000000021	00000011
+004356	-0015896000000000041	+0195956000000031	+014870600000000021	00000011
+004754	-0050056000000000	+01916560000000030	+01+0546000000000000	000000000
+005426	-005092600000000000	+0161616000000030	+0153476000000000000	00000010
+004326	-00566760900000040	+017955560000000000000000000000000000000000	+ 0.1.7 ± 8.5 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
+005629	-80740360000000000	+0159036000000033	+0.15979500+0+ +0.15979500+0+	
+004650	-00740350000000000	+01799250000000030	+0171256000000000000	000000000000000000000000000000000000000
F001704	+00 4473600000000000	+0041016000000000000	+00+4816000000000000000	
+034099	+00416460000000000	600000009987500+	\$	
+004573	+004213600000000000	+ 00 42 33 50 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<b>★0043273000000000000000000000000000000000</b>	
	+00 450 1 600 00 00 00 00 3 +00 06 6 6 6 00 00 00 00 3	+004823609000000008	+00431160000000000000	0000000
+00 +00 +	+00 45 5 0 6 0 0 0 0 0 0 0 0 0 7	+ 60434560000000000	+00000000000000+	79000000
+004457	+00065596000000000000	+0039446000000000	+00000003360000000000	10000000
+003967	+004017600000000000	+00424060000000004	+00000000642400+	00000000
+004255	+004550600000000000	+00508550000000000	+00519360000000000000	000000000000000000000000000000000000000
+0101019	+00101860000000000	+ 00 +2 +2 30 30 0 0 0 0 0 3 4 4 0 0 4 0 0 3 0 0 0 0	41412562009000000 +001014660000000000	
\$ T D D D D +	+00228866888898889	ナ ここ イン キッ への との こ のここ こと	なったしだいのいいのいがいだ	0000000

	24151538200300000057 0+0010246000000000051	0+0042386000000058 0+00102260000000062	0+002584600000000059 0+0010246000000000063	0+0000126 0+0010256
+0051	960000000000	+0050696000000000	+00464960000000000000	+004528
0	86000000000000000000000000000000000000	+00424990000000000 +0039526000000007	+00,461,560,000,000,007,400,400,400,400,400,400,40	+004487
+000+	0000000000	+0000000000000000+	+00 457860000000007	+004952
+004	3860000000000 936000000000000	+004854600000000008 +042514000000000	+004179000000000000 +0046736000000000000	+004200+
<b>*00+</b>	43600000000008	+00416250000000000	+00 422960000000000	+004576
+003	95600000000009	6000000000067700+	+004157600000000000	+041793
+00+	82600000000009	+00410950000000000	+000674600000000000	F001703
+017	24600000000020	+01799360000000030	-007403600000000	+004450
+012	6969090000320 8360000000000	+016/62600000000000	-002896600000000000	+004082
+015	446000000000000	+0161615000000030	-00529660000000000	+005354
+014	496000000020	+01804360000000030	-00223960000000000	+004260
+014	626000000021	+0183966000000031	-0015656000000000041	+004145
+01	20600000002	+01558460000000031	-0019356000000000041	+005632
+01	8086000000021	+0155856000000031	-0020516000000000041	+004050
+01	21360000000021	+01553550000000031	-002222600000000041	+002167
+01	21460000000021	+01557450000000031	-00191460000000041	+004826
+01	68760000000022	+02190450000000032	-0054546000000000-	9794994 40004
+05	03500000000022	+0212995000000000	240 00 00 00 00 00 - 270 00 00 00 00 00 -	4007910 4007910
+ 102	21460000000022 7176000000000	+ 02 38 48 56 00 0 000 32 + 02 46 4 66 00 0 00 0 32	-0021455000000000042 -001663600000000042	+005442
+02	620600000000022 6206000000000022	+02407950000000032	-00200860000000042	+005564
+011	076009000023	+02371760000000033	-0033956000000000043	+004318
+010+	696000000023	+02284950000000033	-0027796000000000043	+006155
+014	6260000000023	+02328560000000033	-004021600000000043	+004460
+015	576000000023	+02383550000000033	-0028916000000000	+005315
+015	2560000000023	+0238275000000033	-003302600000000000	+002640
+017	2560000000054	+01799250000000034	-00 240 26 00 00 00 00 044	+00000+
+017	276000000024	+01739260000000034	-0074046000000000	776000+
+035	55 p 0 0 0 0 0 0 0 5 4	+0365486000000034	+40.00000000000000	2027004
+053	47600000000024	+02554369000000034	+0028660000000004	14794

5. Test 208241514982

+000013 +001029 +004536 +003978 +004551	0+0045706 0+0045706 0+0045736 0+0045736 0+0045736 0+004576 0+004576 0+0057706 0+0057706 0+0057706 0+0057706 0+0057706 0+0057706 0+00057706 0+00057706 0+00057706 0+00057706
+0025906000000000005 +004028600000000006 +004633600000000000007	+ 00 4153600000000033   + 00 4236000000000033   + 00 4236000000000003   + 00 4124600000000003   + 00 442460000000003   + 00 4424600000000403   - 00 7404600000000403   - 00 193760000000413   - 00 193760000000413   - 00 193760000000413   - 00 193760000000423   - 00 1937860000000423   - 00 1937860000000433   - 00 1937860000000433   - 00 1937860000000433   - 00 193786000000004433   - 00 193786000000004433   - 00 1937860000000004433   - 00 1937860000000004433
+004216500000000058 +0310255000000000052 +00503750000000066 +004253500000000070	0+0049009000000000000000000000000000000
4161498200000000057 +001029600000000000 +00526260000000000065 +00436860000000000069	0+00+3636000000000000000000000000000000
00 000 020 00 000 036 00 000 036 00 000 036 00 000 000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

0+0000126 0+0010346	+004534	+003973	+004548	+005145	+004836	+004170	+004513	+033164	F001702	+003230	+004872	+002216	+005037	+002756	+003143	+004727	+001845	+034757	+002884	+003020	+004921	+001893	+004752	+003151	+003528	+00000+	140200+	+004971		676000+	+007837	+014798
0+0025826000000000059 0+001032600000000063	+0000000000659400+	+004054600000000000	+00 432960000000000	+0004979600000000000	+00 4197600000000000	+00 4656600000000000	+004234600000000000	+0000000000000000	+0000000000000000	-00740560000000000	-007406600000000040	-008373600000000040	-008497600:000000040	-00631060000000000	-0015866000000000041	-001947600000000041	<u>-002055600000000</u>	-00223660000000041	-001922600000000000	-002423600000000042	-001871600000000042	-002142600000000042	-0915696000000000	-00201660000000042	-003366600000000000	-00 set/eannan-	-00546160300000043	-003137500000000000	7 10 11 11 11 12 12 14 15 16 16 17 17 17 17 17 17 17 17 17 17 17 17 17	-00/40/600000000-	55000000000000000000000000000000000000	+00628760000000004
0+004137600000000058 0+001029600000000062	+0050366000000000	+004254600000000007	+0039556000000000000	+000000000000000000+	+0049956000000000	+00439950000000000	+00336406000000000000	+00464660000000000	+004163560000000009	+01799560000000030	+01677160000000030	+01795860000000030	+0161556000000030	+01064750000000030	+0108015000000031	+01557660000000031	+01557850000000031	+01552760000000031	+01556160000000031	+0219085000000032	+02130960000000032	+01855960000000032	+018398500000032	+019144600000000032	+01847550000000033	+01/35150000000033	+017944600000000	+018795600000000033	**************************************	+01/39360 00 00034 +01/399460 00 00034	<b>→£0000000006→99£0→</b>	+0555285000000034
24171328200000000057 0+00103260000000000061	+005193600000000000	+0043586000000000000	+0000000000000000	+004042600000000000	+000+48650050000000	+003989600000000000	+0047216000000000000	+00336560000000000000	+004142600000000000	+6171256000000000020	+015941600000000020	+0170915000000000	+015338600000000	+014943600900000020	+014850600000000021	+614901600000000021	+015800600000000321	+0172056000000000	+017225600000000021	+0.19678600000000022	+0207036000000000	+021197600000000	+0217066000000000022	+021614600000000	+0116646000000000	+01647950000000023	+00100000000000000000000000000000000000	+006904600000000023	+ <b>00</b>	+0171276000000000000	+036366000000000+0363666	+05336460000000024
00000000208	00000000	00000000	200000000	00 000 007	80000000	0000000	0000000	60000000	60000000	000000000	00000000	000000010	00000000	00000000	00000011	00000011	00000011	00000011	00000011	00000012	0000012	00000012	00000012	00000012	000000	STOCOCO	00060013	00000013			000000 0000000000000000000000000000000	00000014

48. Test 208241810082

0 + 100 0 0 126 0 + 100 10 10 3 0 6 0 + 100 10 3 0 6 0 + 100 10 3 0 6 0 + 100 10 2 0 6 0 + 100 10 10 6 0 + 100 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 6 0 + 100 10 10 10 10 6 0 + 100 10 10 10 10 10 10 10 10 10 10 10 10	+003410 +003410 +00351 +002351 +000973 +000973 +000973 +000973
0+0025846000000000000000000000000000000000000	-00406160000000043 -00406160000000043 -00364960000000043 -005286000000044 -0074066000000044 -0076076000000044 +0052846000000044
0+00408660000000088 0+0010236000000000000000000000000000000000	+ 0152466000000033 + 014446000000033 + 015006000000033 + 0157185000000033 + 017993600000034 + 01799360000034 + 03665360000034
2+1810032000000000000000000000000000000000	+01165/6000000000000000000000000000000000
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000114 000000113 000000113 000000114 000000114 000000114

0+0000126	+00425	+00396	+00471	+00200	+00501	+00432	+00435	+03405	F00170	÷00297	+00333	+00327	+00366	+00150	+00411	+00316	+00541	+00379	+00122	+00418	+00372	+00174	+00389	+00100+	+00417	4004CA	+10235	+00389	42100+	0+0003786	+00294	+01419
0+0025886000000000059	+00100000000000000000000000000000000000	+00 40 21 600 00 00 00 00 7	+004431600000000007	+00501460000000000	+004360600000000008	+00 45826000000000	+00 +1 0 66 0 0 0 0 0 0 0 0	+0038906000000000000	+00417360000000000	-00740660000000000	-00740550000000000	-0083776000000000	-003648600000000000	-0.0861360000000000000	-001575600000000041	-0019505000000000041	-0020606000000000041	-00223760000000041	-00191760000000000	-002435600000000042	-001862600000000042	-002146600000000042	-00166660000000000	-002019600000000000	-0044616000000000043	5 + 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-0048076000000043	-004675630000000043	-0055075075000000043	0-00/408800000000041 0-00/40880000000000441	+000000009509000-	+006286600000000044
+003990600000000	+ 00 1 0 5 / 20 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+00425560000000000	+00395260000000007	+0044276000000000007	+00507960000000000+	+00434160000000008	+0000000000000000+00+	+00452060000000000	+003848600000000000	+01799360000000030	+0167856000000030	+01795860000000030	+01615960000000030	+00232760000000030	+0035896000000031	+01556750000000031	+0155636000000031	+01551560000000031	+015563600000000031	+02190460000000032	+02131960000000032	+0068236000000032	+00669450000000032	+00650760000000032	+006293600000000033		+005/3850 00 000033	+ 00223530000000033	+ 00655750 00 000033 - 64 70566 6 6 6 6 6 6 6 7 6	t t	+0365616000000034	+0555316000000434
41900982000000000	+00103250000000000000 +0010485500000000000	+007Te22000000000000000000000000000000000	+00404260000000000	+00465260000000007	+004492600000000000	+004130600000000000	+0048156000000000000	+0038256000000000000	+00397560000000000000	+01712660000000000000	+01593160000000020	+017089600000000020	+01533460000000000000	+0140436000000000020	+0148446000000000021	+0148996000000000	+015783600000000021	+017199600000000021	+01722+600000000021	+11967663838800822	+020709600000000022	+0211976000000000022	+021695600000000022	+0216146000000000022	+011662600000000	+0.555555555555555555555555555555555555	+00/0/2000/000/00/23	+0057406000000000023	+003046000000000000000000000000000000000	0+01/12+659900000541	+0353616000000024	+053841600000000024
00 00 0 0 50	300000000000000000000000000000000000000		000000000000000000000000000000000000000	00000000	000000000	00000000	00000000	60000000	600000000	00000000	000000000	000000000	00000010	00000010	00000011	00000011	00000011	00000011	00000011	00 900 015	00000015	00000012	00000012	060000012	000000013		0.0000013	0000013		0.00.00.0141	00000014	0000000

50. Test 208242015460

l. Test 208242715760

0 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3+003796 0+000983 0+000983 0+007850 1+014804
0+00295050000000053 0+001052500000000053 0+002790500000000071 0+002790500000000075 0+002796500000000075 0+002855600000000075 0+002855600000000075 0+0028656000000000000000000000000000000000	-004822600000000043 -00740860000000044 -00740850000000044 -0006046000000044 +00528460000000044
0+00277460000000062 0+00104860000000062 0+00283860000000070 0+00283860000000074 0+002119600000000094 0+002888560000000094 0+002888560000000094 0+01288560000000094 0+01277660000000094 0+012776600000000303 0+0177660000000303 0+0177660000000333 0+0164316000000333 0+0164316000000333 0+022206000000333 0+0222606000000333 0+0224636000000333 0+0222206000000333 0+0222206000000333	+ 0223385000000033 + 01800250000000034 + 0140025000000034 + 0365745000000034 + 05554950000034
242115760000000000001 0+0010526000000000000000000000000000000000	+61909460000000023 +01713460000000024 +01713360000000024 +0353726000000024 +0538686000000024
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000013 00000014 00000014 00000014

. Test 208300113490

0+0000106	+005259	+004562	+002594	+002957	+005587	+804692	+005277	+066871	F001864	+004333	+002632	+00500+	+005611	+003095	+003866	+002362	+00500+	+005379	+00200+	+003248	+102535	+001962	+002462	+003193	+004133	+002780	+0052400+	4 uu 5680	+00 37 0 4 7 0 0 0 0 4 7	+000018	+0022200+	+014694
0+0021946000000000000000000000000000000000000	+00543160000000006	+004619600000000007	+004928600000000007	+005690600000000000	+0047026000000000000	+0026536000000000000	+00000000000000000000	+0072326000000000000000000000000000000000	+00501660000000000	-007374600000000000	-007375600000000000	-0080796000000000000	-00862360000000000	-006489600000000000	-0001796000000000041	-0007466000000000041	-0000000000000000-	-001091600000000000	-000837600000000041	-001436600000000042	-0007186000000000042	-0000324600000000042	-00063660000000000	-001044600000000045	-003193600000000043	-003129600000000043	-004873600000000043	-00262560000000000	-0052446000000000043	***************************************	+00000000000000-	+00627360000000044
0+00+53+600000000058	+0059266000000000	+00491460000000004	10445160090000007	+00491760000000000	+00579150000000000	+00497050000000000	+004478500000000000	+005302600000000000	+00450760000000000	+018057500000000030	+016752500000000030	+018013600000000030	+01606160000000030	+000640500000000030	+00970560000000031	+01540160000000031	+0153876000000031	+01533650000000031	+01535850000000031	+0225496000000032	+0215206000000032	+0190606000000032	+0190586000000032	+0194806000000032	+01857460 00 0 00 0 133	+01755460000000033	+01856660000000033	+01924360000000033	+01887450000000033	+ 01 855560 00 0 000 34 + 01 805550 00 000 34	+ 03656160 00 0 00 0 34 + 03656160 00 0 0 0 0 0 34	+02240660000000004
30011349000000000057	+305087630000000000	900000009600500+	+00445760000000000000	+0045696000000000000	+0020346030000000	+00451160000000000	+005388600000000000	+0000000009464400+	+00010000000000000000000000000000000000	+017230600000000020	+015937600000000020	+0171886000000000000	+015288600000000020	+01368660000000020	+014675600000000021	+014765600000000021	+01564060000000321	+017053600000000021	+01725660000000021	+01972760000000022	+02068860000000022	+02152760000000022	+022490500000000022	+92219260000000022	+01144360000000000	+010697600000000023	+007222600000000023	+110802450000000023	+00898160000000000	+01/2306000000000002+ +01/23460000000000000	+0300000000 <del>111111</del>	+05385060000000024
000000000000000000000000000000000000000	00 00 000	00000000	00000000	00000000	00000000	00000000	0000000	60000000	600000000	000000000	000000000	00000000	00000010	00000010	00000011	00000011	00000011	00000011	00000011	00000012	00000012	00000012	00000015	00000015	00000013	00000013	00000013	00000013	00000013		000000000000000000000000000000000000000	00000014

. Test 208300113490

0+0000106	+005564	+004572	+005291	+005952	+005289	+004695	+005260	+032220	F001865	+004333	+005595	+005430	+005610	+003075	+003874	+005313	+002091	+002333	+003110	+003541	+002573	+001976	+002455	+003202	+004111	+002500+	+302110	+005683	+003714	+000013	+000914	+00//00+	+014691
0+002191600000000059	+00 243 960000000000	+004622600000000007	+0049446000000000000	+0022336000000000000	+00047076000000000008	+002431600000000000	+00#7326000000000000	+004528600000000000	+002050586000000000000	-00737860000000000	-0022386000000000000	-00808360000000000	-003627600000000040	-11064946011011010040	-0000179601000000041	-00075065000000041	-000036000000000	-051087600909000041	-0003416000000000041	-00144260500000042	-00072360000000042	-0009156000000000	-0000643600000000045	-001044600000000000	-0031886000000000	-003140600000000043	-0050156000000000043	-00262260000000000	-005251600000000043	-007378600000000000	-0073736000000000	-00058660000000000	+80 627460000000000
0+0045326000000058	+00233460000000000	+00000000000016400+	+004455500000000000	+00491150000000000	+00577260000000000	+00497550000000000	+0000000000000000++000+	+00531100000000000	+00450550000000000	+01304850000000030	+01671560000000030	+01800550000000030	+01605650000000039	+00363660000000030	+0097046000000031	+01533650 00 0 00031	+0153796000000031	+0153316000000031	+0153545000000031	+02254360000000032	+0215936000000032	+01905756.00000032	+0190506000000032	+61948160000000032	+0.1857860000000033	+0175526000:0000033	+0185636000000000	+01922050000000033	+01885260000000633	+01804960000000034	+0130495900000000	+036650600000000034	+052418500000000034
3001134900000000000057	+00000009960900+	+0050056000000036	+004569600000000000+	+00457160000000000	+305085600000000000	+004520600000000000	+005379600000000000	+0000000009867700+	+0047006000000000000+	+0172256000000020	+01591360000000020	+0171876000000000000	+01528060000000020	+01367960000000020	+014565600000000	+014755600000000021	+0156356000000021	+01702360000000021	+01725460000000321	+01974260000000322	+02056560000000022	+0215386000030322	+02249060000000022	+02217060000000022	+0114385000000000023	+01,0683600000000023	+107205600000000023	+0050155000000000023	+008992500000000023	+017225600000000024	+01722760000000324	+032+3360100000005+	+05386860000000000
000000000000000000000000000000000000000	90000000	000000000	00000000	70000000	0000000	00000000	00000000	90000000	0000000	00000000	000000000	00000000	000000000	01000000	00000011	00000011	00000011	00000011	00000011	00000012	00000112	00000012	00000012	00000012	0000000	00000013	210000000	00000013	00000013	00000014	0000000	00000014	0000000

l. Test 208300215890

1+000000000000000000000000000000000000	+0.00000000000000000000000000000000000
0+0024956000000053 0+00098560000000053 0+00546160000000053 0+005461600000000071 0+00531760000000075 0+00515460000000075 0+00412600000000003 0+00473560000000003 0+0047356000000003 0+0047356000000003 0+0047356000000003 0+0047360000000003 0+0047360000000003 0+00473600000000003 0+00473600000000003 0+00473600000000003 0+00473600000000003 0+0047360000000000000000000000000000000000	-01195450000000043 -01260560000000043 -01738160000000044 -01738160000000044 -0105846000000044
0+00479160 00 00 00 062 0+00034150 00 00 00 062 0+00033260 00 00 00 00 00 0+00465760 00 00 00 074 0+00497360 00 00 00 074 0+00474360 00 00 00 00 074 0+00474360 00 00 00 00 00 0+00474360 00 00 00 00 00 0+014045460 00 00 00 00 00 0+0154660 00 00 00 00 30 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+0154660 00 00 00 31 0+015460 00 00 00 31 0+015460 00 00 00 31 0+015460 00 00 00 31 0+015460 00 00 00 31 0+015460 00 00 00 31 0+015460 00 00 00 31 0+02760 00 00 00 33 0+0264760 00 00 00 33	+ 0274385000000033 + 02743850000000033 + 0180545000000034 + 018054500000034 + 0366726000000034
30021589000000000000000000000000000000000000	+019787690000000000000000000000000000000000
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000013 00000013 00000013 00000014 00000014

55. Test 208300315990

059	1995 1+024145 1999 0F001864 401 0+005662 403 0+006627 405 1+005358 407 0+005358 411 0+005813 411 0+005324	1415 3+0053346 1417 3+00603546 1423 3+0060795 1425 0+0056246 1425 0+0056246 1427 3+0060276 1433 3+0069946 1435 0+0054756 1435 0+005946 1437 3+0069946 1441 0+0009186 1443 3+0009186
+0022026900000 +0010016000000 +0054826000000 +0053376000000 +005296000000 +0047546000000	+0047105000000000000000000000000000000000	0-0011786000000000000000000000000000000000
491260 00 0 0 0 0 0 6 6 9 9 7 5 6 0 0 0 0 0 0 0 0 6 6 9 4 6 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+0.051.0260.000000000000000000000000000000000	0+01546660 00 000 315 0+01546660 00 000 315 0+01542060 00 000 315 0+0214360 00 000 0321 0+0272650 00 000 0325 0+02735950 00 000 0325 0+02726760 00 000 327 0+02726760 00 000 331 0+02726760 00 000 331 0+02726760 00 000 331 0+02731950 00 000 335 0+01305350 00 000 341 0+01805350 00 000 342
003159900000 +00100160000 +00501450000 +0050346000 +0046426000 +0048656000 +0048656000 +0048656000 +0048656000	+01722760000000000 +017227600000000000 +0179756000000000000 +0171386000000000000000 +0137896000000000000000000000000000000000000	0+01574360000000215 0+01709160000000215 0+017091600000000219 0+019615600000000221 0+0216460000000223 0+02240560000000223 0+012240560000000223 0+01232560000000233 0+01163260000000233 0+011723060000000235 0+01723060000000235 0+01723060000000245
00000000000000000000000000000000000000	00000000000000000000000000000000000000	0 0 0 0 0 0 0 115 0 0 0 0 0 0 0 115 0 0 0 0 0 0 0 117 0 0 0 0 0 0 0 123 0 0 0 0 0 0 0 123 0 0 0 0 0 0 0 131 0 0 0 0 0 0 0 133 0 0 0 0 0 0 0 133 0 0 0 0 0 0 0 133 0 0 0 0 0 0 0 133 0 0 0 0 0 0 0 143 0 0 0 0 0 0 0 143 0 0 0 0 0 0 0 143

56. Test 208300315990

0+000106 0+0053136 0+0053136 0+0053136 0+0051076 0+0051976 0+0051976 0+0051906 0+0051906 0+0051906 0+0051906 0+0051906 0+0051906	1+000000000000000000000000000000000000
0+002205600000000053 0+001002600000000053 0+0010260000000000011 0+004546600000000007 0+004739600000000007 0+00471560000000000 0+00730960000000000 0+0075560000000000 0+0073090000000000 0+00738260000000009 0+00738260000000000 0-00738260000000000 0-007382600000000000 0-00173826000000000000000000000000000000000000	$\begin{array}{c} -00117060000041 \\ -00099660000000041 \\ -001432600000000042 \\ -001153600000000042 \\ -001153600000000042 \\ -001032600000000042 \\ -001717600000000043 \\ -00273360000000043 \\ -00273360000000044 \\ -00273360000000044 \\ -00259260000000044 \\ -00738160000000044 \\ +50627060000000044 \end{array}$
0+004616600000000058 0+009986000000000065 0+0059450000000000000 0+005486000000000074 0+0054826000000000078 0+004779600000000000 0+00477960000000000 0+00477960000000000 0+00477960000000000 0+00477960000000000000 0+01511050000000000000 0+0154716000000000000000000000000000000000000	+ 0.1542060000000031 $+ 0.154206000000031$ $+ 0.2243750000000032$ $+ 0.243750000000032$ $+ 0.274206000000032$ $+ 0.275686000000032$ $+ 0.2756860000000033$ $+ 0.275686000000033$ $+ 0.275686000000033$ $+ 0.2756860000000033$ $+ 0.2756860000000033$ $+ 0.2756860000000033$ $+ 0.2756860000000033$ $+ 0.27568600000000033$ $+ 0.27568600000000033$
3003159900000000000000000000000000000000	+0171276001000021 $+01724960000000022$ $+01963360000000022$ $+0207160000000022$ $+0215676000000022$ $+0224360000000022$ $+0156160000000022$ $+01531600000000023$ $+0172360000000022$ $+0172360000000022$
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000011 000000112 00000012 00000012 00000012 00000013 00000013 00000013

. Test 208300415890

3. Test 208300415890

+01470	+0005273600000000004	+05541960000000034	+053877600000000024	00000014
0+002220	0-000288600000000445	0+018055600000000345 0+035570500000000345	0+01/230500000000000245	00000000143
+00001	44000000000000000	+0190526000000034	+0172296000000000	00000014
+00676	-002748600000000043	+02681950000000033	+0200036000000033	00000003
+006112	-002031600000000043	+02591850000000033	+018785600000000023	0000013
+005730	-002873600000000043	+0263105000000033	+0175506000000000023	00 00 0 0 13
+00700+	-001705500000000043	+0253146000000033	+01155760000000023	00000013
+005291	-00228060000000000	+0267586000000033	+01154860000000023	0000013
+006382	-0010636000000000042	+02715060000000032	+02218+5003030322	00000012
+002937	-00000009660000-	+02675060000000032	+32245260000000022	00000012
+002416	-001047600000000042	+ 0253245000000032	+0215446003000022	00000012
+006849	-0000185600000000000	+0215756000000032	+4206986003000022	000003012
+005089	-00143660060000042	+0224925000000032	+0196906000000000	00000012
+105968	-00030460000000041	+0153966000000031.	+0172536000000000021	00000011
+002127	-0010/2800000000000	+0154245000000031	+01569760000000021	00000011
+006700	-00011460000000000	+0154295000000031	+01483269990000021	00000000
+005135	-00022760000000041	+0217686000000031	+01472460030000021	00000011
+005656	-004060606060606-	+02127460000000030	+01374060000000020	00000010
+006152	-00422060000000040	+0160816000000030	+015311600000000000	00000010
+005185	0 40 00 00000000000000000	+0130115003000030	+017185600000000000000	00000010
+009900+	-007384600000000040	+01673969000000030	+0159686000000000000000	66 000 010
+005502	-007385600000000000	+0190515000000030	+01722760000000020	00 00 0 010
F001863	6000000009660500+	+00462050000000000	+002000000000000+	60000000
+035235	+0000000009489400+	+00 50 5850 00 0 0000000+	+00453360000000000000	60000000
+005188	+004775600000000000	+0047346000000000000	+ 10 0000000000000000000000000000000000	000000000000000000000000000000000000000
+005183	+00233355500+	+ 00 49 00 50 00 00 00 00 00 00 00 00 00 00 00	+3049356368888888888888888888888888888888888	
+005110	+0048116000000000000	+ 0054915000000000000000000000000000000000	+0048856000000000000000000000000000000000	***************************************
+005587	+00517560000000000	+004+0045000000000+004+004+004	+0045560000000000000	76966666
+004003	+004637600000000000	+ 66 493550 66 6 66 6 7	+005024603300030	.u00000005
+005285	+00245160000000000	+0029455000000000000	+0061255000000000000	00000000
+0000+	+0000000095860000+	+00003035000000000+	+000000000000000000000	00000000
+00000+	+002191600000000000	+014919600000000005	0041589000000000000	09000020

). Test 208300515690

000000000000000000000000000000000000000	300515690000000000057 0+000997600000000000	0+004840600000000058 0+000394600000000062	0+0021836000000000059 0+000996600000000053	9600000+0 9600000+0
90000000 90000000	+006115600000000 +00503760000000000	+005964600000000000 +004937500000000007	+005454699690000000 +00462260000000000	+005293
70000000	+004531600000000000	+00447860000000007	+00533960000000000	+00514
80000000	+0000000000000+00+	+005269500000000000	+0047956000000000000000000000000000000000000	+005137
00000000	+000000009906+00+	+000000000000000+	+005342600000000000	+002179
00000000000000000000000000000000000000	+4050956000000000000 +4046376000000000000	+ 00 47 1460 00 0 0 00 0 0 0 0 0 0 0 0 0 0 0 0 0	+00 48346000000000000 +00 48 86900000000	+005215
6000000	+0020460000000000+	+00 <i>4</i> 535600000000000	+00203260000000000+	F001863
00000010	+01723060000000020	+0189556000000030	-00738160000000000	+005212
0000010	+015937600000000000	+01672360000000030	-007381600000000000	+006498
	+0171926000000000020 +01529560000000000	+01801850000000030 +01505950000000030	-005231500000000040 -00467150000000040	+004835
01000000	+01371160000000000	+0193856000000030	0 10 00 00 00 96 911 00 -	+005395
00000011	+01467760000000021	+0197816000000031	1400000000000000-	+004798
00000011	+01477060000000021	+0153945000000031	-00074660000000041	+006626
00000011	+015676600000000021	+0153896000000031	-000037760000000041	+004737
00000011	+01708060000000021	+0153406000000031	-00111760000000041	+005727
0000011	+0172566000000021	+01536360 00 00 00 031	-000861600000000041	+005643
000000000000000000000000000000000000000	+0197696000000000	+02251160000000032	-0014356000000000042	+004/39
	+UZUSSUSUUUUUUUUUKZ +D2153560000000000	+021616600000000000000000000000000000000	-000730600000000042	+00498
00000012	+022479600000000022	+0256006000000032	-0000000000000-	+005693
00000012	+02218460000000022	+0261206000000032	-001052600000000042	+006122
0000013	+01147960000000023	+ 0257 0560 00 0 000 33	-002440600000000043	+004939
000000000000000000000000000000000000000	+0103666000000000023	+02465160000000033 +02646760000000033	-0017636000000000043	+00720
00 00 0 0 13	+01718560000000000 +0171856000000000	+02587460000000033	-002172609000000043	+000589
00000013	+01823860000000023	+0257946000000033	-00302460000000043	+00655
41000000	+017229600000000024	+0180555000 u00034	-00738160000000044	+000052
00000014 00000014	+01/22260000000000 +03544760000000000024	+016054600000000000 +03656160000000034	-0000288600000000-044	+00077777
00000014	+0538736000000000	+022452000000000000000	+0062766000000000+	+01470

60. Test 208300515690

+01470	+00 627 06 09 00 00 044	+0554366000000034	+053876600000000024	00000014
+00777	-00002886000000000-	+0366636000000034	+035450500000000000	0000000
0+000019	0-00738360000000043	0+01805160000000343	0+0172356000000000243	0000000143
+00651	-00306460000000043	+025760600000033	+01824760000000023	00000013
+00289	-00217260000000043	+0258776000000033	+01718560600000023	00000013
+00230	-00318060000000043	+ 02515860 00 0 00033	+0.161046000000000023	000000000
+00715	-001762600000000043	+02565760000000033	+011962600000000000	000000000000000000000000000000000000000
+00610	-0010505000000000042	+02609860000000032	+022179600000000022	00000012
+002500+	-000065950000000042	+02551560000000032	+02249360000000322	00000015
+00498	-000951600000000042	+0256896000000032	+02153560000000022	00000012
+00688	-00072460000000042	+0216226000000032	+020661600000000022	00000012
+00200+	-0008646060000000 -0016346000000000	+01537260000000031 +n2260250000000032	+01725860000000021	00000011
+00272	-00112060000000000	+01534560000000031	+01707160000000021	00000011
+000+	-000986600000000041	+0153916000000031	+01568560000000021	00000011
+00660	-00007466000000000041	+0197666000000000 +015408600000000031	+014581530000000021 +01478060000000000	00000011
+00535	-004471600000000000	+0193546000000030	+01370960000000000000	00000010
+00296	-00457260000000040	+0160476000000030	+0152805000000000000	000000000
+30484	-0052346000000040	+0180126000000030	+017185600000000000	00000010
+00651	-007383600000000000	+01673460000000030	+01592060000000000	00000010
+00550	-007383600000000040	+0180506000000030	+0172266000000000000	
+02994 F00186	+004/008000000000	+ 00509850 00 0 000009 • 90 / 5 7 5 9 9 9 9 9 9 9 9 9	+0045386000000000000	60000000
+000521	+00000000000000000	+004726500000000009	+0.05096600000000000	00000000
+00517	+005346600000000000	+00487250000000000	+004911600000000000	000000000000000000000000000000000000000
+000514	000000000962400+	+005575500000000000	+0049215000000000000000000000000000000000000	מים מים מים מים מים מים מים מים מים מים
+00200+	+00524263000000007	+00#4786000000000000	+004539600000000000 +0046246000000000000	70000000000
+00 400	+00463460000000000	+00493250000000000	+002042600000000000	00000000
+00230	+00547260000000000	+005353600000000000	+00610460000000000	000000000000000000000000000000000000000
+00100	+001002600000000006	+00100160000000000	+00100+6000000000000	9000000
+00000+	+00218460000000000	+0048545000000005	500000000000000000000000000000000000000	שכוו נישט ניני

61. Test 208300615090

63 0+601012	67 0+005314	71 3+004608	75 0+005262	79 0+005820	37 0+005060	91 0+005204	95 0+035165	99 0F001863	01 U+0U4624	05 0+003982	07 0+005720	199 0+00 4667	11 0+004175	13 0+006100	15 0+003795	17 0+005448	19 0+004890	21 0+004199	23 1+006547	25 0+003699 25 0+003699	24 34002448	24 0+00535C	33 0+007005	35 3+004504	37 0+005738	34 04 00 00 00 00 00 00 00 00 00 00 00 00	41 J+0009246 43 J+0009246	45 0+007780	+7 0+014706
0+0021795000000000000000000000000000000000000	+002458600000000	+00 4635600000000	+005205600000000	+005330500000000	+0047616000000000000000000000000000000000	+004827600000000	+004654600000000	+0020306000000+	-007382600000000	-00/38160000000	-00512360000000	-005103600000000	-000201600000000	-000162600000000	-000000092960000	-00109660000000	-000086360000000	-001436600000000	-00072060000000	-000916600000000	-000028600000000	-00104440100100	-002027600000000	-00386860000000	-00235660000000	-00372260000000	-007382600000000 -007383600000000	-000028360000000	+006274600000000
0+004773600000000058 0+001007600000000062	+002962600000000000	+00+934500000000000	+00000000000000++00+	+00494960000000000	+ 111555451 111 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+004550500000000000+	+00515060000000000	+00 +61360 00 0 000 09	+01405850000000030 • 64672460000000030	+ 018/2480 00 000030 + 018/18/20 00 0 00030	+0160526000000030	+0157745000000030	+0161396000000031	+0.1540069000000031	+0153866000000031	+01534160000000031	+01535760000000031	+02254860000000032	+02153150000000032	+0233986000000032	+02325460000000032	+0236466000000033 +0336746000000033	+ 02 3 4 7 4 60 00 0 0 0 0 0 3 3 + 02 2 1 2 2 60 00 0 0 0 0 0 3 3	+0229156000000033	+0237205000000033	+ G2:365 760 00 0 000 33	+0130565000000000 +01305550000000034	+036655000000034	05540760000000034
300515090000000000057 $0+001012600000000000000$	+00011460000000000	+0050315000000000000	+004535500000000000	+004559603000000000	+8050496000000000 +0048245000000000000	+00518160000000000	+00447660000000000000	+005031600000000000	+0172316000000000020	+012322600000000000 +0171936000000000000000	+01528060000000000000	+0137086000000020	+01456760000000021	+01476060000000021	+015677560000000021	+017045600000000021	+01725450000000021	+019816600000000	+020649600000000022	+02154060000000022	+022490600000000022	+0221596039000922	+0114256000000000 +0106486000000000	+01332160000000023	+014445600000000023	+0149046000030023	+0172396000000000 +017233600000	+032444600000000000	+0538636000000000
00000000208	00 000 000	00000000	0000000	700000000		0000000	60000000	66000000	010000000		0000000	00000000	00000011	00000011	00000011	00000011	00000011	00 00 0 0 12	00000015	0000012	00000012	000000012	00000013	00000013	00 u00 013	000000	00000014	00000014	41000000

62. Test 208300514090

0+0058626 0+0009226 0+0009226 0+0077776	0-00372160000000439 0-007383600000000441 0-00738360000000443 0-00059060000000443	0+02367360000000333 0+02367360000000333 0+01805260000000341 0+03655460000000345	0+014894600000000239 0+017227600000000241 0+01722860000000243 0+03544460000000245	0 00 000 0133 0 00 000 0141 0 00 00 0 0 143 0 00 00 0 0 143 0 00 00 0 0 145
+004788 +007007 +004202	-002695600000000043 -001984600000000043 -00386860000000043	+ 02 3+ 81 50 00 0 0 00 0 33 + 02 21 22 50 00 0 0 0 0 0 33 + 02 28 16 60 00 0 0 0 0 33	+01142460010000023 +01064560000000023 +01332960000000023	00 00 0 0 1 1 3 90 00 0 0 1 3 00 00 0 0 1 3
+005438	-0006566000000000042 -001035600000000042	+ 02 32 67 60 00 0 0 0 0 0 32 + 92 39 55 60 00 0 0 0 0 32	+022503600000000022 +022168600000000022	000000012
+003937	-00003760000000655	+ 02340660 00 0 00032 + 02340660 00 0 00032	+021558600000000022	0000015
+004222	-001436600000000042	+02253560000000032	+019805600000000000000000000000000000000000	00 00 0 0 12
+0064851	-00000000000000000000000000000000000	+ 01533454 44 44451 + 01535560 00 0 00 0 031	+01/0656000000000000000000000000000000000	0000011
+003773	-00000000000000-	+0153826000000031	+01567560000000321	00000011
+006100	-00075460000000041	+01539560000000031	+0147676000000000021	00000011
+004640	-005102600000000000	+01575760000000030	+013712500000000220	00000013
+305775	-005116600000000040	+016059500000000030 +016059500000000030	+0152896000000000000000000000000000000000000	0 T 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
+006154	-00738260000000000	+0165886000000030	+01593460000000000000	00000010
+004653	-007383600000000040	+0180516000000030	+0150155600300000004 +017225600300000020	000000000000000000000000000000000000000
+023920	+004627699999999999	+00512960000000009	+00445850000000000+	60000000
+005187	+004815600000000000000000	600000000000555900+	+004/355000000000000000000000000000000000	000000000000000000000000000000000000000
+005228	+00 47 37 60000000000	+0022376000000000	+0000000099+0500+	0000000
+005792	+0053096000000000+	+00#932500000000007	+0045526033000337	20000000
+004290	+004529600000000000 +0051966000000000000	+ 0049255000000007 + 0046805000000007	+0050256000000000000	000000000000000000000000000000000000000
+002533	+002451600000000000	+002357600000000000	+006115600000000000	00000000
+001003	+00 T00 00 0000 00 000 +00 T00 T00 000 0	+ 00 475450 00 0 000 05 + 00 033550 00 0 000 05	90000000000000000000000000000000000000	000000000000000000000000000000000000000
+ 20 00 1 1	+00/04 A 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10000000000000000000000000000000000000		000000

3. Test 208300713490

4204	0+006270600000000445	0+05543160000000347	0+053875600000000247	2410000000
+00092	-00738360000000044	+0130536000000034	+01722960000000024	00000014
+000925	-0073826000000000	+01805360000000034	+0172276000000324	00000000
+003753	-005243500000000043	+01893060000000033	+009032606000000033	00000013
+005651	-00261160000000043	+0192936000000033	+00603360000000023	00000013
+002163	-00438560000000000	+0185136000000033	+00718760000000023	00000013
+005796	-00304160000000043	+01758260000000033	+01061660000000023	0000013
+004137	-003204600000000043	+01856360000000033	+0114146000000000023	00000013
+003267	-00106260100000042	+01957060000000032	+022172699999992	00000012
+002400+	-00064160000000042	+0190936000000032	+0224816000000022	00000012
+001996	2400000009946000-	+01909260000000032	+0215136000000322	00000012
+002324	-0011424600000000-	+ 02 154250 00 0 00 0 0 32	+020670600000000000	00000012
+003135	-00036460000000001	+0153606000000031	+0172496000000021	00000011
+002324	-001116600000000041	+01534260000000031	+01707260000000021	00000011
+002141	-00000000000000-	+01539260000000031	+0156686000000021	00000011
+0005343	-0000262200-	+01540360000000031	+01476560000000021	00000011
4012800+	-0001825000000000000000000000000000000000	+ 00 97 54 60 00 0 00 00 34	**************************************	00000011
+000000	6400000000629900 <del>-</del>	+ 0.00 0 0.00 0.00 0.00 0.00 0.00 0.00	+01/E3399999999999999999999999999999999999	
+0024/3	-008085600000000040	+01801060000000030 +01606150000000030	+01/188600000000020 +01526360000000000020	
+002649	-00738260000000000	+01671360000000030	+0159136000000000000	00000000
+004363	-00738160300000040	+01805460000000030	+01723160000000020	00000010
F001863	+0050496000000000+	+004640600000000000+	+00471560000000000	60000000
+036020	+00455560000000000	+0053216000000000	+00+505600000000000	60000000
+005297	+004772600000000000	+004505500000000000	+005397600000000000	00000000
+004715	+0020000000000000+0000+	+004992600000000000	+00455160000000000	00000000
+005291	+00471960000000000	+00590950000000000	+0051136 10000000000	00000000
+005992	+002690600000000000	+00+937600000000007	+000000000000000+00+000+	00000000000
1004207	+10 48 > 1800 00 00 00 00 1	+ 00 49 53 80 00 0 00 00 00 00 00 00 00 00 00 00 0	+0002374000000000000000000000000000000000	
+005279	+002455600000000000	+002936600000000000	+006107600000000000	0000000
+001006	+001003600000000006	+000399860000000006	+0010026000000000000	00000000
+000001	+0021876000000000005	+0046686000000000	0071349000000000000	00000020

+000010	+001005	+005288	+004296	+005307	+002977	+00500+	+1004715	+002500+	+025656	F001863	+004323	+002684	+005436	+005603	+00200+	+003883	+0022200+	+005154	+005393	+003112	+003585	+002584	+001097	+002414	+003279	+004128	+300810	+005160	+005639	**************************************	0+0000000000000000000000000000000000000	+007779	+014706
+00218360000000000	+00100060000000000000	+002460660300000006	+0000000000000000000	+000000000000000000000+	+00570960000000000	+004727600000000000	+0024516000000000000	+0000000009652400+	+00 +22 5000000000000	+002041600000000000	-007384600000000000	-007384600000000000	-008081600000000000	-008627600000000000	-006470600000000000	-0001916000000000041	-0007636000000000041	-00095560000000041	-001108600000000041	-000829600000000041	-0014466000000000042	-00008860000000000	-00000436000000000045	-000647600000000042	-001053600000000000	-0031886006000043	-0030406000000000043	-00496760000000000	-00252,7600000000043	-00522660000000000000	0-00/383500000000041	+10000000000000000=	+006277600000000+
+00456160000000000	+00000000000000000000000000000000000000	+002365600000000006	+004932600000000007	+00447550000000000	+004939600000000000	+00581450 00 0 000 08	+0000000009566700+	+000000000000000000+	+00531560000000000	+00453360000000000	+0180505000000030	+0167175000000033	+0190076000000030	+0.1606060000000030	+00365560000000030	+0097196000000031	+01533360 00 000031	+0253396000000031	+0153305000000031	+01536550000000031	+02256760000000032	+02156560000000032	+0191016000000032	+0190815000000032	+0195566000000032	+0186676000000033	+01757360000000033	+01861560000000033	+01930360000000033	+0189446000000000	0+018051600000000341	+ 0.365 66 60 00 0 00 00 00 00 00 00 00 00 00 0	+0227446000000034
0071349000000000000	+00000000000000000000000000000000000000	+00610860000000000006	+005031600000000000	+0045306000000000000	+004585600000000000	+005120600000000000	+30454560000000000000	+00539060000000000	+0045036000000000000	+0047226000000000000	+017225600000000020	+01593060000000020	+01718460000000020	+01523160600000020	+01371560000000020	+0146586003000321	+01475460000000021	+01565764000000021	+01704360000000021	+01725160000000021	+01974360000000022	+02065760000000022	+02153160000000022	+02248960000000022	+0221806000000122	+01141560000000000	+010618600000000023	+0071835000000000023	+0060316003000023	*0090256000000023	+017226600000000024	*01/2308000000000 *035445600000000000	63600000000
00000050	00000000	<b>30000000</b>	00000000	00000000	70000000	000000	0000000	00000000	60000000	00000000	00000000	00000010	000000000	0000000000	00000010	00000011	00000011	00000011	00000011	00000011	00000012	00000012	00000012	00000012	00000015	00000013	00000013	00000013	00000013	00000013	00000014		0 0 0 0 0 0 0 1 4 7

65. Test 208300813400

1+0000116 0+0009776 0+0063986	+002302 +006302 +007089	+026704	+016404 +039262 F002070	+003774 +006195	+004000+	+003740 +0031,58	+006002 +002966	+006098 +003559	+002905	+002579	+003555	+006719	+006638	+000929	+007788 +014718
0+0021576000000000000000000000000000000000000	+005666600000000000 +006435600000000000 +00679560000000000	+0059466000000000000000000000000000000000	+0025-65600000000000000000000000000000000	-007383600000000040 -00738360000000040	-0074936000000000040 -00309760000000040	-007590600000000040 +002206600000000041	+000740609090000041 +001254600000000041	+00 021 8600 00 00 00 041 +00 17 3 86 00 00 00 041	-000133600000000042 +0014646000000000	+000248600000000042 +0015646000000000	+000081600000000042 -0033896000000043	-001112550000000043 -002503500000000	-00143260000000043 -00504860000000043	-00 <i>7</i> 3856000000000044 -00 <i>7</i> 3866000000000	-000588600000000044 +006274600000000044
10545 00097 00717	+0059896000000000000 +00525660000000000 +0061576000000000	+00695360,0000008	+ 00 56 0 1 50 JJ 0 0 0 0 0 0 0 9 + 00 6 3 4 3 50 0 0 0 0 0 0 0 0 9 + 00 5 4 6 6 6 0 0 0 0 0 0 0 0 0	+0180516000000030 +0165556000000030	+01801350000000030 +01578750000000030	+ 00612350 00 0 00033 + 00614850 00 0 00031	+01496160000000031 +01504060000000031	+01487950000000031 +01500860000000031	+ 02441450 00 0 0 0 0 0 32 + 02253260 00 0 0 0 0 0 32	+01995660000000032 +01821250000000032	+0198376000000032 +0199176000000033	+01870160000000033	+ 01 94 02 60 00 0 00 0 33 + 01 91 4860 00 0 0 0 0 0 33	+ 01 80 5960 00 0000 34 + 01 30 5960 00 0 000 34	+ 0365 7960 00 0 0 0 0 0 34 + 0554 3660 00 0 0 0 0 0 34
	+06615460060000000 +00342460000000000 +00576250000000000	+00605760000000000 +00585460000000000	+00645160000u0000 +005389600000000 +0061836000	+0.17233600000000000000000000000000000000000	+0171866000000000000000000000000000000000	+013293600000000020 +0144176000000000	+014510600000000021 +01547760000000021	+017471630000000021 +01727960000000021	+0192156000000000000000	+02131160000000022 +021311600000000022	+0240086000000002	+0100916000000023	+006303600000000023 +0066016000000000023	+017233600000000000 +017232600000000	+032458600000000024 +0538806000000000
00000000000 00000000000 0000000000	00 000 005 00 000 007 00 000 007	00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000010	010000000000000000000000000000000000000	00000010	00000011	60 00 0 011 00 40 0 011	00000012	00000012	00000013	0000013	00 00 0 0 13 00 00 0 0 13 00 30 0 0 13	00000014	00000014

5. Test 208300813400

00000020	0031340000000000000	+00546150000000005	+002153690999999	+00000+
0 0 0 0 0 0 0 0 0 0	0+00098350000000000000	0+000380600000000062	0+0003846003000000063	9986000+0
000000000000000000000000000000000000000	+007367600000000000	+0071905000000000006	+00655860000000000	+006392
000000000	+0051656000000000	+0059905000000000+	+002649600000000000	+005514
70000000	+0054325001000137	+00525850000000007	+000642960000000000	+006301
0000000	+005701630300030	+006148600000000007	+006801600000000000	+007072
90000000	+006067600000000000	+00694760000000000	+0023246000300000	+006689
00000000	+005840600000000000	+005848500000000008	+000288800000000000	+006202
00000000	+006460500000000000	+002238600000000000	+002283800000000000	+006406
90000000	+00541+6000000000000	+00634560000000000	+002282600000000000	+054861
600000000	+0050806000000000000	+002475500000000000	+0000000009246500+	F002069
00 00 011	+01722860000000320	+0130556000000030	-007386600000000040	+003725
00000010	+015725600000000020	+01652260000000030	-007386600000000000	+006156
00000010	+0171876000000000	+01801160000000030	-0074996000000000040	<b>550500+</b>
03000000	+01502260009000020	+01579760000000030	-008101600000000000	<b>+006322</b>
010000000	+01331160000000020	+00616650000000030	-00759560000000000	+003657
UU 00 0 0 1 1	+014421600000000021	+00618350000000031	+00221060000000041	+003166
00000011	+01451760000000021	+0075856000000031	+000021260000000004	+006012
50000011	+01549160000000021	+01504650000000031	+0012646000000000004	+005333
0000011	+01750160000000021	+01487250000000031	+000213600000000004	+006087
00000011	+017275600000000021	+01433660000000031	+001739600000000004	+003265
0000012	+019215600000000022	+0243796000000032	-00015260000000042	+002915
00000012	+0219316000000022	+0225185000000032	+001469600000000042	+005978
00000012	+021286600000000022	+0199166000000032	+00002860000000000	+002574
00000012	+0224946003000322	+0182676000000032	+001557600000000042	+006141
00000012	+02403060000000022	+01384360000000035	+0000526000000000+	+003245
00000013	+01112160000000023	+01891050000000033	-003336600000000000	+003208
0000013	+01009160000000023	+01874460000000033	-0010916000000000043	+006813
000000	+0075256000000000	+01822050.000000033	-0025436000000000043	+003087
00000013	+0063076000000000	+0194306000000033	-00149560000000000	+006552
0000013	+0045856000000000023	+01914760000000033	-002065600000000000	+004367
00000014	+01722960000000000	+01305550000000034	-0073866000000000044	+0000358
00000014	+01723060000000000	+01805560000000034	-0073866000000000044	+000052
00000014	+03546160000000024	+03567450000000034	-00023020000000000	+007783
00000014	+053887600000000024	+0554316000000034	+00627360000000004	+014715

67. Test 208300915800

	•			
+014718	+00827960000000000	+05544450000000034	+053894600000000	00000014
+007788	+000000000000- -000028860000-	+03667950 00 00 00 00 00 34	+032422600000000000	00.000014 00.000014
0+0009296 1+0009286	0-00738760000000004+1	0+01806060000000341	0+017237600000000241	0000000141
+007920	-001909600000000000	+0285346000000033	+02005560000000023	00000013
+007108	-0006836000000043	+02653460000000033	+01881060000000023	00000013
+0084274	-00 04586 00 00 00 00 643	+ U2/31358	+01423160000000023 +0179756000000000023	000000013
+005991	-001314600000000043	+0284896000000033	+01124760000000023	00000013
+007427	+00022760000000042	+0288906000000032	+023287600000000022	00000015
+006981	+001023600000000004	+0282505000000032	+02290360000000022	0000012
+006063	+0000347600000000004	+0285116000000032	+02169760000000022	00000012
+008164	2400000009896000+	+02213760000000032	+02124560000000000+025	00000012
+300868	+0011555009000041	+ 01 5 8 6 6 6 9 8 8 9 8 8 7 7 7 8 7 7 8 7 8 7 8 7 8 7	+01/20>60000000000021 +01948160000000000	00000011
+007112	+000031960000000000+	+01500050000000031	+017200600000000021	00000011
+005805	+00021660000000004	+0151000000000031	+01554060000000021	0000000
+007939	+0008366000000004	+0150756000000031	+01457160000000021	00000011
+06500+	+00180550000000041	+02131660000000031	+01446560000000021	00000011
+006509	-0034056060000000	+02135960000000030	+01336660000000020	00000010
+007407	-003224600000000000	• 01583950 00 0 00 0 030	+015066600000000020	00000110
+80/923	-00/2332600000000000000000000000000000000	+ N165 925U UU U U U U 3U	+015/836000000000000	
+0006424	-0073856000000000000	+0180626000000030	+0172346000000000	00000000
F002071	+00603860000000000	+005570600000000000	+00605660000000000+	60000000
+039579	+00561460000000000	+0060545000000000+	+002445600000000000000	60000000
+006155	+00570560000000000	+00224000000000000+	+0060875000000000	0000000000
+006107	+0000000000000000000000000000000000000	+ 0.057 31 60 00 0 00 0 00 0	+00000000000000000+	
+006692	+00626860000000007	+002340600000000000	+00221960000000000	200000000
+006027	+006275600000000000	+005275500000000007	+0053956000000000000	0000000
+002244	+005537600000000000	+00664360000000000	+0061646000000000000	0000000
+006433	+00560560000000000	+007210600000000006	+007411600000000000	90000000
+001000	+00100660000000000	+00100560000000000	+00100760000000000	00000000
+000011	+002159600000000000	+00579160000000000	0091580000000000000	00000020

3. Test 208300915800

				770000
00 60 9 0 2 0	0091580000000000000	+ 00281354 00 0 000 000	+10<16/6000000000000000000000000000000000	+00000+
	0+00101255000000000000000000000000000000	0+007233500000000055	0+005600500000000055	0+0064316
	+001 +0 20000000000000000000000000000000		+000000000000000+	+005560
	+11277777777777777777777777777777777777	+ 002532000000000000000000000000000000000	+006287600000000007	+006043
7000000	+00222200000000000000000000000000000000	+0059105000000000	+006260600000000000	+006685
000000000	+005840600000000000	+00655660000000000	+00572360000000000	+006161
00000000	+0058116000000000008	+00274660000000008	+006277600000000000	+006109
00000000	+00608160000000000	+105637600000000009	+002727600000000000	+006154
60000000	+0024536900000000000	+00606060000000000000	+00562560000000000	+035389
00000000	+00000000000000000000000000000000000000	+005581600000000000	+002000000000000+	F002070
000000000	+017239600000000020	+0180566000000030	-007337500000000000	+006410
00000010	+01578660000000020	+01656060000000030	-0073876000000000	+1107868
000000110	+01718360000000020	+01301460090000030	-00 <i>4</i> 23060000000000	+006002
00000310	+01506160000000020	+01583350000000030	-003558600000000000	+007376
00000010	+01336060000000020	+0213565400000030	-00340860000000000	+006507
00000011	+01447060900000021	+02182350000000031	+0017876000000000041	+005869
00000011	+01457160000000021	+015072500000000031	+00008446000000000004	+00200+
00 00 0 012	+0155376000000021	+0150865000000031	+00068560000000041	+005806
00000011	+01718360000000021	+0149886000000031	+00031260033000041	+007025
00000011	+01726260000000021	+0150695000000031	+001133600000000041	+006877
00000012	+01947460000000022	+02394960000000032	-0000126000000000	+005775
00000012	+021295600000000022	+0221406000000032	+00000136000000004	+008135
00000012	+021704600000000022	+0285126000000032	+00033560000000000	+006016
00000012	+0228906000000022	+0282426000000032	+001022600000000042	+006925
00000012	+02329560000000022	+02887960000000032	+00000000000000+	+007397
00000013	+011241600000000023	+028467600000000	-00133660000000000	+005962
00000013	+014200600000000023	+02729160000000033	-000211600000000	+ ID ID 8 4 2 10 ID ID ID ID ID ID ID ID ID ID ID ID ID
00000013	+017967600000000023	+02784450000000033	-00199060000000043	+000235
0000000	+018312600000000023	+02861760000000033	50000000000000000	*******
00000013	+020050600000000023	+02861360000000033	-007880900000-	100000
91000000	+01723260060000024	+018058600000000034	**************************************	700000+
9000000	+0172336000000000	+ 01 30 2 / 20 00 0 00 0 3 / 4 0 / 4	770 00 00 00 00 00 00 00 00 00 00 00 00	+0000+
00000014	+03246060000000000	+ 03655560 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	770 CC CC CC CC CC CC CC CC CC CC CC CC CC	+ C 4 4 7 7 4
00000014	+65389560000000000	+ nan n nancheen +		

+00001	+00100+	+006434	+002244	+006078	+006762	+006199	+006103	+006173	+040105	F002070	+006229	+007845	+005782	+007427	+006279	689 <u>5</u> 00+	+~04640~+	+002465	+007020	+006638	+005551	+008177	+005611	+00 7015	+007167	+002804	+000235	+002983	+007166	+001184	260	4000000	+014722
+002181600000000005	+001006600000000000	+00020000000000000000000000000000000000	+005661600000000000	+00628360000000000	+00062396000000000000	+002684600000000000	+0063126000000000008	+0057476,00000000000	+000203000000000000000	+006011600000000000	-0073866000000000000	-007386600000000000	-00444600000000004	-0037536000000000000	-00366560000000000	+00200260000000004	+0000283600000000000	+00000000000000+	+00029760000000004	+00142760000000041	-0000020202000000000	+001218600000000042	+000351600000000000	+001285600000000042	+0001826000000000042	-001360600000000043	-000522600000000043	-002148600000000043	-000626600000000043	-00203360000000000	007387	***************************************	+0002546000000004+
+00280460000000000	+0010036000000000	+007217500000000000	+00603760000000007	+00528660000000007	+00589260000000000	+00659860000000008	+00577260000000008	+002625600000000000	+00605860000000000	+00558260000000000	+0180616000000030	+01654160000000030	+0180156000000630	+01581460000000030	+01977850000000030	+0202086000000031	+01504550000000031	+0150756000000031	+0149376000000031	+0150316000000031	+024140500000000032	+0223736000000032	+ 02779860 00 0 00032		+(02821860000000032	402798360000000033	+02655760000000033	+02707460000000033	+0279536000000033	+02840060000000033	1806060000000034	**************************************	+05544760003
0101570000000000000	+0010056000000000000	+0073956000000000000	+005180600000000006	+005431600000000000	+0025056000000000000	+0058746000000000008	+005786600000000000	+006104600000000000	+005 441600000000000	+03603460000000339	+0172346000000000020	+015738600000000020	+01718860000000020	+01503360000000020	+0133276030000320	+01443560000000021	+014543600000000021	+01550700000000021	+01731460000000021	+01726960000000021	+019437600000000022	+021552600000000022	+021560600000000022	+02279060000000022	+02363160000000122	+01111460000000023	+012262600000000023	+016682600000000023	+0174596000000000	+018560600000000023	+0172356000000000	**************************************	6000000
00000000	00000000	90000000	00000000	20000000	0000000	80000000	90000006	0000000	60000000	60000000	00000010	00000010	00000010	0000000	00000010	00000011	00000011	00000011	60000011	00000011	0000000	00000012	00 000 015	0000000	00000015	00000013	00000013	00000013	00000013	00000013	00000014	**************************************	0000000147

70. Test 208301015700

+ + + + + + + + + + + + + + + + + + + +
a o o o o o o o o o o o o o o o o o o o

l. Test 208301115500

0+000116 0+001116 0+001116 0+0064306 0+0065236 0+00661106 0+0062206 0+0062206 0+0062206 0+0062206 0+0062206 0+0062206 0+0062206 0+0062206 0+0063126 0+0063126 0+0063126 0+0063126 0+0063126 0+0063126 0+0063126	+007556 +007556 +000932 +007792 +014718
0+0021576 0000 00065 0+0065766 000 00000 0+0065516 000 00000 0+00652860000 000075 0+00632860000 000075 0+00532860000 000093 0+00556660000 000093 0+00556660000 000093 0+0055660000 000093 0+0055660000 000093 0+00587260000 0000413 0+00124600 00000 0415 0+0011606600 0000 0415 0+00150000 0000 0425 0+001500600 0000 0433 0+001500600 0000 0433	-00235960000000043 -007388600000000044 -007387600000000044 -00058860000000044
0+0057985000000058 0+007201500000000065 0+0072015000000000056 0+00575500000000074 0+0057550000000000000000000000000000000	+0273355000000033 $+0273355000000033$ $+01806460000000034$ $+0180655000000034$ $+0355850000000034$
301115500000000000057 0+000996000000000061 0+0051956000000000059 0+0054376000000000077 0+0054376000000000077 0+0054376000000000077 0+005427600000000095 0+0051256000000000000000000000000000000000	+017303600000000023 +01723760000000024 +0172376000000024 +0354686000000024
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000013 00000013 00000014 00000014

72. Test 208301115500

0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
00 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

73. Test 208301215100

063 0+0009946 067 1+0064256	71	6900+0 62	82 U+UUSS8 87 O+OO596	91 0+00620	95 0+03764 90 0E06206	01 0+00541	03 0+00756	05 0+00456	76700+0 VO	11 0+00477	13 0+00747	15 3+00403	17 1+00715	19 U+UU528	23 3+00762	25 0+00392	27 3+00727	29 0+00581	31 3+00540 27 0+00844	7670010 56	25 0 + 0 0 + 2 + 2 + 2 + 2 + 2 + 2 + 2 + 2	84900+0 68	41 3+00092	43 0+00092	45 0+00778	47 0+01472
+0002222000000000000	0+00566160000000000000000000000000000000	+006507600000000	+002330600000000000000000	+00573860000000	+005489600000000	-007388600000000	-00738860000000	-00746160000000	-604451500000000	+002221600000000	+00002000000000	+00128860000000	+000222600000000	+001755600000000	-000139660000000 +0014846000000000	+00025260000000	+001570600000000	+0000106600000000000	-001736600000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	00000009/29000-		-00738960000000	-000020160000000	+006231500000000
+ 00 7 2 0 8 5 0 0 0 0 0 0 0 0 0 0 6 0	0+0060086000000000000000000000000000000	+002000000000000+	+00669460000000008 +00584060000000008	+002493500000000000	+006100600000000009	+0180666000000030	+01652950000000030	+0180166000000030	+01580150000000030	+ 01521360 00 0 000 31	+0149765000000031	\$ 0150406000000031	+01497260000000031	+01500660000000031	+ ((< 44186) 00 0 0 0 0 0 32 + (< 524186) 00 0 0 0 0 32	+0246735000000032	+0240356000000032	+02512450000000032	+02483960000000033	+02315860 00 0 000 33	+ 42 355769 88 8 88 83	+0248866000000000000000000000000000000000		+01306450000000034 +01306460000000034	+0365805000000034	+02246750000000034
+00736760000000000000000	0+00619960000000000000000000000000000000	+0024496000000000000	+30599060000000000000	+0062156000000000000	+002269600000000000	+005917503000000000 +0172356000000000	+0157276000000000000	+01718960000000000000	+015020500000000000000	+01330260090000024	+014509600000000000000	+01547960000000021	+017502600000000021	+017279600000000021	+019254600000000000	+021374600000000022	+02254660000000022	+02404760000000022	+011115600000000023	+010073600000000	+0102946030000123	+013468600000000000	+0.14Z4300000000+Z4I0+	+01/23/500000000000 +01/23/500000000000	+0354616000000024	+0236000000000000+
00 00 00 00 00 00 00 00 00 00 00 00 00	0 00 00 0 00 6 9	200000000000000000000000000000000000000	800000000	000000000000000000000000000000000000000	60000000		000000000000000000000000000000000000000	00000000	00000010		00000011	00000011	00000011	00000011	00 30 0 012	00000012	0000012	00000012	00000013	00000013	00000013	00000013	0000000		*T000000	00000000

74. Test 208301215100

	•			1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0+0077886 0+0147186	0-000591600000000445	0+036584600000000345	0+0354646000000003245	0000000145
+000927	-0073906000000000044	+01306250000000034	+017235600000000000	00000000
+0000926	-00738960000000044	+01806260000000034	+017245600000000024	00000014
+006491	-0032246000000000043	+0250586000000033	+014277600000000023	00000013
+007569	-00002009629000-	+02489350000000033	+01350160000000023	00 00 0 13
+004237	-002763600000000043	+0236516000000033	+0103716000000023	00000013
+008280	-080365600000000043	+0231776000000033	+01007060000000000	00000013
+002453	-001775600000000043	+02+8046000000033	+0111086000000023	0000003
+005807	+000132600000000004	+0251226000000032	+02403060000000022	00000012
+007218	+001547600000000042	+0240566000000032	+022592600000000022	00000012
+003962	+00002626000000000042	+0246866000000032	+02143060000000022	00000012
+007799	+001467600000000042	+0225195000000032	+02195460000000022	00000012
+004822	-000121600000000042	+0243916000000032		00000012
+005320	+00025350400000041	+ 0.1 + 0.5 / 50 0.0 0.0 / 5.1 + 0.1 + 0.5 / 5.1 + 0.5	+01/4/3600000000021	90000011
+004022	+0012636000000000041	+0150325000000031	+015476600000000021	00000011
+007441	+000137600000000041	+0149706000000031	+01451350000000021	0000011
+004787	+00220260000000041	+0152416000000031	+014+04600000000321	00000011
+005127	-004225600000000000	+0143555000000030	+01329060000000020	00000000
+007477	-004442600000000040	+0157546000000030	+01+994600000000000000000000000000000000000	00000010
+004512	-0074696000000000000	+0180145000000030	+01719260000000000	000000000000000000000000000000000000000
+007543	007390600000000000	+0165435000000030	+0157476000000000000	000000000000000000000000000000000000000
+005443	-00738968000000040	+018060.50000000030	+01723360000000000000	000000000000
F002069	+00593160000000009	+00224650000000000	+00231460000000000000	66900000
+028531	+0002485600000000000	+00611650000000009	+00237060000000000+	66666666
+006207	+00572860000000000	60000000000064600+	+00522560000000000000	0000000
+005963	+00633360000000000	+ 0028 + 450 00 0 000 038	+112620600000000000000000000000000000000	
+006373	+00570250000000000	+0065926000030008	+0059416000000000000000000000000000000000000	3000000000
606900+	+00651860000000000	+ 00 23 23 23 23 23 24 25 25 25 25 25 25 25 25 25 25 25 25 25	+302444000300031+4400	להים היהת הח
**************************************	+00266000000000000000000000000000000000		+00018460000000000000	00000000000
+000417	+006576500000000000	- 00719750 00 0000006	+007370500000000000	00000000
566000+	+0000000000000000000+	+0000000009886000+	+0009926000000000+	0000000
+000015	+0021656000000000000	+00270460000000005	0121510000000000000	000000000

5. Test 208301314300

76. Test 208301314300

0+01496950 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ヤヤヤならをををとててててもてて
	+015039600000 +014999600000 +014999600000 +024419600000 +021468600000 +021458600000 +021425600000 +021425600000 +0219775000000 +021628600000 +018063500000
0+0.1548160000000217 $0+0.1728560000000217$ $0+0.193260000000221$ $0+0.193260000000221$ $0+0.195660000000223$ $0+0.2512600000000223$ $0+0.110560000000223$ $0+0.110560000000233$ $0+0.0751960000000233$ $0+0.0751960000000233$ $0+0.1723560000000233$ $0+0.1723560000000241$ $0+0.1723560000000243$	

77. Test 208301413400

0+0000116 0+0010096 0+0064456	+005551+006332	+006751	+006455	F002072+003801	+006223	+006283	+003788	+005985	+302972	+006014 +003685	+003005	+002974	+002584	+003659	+003557	+006691	+006672	+004476	+26000+	+ 5 C C C C C C	962200+	627 <b>4</b> 10+
$\begin{array}{c} 0+00.21.75600000000000000\\ 0+00100760000000000000\\ 0+00659560000000000057 \end{array}$	+005700600000000007 +0064306000000000007 +00687460000000000	+ 00 00 1 1 00 00 00 00 00 00 00 00 00 00	+005611600000000000000000000000000000000	+0059846000000000000	-00738960000000040	-0081356000000000000	-0376316000000000040	+00083160000000004	+00117760000000000+	+00026760000000041 +00172360000000	-0000008600000000-	+0014445000000000045	+000280600000000042	+00022160000000042	-00346560000000043	-0012776000000000043	-001400600000000043 -001400600000000043	-00510560000000043	+000000000000000	+00 /33 46 00 00 00 04+	-00059060000000044	+80 02 81 60 6 06 00 044
0055 0010 0072	+00505950000000000 +00530550000000007 +0052255000000007	+ 0069746000000000 + 00697460000000008 + 00588350000000008	+005642500000000009 +005642500000000009	+0055186000000000	+0165265000000000000000000000000000000000	+01581260000000030	+00649350000000030	+01495950000000031	+0150415000000031	+01488750000000031 +01439560000000031	+02445150000000032	+02245350000000032	+01994850000000032	+0197906000000032	+0189445000000033	+ 01 85 76 50 00 0 0 0 0 0 33.	+0193916000000033	+0121885000000033	+018066500000034	+ 01 80 65 60 00 0 00 0 34	+ 03653860 00 0 00 034;	+ 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.
000000000000000000000000000000000000000	+006211633400000036 +005446600000000000 +08576060000000000	+ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+0024%+20060000000000000000000000000000000000	+006105600000000000000000000000000000000	+0157156000000000000000000000000000000000	+01503260000000020	+0133056000000000020	+01450860600000001	+015491600000000021	+017492600000000021 +017285500000000	+01933250000000022	+02201460000000022	+0215526000000000022 +022609600000000	+02+00960000000025	+01110750000000023	+0*000000000000000000000000000000000000	+04/224690909090923 +046282609909090933	+00491460000000023	+017236500000000324	+n1/42/20000000000000000000000000000000000	+032468600000000000	+0>>9155000000000+0+
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00 400 405 00 400 0 437 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	01000000	00000010	00000011	00000011	00000011 00000011	00000000	00000015	00 00 0 0 12 71 6 9 0 0 0 0 0	00000012	00000013	000000013	\$1000000 000000	00000013	00000014	+ Tn nan nn	63 90 0 0 14 63 90 0 0 14	<b>។</b> ពេក្យព្យព្ធព

'8. Test 208301413400

+014731	+00027960000000000+	+0020000000000000+	+05392160000000024	00000014
1667700+ +007793	-000288600000000++	+ 01 8 0 6 3 6 0 0 0 0 0 0 0 3 <del>4</del> + 0 3 6 6 8 8 6 0 0 0 0 0 0 0 3 <del>4</del>	+01723560000000000 +035474500000000000	00000014
226000+	-0073916000000000000	+01806460000000034	+017233600000000000	0000000
0+00+4+36	0-005082600000000439	0+01917060000000339	0+004988600000000000000	0.00.00.0139
+003063	-002524600000000043 -001506500000000	+ 01 85 37 50 00 0 0000 33 + nt 94 n7 50 00 0 0000 33	+0075236000000000000	000000013
+006693	-001270600000000043	+01869260000000033	+01009360000000000	00000013
+003200+	-003513600000000043	+01894250000000033	+0111096003000023	0000000
+003622	+00 050 56 0000000 045	+01380050000000032	+1240776033000022	000000112
+006134	+001244600000000045	+01864550000000032	+022592600000022	00000012
+002583	+000255500000000042	+01998060000000032	+0214826000000022	0000012
+005925	+001449600000000045	+02243250000000032	+0755534600000000000+0754	
+003698	+001714600000000041	+0143316000000031	+01728360000000021	00000011
+00000+	+0000542600000000041	+01487850000000031	+01749760000000021	110000000
+002954	+00117360000000041	+0159285000000031	+91549760390909031	00000011
+0005982	+0021999000000041	+0149745000000000	+01440550000000000	00000011
+903780	-00753260000000000	+00645650000000000	+01330260000000000	00000010
+006336	-008137600000000040	+01579860000000030	+0150326000000020	000000000000000000000000000000000000000
+003852	-0075446000000000000	+01801860000000030	+0171636000000020	000000000000000000000000000000000000000
+006145	0400000000000000000	+0155626000000000	+01575160000000000	00000010
+003795	+00298280000000000 -00739160000000000	+ 00 55 15 66 60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	+ 885185688684888888	
+024890	+002332600000000000	+006370500000000000	+0024495000000000	60000000
+1006459	+00563160000000000	+00552860000000000	+00647750000000000	0000000
+006218	+00651760000000000	+0059795000000000000	+0028736000000000000000	0000000
+006769	+00601460000000000	+00697350000000008	+00000000000000000000000000000000000000	00000000
+007105	+006890600000000+	+006225500000000007	+102254530000000357	20000000
+0000000+	+00270780000000004 +00242420000000000007		+9462120490449145	40 888 898 40 6 6 6 7 9 6
+006463	+0000000000000000+	+007220500000000006	+0674025000000000000	000000000
+001011	+001009600000000+	+00100550000000000+	+001003600000000000000000000000000000000	00000000
+00000+	+00218060000000000	+0055135000000000	014134000000000000000	000000020

## REFERENCES

- 1. Wennerstrom, A.J. and Hearsey, R.M., "The Design of an Axial Compressor Stage for a Total Pressure Ratio of 3 to 1." Aerospace Research Laboratories, Wright-Patterson Air Force Base, Ohio, ARL TR 71-0061, AD 727001, March 1971.
- 2. Haugen, R.L., Moore, D.G., and Wennerstrom, A.J., "Velocity Profile Measurements in a Model Settling Chamber." Internal ARL Paper (available upon request), April 1969.
- 3. Stickney, T.M., "Recovery and Time Response Characteristics of Six Thermocouple Probes in Subsonic and Supersonic Flow." NACA TN 3455, 1955.
- 4. Frost, G.R., "Phase I Data Reduction for a Single Stage Research Compressor." Aerospace Research Laboratories, Wright-Patterson Air Force Base, Ohio, ARL TR 71-0253, AD 738658, November 1971.
- 5. Hearsey, R.M., "Computer Programs for Single-Stage Axial Compressor Test Data Analysis." Aerospace Research Laboratories, Wright-Patterson Air Force Base, Ohio, ARL TR 73-0177, Volumes I and II.